#### CONTRACTOR REPORT

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# Solar One Solar Thermal Central Receiver Pilot Plant 1983 Meteorological Data Report

McDonnell Douglas Astronautics Company

Prepared by Sandia National Laboratories, Albuquerque, New Mexico 87185 and Livermore, California 94550 for the United States Department of Energy under Contract DE-AC04-76DP00789.

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# SOLAR ONE SOLAR THERMAL CENTRAL RECEIVER PILOT PLANT 1983 METEOROLOGICAL DATA REPORT

JUNE 1984

MCDONNELL DOUGLAS ASTRONAUTICS COMPANY

#### ABSTRACT

Meteorological data recorded at the Solar One 10 MWe Pilot Plant during a Startup and Initial Evaluation Test Program during 1983 are presented. Additionally, a General Plant Description is provided, plus specific information on the type, quantity, and location of meteorological equipment and instrumentation at the Power Plant which are being used to record the meteorological data.

#### **PREFACE**

This document is provided by the McDonnell Douglas Astronautics Company in accordance with Sandia Contract 84-8173. The data contained in this document were recorded as part of the Solar One Startup and Initial Evaluation Test Program being conducted for Sandia under the subject contract.

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#### SECTION 1

#### INTRODUCTION

This report contains meteorological data which were recorded during the January 1 - December 31, 1983 time period at the Solar One site in parallel with the startup and initial evaluation program.

The contents of this report are organized to contain: a plant description for general orientation, an identification, location, and description of meteorological equipment and instrumentation used at the Solar One site, a description of summary data tapes that have been developed in parallel with this report, and finally, presentation and discussion of the meteorological data.

The intent of this report is to provide a description of the meteorological data system and of the data that are available on data tapes. Summary data are included for temperature, wind, rainfall, direct normal insolation, and the nepholometer. Rainfall data for the years 1956 through 1970 are included for comparison with 1983, which shows that 1983 had higher than average rainfall and more than the average number of occurrences of rain. Barstow insolation data for 1976 are compared to the 1983 data, which shows that 1983 was a bad year for total insolation and that the peak values are also lower. The average peak insolation values for 1983, however, are higher than the 1975-76 data in all but two months of the year.

Insolation data plots are included for three partially cloudy days and three clear days as measured by pyranometers located throughout the field. These plots show the type of data that is available if someone wishes to make cloud passage studies. Direct normal insolation data plots are shown for 289 days between January 1 and December 31, 1983. These were days that had NIP activity, when the data acquisition system was operating. The plots show that the amount of time when the peak direct normal insolation exceeded  $900~\text{W/m}^2$  was small, relating to the total operating time. These plots also show the type of cloud passage transients that the plant must operate through.

Annual and monthly summary wind speed and direction data from Solar One are included in this report, based on wind data recorded during 312 days of data acquisition system operation. The number of days in each month when the wind speed exceeded 30 miles per hour are identified, as well as the fraction of time when this is true. Wind speed exceeded 30 miles per hour on 67 days in 1983 when data were being recorded and the NIP values were greater than  $450 \text{ watts/m}^2$ .

The range of high and low temperatures for each month is included. There were five months when the maximum temperature exceeded 100°F and three months when it was below 32°F. Dewpoints were also recorded and compared to mirror module temperatures on two instrumented heliostats to determine times when the dewpoint exceeded mirror module temperatures. This did occur on 32 days during which the data acquisition system was operating.

The nephalometer became operational during the last half of 1983 at the Solar One location, and representative data for 8 days are included to show a mix of partly cloudy and clear days, some of which are the same days as those used for the NIP and pyranometer plots.

The meteorological instrumentation at Solar One was kept in better working order during 1983 than in 1982, and the data acquisition system was on-line recording meteorological data for 312 days during the year, thus making this meteorological data report far more complete than the 1982 version.

# SECTION 2 PLANT DESCRIPTION

#### 2.1 GENERAL

Solar One is a 10 MWe Solar Thermal Central Receiver Pilot Plant which generates electricity exclusively from solar energy. The pilot plant is a joint undertaking between the U.S. Department of Energy and the Utility Associates, which consists of the Southern California Edison Company, the Los Angeles Department of Water and Power, and the California Energy Resources Conservation and Development Commission.

Since this pilot plant is the first large scale demonstration of the generation of electricity using a solar central receiver, the pilot plant design, construction, and operation activities are intended to support the program objectives as defined by the Department of Energy and the Utility Associates. These program objectives are:

- 1) To establish the technical feasibility of a solar thermal power plant of the central receiver type, and to identify areas where research and development may lead to significant performance improvements and increased capabilities.
- 2) To obtain development, production, operating, and maintenance cost data to (a) support private sector decisions to invest in solar central receiver energy systems, and (b) identify areas where research and development may most effectively be applied to reduce costs and extend areas of application of such systems.
- 3) To determine the environmental impacts of the construction, operation and maintenance of solar thermal central receiver plants.

The plant is designed to produce at least 10 MWe of electrical power to the utility grid (after supplying the plant parasitic power requirement) for a period of 4 hours on the plant "Worst Design Day" (Winter solstice) and for a period of 7.8 hours on the plant "Best Design Day" (Summer solstice). The "Worst" and "Best Design Days" are based on assumed insolation (solar intensity) conditions which have been developed from actual site insolation measurements. During actual plant operation, the plant capability and electrical output will depend on the current sun and atmospheric conditions. During certain periods of the year (near noon from March through September), the plant energy collection capability can exceed the 12.5MWe turbine-generator rating.

An aerial photograph of Solar One is shown in Figure 1.

#### 2.2 LOCATION

The pilot plant is located on a 130-acre site of Southern California Edison property near the Coolwater Generating Station which is located east of Daggett, California and approximately 12 miles east of Barstow, California. The site is at a latitude of 34.8 °N and longitude of 116.83°W. The site is contained in the western half of Section 13, Township 9N - Range 1E, San Bernardino County: San Bernardino Meridian. The reference location for the pilot plant is the receiver tower vertical centerline with coordinates N 501, 260 and E 2, 349, 950. The nominal elevation of the site is 1,946 feet above mean sea level. A vicinity map is shown in Figure 2.

#### 2.3 GENERAL ARRANGEMENT

A general arrangement of the pilot plant site is shown in Figure 3. The site boundary, excluding the main parking area, is established by a perimeter security fence shown as a dashed line in the Figure.

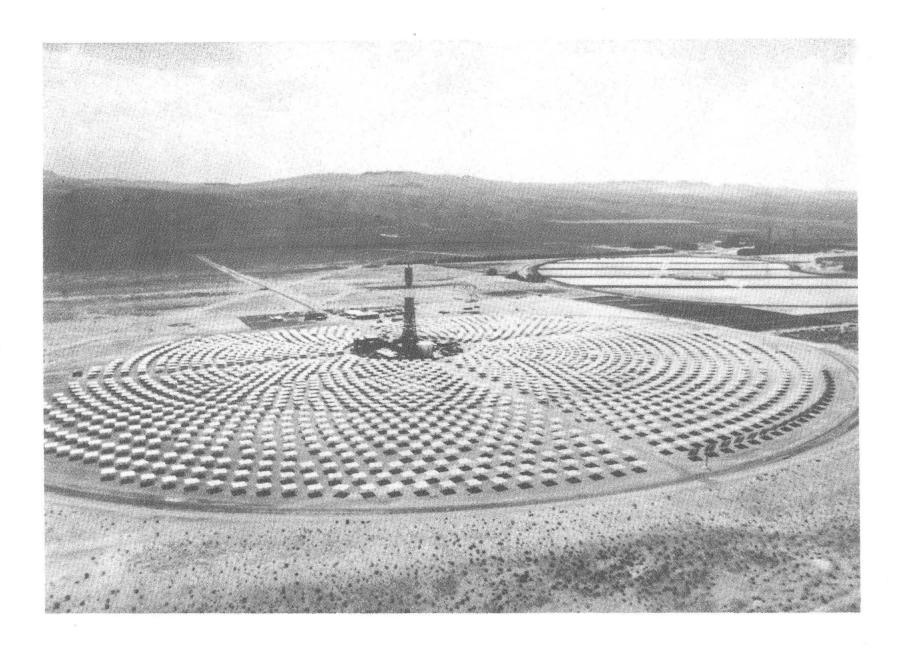


FIGURE 1. AERIAL PHOTOGRAPH OF SOLAR ONE

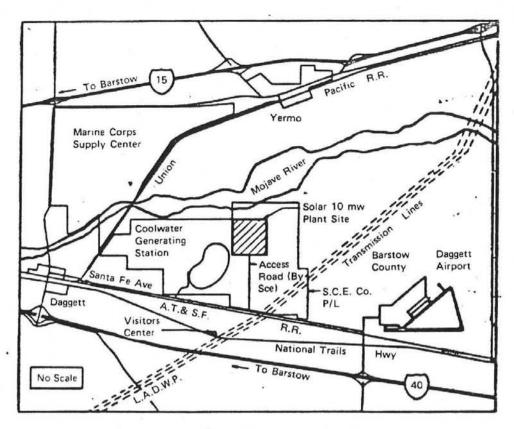


Figure 2 Vicinity Map

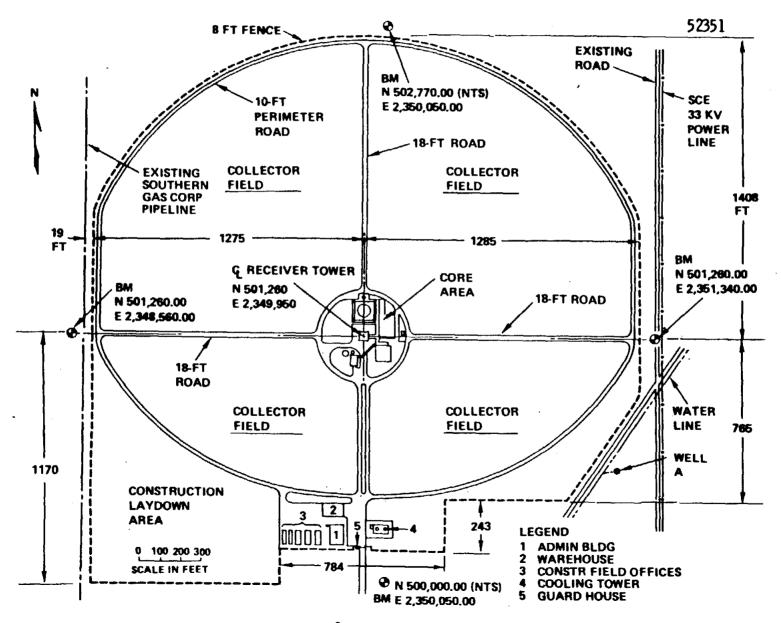


Figure 3 General Arrangement

A central core area of approximately three acres is utilized for the receiver tower and the support equipment for the solar system, such as the receiver system, thermal storage system and electrical power generating system, as well as other necessary support systems. The core area also contains electrical power generation equipment, related peripheral equipment and a plant control room. The core area has a radius of 201 ft, with its center coincident with the tower centerline. The center of the receiver tower is located at coordinates N501, 260 and E 2, 349, 950. The center of the receiver panels is at an elevation of 260 feet above the theoretical intersection of the collector field planes with the receiver tower centerline.

A 75-acre collector field surrounds the receiver tower. The northern field boundary can be described by an arc of 1,390 feet radius from the receiver tower centerline. The southern field boundary can be described by an arc of 2,145 feet radius whose center is 1,395 feet north of the receiver tower center. An area 243 feet by 784 feet within the perimeter fence and near the (southern) main entrance has been utilized for placement of the administrative building, warehouse, cooling tower and other service equipment not required in the central core area.

The collector field occupies 75 acres and contains 1818 heliostats in an optimized arrangement around the tower. The heliostat locations are depicted on Figure 4. In addition, numerous monitoring and measurement devices are located in the collector field, as shown in Figure 5. The collector field is graded to provide adequate drainage and to minimize elevation differentials between heliostats. It is also compacted to permit vehicular access to the heliostats and ancillary electrical equipment for installation, maintenance and washing functions.

#### 2.4 TOWER AND BUILDINGS

#### 2.4.1 Tower

The receiver tower is designed to support the receiver assembly at the required elevation above the collector field. In addition to the receiver panels, the tower supports a heliostat beam characterization system (BCS) target as well as the piping and auxiliary equipment for the receiver.

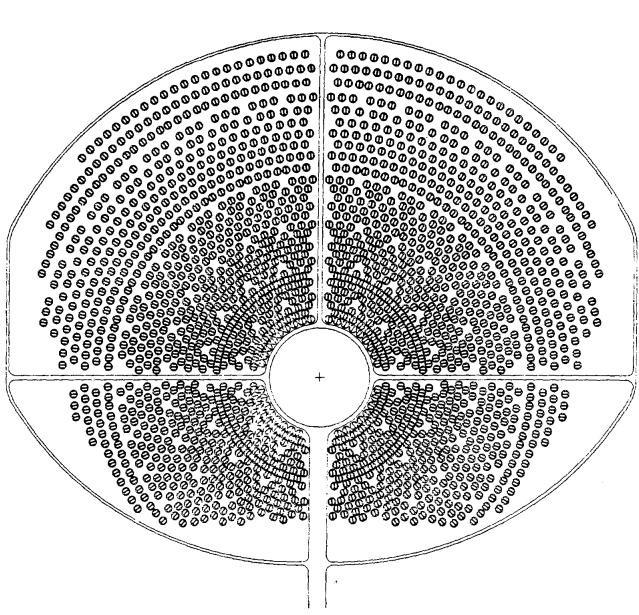


Figure 4 10 MW Central Receiver Collector Field Layout

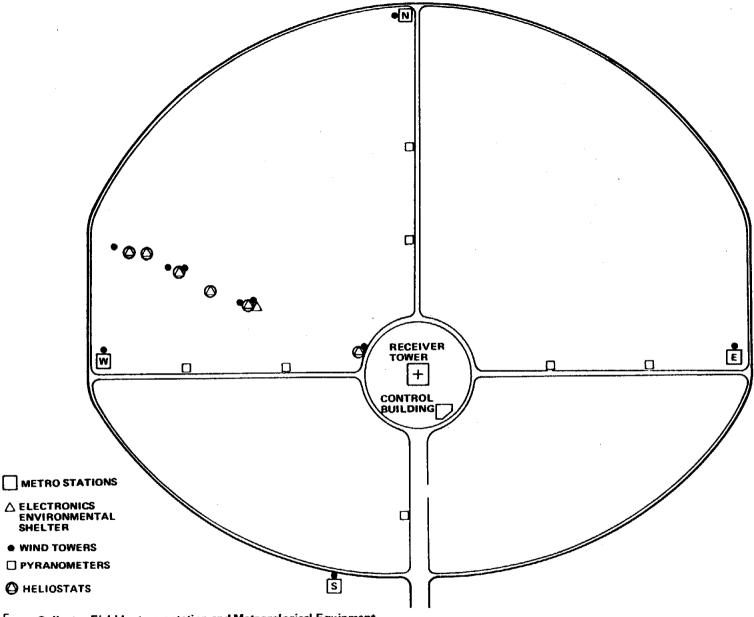


Figure 5 Collector Field Instrumentation and Meteorological Equipment

The tower (depicted in Figure 6) has a total height of approximately 295 feet above ground level, including 22 working levels above ground. It is an open, four-sided steel structure resting on a reinforced concrete foundation. At the base, the tower is 39 ft. 11 in. square, and tapers to 15 ft. 1/2 in. square at the 15th level (211 ft above ground level). However, at that level, the structure extends to support the BCS target, and is 47 ft. 8 in x 37 ft. 8 in. The tower has a stairway up to the base of the receiver and an elevator to transport three personnel and/or small parts to a working level near the top of the tower and other appropriate working levels. Ladders are provided from the base of the receiver to the top of the receiver assembly. A photograph of the receiver and tower assembly is shown in Figure 7. The heliostat beams are reflecting moisture droplets in the air, with the concentrations of the beams shown as bright spots at the collector field standby points.

#### 2.4.2 Control Building

The control building is a two-story reinforced masonry block structure shown at the base of the tower in Figure 7. The Plant Control Room, Equipment Room and Personnel Office space are located on the second floor, with the electrical switchgear and battery rooms located on the first floor. Building plan dimensions are approximately 45'-0" by 7'-0". The elevation of the second floor is 20'-0" to allow direct access to the Auxiliary Bay structural deck. The roof is of timber construction and the second floor is a reinforced concrete slab supported by structural steel members.

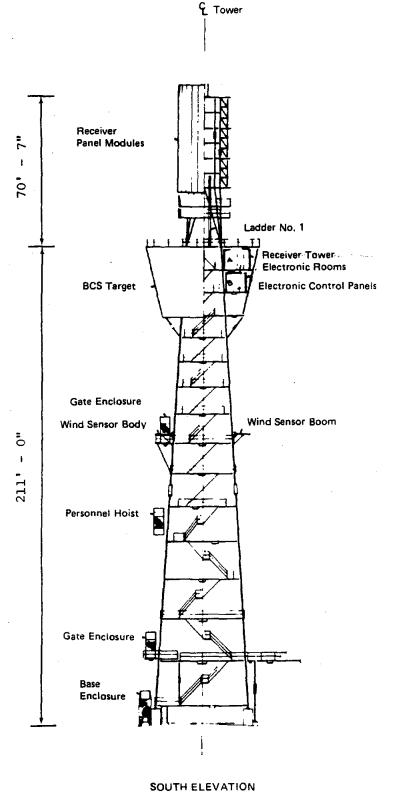


FIGURE 6 RECEIVER TOWER



FIGURE 7. RECEIVER TOWER ASSEMBLY

#### SECTION 3

#### METEOROLOGICAL EQUIPMENT AND INSTRUMENTATION

The meteorological measurements equipment consists of wind velocity and direction devices, fixed position pyranometers (measures total insolation), normal incidence pyrheliometer (NIP), which measures direct insolation, hail cubes (measure size and velocity of hail impact), rain gages, various temperature, pressure and humidity measurement devices, and a nephelometer. This equipment is placed in various stations throughout the site, as follows:

- South Station
- West Station
- North Station
- East Station
- Receiver Station (7th level)
- WNW Station
- Control Room Roof

#### 3.1 LOCATION

Figure 8 shows the locations of the meteorological instrumentation for the Solar One Site. There is one meteorological station (shown as a hexagon) at each compass point of the field, at the central receiver tower, and at the Control Room roof. There are wind towers plus an environmental enclosure within the field in the West-North-West (WNW) direction adjacent to heliostats instrumented for structural, thermal and power studies. One hail cube is in the middle of the northwest field and one in the middle of the northeast field. These are shown as HC in the figure. In addition, there are seven pyranometers distributed along the spoke roads for cloud obscuration studies.

#### 3.2 DESCRIPTION

Figure 9 provides a schematic of the overall system, including the sensors, the remote acquisition systems (RAS) at the various stations, the collector field interface cabinet, and the interfacing hardware connecting the meteorological system with the data acquisition system (DAS). Dashed lines also indicate the physical locations of the various equipment. The displays available in



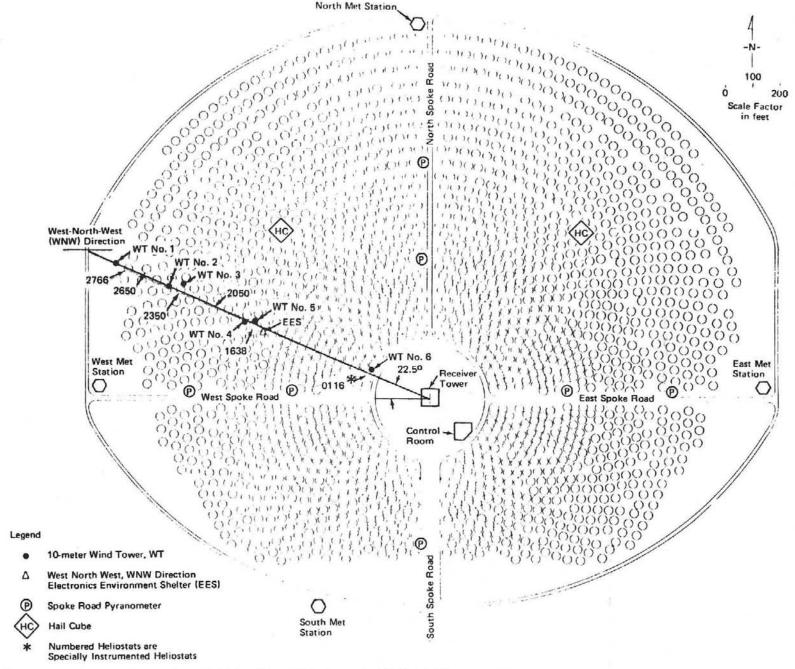


Figure & Collector Field Locations of Meteorological and Specially Instrumented Heliostats Measurements

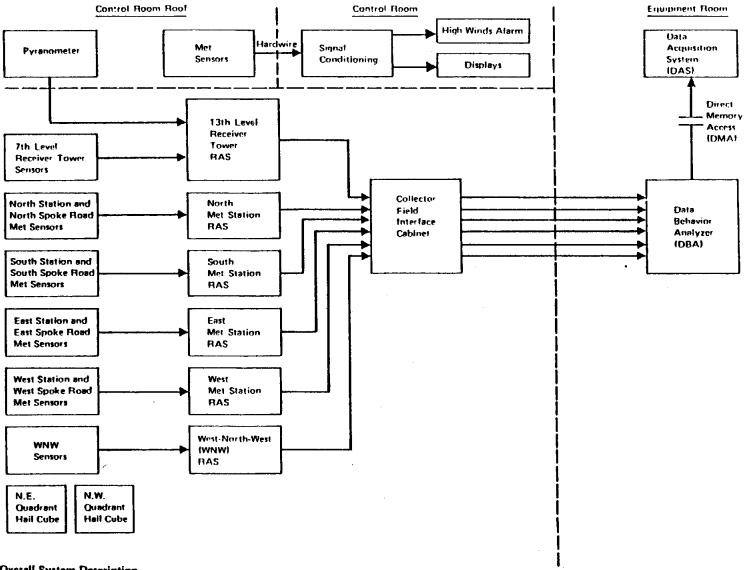


Figure 9 Overall System Description

the control room are the normal incidence pyrheliometer (NIP) readings, plus wind speed and wind direction.

#### 3.2.1 General

Each compass point station has a concrete base to provide the stability and levelness required by the instruments. The base is at least 2 inches above the surrounding finished grade.

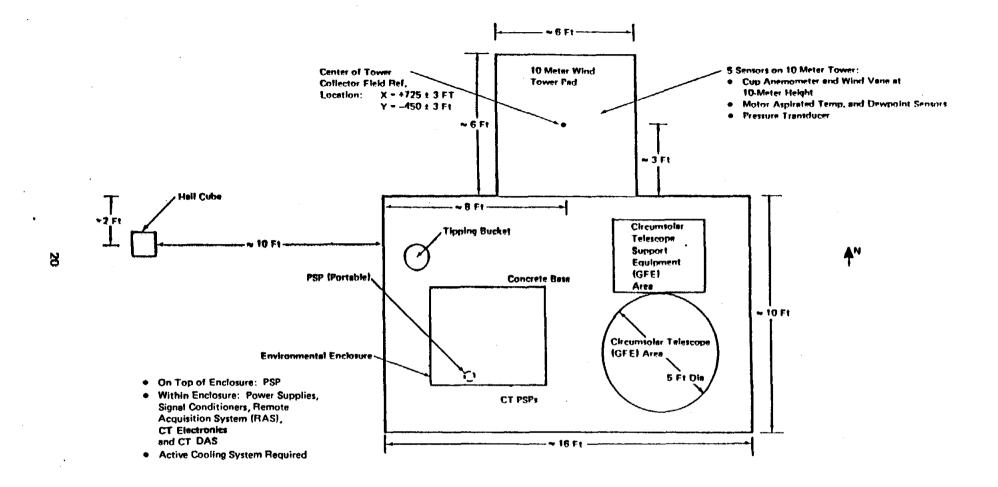
On top of each compass point station base is an environmental enclosure for sensitive equipment such as power supplies, signal conditioners, and the remote acquisition system (RAS). The enclosure is designed to maintain the enclosure area temperature and dust level within the most sensitive temperature and dust range dictated by the electronics hardware environmental specifications. The enclosure is capable of easy access and removal of the electronic equipment.

A power/signal cable distribution panel is mounted within the enclosure. A two-panel door is located at one end for easy access to the front of the electronic packages. A lock is provided on the door to allow access to the equipment for authorized personnel only. All power and signal cables running to and from the enclosure are environmentally protected.

### 3.2.2 South Station

The south station (see Figures 10 and 11) is the main meteorological station, and it is located south of the collector field perimeter road and west of the main entrance road to the core area. The specific XY coordinates are: X = +725 + 3 ft, Y = -450 + 3 ft. (It should be noted that the coordinate convention used for the Solar One Site has the origin (0,0) located at the tower vertical center line, with the +X direction due south and the +Y direction due east.) The station is equipped with instrumentation for measuring rainfall, wind speed, wind direction, barometric pressure, temperature, and dewpoint. Additionally, the signal conditioning for the south spoke road pyranometer is done here, and there are provisions for a circumsolar telescope (CT) installation and a portable precision spectral pyranometer (PSP), as indicated in the schematic of Figure 10 and the general arrangement of Figure 11. These instruments are not currently installed and operating.

Figure | OSouth MET Station (Main Station) System Schematic



Scale: - 1,0 Foot

Figure 11. SOUTH STATION GENERAL ARRANGEMENT

The south station has a concrete slab base of approximately 16 by 10 ft, as indicated in Figure 11. A rigid environmental enclosure is sized to accommodate all instrumentation electronics (power supplies, signal conditioners, RAS electronics, CT electronics and CT data acquisition system (DAS). The approximate size of this enclosure is 80 inches wide by 96 inches high by 72 inches deep. It is located on the southwest end of the concrete base, 2 feet away from the base's edge with the long dimension in the eastwest direction.

The CT electronics and CT DAS would dissipate approximately 1 kW of heat during operation and it requires a dust-free operational environment at a temperature of  $70 \pm 10^{\circ}$ F. This dictated the major cooling capacity requirement of the enclosure's cooling system. The top of the enclosure has provisions for mounting one portable PSP. Figure 12 shows a photograph of the south station, as viewed from the west.

On the southeast corner of the base is a 5 foot diameter vacant area where the circumsolar telescope could be located. The 5 foot diameter vacant area is at least 1 foot from the base's edge and at least 2.5 feet from the environmental enclosure.

North of the circumsolar telescope area is a 3 by 4 foot area reserved for the circumsolar telescope support equipment.

A tipping bucket rain gauge is located on the west end of the base and at least 1.0 foot in from the edge of the base. Figure 13 shows the instrument.

Adjacent to the base (north of base) is a 6 by 6 foot square concrete area where a 10 meter tower is located. On the tower at the 10 meter level is a cup anemometer and wind vane mounted on a cross arm. (See Figure 14) A motor aspirated temperature and dewpoint sensor is mounted just below the wind sensors (see Figure 15). A pressure transducer is mounted at the 6 foot level of the tower. A hail cube is mounted on a pole 10 feet from the concrete base in the westerly direction. This installation can be seen in Figure 12.

#### 3.2.3 West Station

The west station (Figures 16 and 17) is located per collector field reference XY coordinates as indicated in Figure 17. It is a 9 by 6.5 feet concrete slab base with the long end in the east-west direction. The surface of the base is at least 2 inches above the surrounding finished grade.

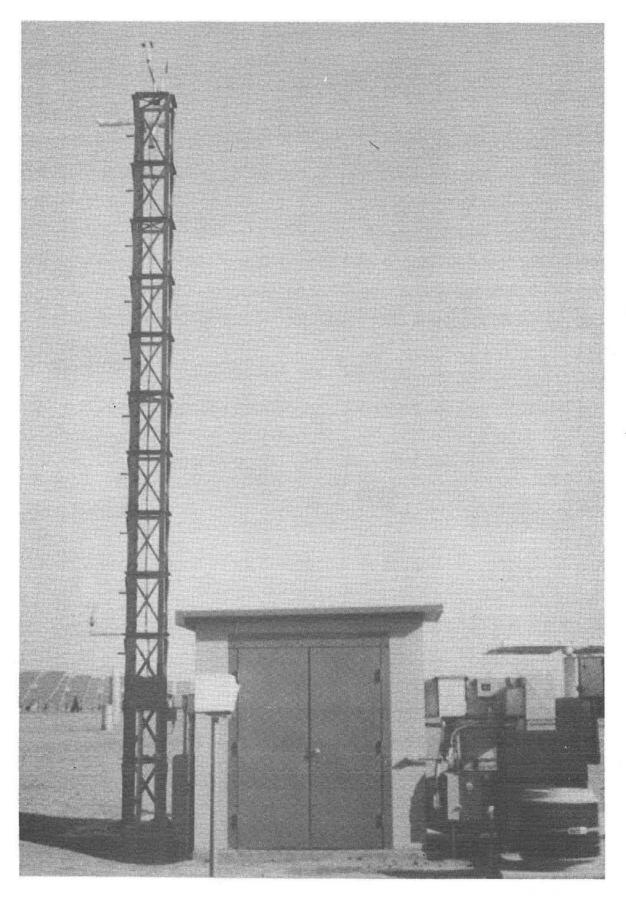


FIGURE 12. SOUTH STATION - VIEWED FROM THE WEST

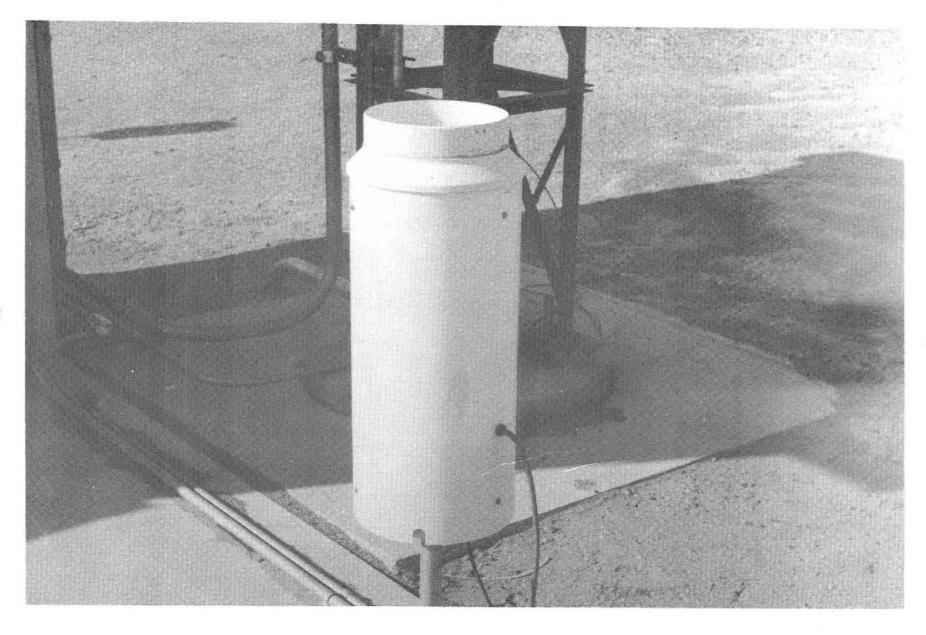


FIGURE 13. TIPPING BUCKET RAIN GAUGE INSTALLATION

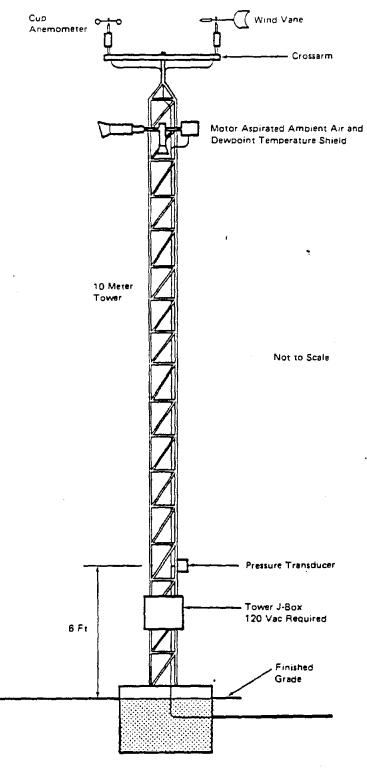


Figure 7 4 Mounting Location of Meteorological Sensors on 10-Meter Tower

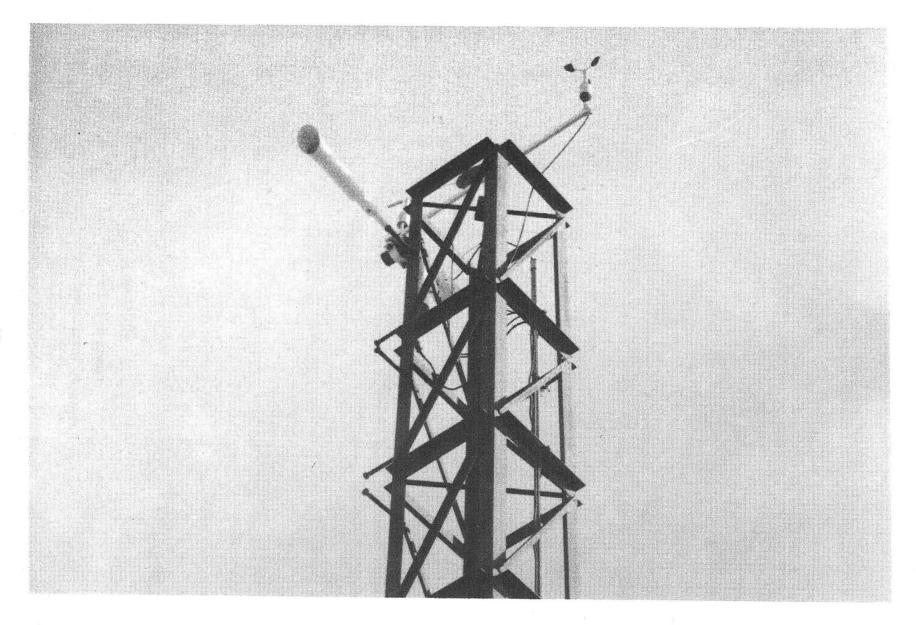


FIGURE 15. SOUTH STATION TEMPERATURE AND DEWPOINT SENSOR

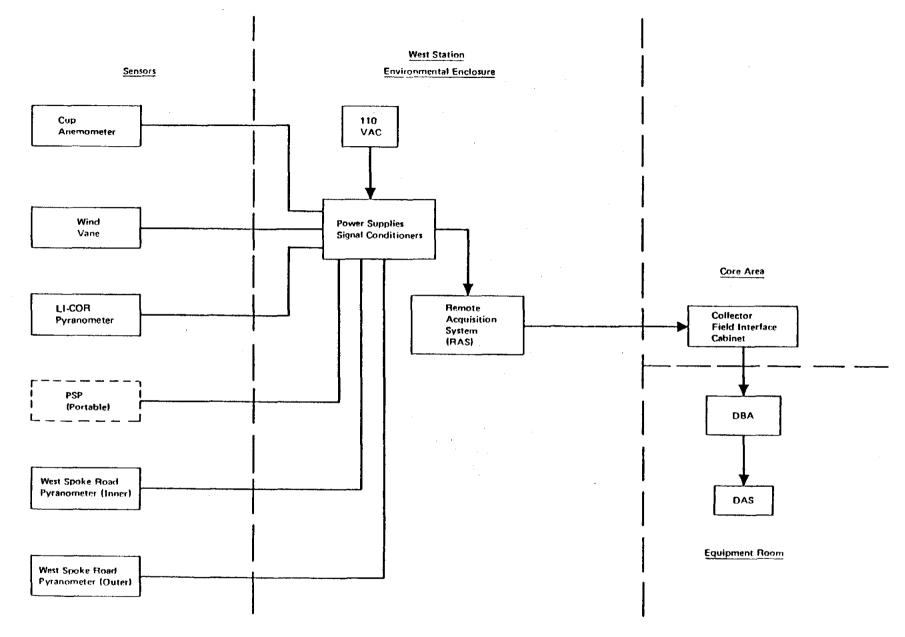


Figure 7 6 West MET Station System Schematic



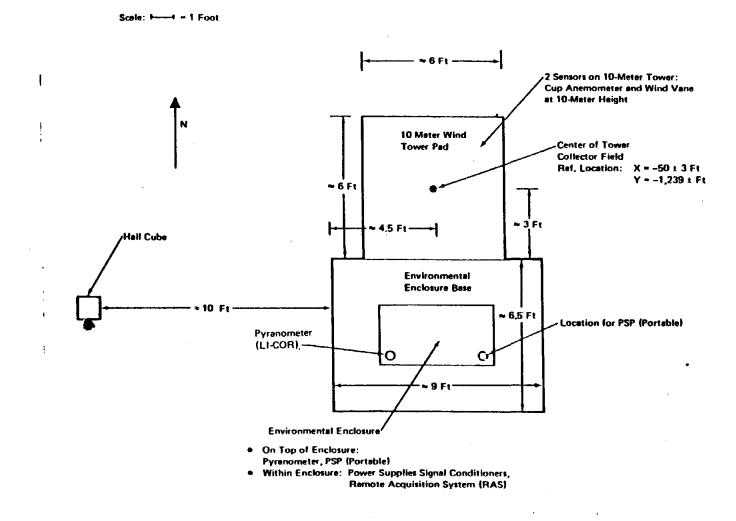


Figure 17. WEST MET STATION GENERAL ARRANGEMENT

An environmental enclosure approximately 24 inches wide by 72 inches high by 30 inches deep to accommodate all station electronics is located at the south side of the base. A pyranometer is permanently located on top of the enclosure, as well as cabling provisions for the portable PSP. Requirements for electronics environmental protection, access, drainage, cable connections, and safe guarding are the same as that for the south station environmental enclosure. An active cooling system is provided.

A 6 ft by 6 ft wind tower base is located north of the environmental enclosure base. A cup anemometer and a wind vane are mounted on a crossarm at the 10 meter height. A hail cube is located 10 feet west of the concrete base. The environmental enclosure, wind tower, and hail cube can be seen on Figure 18.

#### 3.2.4 North Station

The north station (Figures 19 and 20) is located per collector field reference XY coordinates as indicated in Figure 20. The specifications of the base, environmental enclosure, wind sensors and 10 meter tower are identical to that of the west station. There is a pyranometer on top of the environmental enclosure, as well as provisions for a portable PSP. A NIP is mounted on a solar tracker on a table adjacent to the environmental enclosure. Space for an active cavity radiometer (ACR) is also provided. A hail cube is located 10 feet north of the base. The NIP installation and the environmental enclosure for the north station are shown on Figure 21.

#### 3.2.5 East Station

The east station system schematic is identical to that of the west station, as depicted on Figure 16. The general arrangement for the east station is shown in Figure 22, including the collector field coordinates. The station characteristic dimensions and requirements are identical to those of the west station, except for the hail cube, which is located 10 feet east of the concrete base. Figure 23 shows the east station environmental enclosure, the wind tower, and the hail cube pedestal.

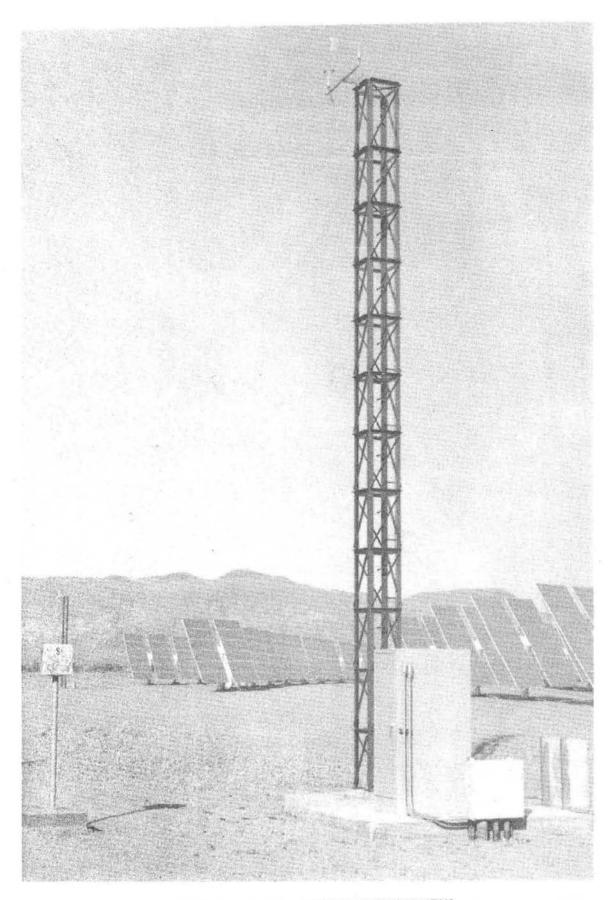


FIGURE 18. WEST STATION INSTALLATION

Figure 19 North MET Station System Schematic

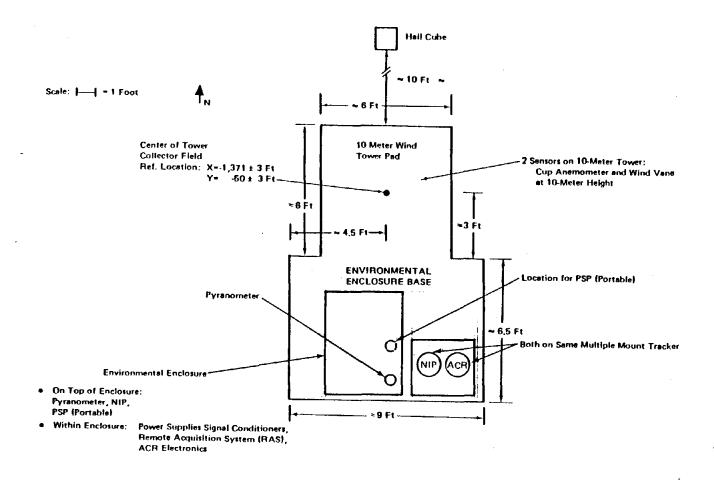


Figure 20. NORTH MET STATION GENEFAL ARRANGEMENT

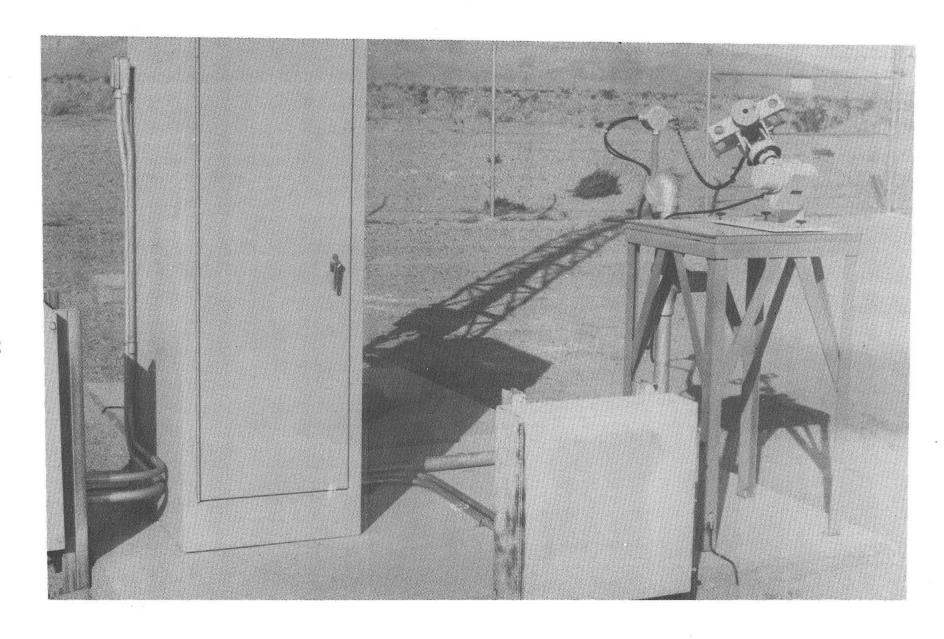


FIGURE 21. NORTH STATION NIP INSTALLATION

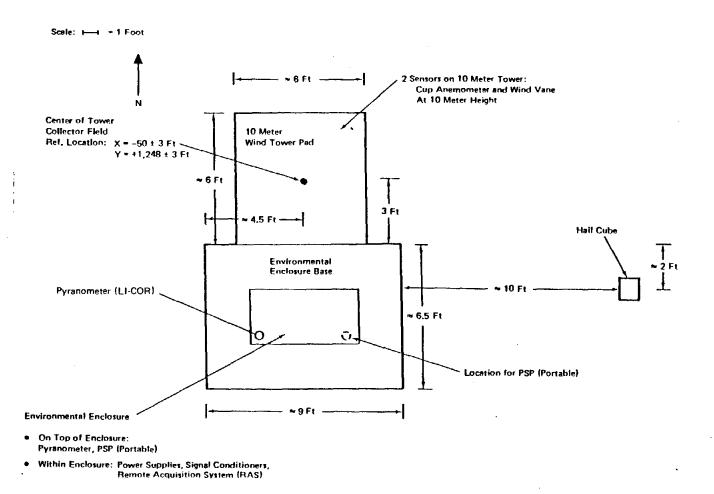


Figure 22. EAST MET STATION GENERAL ARRANGEMENT

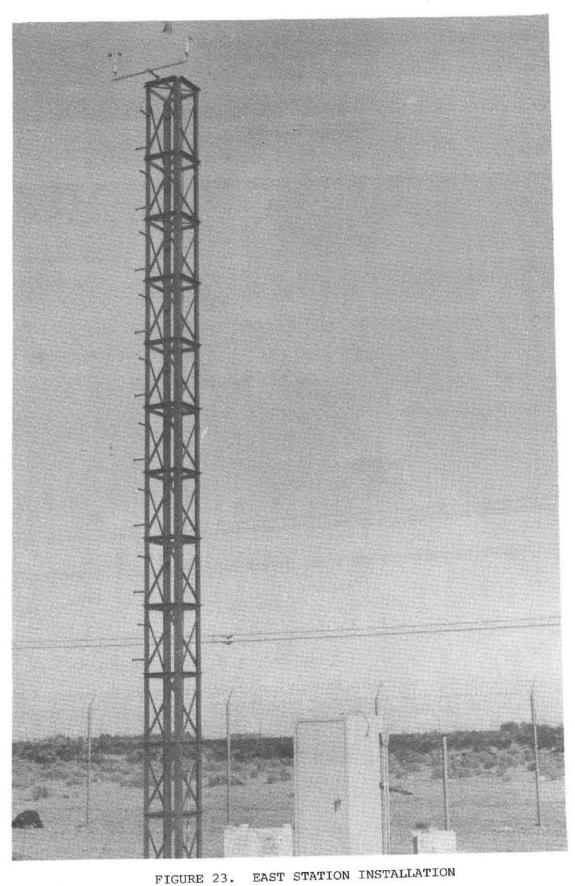


FIGURE 23.

# 3.2.6 Receiver Station

Two sets of wind measuring sensors, each set consisting of a cup anemometer and a wind vane mounted on a crossarm which in turn is mounted on an 8 foot boom, are located in the easterly direction on the east side and also in the westerly direction on the west side of the receiver tower at level 7. The tower MET station system schematic is shown in Figure 24. The instrument and electronics locations are shown in Figure 25, and the eastern and western installations are shown in Figures 26 and 27, respectively.

A nephelometer, motor aspirated temperature, and dewpoint sensor are located within the tower structure on the same level as the wind sensors. The nephelometer is mounted in the environmental enclosure in a vertical position with the sample inlet port down. The nephelometer electronics are located not more than 6 feet from the sensor and are environmentally protected. Power supplies, signal conditioning, and the RAS are located in the environmentally protected area on the 13th level of the receiver tower.

# 3.2.7 West-Northwest Station

A system schematic of the west-northwest station is shown in Figure 28. Six 10 meter towers are located at the designated spots in the west-northwest (WNW) direction in the field. These towers are adjacent to the heliostats that are instrumented by SNLL for wind loading and temperature studies. Each tower (Figure 29) has four sensors: one cup anemometer on a 2 foot boom in the WNW direction at the 10 and 20 foot levels, and one cup anemometer and a wind vane mounted on a crossarm at the 32.8 foot (10 meter) level. The boom mounted cup anemometers are in the WNW direction, i.e., 292.5° (0° is north, angle measured clockwise). The crossarm is mounted perpendicular to the boom. Two of the tower installations are shown in Figures 30 and 31.

An electronics environmental shelter used to house power supplies, signal conditioners, and RAS is located adjacent to wind tower 5 as shown in Figure 32. The shelter has an active cooling system to maintain the temperature limits required by the electronics housed. The shelter is on a concrete base designed to accommodate a light load. The shelter is oriented with the long axis parallel to the circle radius and has double doors and a lock which will permit access only to authorized personnel.

The collector field coordinates for the wind towers and the electronics

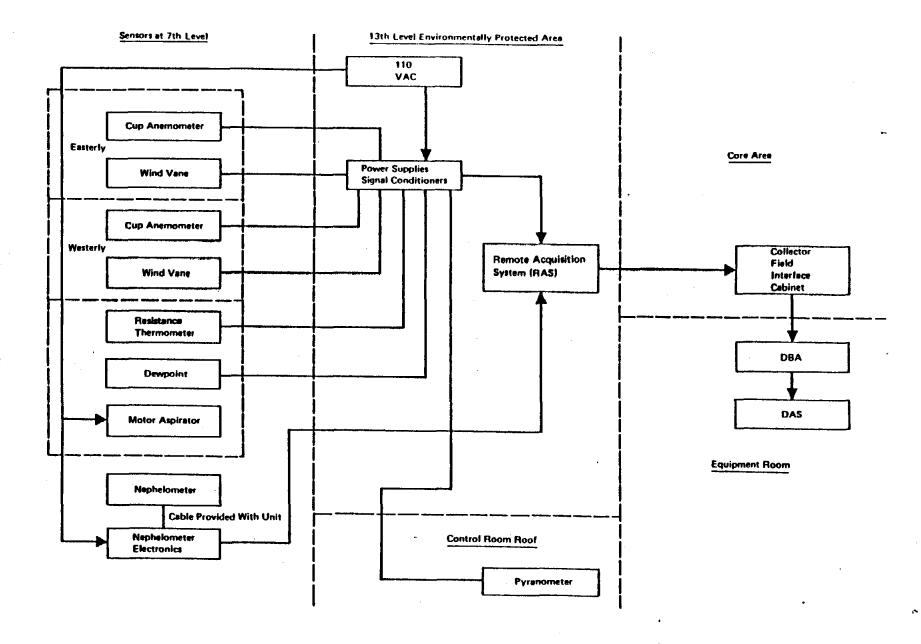


Figure 24 Central Receiver Tower MET Station System Schematic

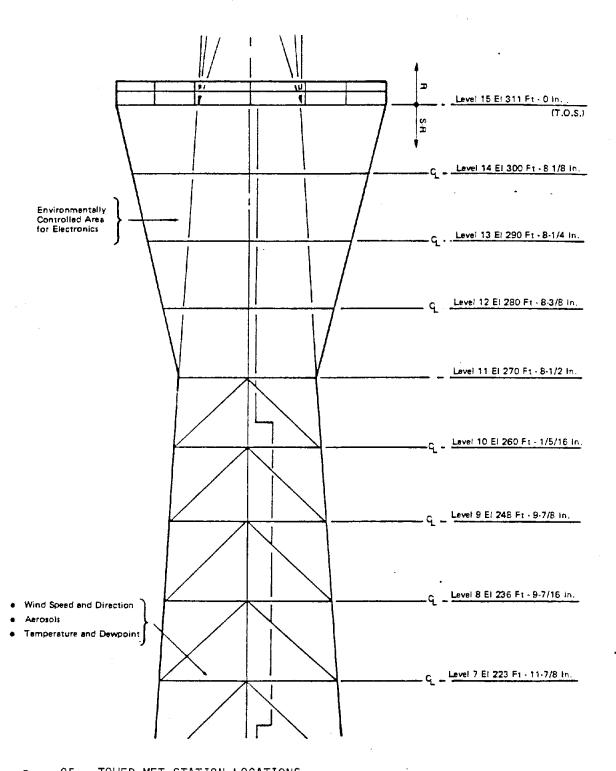


Figure 25. TOWER MET STATION LOCATIONS

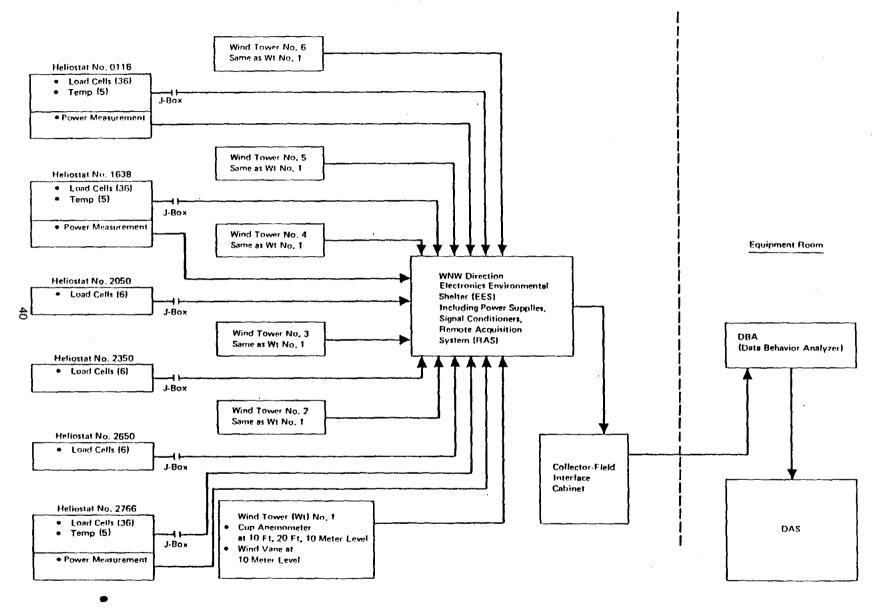
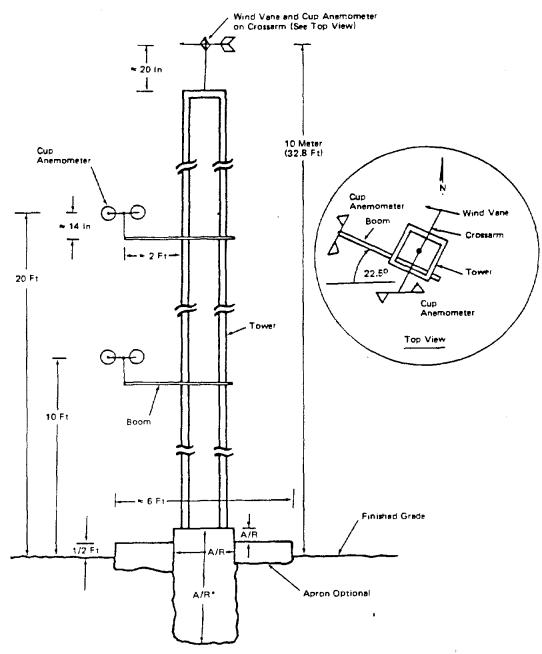


Figure 28 West North-West (WNW) Direction Meteorological and Special Heliostat Measurements System Schematic



\* As Required to Withstand Moment from 90 MPH Winds with Iceland

Figure 29 In Field Wind Tower (WNW Direction)

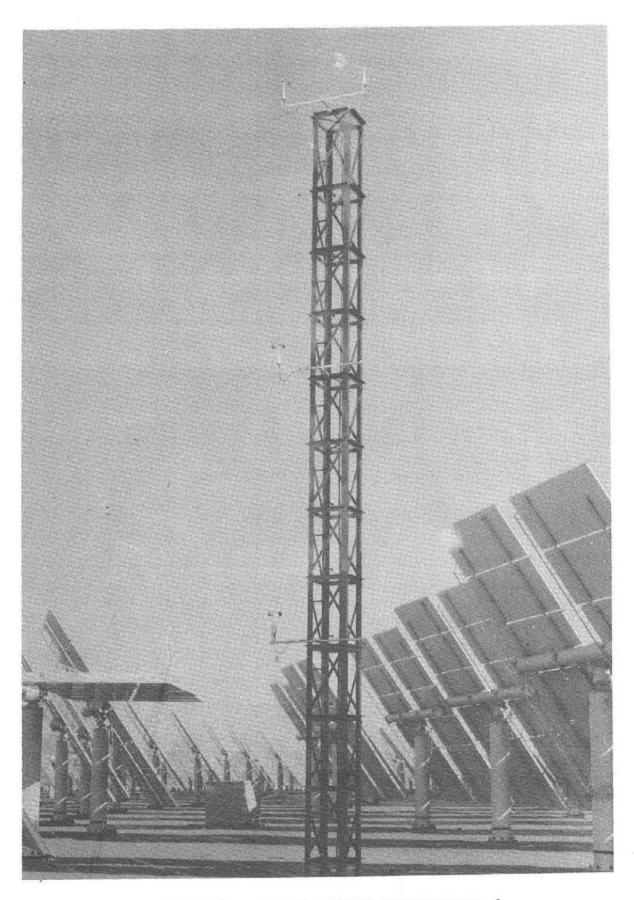


FIGURE 30. WNW WIND TOWER INSTALLATION -1

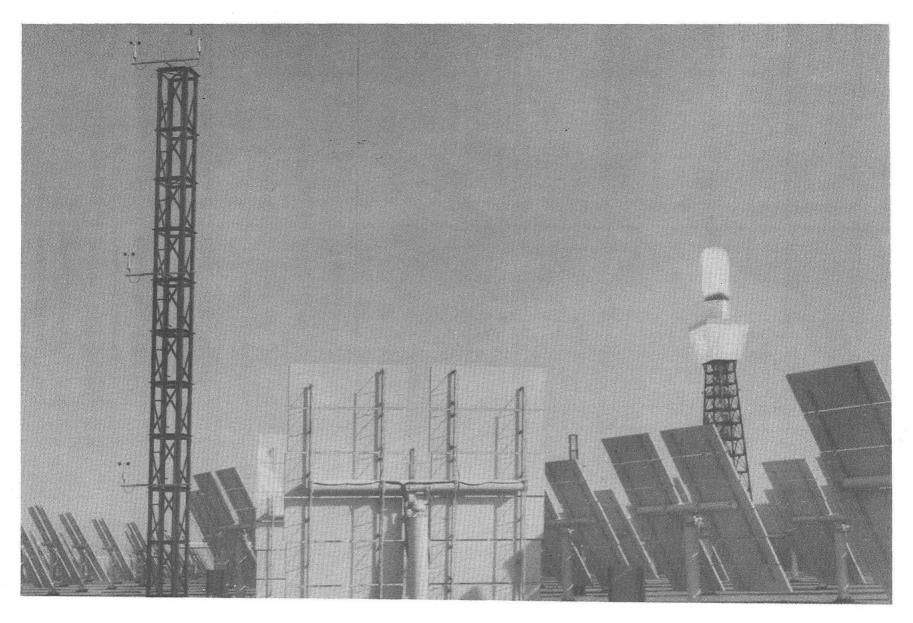


FIGURE 31. WNW WINDTOWER INSTALLATION -2

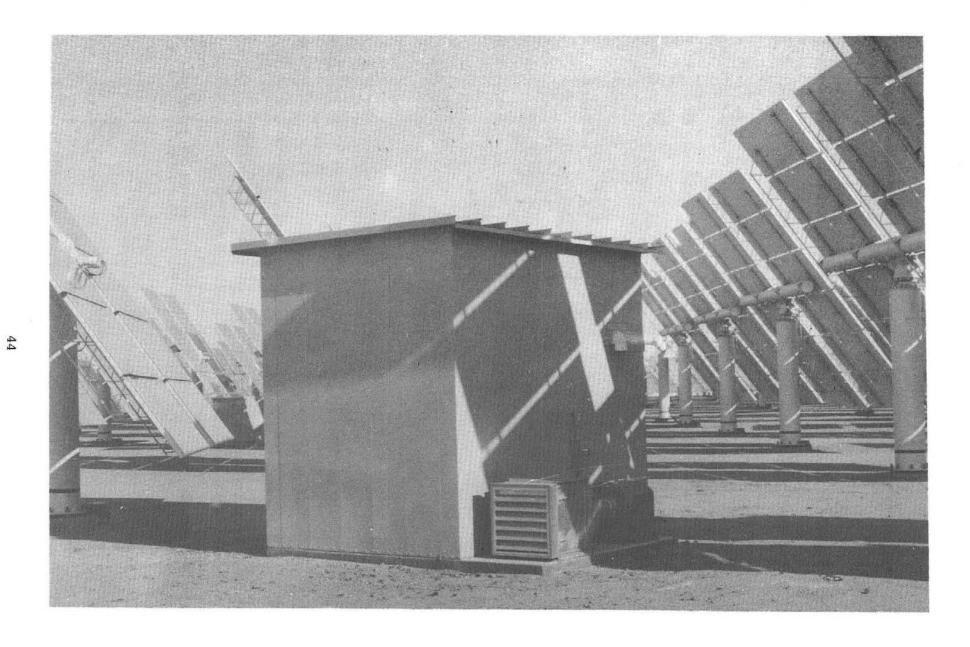


FIGURE 32. WNW ELECTRONICS ENVIRONMENTAL SHELTER

environmental shelter (EES) are shown in Table 1.

Table 1. WNW Wind Towers and EES Collector Field Location Coordinates

TOWER No. or EES	Collector Field	Coordinates (Ft)
	X	Y
. 1	-481.72	-1162.98
2	-405.54	-958.82
3	-408.75	-906.75
4	-275.25	-680.87
5	-281.84	-639.15
6	-105.75	-214.53
· EES	-247.07	-614.47

## 3.2.8 Control Room Roof

Four sensors are located on the control room roof: a normal incidence pyrheliometer (NIP), a pyranometer, a cup anemometer, and a wind vane. The pyranometer and the NIP are placed on a rigid table of approximately 40 inches in height and 3 feet square in table top dimensions. Figure 33 shows the design of the table. The pyranometer is located on the southwest corner of the table and the NIP on the northeast corner. The pyranometer installation is shown in Figure 34. The NIP is mounted on a solar tracker, as shown in Figure 35. The table is located within a 10' by 10' square 10' away from the edge of the building.

The cup anemometer and wind vane are mounted on a crossarm at least 5 feet above the roof floor. Figure 36 shows the design of the sensors and the mount. The assembly is located within the 10 foot by 4 foot area 20 feet north of the south face. The actual installation is shown in Figure 37.

## 3.2.9 In-Field Hail Cubes

Two hail cubes are located within the field in addition to the four at the weather stations. One is in the northwest quadrant of the collector field in heliostat row 19, between heliostats 1930 and 1932. The other is in the northeast quadrant of the collector field in heliostat row 19, between heliostats 1929 and 1931. The collector field layout reference XY coordinates

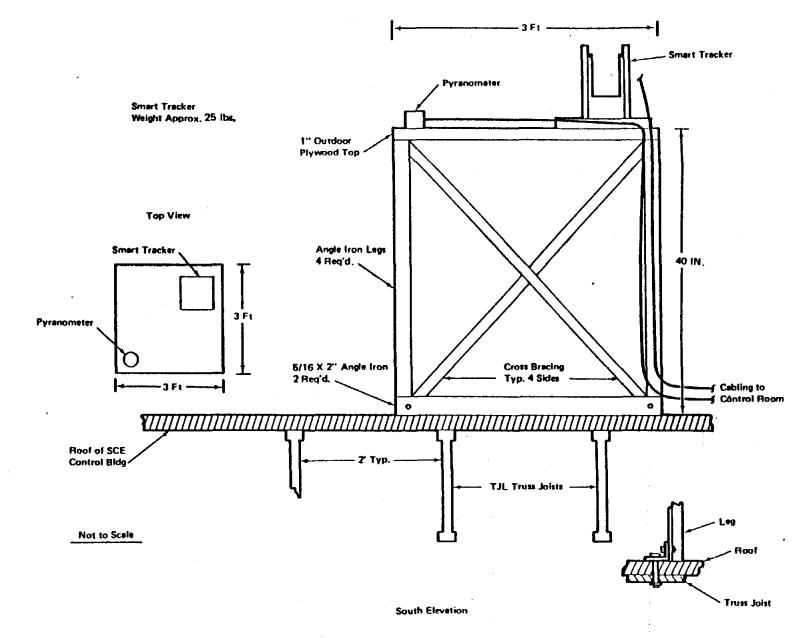


Figure 33 Smart Tracker Support Installation

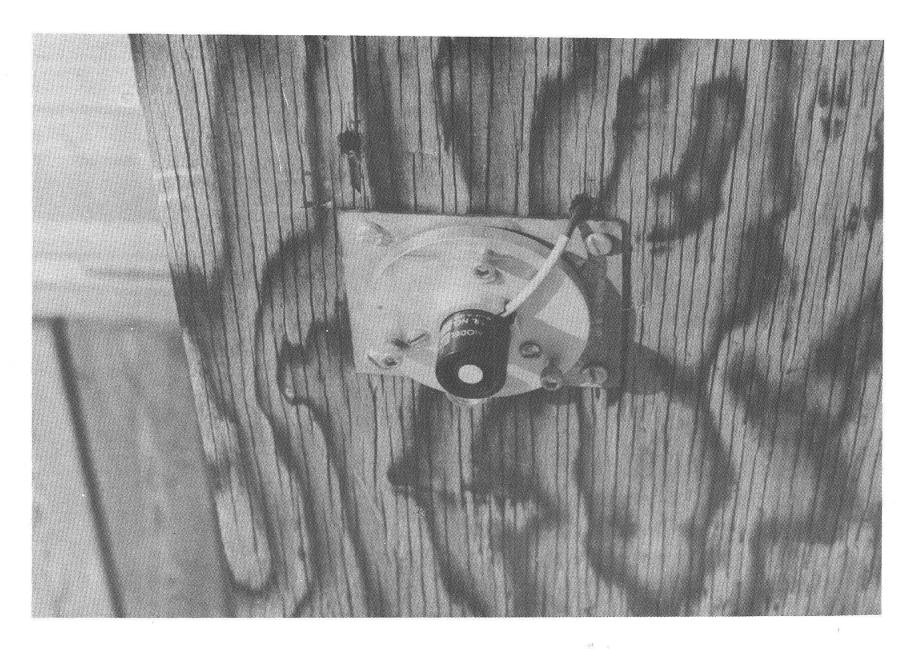


FIGURE 34. PYRANOMETER INSTALLATION - CONTROL ROOM ROOF

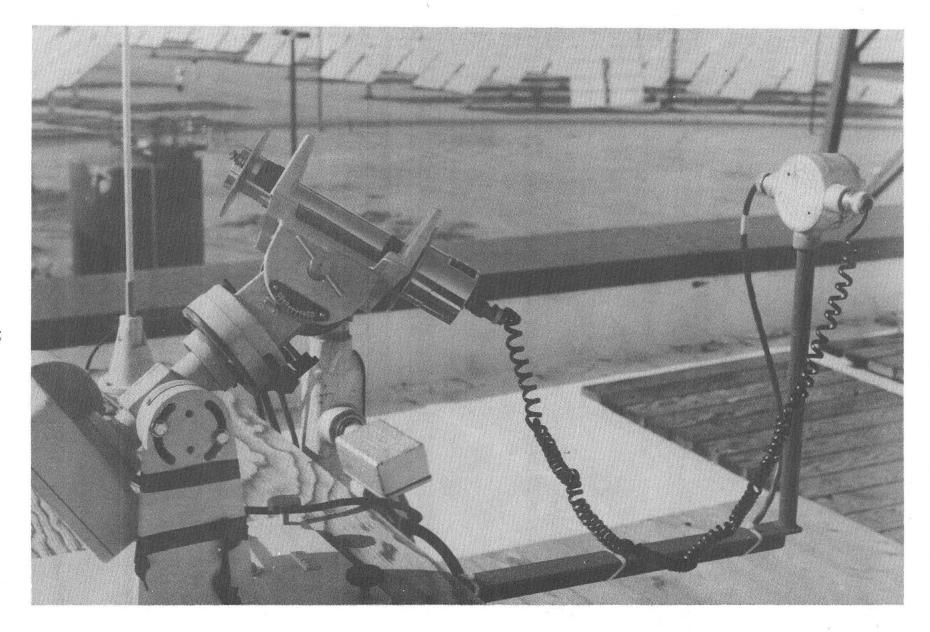


FIGURE 35. NIP-TRACKER INSTALLATION - CONTROL ROOM ROOF

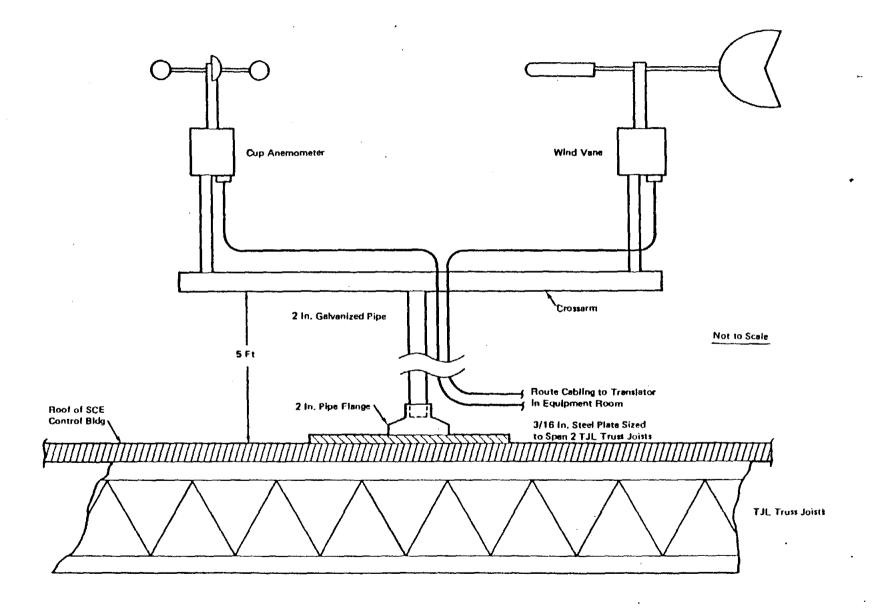


Figure 36. WIND SENSOR DESIGN - CONTROL ROOM ROOF

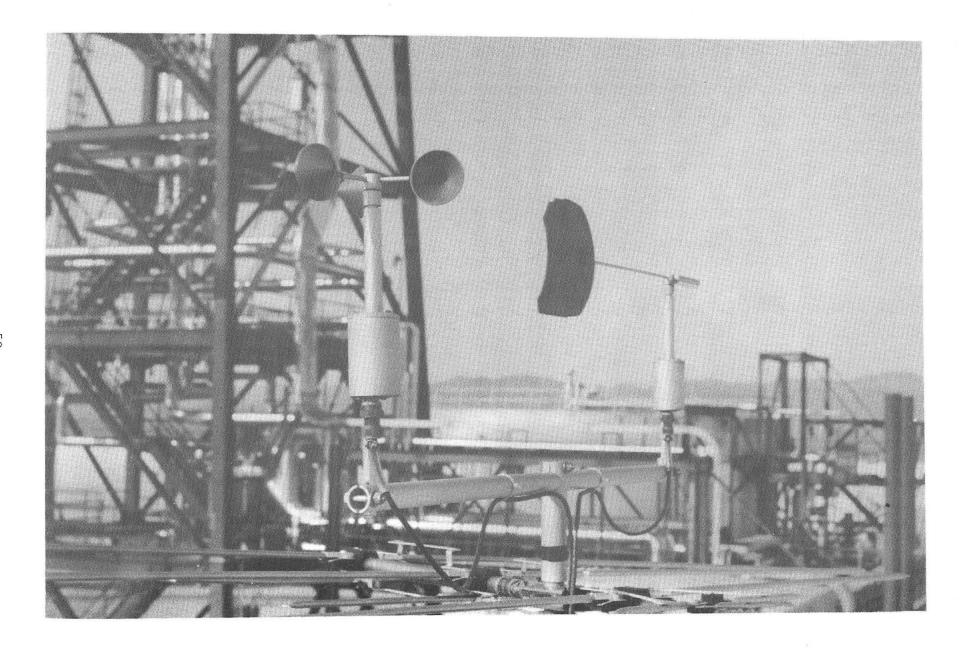


FIGURE 37. WIND SENSOR INSTALLATION - CONTROL ROOM ROOF

are:		Χ	Y
	Hail Cube No. I (NW)	-476.473 ft	-650.038 ft
	Hail Cube No. 2 (NE)	-476.473 ft	+650.038 ft
	(tolerance of + 2 ft)		

The cubes consist of five 1 ft by 1 ft faces of 1 inch thick polystyrofoam which are covered with 1.5 mil thick aluminum foil. A closeup of a hail cube is shown in Figure 38. During 1983, sand shields were installed around the hail cubes located at the four compass point met stations to minimize sand blast damage to the hail cube foil. A sketch of the sand shields is shown in Figure 39. A photo of the south station installation is shown in Figure 40.

# 3.2.10 Pyranometers

Seven pyranometers are located on the four spoke roads for cloud obscuration studies, as shown previously in Figure 8. The specific collector field coordinates for the pyranometers are shown in Table 2.

Table 2. Pyranometer Collector Field Location Coordinates

Pyranometer	Collector Field Co	ordinates
	Χ	Y
South Spoke Road	503.556	-30
West Spoke Road (inner)	-20	-502.282
West Spoke Road (outer)	-22.0	-864.00
North Spoke Road (inner)	-500.701	-20
North Spoke Road (outer)	-853.478	-20
East Spoke Road (inner)	-20	502.282
East Spoke Road (outer)	-22.0	864.00

The pyranometers used are identical to the one installed on the control room roof, as shown in Figure 34. They are each mounted on a tower which is identical to the wind tower design. A spoke road pyranometer tower installation is shown in Figure 41.

## 3.2.11 Instrument Data

The pertinent data for each of the types of meteorological instruments used at the Solar One Site are shown in Table 3.

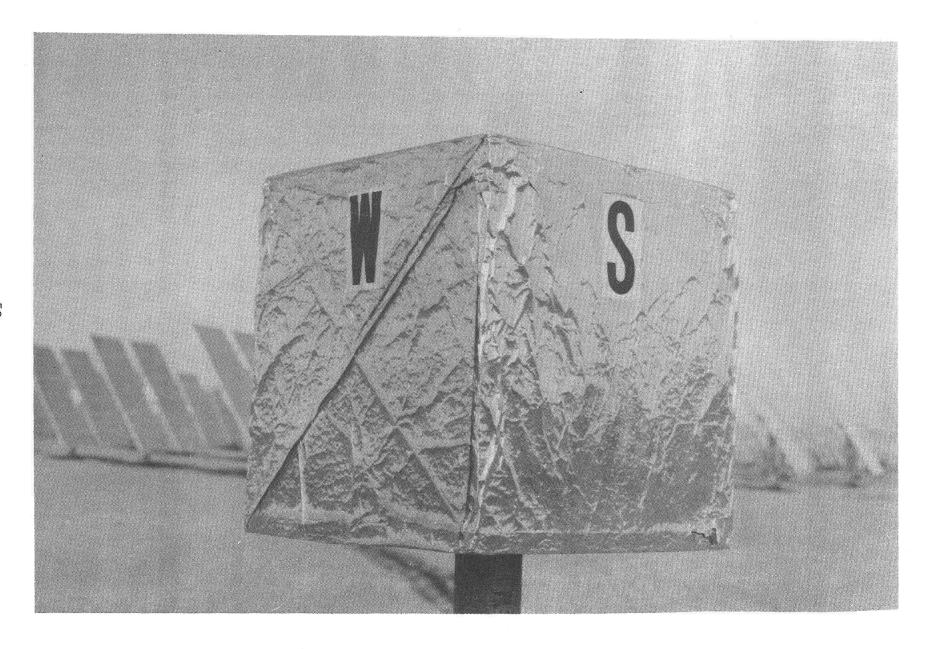


FIGURE 38. HAIL CUBE

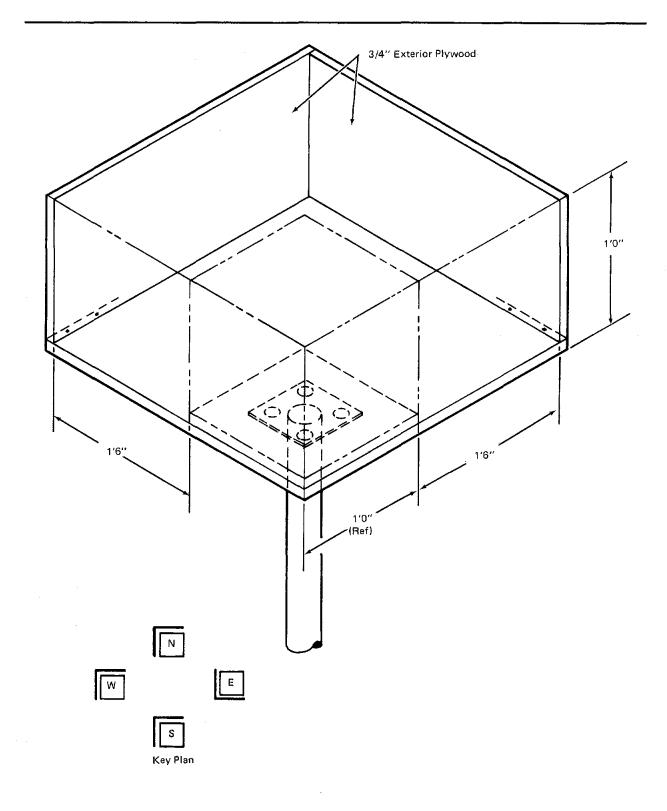


Figure 39. Hail Cube Sand Shield

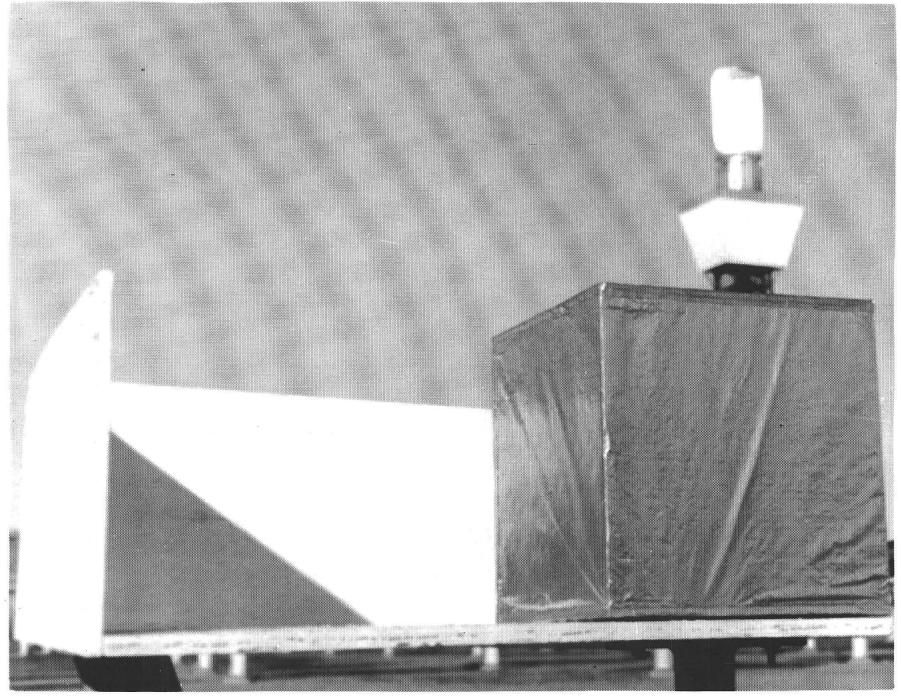


Figure 40. Hail Cube Sand Shield Installation — South Station

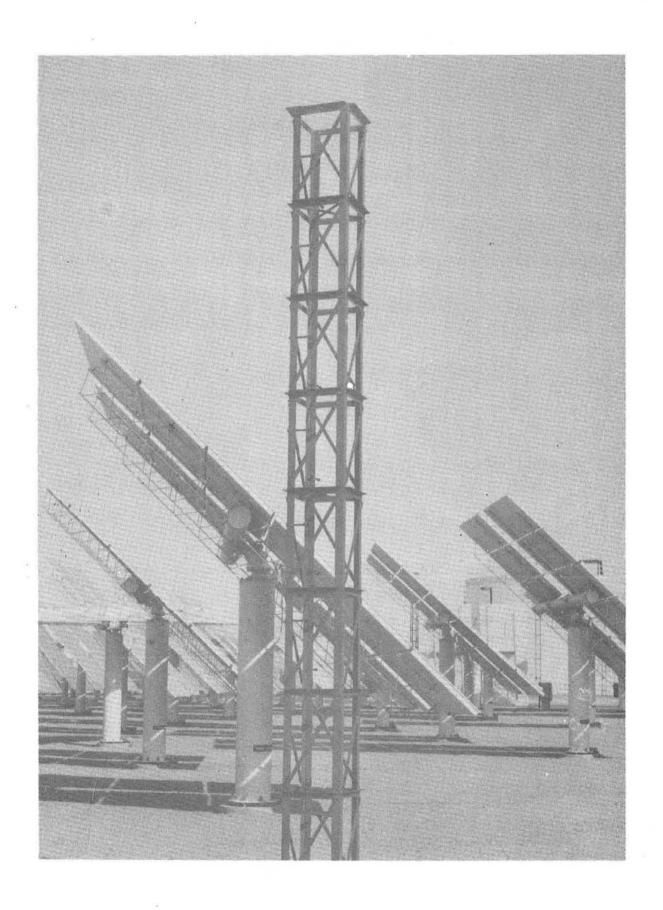


Figure 41. Spoke Road Pyranometer Tower Installation

# Table 3 METEOROLOGICAL INSTRUMENT DATA

SYSTEM

THETOLIMENT	SAMUEACTURE	DAMOR	SYSIEM
INSTRUMENT	MANUFACTURER	RANGE	ACCURACY
<ul> <li>NORMAL INCIDENCE PYHELIOMETER (NIP)</li> </ul>	THE EPPLEY LAB, INC. 12 SHEFFIELD AVE. NEWPORT, RI 02840	0-1394 WATTS/m <sup>2</sup>	<u>+</u> 0.6%
• PYRANOMETER	LI-COR, INC.————————————————————————————————————	0-1250 WATTS/m <sup>2</sup>	<u>+</u> 12 1/4%
• TIPPING BUCKET RAIN GAUGE	METEOROLOGY RESEARCH INC BOX 637 464 W. WOODBURY RD ALTADENA, CA 91001	3 IN/HR	+ 1% + 5%
• NEPHALOMETER	METEOROLOGY RESEARCH INC BOX 637 464 W. WOODBURY RD ALTADENA, CA 91001	40 MILES	<u>+</u> 10%
• DEW POINT SENSOR	CLIMET INSTRUMENT CO. P.O. BOX 151 1320 W. COLTON AVE REDLANDS, CA 92373	0-120°F	<u>+</u> 4%
• CUP ANEMOMETER	CLIMET INSTRUMENTS CO. P.O. BOX 151 1320 W. COLTON AVE. REDLANDS, CA 92373	O-100 MPH -50° - +115°F OPERATING TEMP.	+ 1% OR 0.15 MPH (WHICHEVER IS GREATER)
• WIND VANE	CLIMET INSTRUMENTS CO P.O. BOX 151 1320 W. COLTON AVE. REDLANDS, CA 92373	0-360°	<u>+</u> 3.2%
• HAIL CUBE	NONE (LOCAL FABRICATION)		
PLATINUM RESISTANCE TEMPERATURE SENSOR	ROSEMOUNT, INC. P.O. BOX 35129 MINNEAPOLIS, MINN 55435	0-120°F	<u>+</u> 1/2%
BAROMETRIC PRESSURE	YELLOW SPRINGS INSTR. CO.	24.6-31.5 IN HG	<u>+</u> 0.4%
SENSOR	INDUSTRIAL DIVISION YELLOW SPRINGS, OHIO 45387	-30°F - +180°F OPER. TEMP.	

FOR MORE DETAILS ON THE OPERATION AND MAINTENANCE OF THIS EQUIPMENT, PLEASE REFER TO THE PLANT MAINTENANCE MANUAL, RADL ITEM 2-37, SECTION 8

# SECTION 4

## DATA TAPES

#### 4.1 DESCRIPTION

Summary data tapes have been prepared at McDonnell Douglas and delivered to Sandia for a limited number of tag identifications (ID's), including all of the meteorological measurements of interest, and these data can be used for additional analyses by interested parties. The description of the data tapes is as follows:

- Data have been taken from the archive tapes which contain information for all tag ID's and for the actual data scan rates in effect at the time of the test. The data tapes contain information for approximately 500-900 tag ID's of particular interest, depending upon the month of the year being considered. The data have been written to this tape at 3 minute intervals, with no time averaging.
- Data have been written to tape in 8-bit ASCII. The tapes are 9-track, and have been written at 1600 BPI density through May. All summary data tapes prepared and delivered from June through December have been written at 6250 BPI.
- Each summary data tape contains two weeks of data for the months of January through June. Tapes prepared from July through December contain an entire month's data on a single tape.

#### 4.2 AVAILABILITY

The summary data tapes are currently available from Sandia Livermore for all 12 months of 1983.

## SECTION 5

#### METEOROLOGICAL DATA

#### 5.1 GENERAL

This section contains the meteorological data which were selected from the available data between 1 January and 31 December 1983 for inclusion in this report. The data were principally derived through the computer-centered data reduction system being used at McDonnell Douglas to support the Solar One test program. This system uses a PDP-10 Computer in conjunction with data reduction programs and a Tektronix 4014 printer to produce the plots and tabulations desired.

The plot format has a 10 by 10 grid, on which a maximum of five tag ID's can be plotted. They are identified at the bottom of the page, below the grid. The values of each of the elements of the vertical scale are equal to one-tenth of the range shown for the tag ID. The horizontal time scale is variable, with 1500 minutes being chosen to cover a full day plus, with each element equal to two and one-half hours. The reference time shown is the date of the year, with 1 January being day 001, etc. The start time is shown beside the day, with 00 signifying midnight. The Nth sample average of 1 indicates the data were plotted at 1 minute intervals. In addition to the PDP-10 system, data were obtained from the midnight readings of insolation recorded on the Beckman MV 8000 system, an off-site analysis was performed on the hail cubes, and the rainfall data for this report were obtained from the Barstow-Daggett airport. Additional specific comments are included with the data packages in the following sections.

# 5.2 LIST OF TAG ID'S AND INSTRUMENT

The tag ID's and instruments of interest for the meteorological data report are shown below:

LTX	1806	Tipping Bucket Rain Gauge
TTX	1803	Air Temperature, South Station

	TTX	9002C	Heliostat 1638, MM 7 Temp, Front
	TTX	9002D	Heliostat 1638, MM 7 Temp, Rear
	TTX	9005C	Heliostat 2766, MM 7 Temp, Front
	TTX	9005D	Heliostat 2766, MM 7 Temp, Rear
	MTX	1805	Dewpoint, South Station
	MTX	1832	Dewpoint, Receiver Tower Level 7
	ATX	1817	Normal Incidence Pyrheliometer, North Station
	##ATX	1817A	Normal Incidence Pyrheliometer, Control Room Roof
	ATX	1808	South Station Pyranometer
	ATX	1809	South Spoke Road Pyranometer
	ATX	1812	West Station Pyranometer
	ATX	1813	West Spoke Road Pyranometer, Outer
	ATX	1814	West Spoke Road Pyranometer, Inner
	ATX	1819	North Station Pyranometer
	ATX	1820	North Spoke Road Pyranometer, Outer
	ATX	1821	North Spoke Road Pyranometer, Inner
	ATX	1824	East Station Pyranometer
	ATX	1825 .	East Spoke Road Pyranometer, Outer
	ATX	1826	East Spoke Road Pyranometer, Inner
	ATX	1833	Nephalometer, Receiver Tower Level 7
	ATX	1834	Control Room Roof Pyranometer
Wind	Speed		
	STX	1801	South Station -
	STX	1810	West Station
	STX	1815	North Station
	STX	1822	East Station
	STX	1827	Receiver Tower Level 7, East
	STX	1829	Receiver Tower Level 7, West
	STX	1835	Control Room Roof
	STX	1839	Wind Tower 1, 32.2 Feet
	STX	1840	Wind Tower 1, 20 Feet
	STX	1841	Wind Tower 1, 10 Feet
	STX	1843	Wind Tower 2, 32.2 Feet
	STX	1844	Wind Tower 2, 20 Feet
	STX	1845	Wind Tower 2, 10 Feet
			·

STX	1847	Wind Tower 3, 32.2 Feet
STX	1848	Wind Tower 3, 20 Feet
STX	1849	Wind Tower 3, 10 Feet
STX	1851	Wind Tower 4, 32.2 Feet
STX	1852	Wind Tower 4, 20 Feet
STX	1853	Wind Tower 4, 10 Feet
STX	1855	Wind Tower 5, 32.2 Feet
STX	1856	Wind Tower 5, 20 Feet
STX	1857	Wind Tower 5, 10 Feet
STX	1859	Wind Tower 6, 32.2 Feet
STX	1860	Wind Tower 6, 20 Feet
STX	1861	Wind Tower 6, 10 Feet
Wind Direction		
ОТХ	1802	South Station
OTX	1811	West Station
OTX	1816	North Station
OTX	1823	East Station
OTX	1828	Receiver Tower Level 7, East
ОТХ	1830	Receiver Tower Level 7, West
OTX	1836	Control Room Roof
OTX	1842	Wind Tower 1, 32.2 Feet
OTX	1846	Wind Tower 2, 32.2 Feet
OTX	1850	Wind Tower 3, 32.2 Feet
OTX	1854	Wind Tower 4, 32.2 Feet
OTX	1858	Wind Tower 5, 32.2 Feet
OTX	1862	Wind Tower 6, 32.2 Feet

# 5.3 SPECIFIC COMMENTS ON DATA

The data included in this report have been chosen following an informal discussion of the report format and contents between Sandia and MDAC. Data not published in this report have been submitted to Sandia separately. The total data base recorded on the data acquisition system between 1 January and 31 December 1983 consists of 312 data days. All of these days have been processed and insolation data and summary wind data are included in the report.

Additional comments pertinent to the particular type of meteorological data presented are contained in the following major paragraphs of this section.

Specific comments about the data shown or not shown on the plots are as follows:

- 1. If a tag ID listing is followed by a "tag ID not available," this tag ID was not on the scan list on the day the data were recorded. This may be the case even though the instrument was working.
- 2. If a tag ID listed on the plot shows no data, the instrument was not operating at all, or was operating and reading zero.
- 3. If the data for a tag ID show for only part of a day, the data acquisition system was very probably not archiving data for the missing time periods.

#### 5.4 RAINFALL DATA

A tipping bucket rain gauge (tag ID LTX 1806) is installed at the south meteorological station at Solar One. It is operational, but because of uncertainty in the accuracy of the data, and because it cannot be guaranteed that the data acquisition system will be operating at any time that precipitation occurs, a summary of rainfall as recorded at the Barstow-Daggett airport has been included in Table 4 to provide representative data for the Solar One Site.

The total rainfall recorded for 1983 was 9.48 inches, as compared to 6.32 inches for 1982. The data indicate that 1983 was an unusually heavy rainfall year, since the average annual rainfall for the 15 year period from 1956-1970 is 3.6 inches. In spite of the heavy annual rainfall, it is interesting to note that there was no rainfall during the months of May, June, and July, during 1983. June was the only month in 1982 during which there was no rainfall. The 1956-1970 data indicates that May and June are the lowest rainfall months, but that July generally does have some rainfall. August was the heaviest rainfall month in both 1983 and 1982, which is also consistent with the 1956-1970 data, which indicate that August is the month for heaviest rainfall during the year.

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Table 4. Daggett Rainfall Summary (All Rainfall Values are in Inches)

						MONTH						
<u> 1956 - 1970 Data</u>	J	F	М	Α	M	J	J	Α	S	0	N	D
Ave/Month	0.31	0.32	0.28	0.21	0.07	0.05	0.31	0.60	0.51	0.22	0.37	0.35
Max/Month	0.90	1.50	1.01	1.83	0.49	0.32	0.96	3.22	2.31	1.01	1.74	2.02
Max/24 Hours	0.73	0.70	0.88	0.65	0.37	0.32	0.96	2.06	1.11	0.66	1.08	1.01
Ave Occur/Month	3.20	3.30	2.40	2.10	0.70	0.50	1.80	2.40	1.60	1.90	3.30	2.70
Months With No Rain	-0-	2	2	3	10	10	2	4	6	5	1	4
1983 Data												
Rainfall	1.15	1.08	1.83	0.54	-0-	-0-	-0-	2.59	0.14	1.15	0.30	0.70
Max/24 Hours	0.42	0.33	0.72	0.38	-0-	-0-	-0-	1.01	0.12	0.73	0.28	0.49
No. of Occurrences	7	12	13	6	-0-	-0-	-0-	13	4	5	3	3

## 5.5 TEMPERATURE DATA

Monthly ranges of low and high air temperatures recorded at Solar One during 1983 are shown in Table 5. The data show that low temperatures below freezing were recorded during January, November, and December, during 1983, with 27°F being the lowest temperature recorded for the year. During 1982, below freezing temperatures were recorded during the months of January, February, and December, with 21°F being recorded in January as the lowest temperature for the year. The range of low temperatures recorded at Solar One was basically the same for 1983 and 1982. Similarly, the range of high temperatures for 1983 and 1982 showed about the same characteristics when compared on a month to month basis. Temperatures in excess of 100°F were recorded during May, June, July, August, and September during 1983, with 108°F recorded as the highest temperature, which occurred during July and August. In 1982, temperatures in excess of 100°F were recorded during June, July, August, and September, with the yearly high of 107°F occurring during August and September.

During 1983, the temperatures of the front and rear of mirror module 7 on two specially instrumented heliostats (1638 and 2766) were recorded and compared to the dewpoint at the south station to identify days when the dewpoint equalled or exceeded the mirror module temperatures. The time period examined was from 0400 to 0900 hours. From the total number of 312 data days examined, there were 32 days when the dewpoint equalled or exceeded the mirror module temperatures on at least one of the heliostats. The days when this occurred were:

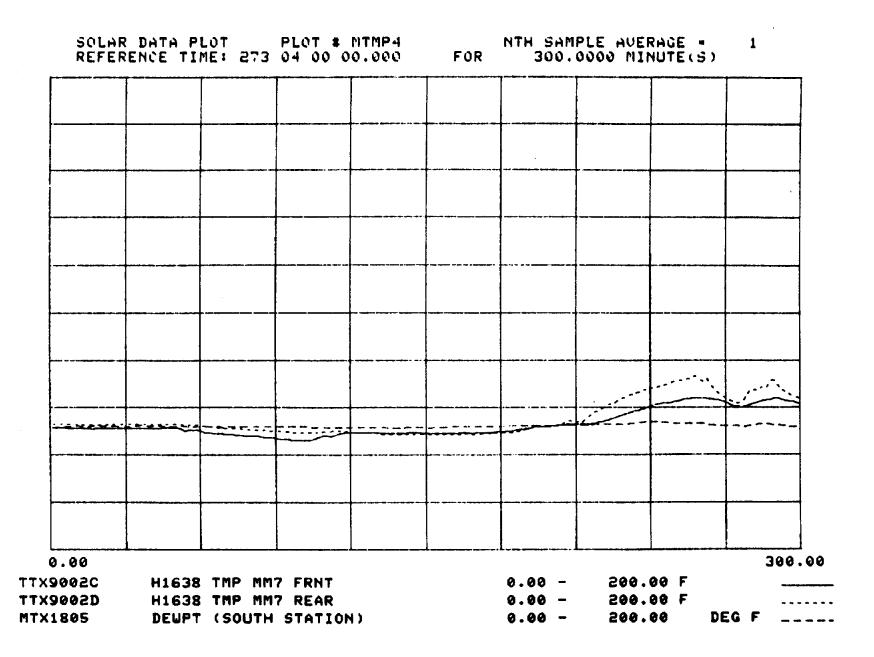
022	091	281
023	231	282
036	233	289
037	264	306
038	266	333
043	267	336
055	273	345
057	274*	348
059	276	357
071	278	359*
083	280*	

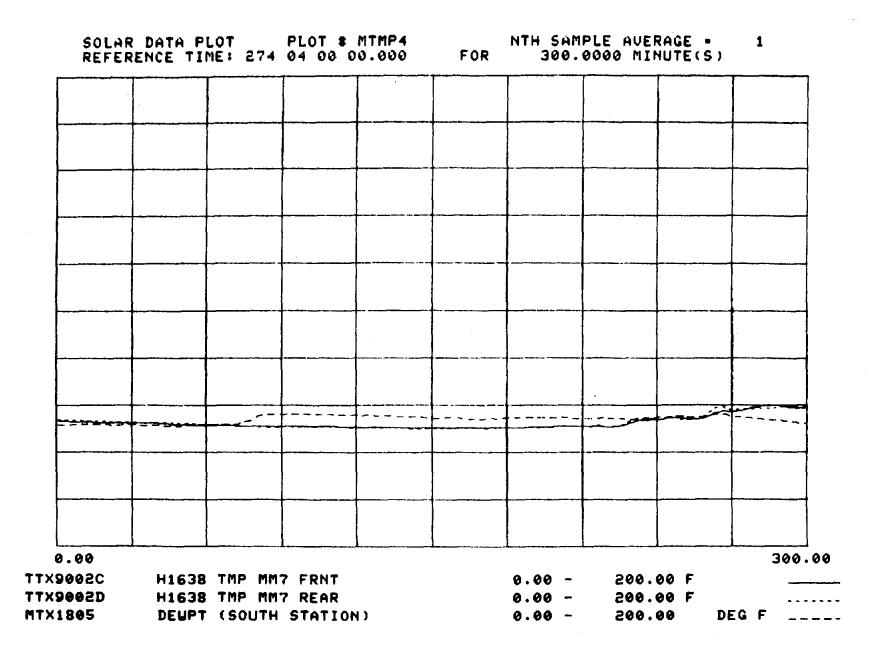
<sup>\*</sup>On these days, the dewpoint equalled or exceeded the mirror module temperatures on both heliostats 1638 and 2766.

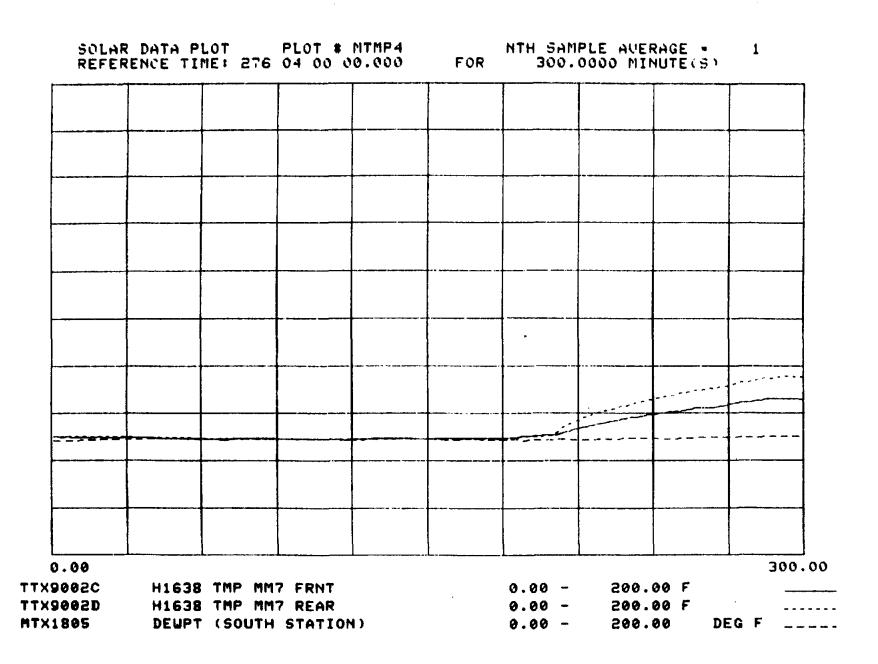
Table 5. HIGH AND LOW TEMPERATURE RANGES AT SOLAR ONE - 1983

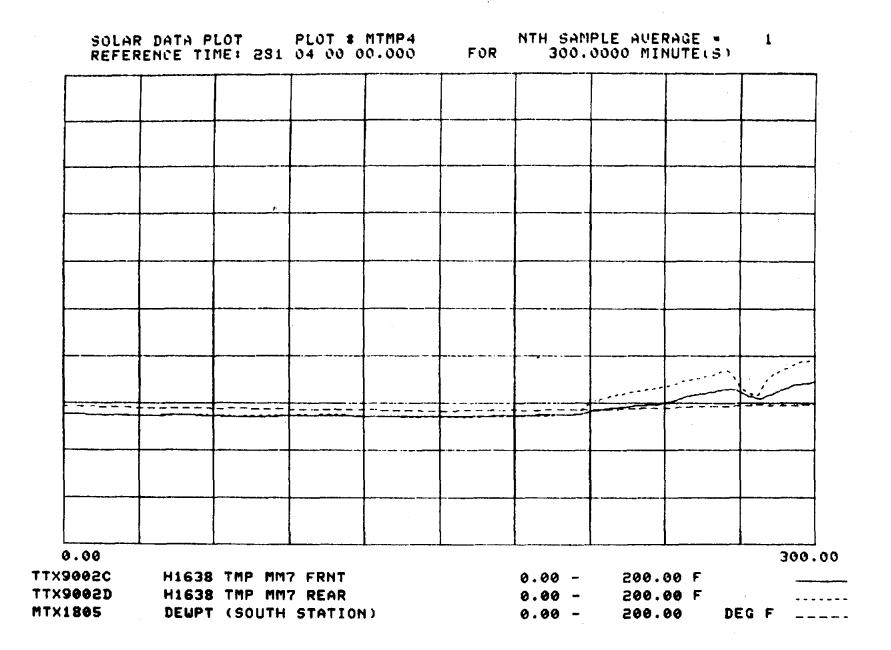
MONTH	RANGE OF LOW TEMPERATURES (°F)	RANGE OF HIGH TEMPERATURES (°F)
January	27-49	48-69
February	34-50	40-72
March	37-55	62-75
April	36-51	57-80
May	44-75	63-105
June	53 <b>-</b> 77	76-104
July	58-81	88-108
August	60-84	72-108
September	60-79	69-104
October	50-62	60-84
November	29-55	50-81
December	31 -54	50-67

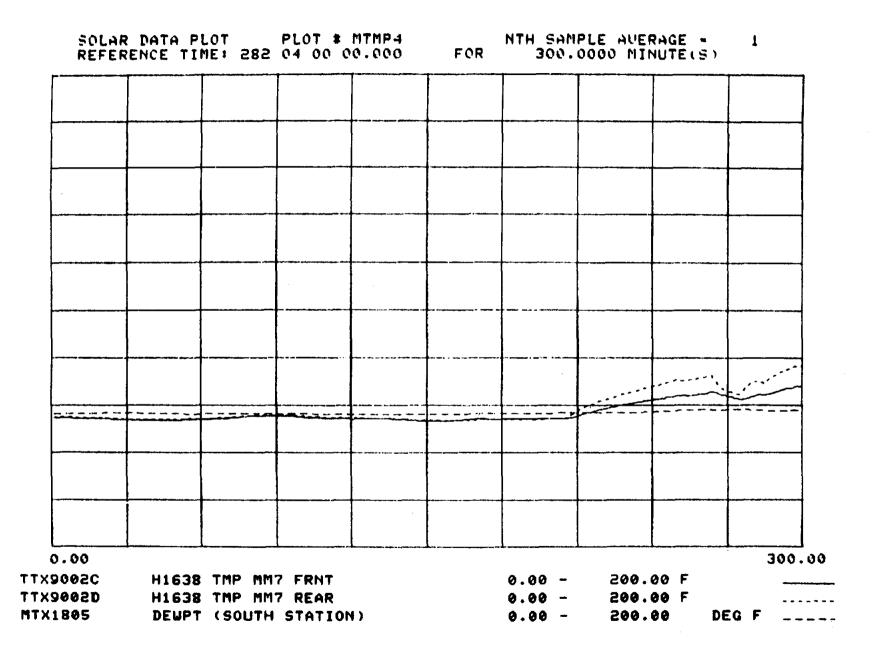
Plots for 6 days of data are included in this report for heliostat 1638. The specific days are 273, 274, 276, 281, 282, and 359. The plots show that the dewpoint reaches or exceeds the mirror module temperatures at around 0400 to 0515 hours. This condition continues until around 0715 to 0800, at which time the mirror modules warm up to stop any further condensation. It should be noted that the wiring for the front and rear mirror module temperatures on heliostat 1638 (TTX 9002C and TTX 9002D) were reversed until 12 October 1983 (day 285), so the data shown on the first five plots are indicating temperatures for the opposite side of the mirror modules relative to what the plot legend indicates. Mirror module temperature traces for day 359 are labelled correctly. With this clarification, it can be seen that the mirror module front face temperatures warm up faster than the back after the sun comes up. The history of the mirror orientation has not been specifically defined for each of these plots, but presumably the mirror modules are in a face-down stow position at the beginning of these plots, with a transition from facedown stow to standby position being completed before sunrise.

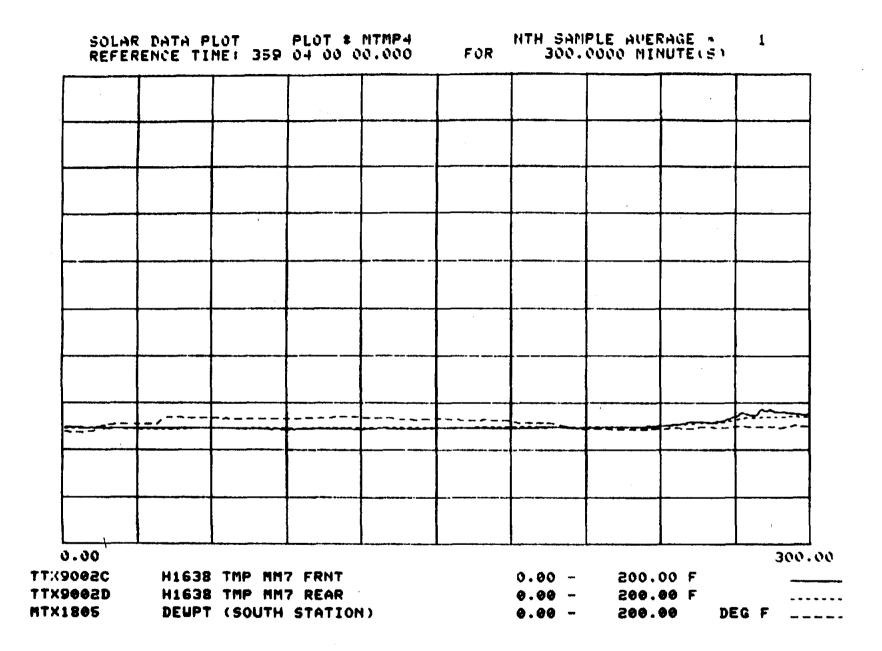












## 5.6 WIND DATA

Wind data were recorded for 312 days at Solar One during 1983. Wind speed and wind direction were recorded for all of the STX and OTX tag ID's listed in Section 5.2 during each of the data days, with the exceptions of any days when a particular instrument was not operational, and for STX 1835 and OTX 1836, which are wind speed and direction instruments on the control room roof that were control room readouts only until they were also wired to DAS in August. Wind speed and direction data for the south, west, north, and east meteorological stations and the control room roof were selected and included in this report following discussions with Sandia.

The wind speed and direction data included in this report are summarized on an annual and monthly basis. These data are derived from the daily summaries, which have been sent to Sandia separately. Figure 42 shows the wind velocity distribution at Solar One for 1983 when the data acquisition system was archiving data (312 days), and when the NIP value exceeded 450 watts/m<sup>2</sup> sometime during the day. This NIP value qualification caused wind data from 36 of the 312 days to be zeroed out, with the inference being that the wind data for a given day are not of interest in this report unless insolation values reach at least 450 watts/m<sup>2</sup> to permit startup of the Solar One plant. The figure indicates that there were 276 days during which the wind velocity reached speeds in excess of 5 miles per hour. Figure 42 also shows that there were 263 days when the wind speed exceeded 10 miles per hour. This means there were 13 days (276-263) with maximum wind speeds in the 5-10 miles per hour range. The number of days when wind velocities were reached in each of the 5 mph ranges can be determined by taking the difference between the number of days indicated in parentheses at adjacent wind velocities. The wind velocity distribution shown on the figure indicates that high winds, that is, values above 40 miles per hour, have not been a major constraint on Solar One operations during 1983. The maximum wind velocity recorded in each month of 1983 was as follows:

Month	Maximum	Wind	Velocity,	MPH
Jan		44		
Feb		56		
Mar		50		
Apr		54		

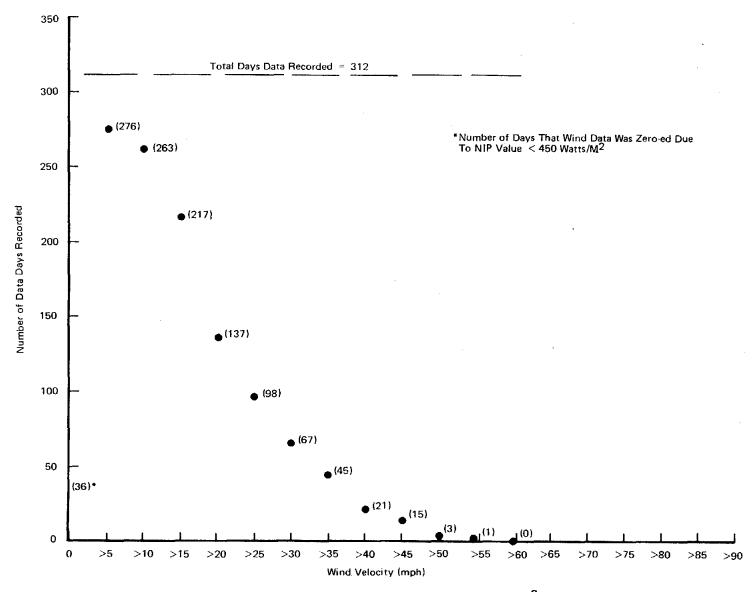


Figure 42. Solar One Wind Velocity Distribution (When Recording Data and With NIP Value > 450 Watts/m<sup>2</sup>)

Month	Maximum	Wind	Velocity,	MPH
May		48		
Jun	*	48		
Ju1		40		
Aug		38		
Sep		36		
0ct		42		
Nov		60		
Dec		52		

Table 6 shows the number of days during each month when wind speeds exceeded 30 miles per hour at Solar One during 1983. The total number for the year was 67, compared to 48 days for 1982, as measured at the Daggett airport. Data are also shown for each of 5 cup anemometers to indicate the total number of data samples recorded by each instrument per month, and the number of data samples within that population that were taken with wind speeds over 30 miles per hour. The equivalent percentage value is tabulated for each instrument and each month. Because of the integer arithmetic used by the computer, the ratio of data samples above 30 miles per hour to total data samples has to equal at least 1 percent in order to register anything above O percent, etc. It can be seen from the data on Table 6 that wind speeds at Solar One were not above 30 miles per hour for any significant time periods. This finding also substantiates the statement that high winds were not a major factor influencing Solar One plant operation during 1983. It should be noted that the meteorological data are recorded at 1 minute intervals when wind speeds are below 45 miles per hour and at 1 second intervals above 45 miles per hour, so the number of data samples are recorded at a rate 60 times faster at the high velocities. Even with this bias, the percent of data samples recorded above 30 miles per hour is still small.

	D	AYS		STX1801		STX1810		STX1815		STX1822		STX1835	
JAN		TOT	27	27476	100	27366	100	27465	100	0	0	Ø	0
	>	30	5	162	0	167	0	176	0	0	0	0	0
FEB		TOT	24	13643	100	13692	100	13510	100	12620	100	0	0
	>	30	2	832	6	714	5	775	5	507	4	0	0
MAR		TOT	25	13359	100	<b>2</b> 1692	100	21691	100	11170	100	0	0
	>	30	8	1273	9	1086	5	1119	5	23	0	0	0
APR		TOT	<b>5</b> 6	29930	100	30642	100	29959	100	24546	100	0	0
	>	30	9	2492	8	2372	7	2423	8	201	0	0	Ø
MAY		TOT	31	19684	100	19682	100	19670	100	19674	100	0	0
	>	30	10	964	4	739	3	1023	5	327	· 1	0	0
JUN		TOT	26	14544	100	14544	100	14541	100	14544	100	0	0
	>	30	6	120	0	65	0	134	0	80	0	0	0
JUL		TOT	18	11662	100	11662	100	11663	100	11663	100	0	Ø
	>	30	8	68	0	51	0	84	0	- 59	Ø	0	Ø
AUG		TOT	20	5951	100	<b>59</b> 51	100	5951	100	5951	100	4902	100
	>	30	1	0	0	0	Ø	1	0	0	0	Ø	0
SEP		TOT	26	29334	100	27874	100	29334	100	29334-	100	29158	100
	>	30	2	5	0	1	0	5	0	0	0	1	0
OCT		TOT	<b>2</b> 9	13337	100	13337	100	13337	100	13337	100	11767	100
	>	30	2	81	0	43	0	107	0	2	0	78	ø
NOU		TOT	29	27371	100	8558	100	27312	100	27337	100	24981	100
	>	30	8	2858	10	526	6	2909	10	474	1	3590	14
DEC		TOT	31	18175	100	18862	100	19789	100	86003	100	4571	
	>		9	785	4	780	4	709	3	591	2	194	4

Annual and monthly wind speed and wind direction summaries for the 4 meteorological stations and the control room roof are included in this report on the following pages. Pertinent comments about wind speeds have already been made in previous paragraphs while discussing Figure 42 and Table 6; however, it is interesting to look at the annual wind direction distribution and draw some conclusions regarding the prevailing wind directions at Solar One for 1983. An analysis of the tabular data presented for annual wind direction, including some adjustments in percentage values to compensate for the rounding-off errors associated with the integer arithmetic, yields the following observations:

Wind Direction (360° = N = 0°)	Percentage of Time (Average of 5 Sensors)
NW-NE Quadrant (315° - 45°)	17
NE-SE Quadrant (45° - 135°)	20
SE-SW Quadrant (135° - 225°)	14
SW-NW Quadrant (225° - 315°)	49

Prevailing winds at the Solar One site are from a westerly direction, with minimal wind activity from the south, and moderate activity from the north and east.

PAGE 1
SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR PERIOD - FULL YEAR 83 - WITH NIPS IN EXCESS OF 450 W/M2

МРН	STX1801*		STX1810*		STX1815*		STX1822*		STX1835*	
0	3078	1%	4158	1%	4481	1%	1172	0 X	270	0 X
2	14151	6%	14226	6×	13523	5×	12551	6%	10767	14%
4	29355	13x	29778	13%	29483	12%	25396	13%	17222	25×
6	38878	17×	35796	16%	38348	16X	34565	18%	11100	14%
8	33970	15×	32509	15%	33306	14%	30914	16%	6834	9%
10	22036	9%	25219	11%	25455	10%	22419	11%	5127	6%
12	20594	9%	17730	8*	18481	7%	16056	8%	3115	48
14	8471	3%	11559	5%	12843	5×	12218	6%	2641	3%
16	6849	3%	8148	3%	9567	48	9369	4%	1948	2%
18	5943	2*	6772	ЗХ	7932	Эх	7310	3%	1859	2×
20	5904	2×	5603	2×	7095	3%	5383	2%	1829	- 5x
22	6158	2×	4560	2×	6151	SX	3767	1%	1797	5x
24	5095	2×	3678	1%	5444	SX	2474	1%	1783	2×
26	4301	1%	<b>2938</b>	1%	4812	2×	1897	0×	1818	5x
28	5507	2×	2524	1%	4258	1%	1395	0×	1683	SX
30	4536	2×	2120	0 X	3578	1×	1064	0×	1723	2×
32	3162	1 %	1643	0×	2814	1%	723	0×	1376	1%
34	2135	0×	1367	<b>8</b> ×	2048	0×	485	0×	858	1%
36	1446	0 ×	1081	0×	1378	0×	368	0×	639	0 X
38	1339	0 X	882	<b>0</b> %	952	0×	243	0×	408	0%
40	690	0×	665	0×	695	0×	149	0×	208	0×
42	437	0×	459	0 X	471	0×	96	0×	187	0%
44	538	0×	225	0×	293	0×	74	0×	88	Ø×
46	151	0 X	167	. <b>0</b> %	536	0×	91	0×	63	0 X
48	36	0×	44	<b>0</b> ×	808	0×	. 26	0×	19	0×
50	5	0 X	9	<b>0</b> ×	55	0×	8	0×	7	<b>0</b> %

PAGE 2
SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR PERIOD - FULL YEAR 83 - WITH NIPS IN EXCESS OF 450 W/M2

МРН	STX1801*		STX1801* STX1810*		ð*	STX1815#		\$18182		STX1835*	
52	1	0X	2	0×	11	0 X	2	0×	4	<b>0</b> %	
54	0	0 ×	0	ØX	4	øx	9	0×	3	0×	
56	0	0×	0	0×	9	0×	0	0 X	S	0 X	
58	0	0%	0	øx	Ø.	0×	. 0	0 X	0	0X	
60	0	0×	Ö	0%	ø	0×	ě	0×		0%	
62	0	0×	ø	0%	ŏ	0 X	0	0 X	1 0		
64	0	0 X	ě	0×	ě	0 X	0	0×	. 0	0 X	
66	0	0×	0	0×	ě	0×	ě	0×	- 0	0× 0×	
68	0	0×	ø	0×	ě	0×	0	0×	0	0×	
70	0	0×	. 0	0 X	ĕ	0×	0	0×			
72	0	0×	9	0×	ő	0×			0	0 X	
74	ø	0×	ŏ	0×	9	0 X	0	0 X	0	0 X	
76	ø	0%	ŏ	0×	0	0X	0	0 X 0 X	0	0 X	
78	Ö	0%	ŏ	0 X	ő	0×	. 0	0 X	0	0×	
80	Ø	0 X	ő	0×	0	0 X			0	0 X	
82	0	øx	ő	0×	ø	0 X	9	0 X	0	0 X	
84	ő	øx	ő	0×	0	0X	0	0 X 0 X	0	0%	
86	0	0 X	ő	ø×	ŏ	0 X	0	0 X	0	0 X 0 X	
88	0	0×	Ö	0×	ŏ	0 X	. 0	0 X	9	0%	
90	0	0 X	8	0×	ě	0 X	0	0%	0	0 X	
92	0	0 X	ő	0 ×	ő	0 X	0	0 X	0	04	
94	0	ØX	ő	0 X	Ď	0×	9	0 X	0	0%	
96	0	0 X	ø	0×	ŏ	0×	0	0 X		0 X	
98	Õ	0 X	ŏ	0×	• 0	0×	0	0 X	0		
100	0	014	Ö	0×	. 0	0 X	0	0 X	0	0× 0×	

PAGE 1
SOLAR ONE WIND (DEGREE) DISTRIBUTION FOR PLOT MD01
TEST DATA FOR PERIOD - FULL YEAR 83 - WITH NIPS IN EXCESS OF 450 W/M2

DEG	OTX180	2*	0TX181	1*	0TX181	<b>6</b> *	OTX182	3 <b>*</b>	0TX183	<b>6</b> *
0	3017	1%	12333	5%	5141	2%	9362	4%	1003	1%
15	3076	1%	4465	1%	3987	1%	4620	2%	2176	5%
30	3327	1%	4057	1%	5107	2%	4493	2%	2959	3%
45	4795	2%	6097	2%	7618	3%	6009	3%	3660	4%
60	7740	3%	9164	.3%	10111	4%	7950	4%	3441	4%
75	13909	6%	11641	5%	10836	4%	10099	5%	2488	3%
90	12141	5%	10032	4%	10917	4%	10341	5%	1501	1%
105	8655	3%	9040	3%	8628	3%	8237	4%	1277	1%
120	5177	2%	6667	2%	4446	1%	6012	3%	2581	3%
135	2525	1%	4853	2%	2827	1%	3457	1%	2809	3%
150	2808	1%	3479	1%	1920	0%	2372	1%	1826	2%
165	1876	0%	2290	0%	1896	0%	1786	0%	1578	5%
180	1605	0%	2092	0%	2326	0%	1763	0%	1089	1%
195	2542	1%	4044	1%	4333	1%	2151	1%	1208	1%
210	3336	1%	4193	1%	11266	4%	3887	2%	2372	3%
225	4873	2%	7414	3%	20599	8%	7885	4%	2957	3%
240	13529	5%	11483	4%	35144	14%	12411	6%	5835	7%
255	27702	12%	21693	9%	32664	13%	15088	7%	9207	12%
270	23071	10%	30602	13%	23580	10%	16183	8%	11874	15%
285	32402	14%	25007	10%	14956	6%	19229	9%	7983	10%
300	21339	9%	17128	7%	6294	2%	17199	8%	2759	3%
315	10746	4%	12075	5%	3771	1%	11422	5%	985	1%
330	7603	·3%	6460	2%	2759	1 %	5651	2%	690	0%
345	7219	3%	3310	1%	2462	1%	3239	1%	746	0%
360	1936	0%	1588	0%	1350	0%	1717	0%	512	0%

PAGE 1
SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - JANUARY - WITH NIPS IN EXCESS OF 450 W/M2

	-									•
NPH	STX1801*		STX181	1810* STX1815		315* STX1822*		3*	* STX1835*	
0	770	2%	1425	5%	1677	6%	0	0%	0	0%
2	2544	9%	2336	8%	2655	9%	0	0%	ø	0%
4	3771	13%	4169	15%	4027	14%	0	0%	ō.	0%
6	7014	25%	6529	23%	6985	25%	0	0%	0	0%
8	5622	20%	5324	19%	4909	17%	0	0%	ø	0%
10	2950	10%	2884	10%	2693	9%	0	0%	. 0	0%
12	2414	8%	2014	7%	1725	6%	0	0%	0	0%
14	656	2%	942	3%	942	3%	0	0%	Õ	0%
16	359	1 %	414	1%	445	1 %	0	0%	0	0%
18	275	1 %	293	1%	323	1 %	0	0%	0	0%
20	235	0%	203	0%	242	0%	0	0%	0	0%
22	239	0%	176	0%	224	0%	0	0%	0	0%
24	186	0%	197	0%	177	0%	0	0%	0	0%
26	5	0%	2	0%	5	0%	0	0%	0	0%
28	156	0%	164	0%	144	0%	0	0%	0	0%
30	118	0%	127	0%	116	0%	0	0%	0	0%
32	64	0%	69	0%	73	0%	0	0%	0	9%
34	48	0%	43	0%	59	0%	0	0%	0	0%
36	25	0%	35	0%	24	0%	0	0%	0	0%
38	21	0%	13	0%	10	0%	0	0%	0	0%
40	3	0%	3	0%	8	0%	0	0%	0	0%
42	1	0%	1	0%	1	0%	0	0%	0	0%
44	0	0%	3	0%	<b>1</b>	0%	0	0%	0	<b>0%</b>
46	0	0 X	0	0%	0	0%	Ø	<b>0</b> %	0	0%
48	0	0%	Ø	0%	0	0×	0	0×	0	0%
50	0	<b>0</b> %	0	<b>0</b> %	0	0%	0	<b>0</b> %	0	0%

PAGE 1
SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - JANUARY - WITH NIPS IN EXCESS OF 450 W/M2

15	DEG	0TX1802*		OTX1802* OTX1811*		OTX1816*		0TX1823*		0TX1836*	
15		146	0X	1969	7%	230	<b>0</b> %	0	<b>8</b> %	0	0×
30	15	240	0 X	1064	3%		0×				0×
45 659 2x 749 2x 786 2x 0 0x 0 0x 60 60 927 3x 1160 4x 1328 4x 0 0x 0 0x 75 1635 5x 1695 6x 1920 6x 0 0x 0 0x 90 1664 5x 1422 5x 1816 6x 0 0x 0 0x 105 747 2x 1434 5x 1086 3x 0 0x 0 0x 120 868 3x 1033 3x 509 1x 0 0x 0 0x 135 361 1x 601 2x 422 1x 0 0x 0 0x 150 325 1x 484 1x 315 1x 0 0x 0 0x 165 219 0x 317 1x 269 0x 0 0x 0 0x 180 155 0x 249 0x 280 1x 0 0x 0 0x 195 144 0x 311 1x 302 1x 0 0x 0 0x 195 144 0x 311 1x 302 1x 0 0x 0 0x 125 587 2x 504 1x 4243 15x 0 0x 0 0x 125 6975 25x 3599 13x 3305 11x 0 0x 0 0x 0 0x 255 6975 25x 3599 13x 3305 11x 0 0x 0 0x 0 0x 285 2386 8x 2103 7x 1316 4x 0 0x 0 0x 0 0x 285 2386 8x 2103 7x 1316 4x 0 0x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x 0 0x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x 0 0x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x 0 0x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x 0 0x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x 0 0x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x		350									9%
60       927       3x       1160       4x       1328       4x       0       0x       0       0x         75       1635       5x       1695       6x       1920       6x       0       0x       0       0x         90       1664       5x       1422       5x       1816       6x       0       0x       0       0x         105       747       2x       1434       5x       1086       3x       0       0x       0       0x         120       868       3x       1033       3x       509       1x       0       0x       0       0x         135       361       1x       601       2x       422       1x       0       0x       0       0x         150       325       1x       484       1x       315       x       0       0x       0       0x         165       219       0x       249       0x       280       1x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144 <td< td=""><td>45</td><td>659</td><td>SX</td><td>749</td><td>2x</td><td></td><td></td><td></td><td></td><td></td><td>0%</td></td<>	45	659	SX	749	2x						0%
75       1635       5x       1695       6x       1920       6x       0       0x       0       0x         90       1664       5x       1422       5x       1816       6x       0       0x       0       0x         105       747       2x       1434       5x       1086       3x       0       0x       0       0x         120       868       3x       1033       3x       509       1x       0       0x       0       0x         135       361       1x       601       2x       422       1x       0       0x       0       0x         150       325       1x       484       1x       315       1x       0       0x       0       0x         165       219       0x       317       1x       269       0x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279 <td< td=""><td>60</td><td>927</td><td>3%</td><td>1160</td><td>48</td><td></td><td></td><td></td><td></td><td></td><td>0×</td></td<>	60	927	3%	1160	48						0×
90	75	1635									
105       747       2x       1434       5x       1086       3x       0       0x       0       0x         120       868       3x       1033       3x       509       1x       0       0x       0       0x         135       361       1x       601       2x       422       1x       0       0x       0       0x         150       325       1x       484       1x       315       1x       0       0x       0       0x         165       219       0x       317       1x       269       0x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975											0%
120       868       3x       1033       3x       509       1x       0       0x       0       0x         135       361       1x       601       2x       422       1x       0       0x       0       0x         150       325       1x       484       1x       315       1x       0       0x       0       0x         165       219       0x       317       1x       269       0x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         270       3164											0%
135       361       1x       601       2x       422       1x       0       0x       0       0x         150       325       1x       484       1x       315       1x       0       0x       0       0x         165       219       0x       317       1x       269       0x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0x       0x         285       2386		868									
150       325       1x       484       1x       315       1x       0       0x       0       0x         165       219       0x       317       1x       269       0x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942		361									
165       219       0x       317       1x       269       0x       0       0x       0       0x         180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         270       3164       11x       3216       11x       1909       6x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         315       591	150							-			
180       155       0x       249       0x       280       1x       0       0x       0       0x         195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         270       3164       11x       3216       11x       1909       6x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942       3x       1437       5x       435       1x       0       0x       0       0x         315       59											
195       144       0x       311       1x       302       1x       0       0x       0       0x         210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         270       3164       11x       3216       11x       1909       6x       0       0x       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942       3x       1437       5x       435       1x       0       0x       0       0x         315       591       2x       1134       4x       320       1x       0       0x       0x         330       408       1x <t< td=""><td></td><td></td><td>0 X</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>			0 X								
210       279       1x       386       1x       1406       5x       0       0x       0       0x         225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         270       3164       11x       3216       11x       1909       6x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942       3x       1437       5x       435       1x       0       0x       0       0x         315       591       2x       1134       4x       320       1x       0       0x       0       0x         330       408       1x       524       1x       133       0x       0       0x       0x         345       468 <td< td=""><td>195</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	195										
225       587       2x       504       1x       4243       15x       0       0x       0       0x         240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         270       3164       11x       3216       11x       1909       6x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942       3x       1437       5x       435       1x       0       0x       0       0x         315       591       2x       1134       4x       320       1x       0       0x       0       0x         330       408       1x       524       1x       133       0x       0       0x       0       0x         345       468       1x       224       0x       110       0x       0       0x       0x											
240       3222       11x       1373       4x       4797       17x       0       0x       0       0x         255       6975       25x       3599       13x       3305       11x       0       0x       0       0x         270       3164       11x       3216       11x       1909       6x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942       3x       1437       5x       435       1x       0       0x       0       0x         315       591       2x       1134       4x       320       1x       0       0x       0       0x         330       408       1x       524       1x       133       0x       0       0x       0       0x         345       468       1x       224       0x       110       0x       0       0x       0       0x											
255 6975 25x 3599 13x 3305 11x 0 0x 0 0x 270 3164 11x 3216 11x 1909 6x 0 0x 0 0x 285 2386 8x 2103 7x 1316 4x 0 0x 0 0x 300 942 3x 1437 5x 435 1x 0 0x 0 0x 315 591 2x 1134 4x 320 1x 0 0x 0 0x 330 408 1x 524 1x 133 0x 0 0x 0 0x 345 468 1x 224 0x 110 0x 0 0x 0 0x											
270       3164       11x       3216       11x       1909       6x       0       0x       0       0x         285       2386       8x       2103       7x       1316       4x       0       0x       0       0x         300       942       3x       1437       5x       435       1x       0       0x       0       0x         315       591       2x       1134       4x       320       1x       0       0x       0       0x         330       408       1x       524       1x       133       0x       0       0x       0       0x         345       468       1x       224       0x       110       0x       0       0x       0       0x											
285											
300     942     3x     1437     5x     435     1x     0     0x     0     0x       315     591     2x     1134     4x     320     1x     0     0x     0     0x       330     408     1x     524     1x     133     0x     0     0x     0     0x       345     468     1x     224     0x     110     0x     0     0x     0     0x											
315 591 2x 1134 4x 320 1x 0 0x 0 0x 330 408 1x 524 1x 133 0x 0 0x 0 0x 345 468 1x 224 0x 110 0x 0 0x 0 0x											
330 408 1% 524 1% 133 0% 0 0% 0 0% 345 468 1% 224 0% 110 0% 0 0% 0 0%											
345 468 1% 224 0% 110 0% 0 0% 0 0%											
											0×
360 349 1% 77 0% 120 0% 0 0% 0 0%	360	349	1%	77	0×						0×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - FEBRUARY - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX1801*		STX1801* STX1810*		STX1815*		STX1822*		STX1835*	
0	467	3%	567	3%	225	1×	808	1%	0	<b>0%</b>
2	1432	9%	1463	9%	1534	10%	1027	7%	ø	0%
4	2587	17%	2871	19%	2312	15%	2460	18%	0	0%
6	2966	20%	2571	17%	2725	18%	2752	20%	0	0%
8	1662	11%	1634	11%	2138	14%	2090	15%	0	0%
10	928	6%	1070	7%	1148	7%	1114	8%	0	0%
12	1199	8%	792	5%	847	5%	707	5%	0	0%
14	408	2%	538	3%	482	3%	530	3%	0	0%
16	217	1%	312	2%	319	2%	366	2%	0	0%
18	143	0%	206	1%	231	1%	346	2%	0	0%
20	150	1%	172	1%	186	1 %	279	2%	0	0%
22	535	1%	235	1%	197	1%	229	1%	0	0%
24	281	1%	305	2%	262	1%	216	1 %	0	0%
26	203	1%	355	2%	272	1%	193	1 %	0	0%
28	340	2%	346	2%	291	1%	144	1 %	0	0%
30	326	2%	277	1%	305	2%	142	1%	0	0%
32	229	1%	278	1%	274	1%	130	0%	0	0%
34	232	1%	195	1%	219	1%	106	0%	0	0%
36	213	1%	151	1%	146	0%	98	0%	0	0%
38	195	1%	106	0%	135	0%	78	0%	0	0%
40	86	0%	89	0%	104	0%	49	0%	0	0%
42	75	0%	63	0%	60	0%	39	0×	0	<b>0%</b>
44	30	0%	31	0%	49	0×	40	0×	0	0%
46	84	0%	53	0%	100	0%	15	0%	0	0%
48	32	0%	23	0%	31	0%	6	0%	0	<b>0</b> %
50	1-1	0%	6	<b>0%</b> ,	13	<b>0</b> %	8	<b>0%</b>	0	0%

SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - FEBRUARY - WITH NIPS IN EXCESS OF 450 W/M2

MPH	MPH STX1801*		STX1801* STX1810*		ð*	STX1815*		STX1822*		STX1835*	
52		0	0%	1	0%	1	0%	1	0%	0	0%
54		0	0%	0	0%	0	0%	1	0%	0	0%
5 <b>6</b>		0	0%	0	0%	0	0%	1	0%	0	0%
60		0	0%	0	0%	0	0%	0	0%	0	0%
62		0	0%	. 0	0%	0	0%	0	0%	0	0%
64	ŧ	0	0%	0	0%	0	0%	0	0%	0	0%
6 <b>6</b>		0	0%	0	0%	0	0%	0	0%	0	0%
68		0	0%	0	0%	0	0%	0	0%	0	0%
70		0	0%	0	0%	0	0%	0	0%	0	0%
72		0	0%	0	0%	0	0%	0	0%	0	0%
74		0	0%	0	0%	0	0%	0	0%	0	0%
76		6	0%	0	0%	0	0%	0	0%	0	0%
78		0	0%	0	0%	. 0	0%	0	0%	0	0%
80		0	0%	0	0%	0	0%	0	0%	0	0%
82		0	0%	0	0%	0	0%	0	0%	0	0%
84		0	0%	0	0%	0	0%	0	0%	0	0%
86		0	0%	0	0%	0	0%	0	0%	0	0%
88		0	0%	0	0%	0	0%	0	0%	0	0%
90		0	0%	0	0%	0	0%	0	0%	0	0%
92		. 0	0%	0	0%	0	0%	0	0%	0	0%
94		0		0	0%	0	0%	Ø	0%	0	0%
96		0		0	0%	0	0%	0	0%	0	0%
98		0		0	0%	0	0%	0	0×	0	0%
100		0	0%	Ø	0%	0	0%	0	<b>0%</b>	0	0 <b>%</b>

SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - FEBRUARY - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0TX1802*		X1802* OTX1811*		0TX1816*		0TX1823*		0TX1836*	
0	176	1%	1583	10%	134	0×	694	5 <b>x</b>	0	0 <b>x</b>
15	155	1 <b>X</b>	374	2x	107	0×	78	0 X	Ŏ	0%
30	118	<b>0X</b>	353	2x	146	0 X	64	0×	ē	0%
45	194	1%	407	2x	355	2x	148	1%	Ŏ	0%
60	506	3%	630	48	739	5×	267	1%	Ŏ	0×
75	1277	8%	759	5×	1255	8%	648	4%	ě	0X
90	974	6X	768	5X	1012	6%	865	6X	ŏ	0×
105	642	4%	829	5X	698	4%	931	6 <b>X</b>	Õ	0X
120	526	3x	797	5×	339	2%	761	5 <b>X</b>	ŏ	0×
135	170	1%	670	48	204	1%	416	3%	ŏ	0×
150	208	1%	410	2X	151	1%	276	2%	ŏ	6×
165	122	0X	237	18	165	1%	173	1%	ŏ	0×
180	172	1%	206	18	187	1%	141	1%	Ŏ	0×
195	93	<b>9</b> %	191	18	205	18	147	1%	Ö	0×
210	213	1%	260	1%	391	SX	181	1%	Ö	0×
225	324	2%	366	2%	991	6X	245	18	Ŏ	0×
240	956	<b>6</b> X	559	3 <b>x</b>	1937	13X	456	3 <b>x</b>	0	0×
255	2185	14%	923	6 <b>X</b>	2544	17%	1128	8%	Ø	8%
270	1811	12x	1030	7 <b>X</b>	1266	8*	1648	11X	0	0×
285	1586	10X	1167	7%	740	5 <b>x</b>	1968	14%	0	0×
300	561	3 <b>x</b>	760	5%	341	24	1210	8%	0	0×
315	513	3%	496	31	305	2x	638	4%	0	0×
330	502	3%	435	2 <b>x</b>	210	1%	364	2×	0	0×
345	590	4%	321	2x	181	1%	240	18	0	0×
360	122	0×	144	0×	76	<b>0</b> ×	85	0×	0	<b>0</b> ×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF T MARCH - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX180	1*	STX181	<b>0</b> *	STX181	5 <b>*</b>	STX182	2*	STX1839	5 <b>*</b>
0	ż	0×	6	0%	7	0×	281	3%	0	0×
2	117	1%	147	0×	129	<b>0</b> %	530	6%	0	0%
4	451	4%	464	2%	378	2%	608	7%	0	0%
6 8	678	7×	741	4%	748	4%	731	9%	0	0×
8	799	8%	1958	11%	1749	9%	906	11%	0	0%
10	784	8%	3215	18%	2818	16%	1067	13%	0	0%
12	1100	11%	2569	14%	2671	15%	1199	15%	0	0%
14	736	7%	1843	10%	1947	11%	950	12%	0	0×
16	704	7×	1118	6%	1333	7%	567	7%	0	0%
18	663	7%	833	4%	988	5%	280	3%	0	0%
20	528	5%	818	4%	896	5%	173	2%	0	0%
22	419	4%	746	4%	821	4%	122	1 %	0	0%
24	306	Э%	629	3%	674	3%	58	<b>0</b> %	0	0%
26	268	<b>5</b> %	54?	3%	535	3%	43	<b>0</b> %	0	0%
28	298	3%	440	5%	416	2×	24	<b>0%</b>	0	0%
30	293	3%	420	2%	350	1%	23	0%	0	0%
32	264	2×	316	1%	304	1%	6	0%	0	0×
34	221	2x	281	1%	230	1%	8	0%	0	0%
36	221	2*	178	1%	187	1%	3	0%	0	0×
38	199	2%	122	0×	146	0%	0	0%	0	0×
40	98	1 %	79	0%	98	0 X	0	0×	0	0×
42	47	0×	63	0%	70	0 X	3	0×	0	0×
44	31	0×	19	0×	46	0 <b>%</b>	3	0×	0	0%
46	10	0×	55	0×	22	<b>0</b> ×	0	0%	0	0 <b>%</b>
48	7	0X	<b>6</b>	0×	13	<b>0</b> %	0	0%	0	0 <b>%</b>
50	2	0×	0	<b>0</b> %	3	<b>0</b> ×	209	2%	0	0×

SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - MARCH - WITH NIPS IN EXCESS OF 450 W/M2

										_
DEG	OTX180	<b>2</b> *	OTX181	1*	OTX181	<b>6</b> *	0TX182	3*	0TX183	<b>6*</b>
0	727	2x	1399	4%	611	1%	673	2%	0	0×
15	672	<b>2</b> %	745	2x	627	2x	1132	3x	ŏ	0X
30	561	18	681	2×	722	2x	1022	3%	ŏ	0×
45	634	2x	881	2x	916	2 <b>x</b>	1161	3%	Õ	0×
60	791	2x	991	3%	882	2X	1064	3%	ŏ	0×
75	1121	XΕ	845	2x	746	2x	991	3x	ŏ	0×
90	861	2x	597	18	589	18	682	2%	ŏ	0X
105	453	1X	494	18	573	1%	471	1%	ŏ	0×
120	338	18	528	18	335	1%	493	1%	ŏ	0 <b>x</b>
135	205	0 X	515	ĪX	559	0×	249	0×	ě	0 <b>%</b>
150	253	0×	410	18	282	0×	211	0×	ŏ	0X
165	187	9×	292	ØX	339	1%	219	0×	Ö	0X
180	147	0×	280	0×	460	ix	558	OX	0	
195	255	0×	307	1%	1111	Эx	472	1%		0×
210	511	1%	722	2×	2360	7 <b>%</b>	1223	4%	0 8	0X 0X
225	1187	3x	1964	6X	3600	11%	2394	8%	9	8%
240	2445	7%	2696	8×	5363	17%	3108	10%	0	
255	4864	15%	3334	11%	4183	13%	2354	74		0×
270	5998	9%	3356	11%	2322	7 <b>X</b>			0	0×
285	4047	13%	3114	10×	1638	5 <b>x</b>	1823	6X	0	0×
300	3106	10×	1985	6 <b>X</b>	939	3 <b>X</b>	2265	7X	0	0 <b>%</b>
315	1554	5 <b>x</b>	1450	4%	671		2527	8%	0	0×
330	1196	3x	1216	4%	600	2x 1x	2115	7×	0	0 X
345	1349	48	848	ž	613	1%	1443 903	4%	9	8×
360	495	1×	454	18	583	0×	395	3% 1%	9 9	0 X 0 X
			,,,,	4.7	603	. ••	333	14	v	04

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - APRIL - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX180	1*	STX181	<b>0</b> *	STX181	5 <b>*</b>	STX182	2*	STX1839	5 <b>*</b>
0	107	0%	1487	4%	364	1%	424	1 %	0	0×
2	1339	4%	1056	3%	1131	3%	1455	6%	0	0%
4	3235	11%	3107	10%	3068	10%	3309	13%	0	0%
6	4280	14%	4409	14%	4072	13%	4331	18%	0	0%
8	4629	15%	4186	14%	4088	14%	3885	16%	0	0%
10	3409	11%	3819	12%	3979	13%	3257	13%	0	0%
12	3452	11%	2524	8%	2825	9%	2097	8%	0	0%
14	1321	4%	1751	5%	1887	6%	1287	5%	0	0%
16	1002	3%	1040	3%	1213	4%	876	3%	0	0×
18	746	2%	826	2%	862	2%	646	2%	0	0%
20	672	5%	750	2%	744	2%	566	2%	0	0%
22	654	2%	696	2%	670	2*	443	1 %	0	0%
24	504	1%	601	2*	637	2%	342	1%	0	0%
26	404	1%	490	1 %	489	1%	284	1%	0	0%
85	482	1%	400	1%	399	1%	858	0×	0	0%
30	419	1%	345	1 %	325	1%	132	0 X	0	0%
32	385	1%	389	1%	345	1%	92	0%	0	0%
34	397	1%	393	1 %	352	1%	56	0%	0	0%
36	382	1%	416	1%	341	1%	20	0%	ø	0%
38	508	1%	415	1%	310	1%	13	0%	ø	0%
40	359	1 %	310	1%	292	1%	6	0%	ø	0%
42	219	0×	238	0%	250	0%	5	0%	0	0%
44	135	0%	112	0%	152	0 x	0	0×	ø	0%
46	81	0%	70	0×	223	0%	8	0%	ø	0%
48	22	0%	25	0×	102	0×	1	0%	Ø	0%
50	3	0×	4	0%	47	0%	0	0%	0	0×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - APRIL - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX180:	1*	STX1816	) <b>*</b>	STX1815	5 <b>*</b>	STX182	2*	STX183	5 <b>*</b>
52	1	0%	0	0%	6	0%	0	0%	0	0%
54	0	0%	0	0%	3	0%	0	0%	ø	0%
56	0	0%	0	0%	0	0%	0	0%	ø	0%
58	0	0%	0	0%	0	0%	0	0%	ø	0%
60	0	0%	0	0%	0	0%	9	0%	ø	0%
62	0	0%	0	0%	0	0%	ō	0%	ě	0%
64	0	0%	0	0%	0	0 X	Õ	0%	. 0	0%
66	Ø	0%	0	0%	0	0×	Ø	0%	ø	0%
68	0	0%	0	0%	0	0×	. 0	0%	ø	0%
70	0	0×	0	0×	0	0%	0	0%	Ö	0%
72	Ø	0%	0	0%	0	0%	0	0%	ø	0%
74	0	0%	0	0×	. 0	0%	0	0%	Ø	0%
76	0	0%	0	0%	0	0×	0	0×	ø	0%
78	0	0×	0	0×	0	<b>0</b> %	0	0%	0	0%
80	0	0×	0	0%	0	0×	0	0%	Ø	0%
82	Ø	0×	0	0×	0	0×	0	0%	0	0%
84	.0	0×	0	0×	0	0×	0	0%	0	0×
86	0	0×	0	0×	0	<b>0</b> %	0	0%	0	0×
88	0	0×	0	0×	0	0×	0	0×	0	0×
90	0	<b>0</b> %	0	0×	0	0 X	0	0 X	0	0%
92	0	<b>0</b> %	0	0 <b>%</b>	0	0 X	0	0%	0	0×
94	0	0 <b>×</b>	0	0 <b>%</b>	0	0×	0	0 X	0	0 X
96	0	<b>0</b> ×	. 0	0%	0	<b>0</b> %	0	0×	0	0 X
98	Ø	0×	0	0×	0	0 X	0	0×	0	0 X
100	Ø	0×	0	0×	0	0×	0	0×	0	0×

DEG	0TX180	2*	0TX181	1*	0TX181	<b>6</b> *	0TX182	3*	0TX183	<b>6*</b>
0	727	2x	1399	4X	611	1%	673	2%	0	0×
15	672	28	745	2x	627	2x	1132	3X	Ø	0%
30	561	1 X	681	2x	722	2x	1022	3 <b>x</b>	9	0%
45	634	<b>2</b> X	881	Sx	916	2 <b>x</b>	1161	3%	0	0×
60	791	2%	991	3%	882	2x	1064	3%	Ö	0%
75	1121	3X	845	28	746	2X	991	3%	Ö	0×
90	861	5X	597	17	589	18	685	2x	Ŏ	0X
105	453	1%	494	1%	573	18	471	1%	Ø	0%
120	338	1%	528	1%	335	18	493	1%	Ö	0X
135	205	0×	515	1%	559	0%	249	0×	Ö	0%
150	253	0 X	410	18	585	0 X	211	0×	Ŏ	0X
165	187	0×	292	0×	339	1%	219	0×	ě	0×
180	147	0×	280	0×	460	1%	828	0×	ě	0×
195	255	0×	307	1.8	1111	3%	472	18	ŏ	0×
210	511	18	722	SX	2360	7%	1223	48	ŏ	0×
225	1187	3x	1964	6 <b>X</b>	3600	11%	2394	8%	Ŏ	ØX
240	2445	78	2696	8%	5363	17%	3108	10×	Ö	0%
255	4864	15X	3334	11X	4183	13X	2354	7 <b>X</b>	Ŏ	0X
270	8998	9%	3356	11%	2322	7 <b>x</b>	1823	6 <b>X</b>	Ŏ	0×
285	4047	13X	3114	10x	1638	5×	2922	7%	Ö	0×
300	3106	10%	1985	6X	939	3%	2527	8%	Ö	0X
315	1554	5%	1450	4%	671	2%	2115	7%	ŏ	0×
330	1196	ЭX	1216	4X	600	1%	1443	4%	. 0	0×
345	1349	4%	848	2%	613	18	903	3%	0	0×
360	495	1%	454	1%	583	øx	395	1%	0	<b>0</b> ×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR NONTH OF - HAY - WITH NIPS IN EXCESS OF 450 W/M2

STX180	1*	STX181	<b>0</b> *	STX181	<b>5*</b>	STX182	2*	STX1839	5 <b>*</b>
25	<b>0</b> ×	11	0×	25	0×	26	9 <b>x</b>	0	0×
		797	44	807	41	821	4%	0	0%
1845	9%	1958	10×	1790	94	1925	10%	0	<b>0</b> %
2482	134			2314	12%	2635	14%	0	0%
3009	15%		14%	2534	13%	3236	17%	0	0%
2530	13%	2752	14%	2493	134	3095	16¥	0	9%
2904	154	2354	124	2445	13%	2375	12%	0	0%
1123	5%	1537	8#	1840	94	1480	78		0%
791	44	982	5 <b>%</b>	1076	5 <b>x</b>	919	4%	0	0%
655	ЗX	672	3%	742	34	579	31		0%
506	51	565	3%	500	214				0%
434	511	474	2%	386	24				014
244	14	377	2%	353	14				øx
233	1%	335	1%		14		1%	0	øx
	. 14	242	1%	235	111	138	04	0	6%
	1%	215	1%	196	14	111	0 X	0	0%
	14	167	01	169	04	79	0 <b>%</b>	9	0×
		121	04	133	Ou	50	0 %	0	04
	014	94	<b>0</b> %	94	0×	29	øx	0	04
	9%	60	0 X	75	01	18	0 X	0	0%
43	04	52	04	47	OX	8	04	0	01
	0%	12	<b>0</b> 4	22	04	5	0×	0	9%
·		1	0%	6	04	2	<b>0%</b>	0	0×
	ox	24	04	<b>16</b> 8	OX	8	0%	0	0%
				54	OX		0×	0	04
0	0%	0	011	0	0 X	0	04	0	04
	25 803 1845 2482 3009 2530 2904 1123 791 655 506 434 244	803 4x 1845 9x 2482 13x 2482 13x 2530 13x 2530 13x 2530 13x 2531 4x 655 3x 655 3x 655 3x 244 1x 244 1x 233 1x 263 1x 263 1x 191 1x 161 0x 134 0x 43 0x 44 0x 45 0x 46 0x 47 0x 47 0x 47 0x 48 0x	25 0% 11 803 4% 797 1845 9% 1958 2482 13% 2375 3009 15% 2651 2530 13% 2752 2904 15% 2354 1123 5% 1537 791 4% 962 655 3% 672 506 2% 565 434 2% 474 244 1% 377 233 1% 335 263 1% 242 238 1% 215 191 1% 167 161 0% 121 133 0% 94 134 0% 60 43 0% 52 38 0% 12 7 0% 1 18 0% 24 2 0% 2	25 0x 11 0x 803 4x 797 4x 1845 9x 1958 10x 2482 13x 2375 12x 3009 15x 2651 14x 2530 13x 2752 14x 2904 15x 2354 12x 1123 5x 1537 8x 791 4x 962 5x 655 3x 672 3x 655 3x 672 3x 506 2x 565 3x 434 2x 474 2x 244 1x 377 2x 233 1x 263 1x 242 1x 238 1x 215 1x 191 1x 167 0x 161 0x 121 0x 133 0x 94 0x 134 0x 60 0x 43 0x 52 0x 38 0x 12 0x 2 0x 2 0x	25 0x 11 0x 25 803 4x 797 4x 807 1845 9x 1958 10x 1790 2482 13x 2375 12x 2314 3009 15x 2651 14x 2534 2530 13x 2752 14x 2493 2904 15x 2354 12x 2445 1123 5x 1537 8x 1840 791 4x 962 5x 1076 655 3x 672 3x 742 506 2x 565 3x 500 434 2x 474 2x 386 244 1x 377 2x 353 233 1x 335 1x 295 263 1x 242 1x 235 238 1x 215 1x 196 191 1x 167 0x 169 193 0x 120 0x 22	25 0x 11 0x 25 0x 803 4x 797 4x 807 4x 1845 9x 1958 10x 1790 9x 2482 13x 2375 12x 2314 12x 3009 15x 2651 14x 2534 13x 2530 13x 2752 14x 2493 13x 2904 15x 2354 12x 2445 13x 1123 5x 1537 8x 1840 9x 791 4x 962 5x 1076 5x 655 3x 672 3x 742 3x 506 2x 565 3x 500 2x 434 2x 474 2x 386 2x 244 1x 377 2x 353 1x 233 1x 335 1x 295 1x 233 1x 242 1x 235 1x 238 1x 215 1x 196 1x 191 1x 167 0x 169 0x 161 0x 121 0x 133 0x 133 0x 94 0x 94 0x 134 0x 60 0x 75 0x 43 0x 52 0x 47 0x 38 0x 12 0x 24 0x 168 0x 2 0x 2 0x 54 0x	25 0x 11 0x 25 0x 26 803 4x 797 4x 807 4x 821 1845 9x 1958 10x 1790 9x 1925 2482 13x 2375 12x 2314 12x 2635 3009 15x 2651 14x 2534 13x 3236 2530 13x 2752 14x 2493 13x 3095 2904 15x 2354 12x 2445 13x 2375 1123 5x 1537 8x 1840 9x 1480 791 4x 962 5x 1076 5x 919 655 3x 672 3x 742 3x 579 506 2x 565 3x 500 2x 461 434 2x 474 2x 386 2x 357 244 1x 377 2x 383 1x 259 233 1x 335 1x 295 1x 197 263 1x 242 1x 235 1x 198 238 1x 215 1x 196 1x 111 191 1x 167 0x 169 0x 79 161 0x 121 0x 133 0x 50 133 0x 94 0x 94 0x 29 134 0x 60 0x 75 0x 18 43 0x 52 0x 47 0x 8 38 0x 12 0x 24 0x 168 0x 2 7 0x 1 0x 6 0x 2 18 0x 24 0x 168 0x 2 2 0x 54 0x 2	25 0x 11 0x 25 0x 26 0x 803 4x 797 4x 807 4x 821 4x 1845 9x 1958 10x 1790 9x 1925 10x 2482 13x 2375 12x 2314 12x 2635 14x 3009 15x 2651 14x 2534 13x 3236 17x 2530 13x 2752 14x 2493 13x 3095 16x 2904 15x 2354 12x 2445 13x 2375 12x 1123 5x 1537 8x 1840 9x 1480 7x 791 4x 962 5x 1076 5x 919 4x 6555 3x 672 3x 742 3x 579 3x 506 2x 565 3x 500 2x 461 2x 434 2x 474 2x 386 2x 357 1x 244 1x 377 2x 353 1x 259 1x 233 1x 235 1x 259 1x 233 1x 235 1x 259 1x 233 1x 242 1x 235 1x 138 0x 238 1x 242 1x 235 1x 138 0x 238 1x 242 1x 235 1x 138 0x 238 1x 215 1x 196 1x 111 0x 191 1x 167 0x 169 0x 79 0x 161 0x 121 0x 133 0x 50 0x 133 0x 94 0x 94 0x 29 0x 134 0x 60 0x 75 0x 18 0x 23 18 0x 23 10 0x 50 0x 13 0x 50 0x 12 0x 20 0	25 0x 11 0x 25 0x 26 0x 0 803 4x 797 4x 807 4x 821 4x 0 1845 9x 1958 10x 1790 9x 1925 10x 0 2482 13x 2375 12x 2314 12x 2635 14x 0 3009 15x 2651 14x 2534 13x 3236 17x 0 2530 13x 2752 14x 2493 13x 3095 16x 0 2904 15x 2354 12x 2445 13x 2375 12x 0 1123 5x 1537 8x 1840 9x 1480 7x 0 791 4x 962 5x 1076 5x 919 4x 0 655 3x 672 3x 742 3x 579 3x 0 506 2x 565 3x 500 2x 461 2x 0 434 2x 474 2x 386 2x 357 1x 0 244 1x 377 2x 353 1x 259 1x 0 233 1x 335 1x 295 1x 197 1x 0 244 1x 377 2x 353 1x 259 1x 0 253 1x 242 1x 235 1x 138 0x 0 258 1x 242 1x 235 1x 138 0x 0 131 0x 121 0x 133 0x 50 0x 0 133 0x 94 0x 94 0x 29 0x 0 134 0x 60 0x 75 0x 18 0x 0 28 0x 24 0x 12 0x 22 0x 2 0x 0 18 0x 24 0x 168 0x 2 0x 0

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SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - MAY - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0TX180	2*	OTX181	1*	0TX181	<b>6</b> *	SSIXTO	<b>3</b> *	0TX183	6 <b>*</b>
0	239	1%	269	1%	376	2%	245	1%	0	9 <b>x</b>
15	285	18	337	1%	439	2%	343	1%	. 0	0×
30	311	18	407	2x	489	2x	390	2%	Ö	0×
45	375	5X	503	2x	542	3%	457	2×	Ō	0%
60	491	2 <b>x</b>	543	3X	598	3%	517	2x	Ŏ	0%
<b>7</b> 5	859	4X	585	3 <b>x</b>	528	2×	615	3x	ě	0×
90	609	3%	434	<b>5</b> %	494	2x	595	3%	Ö	0×
105	377	2x	393	2x	384	2×	447	2%	Õ	8%
120	321	1%	364	2x	285	1%	356	1%	Ö	0×
135	160	9×	314	1%	218	1%	294	1%	ĕ	0%
150	257	1%	270	1%	137	0×	252	1%	Ŏ	0%
165	235	1%	239	1%	107	0×	172	0×	ŏ	0%
180	167	0 X	156	0X	144	0×	128	0×	Ö	0%
195	106	9×	162	0×	276	1%	113	0×	Ŏ	0X
210	183	1%	191	1%	774	4%	192	1%	ě	0×
2 <b>2</b> 5	234	1 X	316	18	1335	7%	607	3x	Ŏ	0X
240	596	3 <b>x</b>	683	3%	2790	15 <b>%</b>	1131	6%	Ŏ	0X
255	1537	8%	1716	9%	3156	17%	1702	9%	ŏ	0%
270	1678	9×	2928	16X	2486	13%	1841	10%	ŏ	0×
285	3385	18%	2689	14X	1234	6 <b>%</b>	2465	13%	ŏ	0%
300	2494	13 <b>x</b>	2125	11%	390	24	2419	13%	ě	0%
315	1192	6 <b>X</b>	1363	7 <b>x</b>	224	12	1425	7%	ě	0×
330	960	5 <b>x</b>	514	SX	245	1%	608	3%	ő	0×
345	835	4%	276	18	265	1%	409	2%	ě	0X
360	107	<b>0</b> ×	136	0×	179	0×	828	1%	ŏ	0×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - JUNE - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX180	1*	STX181	<b>0</b> *	STX181	<b>5</b> *	STX182	2*	STX183	5 <b>*</b>
0	4	0×	11	<b>0</b> ×	10	0×	9	0×	0	0×
2	490	3%	445	3%	467	3%	537	3%	0	0×
4	1201	8×	1154	7%	1152	7×	1322	9%	0	0%
6	1859	12x	1642	11%	1463	10×	2030	13x	´ 0	<b>0%</b>
8	2351	16 <b>%</b>	2042	14%	1784	12%	2604	17X	0	<b>0%</b>
10	2045	14X	2214	15%	2056	14X	2502	17x	0	<b>0</b> %
12	2349	16X	1934	13%	2026	13x	1873	12x	0	0×
14	1114	7×	1462	10%	1662	11%	1275	8*	0	<b>0%</b>
16	820	5X	1088	7%	1205	8×	822	5 <b>%</b>	0	0 X
. 18	656	4 <b>%</b>	784	<b>5</b> %	806	5 <b>%</b>	551	3%	0	0×
20	522	3%	595	4%	609	4%	340	2x	0	<b>8%</b>
22	384	SX	391	2x	440	3%	233	1%	0	9%
24	196	1%	304	2%	274	1%	152	1%	0	0×
26	149	1%	199	1%	212	1 X	90	0 X	0	8%
58	171	1×	131	0×	152	1%	69	0×	0	0×
30	113	0×	83	0×	89	0×	55	0×	0	0×
35	67	0×	32	0×	54	0×	31	0 X	0	<b>0</b> ×
34	25	0 X	19	<b>0</b> ×	35	<b>0×</b>	20	0×	0	0×
36	17	0 <b>x</b>	11	0×	23	0×	16	<b>0</b> ×	9	0%
38	<b>,</b> 9	<b>0</b> %	3	0 X	8	<b>0</b> %	1	0×	0	8×
40	'i	<b>0</b> %	0	<b>0×</b>	5	0 X	5	<b>0</b> %	0	0×
42	0	0×	0	0×	4	0×	1	0×	0	0 X
44	0	0×	0	0×	1	0 X	1	0×	0	0×
46	1	0×	0	0×	. 3	<b>0</b> ×	4	0×	9	0 X
48	0	0×	0	0X	1	0×	1	0 X	. 0	0×
50	0	0 <b>%</b>	0	0×	. 0	0 <b>×</b>	0	<b>0</b> ×	0	0 X

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SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - JUNE - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0TX180	2	OTX181	1*	0TX181	<b>6</b> *	0TX182	3*	0TX1836	5 <b>*</b>
0	180	1%	141	0×	283	1×	159	1%	0	9×
15	162	1%	174	1%	171	1%	195	1%	ě	0×
30	128	<b>0</b> ×	183	1%	170	1X	176	1%	ĕ	0%
45	131	0 X	190	18	195	1%	170	18	ŏ	0%
60	171	1%	201	18	188	18	206	1%	ŏ	0×
75	288	1%	196	1%	157	1%	204	1%	ě	0×
90	167	1%	142	0×	129	0×	211	18	ě	0×
105	152	1%	98	0 X	124	0×	142	0×	ŏ	0×
120	84	0×	86	ex	84	0×	111	0×	ŏ	0×
135	45	0 X	67	0×	71	0×	72	9%	· ŏ	0×
150	51	0×	68	0×	57	0×	49	0×	ŏ	0×
165	47	0 X	57	0×	72	0×	55	0×	ŏ	0×
180	41	0×	37	0×	115	ØX	56	0×	Ŏ	0 X
195	60	9×	89	0×	268	1%	67	0×	ŏ	0×
210	95	0×	83	0×	608	4%	130	θX	ŏ	0 X
225	201	1%	254	1%	1161	7%	613	48	ŏ	0×
240	635	4%	700	4%	2255	15X	1058	7%	ě	0×
255	1236	8%	1433	9 <b>x</b>	5833	19 <b>x</b>	1228	8×	ĕ	0X
270	1195	8%	2110	14%	2627	18%	1446	9 <b>x</b>	ő	0×
285	2587	17%	2416	16X	1637	11 <b>x</b>	2337	16 <b>X</b>		0X
300	2669	18%	2422	16%	589	4%	2712	18%	0	0X
315	1709	11%	1943	13%	305	2×	1730		0	
330	1368	9%	843	5 <b>X</b>	535	1%	818	11X 5X	0	0X 0X
345	1005	6 <b>X</b>	374	5 <b>x</b>	156	1%	415	2% 2%	0	0X
360	143	0×	167	1%	68	θx	165	1%	0	0×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - JULY - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX180	1*	STX181	<b>0</b> *	STX181	5 <b>*</b>	STX182	2*	STX183	5*
0	5	0%	13	0%	4	0%	23	0%	0	0×
2	403	3%	474	4%	424	4%	454	4%	ø	0%
4	1229	11%	1216	11%	1161	10%	1114	10%	0	0%
6	1431	13%	1469	13%	1502	14%	1633	15%	0	0%
8	1433	13%	1451	13%	1576	14%	1681	15%	0	0%
10	1225	11%	1220	11%	1194	11%	1405	13%	0	<b>0%</b>
12	1145	10%	799	7%	851	8%	916	8%	0	0×
14	517	4%	574	5%	725	6%	701	6%	0	0×
16	573	5%	626	5%	663	6%	538	5%	0	0%
18	662	6%	663	6%	636	6%	501	4%	0	0%
20	640	6%	631	5%	568	5%	420	3%	0	0%
22	523	4%	549	5%	442	4%	384	3%	0	0×
24	285	2%	411	3%	302	2%	290	2%	0	<b>0</b> %
26	186	1%	253	2%	553	2%	246	2%	0	0×
28	161	1%	120	1%	152	1%	140	1%	0	0×
30	101	0%	67	0%	81	0%	83	0%	0	0%
32	45	0%	34	0%	45	0%	34	0%	0	0%
34	17	0%	14	0%	24	0%	17	0%	0	0%
36	6	0%	3	0%	10	0%	3	0%	0	0%
38	0	0%	0	<b>0</b> %	4	0%	5	0%	0	0×
40	0	0%	0	0%	1	0%	0	0×	0	0%
42	0	0%	0	0×	0	0%	0	0%	0	0%
44	0	0%	0	0%	0	0%	0	0%	0	0 X
46	0	0%	0	<b>0</b> %	0	0%	0	0%	0	<b>0</b> ×
48	0	0%	0	<b>0</b> %	0	0%	0	<b>0</b> %	0	0×
50	0	0%	0	0%	0	0%	0	0%	0	<b>0</b> %

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SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - JULY - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0T×180	2*	OTX181	1*	OTX181	6*	0TX182	Э*	0TX183	6 <b>*</b>
0	130	1%	81	0%	180	1%	74	0%	0	0%
15	144	1%	155	1%	212	2%	131	1 %	0	0%
30	117	1%	203	1%	828	2%	196	1%	0	0%
45	180	1%	244	2%	246	2%	237	2%	0	0%
60	278	2%	309	2%	287	2%	291	2%	0	0%
75	395	3%	261	2%	258	2%	260	2%	0	0%
90	- 267	2%	163	1%	184	1%	247	2%	0	0%
105	246	2%	181	1%	113	1%	221	2%	0	0%
120	149	1 %	177	1 %	72	0%	185	1%	0	0%
135	101	0%	156	1%	70	0%	118	1%	0	0%
150	96	0%	100	0%	40	0%	80	0%	0	0%
165	43	0%	67	0%	54	0%	62	0%	0	0%
180	45	0%	46	0%	108	1 %	51	0%	0	0%
195	30	0%	67	0%	378	3%	60	0%	0	0%
210	94	0%	109	1%	929	8%	161	1%	0	0%
225	310	2%	515	4%	1427	13%	850	8%	0	0%
240	926	8%	985	9%	1941	18%	1290	12%	0	0%
255	. 1362	12%	1529	14%	1552	14%	1158	10%	0	0%
270	994	9%	1605	15%	973	9%	1235	11%	0	0%
285	1834	17%	1371	13%	605	5%	1373	12%	0	0%
300	1298	12%	908	8%	249	2%	1000	9%	0	0%
315	558	5%	587	5%	182	1 %	679	6%	0	0%
330	457	4%	373	3%	133	1 %	328	3%	0	0 X
345	435	4%	203	1 %	104	0%	199	1 %	0	0×
360	93	0%	126	1 %	63	<b>0</b> %	87	<b>0</b> ×	0	<b>0</b> ×

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SOLAR WIND SPEED DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - AUGUST - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX180	1*	STX181	<b>0</b> *	STX181	5*	STX182	2*	STX183	5 <b>*</b>
0	4	0%	12	0%	2	0%	15	0×	249	5%
5	480	9%	488	9%	443	8%	504	9%	886	18%
4	1124	21%	1223	23%	1078	20%	1094	20%	1429	29%
6	1323	24%	1403	26%	1367	25%	1453	27%	963	19%
8	1258	23%	1142	21%	1132	21%	1249	23%	598	12%
10	760	14%	670	12%	690	12%	666	12%	386	7%
12	294	5%	264	4%	451	8%	231	4%	204	4%
14	37	0%	72	1 %	86	1 %	66	1 %	126	2x
16	16	0%	16	0%	9	0%	25	0 X	46	<b>0%</b>
18	10	0%	14	0%	0	<b>0</b> %	4	<b>0</b> %	13	0%
95	5	0%	5	0%	0	0%	3	0×	2	0%
25	2	0×	1	0%	0	0%	0	0%	0	0%
24	0	0%	0	<b>0</b> %	14	<b>0</b> %	. 0	0%	0	0%
26	0	0%	0	0%	37	0×	0	0%	0	0%
28	0	0 X	0	<b>0%</b>	0	<b>0</b> %	0	0×	0	0%
30	0	<b>0</b> %	0	0×	0	0%	0	0%	0	0×
32	0	0%	0	<b>0</b> %	0	<b>0</b> %	0	0%	0	0×
34	. 0	0×	0	<b>0</b> %	0	0%	0	0%	0	0×
36	, 0	0×	. 0	0%	0	0%	0	0%	0	0×
· 38	0	0×	0	<b>0</b> %	1	0×	. 0	0×	0	<b>0</b> %
40	0	0 X	0	<b>0</b> %	0	0×	0	0×	0	0×
42	0	<b>0%</b>	0	<b>0</b> ×	0	0×	0	0%	0	0×
44	. 0	0×	. 0	0×	0	0×	0	0×	0	0%
46	0	<b>0</b> ×	: 0	<b>0</b> %	0	<b>0</b> ×	0	- 0×	0	0×
48	. 0	<b>0</b> ×	0	<b>0</b> %	0	0×	0	0×	9	<b>0</b> %
50	• 0	0 X	0	<b>0</b> %	0	<b>0</b> %	0	0×	0	0×

PAGE 1
SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - AUGUST - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0TX1802*		0TX1811*		OTX1816*		0TX1823*		0TX1836*	
0	168	1%	110	1%	240	2%	165	1%	113	2%
15	229	2*	244	2%	356	3%	250	2%	233	4%
30	249	2%	258	2%	512	5%	314	3%	267	5%
45	422	4%	486	4%	704	6%	613	6%	343	6%
60	808	7%	735	7%	865	8%	751	7%	299	6%
75	1005	9%	847	8%	698	6%	745	7%	203	4%
90	635	6%	646	6%	591	5 <b>x</b>	652	6×	110	2×
105	473	4%	516	5%	352	3%	437	4%	84	1%
120	313	Э*	346	3%	147	1%	402	3%	170	3%
135	192	1 %	295	2*	96	0%	209	2%	171	3%
150	160	1%	234	2%	73	0%	142	1%	94	1%
165	112	1*	135	1%	83	0×	. 97	0×	77	1%
180	52	0×	124	1%	75	0×	61	0%	56	1 %
195	49	<b>0</b> ×	85	<b>0</b> %	129	1 %	77	. 0%	61	1%
210	159	1%	101	0%	399	3%	86	0%	90	1*
225	92	0×	113	1 %	637	6%	140	1 %	121	2%
240	154	1%	202	1%	1010	9%	274	2%	293	5 <b>%</b>
255	508	4%	656	6%	917	8%	767	7%	490	9%
270	911	8%	1122	11%	820	8%	851	8%	642	13%
285	1117	10×	825	8%	554	5x	1091	10%	515	10%
300	864	8%	694	6*	344	3%	804	7%	192	3%
315	395	3%	592	5%	214	2x	563	5 <b>%</b>	<b>89</b>	1%,
330	430	4%	393	3%	149	1 %	346	3%	<b>65</b> .	18
345	620	<b>6</b> %	232	2x	161	1%	246	<b>2</b> %	71	1 %
360	95	<b>0</b> ×	135	1%	86	<b>0</b> ×	111	1%,	- 52	1%

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SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - SEPTEMBER - WITH NIPS IN EXCESS OF 450 W/M2

МРН	STX1801*		STX1810*		STX1815*		\$TX1822*		STX1835*	
0	202	0%	224	0%	63	0%	63	0%	12	0%
2	2516	8%	3402	12%	2261	7%	1850	6%	5543	19%
4	5587	19%	6186	25%	6763	23%	5507	18%	9164	31%
6	7995	27%	6353	25%	7975	27%	8528	29%	5967	20%
8	6059	20%	4869	17%	5536	18%	6232	21%	3038	10%
10	2620	8%	2720	9%	3086	10%	3023	10%	1517	5%
12	2059	7%	1657	5%	1436	4%	1462	4%	1121	3%
14	925	3%	944	3%	923	3%	879	2%	942	3%
16	719	2%	712	2%	612	2%	591	2%	672	2%
18	340	1%	426	1%	340	1 %	487	1%	564	1%
20	180	0%	245	0%	208	0%	371	1%	331	1%
25	92	0%	100	0%	85	0%	202	0%	178	0%
24	21	0%	29	0%	30	0%	97	0%	73	0%
56	9	0%	3	0%	8	0%	30	0%	23	0%
28	4	0%	2	0%	2	0%	11	0%	11	0%
30	1	0%	1	0%	1	0%	1	0%	1	0%
32	5	0%	1	0%	2	0%	0	0%	1	0%
34	0	0%	0	0%	2	0%	0	0%	0	0%
36	0	0%	0	0%	1	0%	0	0%	0	0%
38	0	0%	0	0%	0	0%	0	0%	0	0%
40	0	0%	0	0%	. 0	0%	Ø	0%	0	0%
42	0	0%	0	0%	0	0%	0	0%	Ø	0%
44	0	0%	. 0	0%	0	0%	0	0%	Ø	0%
46	0	0%	0	0%	0	0%	0	0%	Ø	0%
48	0	0%	0	0%	0	0%	0	0%	0	0%
50	0	0%	0	0%	0.	0%	0	0%	0	0%

DEG	0TX1802*		OTX1811*		OTX1816*		*E581XTO		0TX1836*	
0	438	1%	252	<b>0</b> %	1028	3%	522	1%	620	2%
15	707	2%	611	2×	1217	4%	1063	3%	1273	4%
30	873	2%	<i>"</i> 700	2×	1552	5%	1254	4%	1492	5%
45	1265	4%	1473	<b>5</b> %	2148	7%	1805	6%	2409	8%
60	2167	7%	2387	8%	2837	9%	2296	7%	2137	7%
75	3184	10%	5659	9%	2681	9%	2428	8*	1590	5%
90	3108	10%	2039	6%	2672	9%	2692	9 <b>x</b>	886	3%
105	2582	8%	1917	6%	1742	5%	2549	8*	742	2 <b>%</b>
120	1199	4%	1288	4%	682	<b>5</b> %	1812	6*	1513	5%
135	634	2%	1091	3%	374	1%	850	2%	1474	5%
150	699	2%	627	2%	322	1%	465	1 %	898	3%
165	483	1%	325	1 %	393	1%	368	1%	570	1%
180	454	1%	411	1 %	514	1%	546	1%	689	2*
195	502	1%	2155	7×	962	3%	559	1 %	763	5×
210	1026	3%	1332	4%	1317	4%	E06	3%	1330	4%
225	856	2%	1573	5 <b>%</b>	1317	4%	1395	4%	1276	4%
240	1661	5%	1393	4%	1520	5%	1329	4%	1900	6%
255	1400	4%	1015	3%	1531	5%	967	3 <b>x</b>	1941	6%
270	818	. 2%	1081	3%	1409	4×	896	3%	1918	6X
285	1271	4%	1296	4%	962	3 <b>x</b>	1421	4%	1758	5%
300	1363	4%	1317	4×	455	1%	1324	4%	751	2×
315	862	2*	996	3x	372	1%	841	2x	379	1%
330	750	2x	613	2×	482	1 %	409	1×	315	1%
345	766	2%	415	1 X	520	1 %	342	1×	384	1%
360	258	0×	237	0 <b>%</b>	325	- 1X	556	0×	302	1%

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SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - OCTOBER - WITH NIPS IN EXCESS OF 450 W/M2

мен	STX1801*		STX1810*		STX1815*		STX1822*		STX1835*	
0	219	1%	43	0%	152	1%	54	0%	2	0%
2	1020	7%	1181	8%	1122	8%	1282	9%	1361	11%
4	2347	17%	2404	18%	2101	15%	2169	16%	2703	22%
6	2577	19%	2658	19%	2497	18%	2942	22%	1847	15%
8	2328	17%	2391	17%	2488	18%	2711	20%	1517	12%
10	1898	14%	1896	14%	1978	14%	1910	14%	1941	16%
12	1502	11%	1187	8%	1213	9%	1062	7%	748	6%
14	407	3%	482	3%	602	4%	542	4%	550	4%
16	231	1%	241	1%	269	2%	287	2%	279	2%
18	143	1%	165	1%	196	1%	176	1%	165	1%
20	140	1 %	163	1%	167	1%	94	0%	137	1%
25	123	0%	127	0%	120	0%	59	0%	116	0%
24	96	0%	114	0%	107	0%	22	0%	98	0%
26	75	0%	102	0%	36	0%	13	0%	111	0%
28	87	0%	84	0%	73	0%	10	0%	52	0%
30	63	0%	56	0%	59	0%	2	0%	62	0%
32	46	0%	23	0%	50	0%	1	0%	33	0%
34	20	0%	14	0%	29	0%	1	0%	24	0%
36	11	0%	6	0%	16	0%	0	0%	12	0%
38	3	0%	0	0%	6	0%	0	0%	4	0%
40	1	0%	0	0%	6	0%	0	0%	3	0%
42	0	0%	0	0%	0	0%	0	0%	2	0%
44	Ø	0%	0	0%	0	0%	0	0%	0	0%
46	0	0%	0	0%	0	0%	0	0%	0	0%
48	0	0%	0	0%	0	0%	0	0%	. 0	0%
50	0	0%	0	0%	0	0%	0	0%	0	0%

DEG	0TX180	2*	0TX181	1*	OTX181	<b>6</b> *	0TX182	3*	0TX183	<b>6</b> *
0	147	1%	123	<b>0</b> %	288	2%	237	1%	128	1%
15	203	1%	179	1%	312	2%	222	1%	308	2%
30	229	1%	189	1%	405	3%	244	1%	281	2%
45	297	2%	336	2%	725	5%	. 377	2×	413	3%
60	440	3%	610	4%	918	6%	545	4%	514	4%
75	977	7%	1044	7%	901	6%	758	5%	352	2x
90	1080	8%	912	6%	676	5%	920	6%	260	2%
105	899	6%	734	5%	493	3%	867	6%	206	1%
120	414	3%	525	3%	252	1%	651	4%	408	3%
135	228	1 %	303	2%	172	1%	353	2%	403	3%
150	212	1 %	214	1%	119.	0%	217	1%	253	2%
165	136	1 %	151	1*	106	<b>0</b> ×	147	1*	152	1 %
180	124	<b>0</b> %	90	0%	124	0×	102	0×	118	1 %
195	117	0%	118	<b>0</b> ×	169	1*	123	0×	148	1 X
210	155	1 %	172	1%	544	4%	156	1*	556	4%
225	160	1 %	248	1%	1131	8%	260	1%	398	3%
240	316	5x	367	2*	. 1636	12%	446	3%	721	6%
255	1039	7%	1271	9%	1351	10%	770	5%	1315	11%
270	1278	. 9%	1632	12%	1342	10%	1107	8x	2460	20%
285	1684	12%	1291	9%	815	6*	1575	11%	1413	12%
300	1365	10×	1083	8%	313	2%	1566	11%	498	4%
315	724	5*	935	7%	148	1%	1004	7%	172	1%
330	493	3%	487	3%	135	1 %	351	2%	94	0×
345	502	3%	198	1×	168	1 %	176	1%	110	0 X
360	113	<b>0</b> %	82	0×	94	0×	90	<b>0</b> ×	77	0 X

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SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - NOVEMBER - WITH NIPS IN EXCESS OF 450 W/M2

MPH	STX1801	L*	STX181	<b>0</b> *	STX181	5*	STX182	2*	S <b>T</b> X183	5*
Ø	372	1 %	57	0%	532	1%	104	0%	5	0%
2	1027	3%	661	7%	1028	3%	1461	- 5%	2351	9%
4	2122	7%	1020	11%	2073	7%	2025	8%	3121	12%
6	2278	8%	958	11%	2043	7%	2503	9%	1734	6%
8	1807	6%	1102	12%	1795	6%	2257	8%	1370	5%
10	1205	4%	906	10%	1211	4%	2176	7%	1084	4%
12	907	3%	489	5%	777	2%	2491	9%	853	3%
14	511	1%	287	3%	630	2%	2851	10%	799	3%
16	650	2%	197	2%	774	2%	2866	10%	794	3%
18	965	3%	189	2%	1181	4%	2496	9%	943	3%
20	1576	5%	257	3%	1669	6%	1862	6%	1184	4%
22	2211	8%	347	4%	2040	7%	1340	4%	1328	5%
24	2046	7%	378	4%	2261	8%	833	3%	1454	5%
26	1973	7%	440	5%	2363	8%	619	2%	1494	5%
28	2624	9%	425	4%	2183	7%	445	1 %	1525	6%
30	2242	8%	322	3%	1846	6%	360	1%	1352	5%
32	1562	5%	216	2%	1355	4%	219	<b>0</b> %	1281	5%
34	8 <b>3</b> 3	3%	156	1%	801	2%	124	0%	806	3%
36	326	1%	71	0%	421	1%	72	0%	589	2%
38	110	0%	37	0%	16 <b>6</b>	0%	33	0%	370	1%
40	14	0%	23	0%	57	0%	12	0%	192	0%
42	8	0%	7	0%	23	0%	8	0%	182	0%
44	2	0%	7	0%	8	0%	2	0%	83	0%
46	3	0%	9	0%	49	0%	4	0%	56	0%
48	0	0%	0	0%	19	0%	0	0%	. 18	0%
50	0	0%	0	0%	4	0%	0	0%	3	0%

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SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - NOVEMBER - WITH NIPS IN EXCESS OF 450 W/M2

MPH STX1801*		STX1810*		STX1815*		STX1822*		STX1835*		
52	. 0	0%	9	0%	5	0%	Ø	0%	4	0%
54	9	0%	0	0%	1	0%	0	0%	3	0%
56	0	0%	0	0%	0	0%	0	0%	2	0%
58	0	0%	0	0%	0	0%	0	0%	ō	0%
60	0	0%	0	0%	0	0%	0	0%	1	0%
62	0	0%	0	0%	0	0%	0	0%	. 0	0%
64	0	0%	0	0%	0	0%	0	0%	0	0%
66	0	0%	0	0%	0	0%	0	0%	0	0%
68	0	0%	0	0%	0	0%	0	0%	0	0%
70	0	0%	0	0%	. 0	0%	0	0%	0	0%
72	0	0%	0	0%	Ø	0%	õ	0%	0	0%
74	0	0%	0	0%	0	0%	0	0%	0	0%
76	0	0%	0	0%	0	0%	0	0%	0	0%
78	0	0%	9	0%	0	0%	0	0%	0	0%
80	0	0%	0	0%	0	0%	0	0%	0	0%
82	0	0%	0	0%	0	0%	0	0×	0	0%
84	0	0%	0	0%	0	0%	0	0%	0	0%
86	0	0%	0	0%	0	0%	0	0%	0	0%
88	0	0%	0	0%	0	0%	0	0%	0	0%
90	0	0%	0	0%	0	0%	9	0%	0	0%
92	0	0%	0	0%	0	0%	0	0%	0	0%
94	0	0%	0	0%	0	0%	0	0%	0	0%
96	0	0%	0	0%	0	9%	0	0%	0	0%
98	0	0%	0	0%	0	0%	0	0%	0	0%
100	0	0%	0	0%	0	0%	0	0%	0	0%

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SOLAR ONE WIND DIRECTION DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - NOVEMBER - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0TX180	2*	0TX181	1*	0TX181	6*	0TX182	3*	0TX183	6 <b>*</b>
0	118	0%	79	0%	1460	5%	4332	17%	123	0%
15	164	0%	126	<b>0</b> %	344	1%	683	2×	319	1%
30	226	0%	162	0%	440	1%	482	1 %	840	3%
45	311	1%	331	1%	670	2%	528	2%	403	1%
60	518	1%	828	2%	731	2%	670	2%	386	1%
75	876	3%	836	3%	609	2%	709	2%	268	1%
90	728	2×	659	2%	732	2%	642	2%	181	0×
105	610	2%	744	2%	705	2%	559	2*	189	0%
120	361	1%	613	2%	550	2%	596	2%	398	1%
135	255	0%	333	1×	426	1%	542	2%	569	2%
150	345	1%	244	0%	256	0%	456	1%	493	1%
165	148	0%	140	0%	198	<b>0</b> %	372	1%	730	2%
180	164	<b>0</b> %	142	0%	553	0%	312	1 %	187	0%
195	117	0×	120	<b>0</b> %	353	1 %	231	<b>0</b> %	195	0%
210	169	<b>0</b> %	157	0×	1337	4%	269	1 %	314	1 %
225	262	<b>0</b> %	348	1%	1865	6%	585	2×	955	3%
240	1117	4%	1304	4%	6910	25%	1651	6%	2246	8%
255	2764	10×	3356	12%	5430	19%	2332	9%	4507	18%
270	4766	17X	8077	29%	2079	7%	2052	8%	6054	24%
285	8185	29%	5988	21%	984	3%	1934	7%	3775	15%
300	3677	13%	1843	6%	443	1 %	1807	7%	1138	4%
315	614	2×	591	2%	281	1%	1832	7%	292	1%
330	353	1%	351	1 %	193	. 0%	824	3%	188	0×
345	457	1 %	158	0×	95	0 X	232	0×	161	0×
360	106	<b>0</b> %	55	0×	. 41	<b>0</b> ×	71	0×	64	0×

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MPH	STX1801	L*	STX181	0*	STX181	5*	STX182	2*	STX183	5 <b>*</b>
0	898	4%	302	1%	1537	7%	119	0%	2	0%
Ž	1723	9%	1337	7%	1185	5%	2497	12%	626	13%
4	3161	17%	3328	17%	3029	15%	3281	16%	805	17%
	3331	18%	4029	21%	4123	20%	4527	22%	589	12%
6 8	2570	14%	3320	17%	3063	15%	358 <b>7</b>	17%	311	6%
10	1461	8%	1595	8%	1764	8%	1747	8%	199	4%
12	1087	5%	820	4%	901	4%	970	4%	189	4%
14	520	2%	567	3%	540	2%	641	3%	224	4%
16	396	2%	454	2%	533	2%	500	2%	157	3%
18	391	2%	404	2%	377	1%	394	1 %	174	3%
20	457	2%	426	2%	378	1 %	293	1 %	175	3%
22	418	2%	398	2%	414	2%	236	1 %	175	3%
24	314	1 %	345	1 %	359	1 %	181	0%	158	3%
26	209	1%	293	1%	335	1%	179	0%	190	4%
28	240	1 %	253	1 %	272	1%	167	. 0%	95	2%
30	225	1%	222	1%	270	1%	139	0%	308	6%
32	179	0%	154	0%	176	0%	102	0%	61	1 %
34	157	0%	134	0%	162	0%	82	0%	28	0%
36	119	0%	113	0%	99	0%	103	0%	38	0%
38	138	0%	112	0%	84	0%	86	0%	34	0%
40	75	0%	93	0%	67	0%	65	0%	13	0%
42	47	0%	71	0%	37	0%	36	0%	3	0%
44	32	0%	51	0%	26	0%	24	0%	5	0%
46	33	0%	36	0%	42	0%	62	0%	7	0%
48	5	0%	9	0%	15	0%	21	0%	. 1	0%
50	0	0%	5	0%	1	0%	8	0%	4	0%

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SOLAR WIND (SPEED) DISTRIBUTION FOR PLOT MS01
TEST DATA FOR MONTH OF - DECEMBER - WITH NIPS IN EXCESS OF 450 W/M2

										_		
MPH	STX180:	STX1801*		STX1801* STX1810*		ð <b>*</b>	STX1815*		STX1822*		STX1835*	
52	0	0%	г	0%	Ø	0%	2	0%	0	0%		
54	0	0%	0	0%	0	0%	0	0%	0	0%		
56	ð	0%	0	0% .	0	0%	0	0%	0	0%		
58	Ø	0%	0	0%	ø	0%	0	0%	0	0%		
60	ø	0%	0	0%	0	Ø%	0	0%	0	0%		
62	0	0%	0	0%	0	0%	0	0%	0	0%		
64	0	0%	Ø	0%	. 0	0%	0	0%	0	0%		
66	0	0%	0	0%	0	0%	0	0%	0	0%		
68	0	0%	0	0%	0	0%	0	0%	0	0%		
70	0	0%	Ø	0%	0	0%	0	0%	0	0%		
72	0	0%	0	0%	0	0%	0 .	0%	0	0%		
74	8	0%	0	0%	0	0%	0	0%	0	0%		
76	0	0%	0	0%	0	0%	0	0%	0	0%		
78	0	0%	0	0%	Ø	0%	0	0%	0	0%		
80	0	0%	0	0%	0	0%	0	0%	0	0%		
82	0	0%	0	0%	0	0%	0	0%	0	0%		
84	0	0%	0	0%	0	0%	0	0%	0	0%		
86	. 0	0%	0	0%	0	0%	0	0%	0	0%		
88	0	0%	.0	0%	0	0%	0	0%	0	0%		
90	0	0%	0	0%	0	0%	0	0%	0	0%		
92	0	0%	0	0%	0	0%	0	0%	. 0	0%		
94	0	0%	0	0%	0	0%	0	0%	0	0%		
96	0	0%	0	0%	0	0%	0	0%	0	0%		
98	0	0%	0	0%	0	0%	0	0%	0	0%		
100	0	0%	0	0%	0	0%	0	0%	0	0%		

PAGE 1
SOLAR ONE WIND (DEGREE) DISTRIBUTION FOR PLOT MD01
TEST DATA FOR MONTH OF - DECEMBER - WITH NIPS IN EXCESS OF 450 W/M2

DEG	0TX180	*2	0TX181	1 *	0TX181	<b>6</b> *	0TX182	3*	0TX183	<b>6</b> *
Ø	629	3%	181	0%	341	1%	101	0%	19	<b>0</b> %
15	118	0%	78	0 %	80	0%	109	0%	43	0%
90 0E	154	0%	192	0%	138	0%	168	0%	79	1 %
45	263	1 %	341	1 %	266	1 %	484	2%	92	2%
60	701	3%	814	4%	667	3%	1014	5%	105	2%
75	2407	12%	1778	9%	1249	6%	2134	10%	75	1%
90	2009	10%	2078	10%	2190	10%	2384	11%	64	1%
105	1535	7%	1655	8%	2445	12%	1388	6%	56	1%
120	678	3%	862	4%	1235	6%	676	3%	92	2%
135	232	1 %	473	2%	565	2%	345	1 %	192	4%
150	248	1%	364	1%	198	0%	211	1%	88	1%
165	184	0%	248	1 %	131	0%	123	0%	49	1 %
180	97	0%	241	1%	100	0%	135	0%	39	0%
195	145	0%	294	1%	140	0%	295	1 %	41	0%
210	506	2%	491	2%	323	1%	552	2%	82	1%
225	560	5%	592	3%	583	2%	553	2%	207	4%
240	661	3%	600	3%	640	3%	717	3%	675	14%
255	1363	7%	1507	7%	978	4%	1705	8%	954	20%
270	1473	7%	2705	13%	2498	12%	2061	10%	800	17%
285	2121	10%	1672	8%	2295	11%	2204	10%	522	11%
300	1605	8%	1275	6%	1612	8%	1546	7%	180	3%
315	931	4%	697	3%	873	4%	655	3%	53	1%
330	386	1 %	344	1%	308	1%	252	1 %	28	0%
345	338	1 %	165	0%	128	0%	164	0 X	20	0%
360	102	0%	39	0%	34	0%	69	0%	17	0%

## 5.7 INSOLATION DATA

Insolation data were recorded at Solar One during 1983 from two normal incidence pyrheliometers (tag ID ATX 1817 at the north station and tag ID ##ATX 1817A on the control room roof) to provide direct normal data, and from twelve pyranometers located at the four meteorological stations, the four spoke roads, and the control room roof to provide global insolation data. There were a total of 289 days during 1983 when the data acquisition system was recording and there was sufficient insolation to have some NIP activity. NIP plots for each of the 289 days are included in this report, with data from one of the instruments selected for each day. There were 104 clear days, 53 days with light cloud activity, and 132 days with heavy cloud activity in the 289 data days. Pyranometer data from 8 of the data days were selected and are also included in this report to represent 1 clear day, 3 days with light cloud activity, and 4 days with heavy cloud activity.

In addition to the 289 data days recorded by the data acquisition system, daily readings of integrated insolation values were taken from the Beckman MV8000 system in the control room, which records and integrates the insolation from the same normal incidence pyrheliometer on the control room roof that feeds tag ID ##ATX1817A; however, the integrated data are recorded on the Beckman system under the tag ID NIP 1000, and serve as the source of the monthly direct normal insolation data presented in tabular form in this report. The daily integrated values of insolation were recorded for a total of 357 data days during 1983.

The Solar One direct normal insolation data recorded at Solar One from the control room roof NIP during 1983 are shown on Table 7. Monthly totals and daily averages are shown for three Solar One parameters, as follows:

- NIP 1000 The total integrated value of direct normal insolation from horizon to horizon, as recorded by a normal incidence pyrheliometer (NIP).
- NIP Hours -The useable portion of the total, with cutoffs at 500  $\text{W/m}^2$  on startup and shutdown.
- NIP Time A total value of time, per day, as determined by a counter, when insolation levels were above  $450 \text{ W/m}^2$ .

Table 7. Solar One Direct Normal Insolation Data - 1983

		NI (TOT kw hr 1976			NIP 1000 NIP HRS N (TOTAL) ← 500 WATTS/m²) (TIME ABOV kw hr/m² kw hr/m²		(TIME ABOVE 45	NIP TIME VE 450 WATTS/m <sup>2</sup> ) DATA DA hours		
	MONTH	DAILY AVERAGE*	DAILY AVERAGE	MONTHLY TOTAL	DAILY AVERAGE	MONTHLY TOTAL	DAILY AVERAGE	MONTHLY TOTAL	DAILY AVERAGE	
	JANUARY	7.10	4.87	134.260	4.630	103.820	3.580	164.740	5.681	29
	FEBRUARY	6.15	5.51	104.811	4.031	69.823	2.686	127.150	4.890	26
	MARCH	7.33	6.60	134.993	4.655	97.312	3.356	160.430	5.532	29
	APRIL	8.00	8.01	192.278	6.409	138.043	4.601	229.390	7.646	30
110	MAY	8.95	8.69	258.922	8.352	212.212	6.846	318.960	10.289	31
_	JUNE	10.56	9.39	247.117	8.521	204.019	7.035	304.162	10.488	29
	JULY	8.23	8.76	289.846	9.350	241.422	7.788	327.729	10.572	31
	AUGUST	10.13	8.32	178.513	5.758	134.774	4.348	214.060	6.905	. 31
	SEPTEMBER	5.78	7.59	185.106	6.170	142.689	4.756	230.481	7.683	30
	OCTOBER	7.47	6.65	182.346	5.882	145.547	4.695	222,600	7.181	31
	NOVEMBER	7.19	5.52	158.823	5.477	120.176	4.144	195.460	6.740	29
	DECEMBER	6.40	4.83	154.651	4.989	110.801	3.574	187.400	6.045	31

<sup>\*</sup>C. M. Randall, "Barstow Insolation and Meteorological Data Base," The Aerospace Corporation,
Report ATR-78(7695-05)-2, 3/13/78

<sup>\*\*&</sup>quot;Direct Normal Solar Radiation Data Manual," Solar Energy Research Institute, SERI/SP-281-1658, 10/82.

(These direct normal insolation values are estimated from total global data.).

Daily averages for observed total direct normal insolation at Barstow during 1976 are also included in Table 7 for comparison, as well as a set of 25 year daily average direct normal values which were estimated from total global data. The number of data days recorded per month and used for calculating the daily averages is also included.

A comparison of the 1976, 25 year average, and the NIP 1000 daily average values indicates that the 1983 insolation was lower than the 1976 and 25 year average values for all months except July, which was a very good insolation month during 1983. The daily average value for September 1983 also exceeded the September 1976 value slightly. A comparison of 1983 with 1976 on an annual basis, using the same number of data days per month to calculate a comparable 1976 total, indicates that the total available direct normal insolation for 1983 was 20 percent less than 1976. In 1982, considering the time period of only April through December where Solar One data were available, and comparing those insolation data to a comparable period in 1976 with the same number of data days per month for 1976 and 1982, the 1982 total available insolation was 16 percent less than 1976.

The direct normal insolation data were examined to identify the days when the plant was operating, or could have operated as far as insolation values and wind speeds were concerned. The number of data days was adjusted to eliminate the low insolation and windy days and provide modified monthly totals and daily averages. These data are shown in Table 8. A comparison between those values and 1976 data cannot be made, since the number of days per month in 1976 when the plant could have been operating is unknown. Table 8 provides monthly and daily average values for the operable days of the total number of days analyzed.

A comparison of maximum and average peak insolation values for 1976 and 1983 is shown in Table 9. The 1983 peak and average peak insolation was lower than in 1976 for each month. Plots of peak insolation values and average peak insolation values for 1976 and 1983 are shown in Figures 43 and 44.

Table 8. Useful Solar One Direct Normal Insolation Data - 1983

		NIP (TOTAL) kw hr/m <sup>2</sup> 1976 25-year**		NIP (TO kw h	TAL)	NIP HRS NIP TIME  (>500 WATTS/m <sup>2</sup> ) (TIME ABOVE 450 WATTS hours			O WATTS/m	NO. OF DATA DAYS
	МОИТН	DAILY AVERAGE*	DAILY AVERAGE "	MONTHLY TOTAL	DAILY AVERAGE	MONTHLY TOTAL	DAILY AVERAGE	MONTHLY TOTAL	DAILY AVERAGE	
	JANUARY	7.10	4.87	121.238	5.511	98.415	4.473	150.010	6.819	22
	FEBRUARY	6.15	5.51	76.312	6.359	59.672	4.973	96.370	8.031	12
	MARCH	7.33	6.60	106.557	6.660	85,560	5.348	129.270	8.079	16
	APRIL	8.00	8.01	165.838	7.538	131.500	5.977	201.620	9.165	22
112	MAY	8.95	8.69	231.887	8.588	191.722	7.101	286.040	10.594	27
	JUNE	10.56	9.39	241.235	8.616	202.889	7.246	296.872	10.603	28
	JULY	8.23	8.76	287.443	9.581	241.422	8.047	327.729	10.924	30
	AUGUST	10.13	8.32	161.206	8.060	129.176	6.459	194.740	9.737	20
	SEPTEMBER	5.78	7.59	160.713	7.653	134.598	6.409	201.381	9.590	21
	OCTOBER	7.47	6.65	159.920	6.953	136.629	5.940	196.290	8.534	23
	NOVEMBER	7.19	5.52	125.625	6.612	106.259	5.593	156.560	8.240	19
	DECEMBER	6.40	4.83	111.965	5.893	90.514	4.764	139.460	7.340	19

<sup>\*</sup>C. M. Randall, "Barstow Insolation and Meteorological Data Base," The Aerospace Corporation,
Report ATR-78(7695-05)-2, 3/13/78

<sup>\*\*&</sup>quot;Direct Normal Solar Radiation Data Manual," Solar Energy Research Institute, SERI/SP-281-1658, 10/82. (These direct normal insolation values are estimated from total global data.).

Table 9

MAXIMUM AND AVERAGE PEAK INSOLATION VALUES FOR 1976 AND 1983\*

	1	976				
MONTH	PEAK INSOLATION	AVERAGE PEAK INSOLATION	DATA DAYS	PEAK INSOLATION	AVERAGE PEAK INSOLATION	DATA DAYS
JAN	1003	943	31	910	820	27
FEB	1006	942	27	911	820	18
MAR	1036	949	31	968	824	18
APR	992	918	30	941	880	22
MAY	991	902	30	979	889	30
JUN	992	943	30	951	874	26
JUL	995	878	31	945	876	18
AUG	1000	946	30	935	862	13
SEP	961	879	24	948	855	24
OCT	994	927	28	959	869	25
νον	987	907	29	950	863	29
DEC	999	920	25	916	829	30

<sup>\*</sup>Insolation values are in watts per square meter, peak values were not used for averaging when the peak for the day did not exceed 450  $\text{W/m}^2$ .

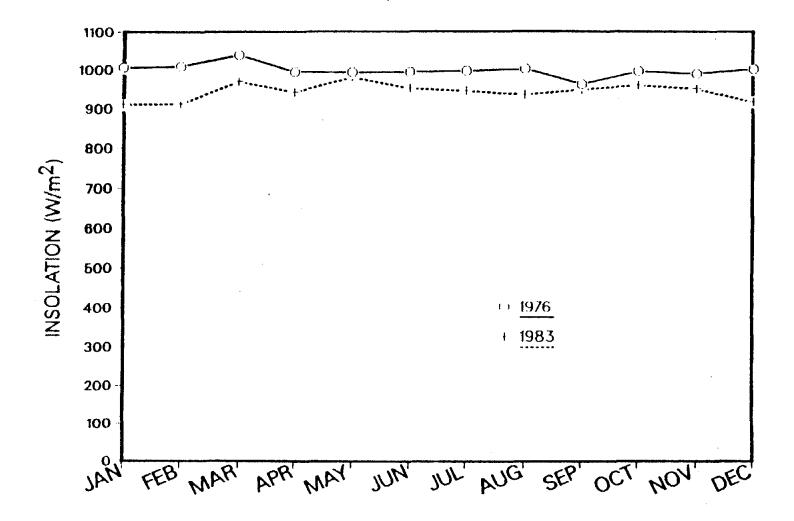


Figure 43. Peak Insolation Values for 1976 and 1983

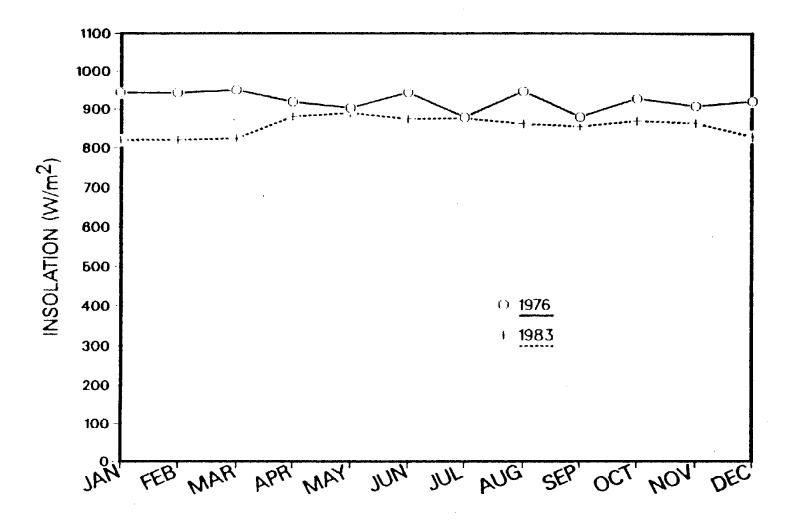
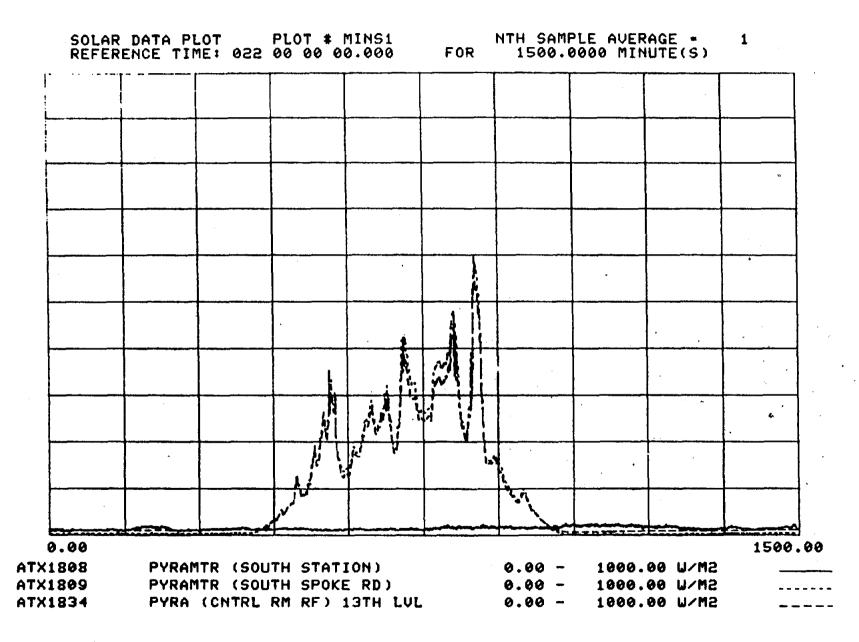


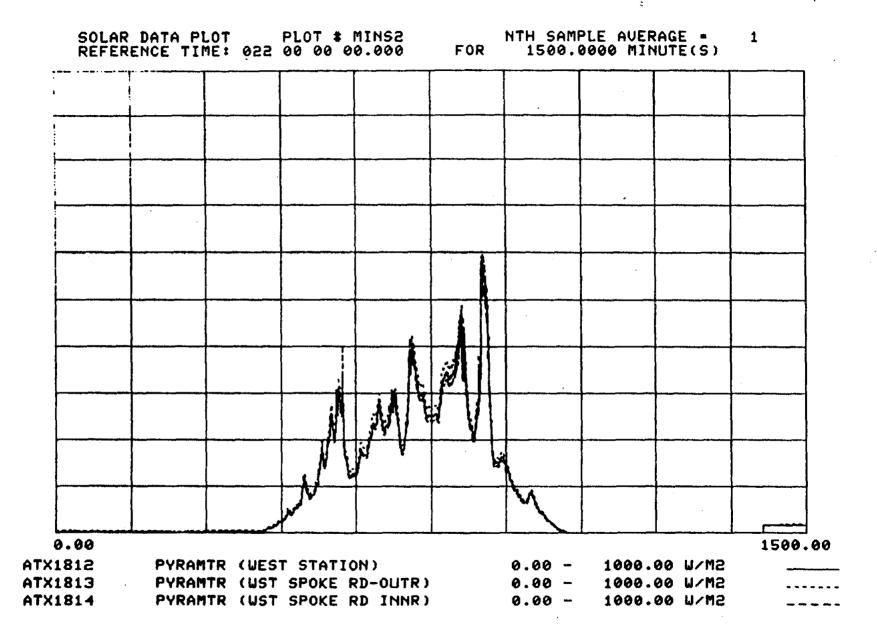
Figure 44. Average Peak Insolation Values for 1976 and 1983

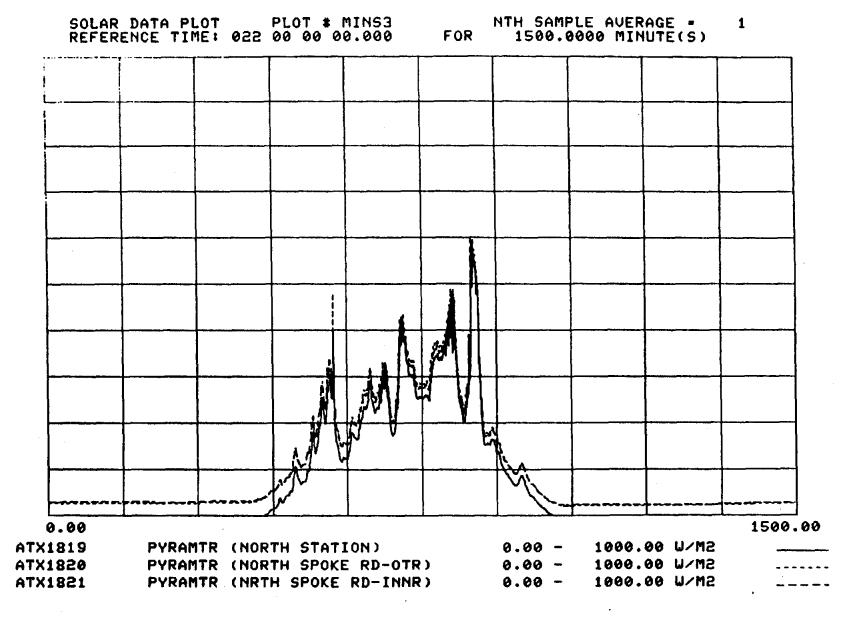
Pyranometer data for 12 instruments are included on the following pages for 6 days which were selected from the total 289 days processed. The specific days selected were 022, 058, 131, 211, 348, 353, 355, and 362. This selection is intended to provide data for a mixture of clear days and days with light and heavy levels of cloud activity. These pyranometers were installed for cloud passage studies and as a potential means of heliostat control during cloudy periods. The purpose of these plots is to show what type of data are available. The start time and date for each plot are noted as "reference time." The day of the year is listed first, followed by the time of day in hours, minutes, seconds, and milliseconds. For example, on the next page, the day is 022 (22 January), and the time is midnight. Table 10 may be used to convert the day of the year to the date. The plot goes for 25 hours. The scale for the ordinate is shown on the bottom of the page, with full scale being 1000 watts/m<sup>2</sup>.

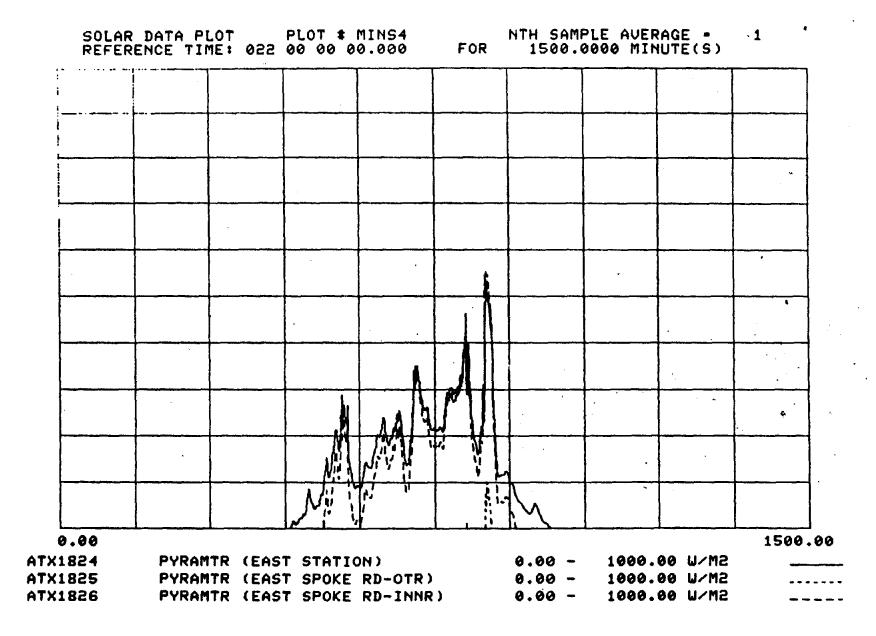
Table 10. DAY OF THE YEAR AND DATE FOR 1983

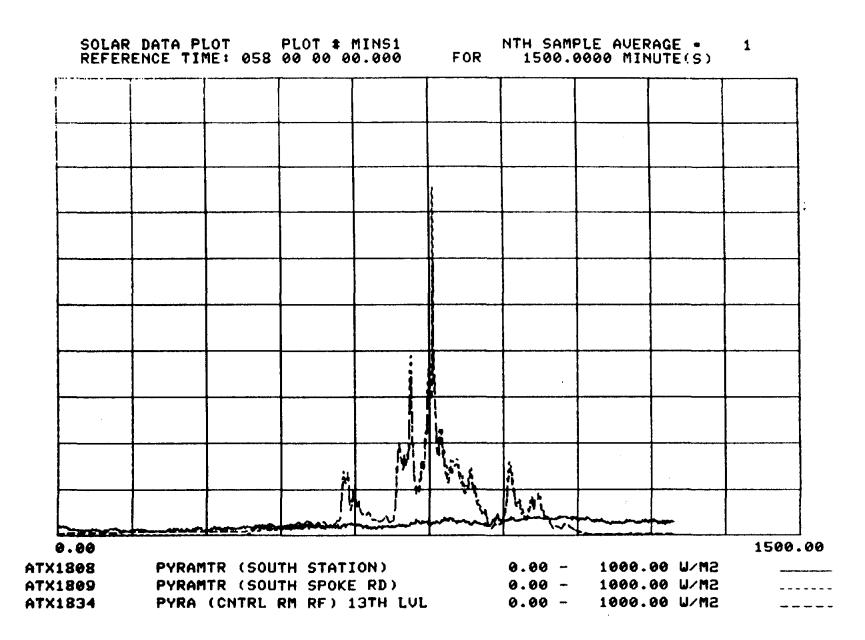
<u>Day</u>	Date	Day	<u>Date</u>
1	Jan 1	182	Jul l
32	Feb 1	213	Aug 1
60	Mar 1	244	Sep 1
91	Apr 1	274	Oct 1
121	May 1	305	Nov 1
152	Jun 1	335	Dec 1

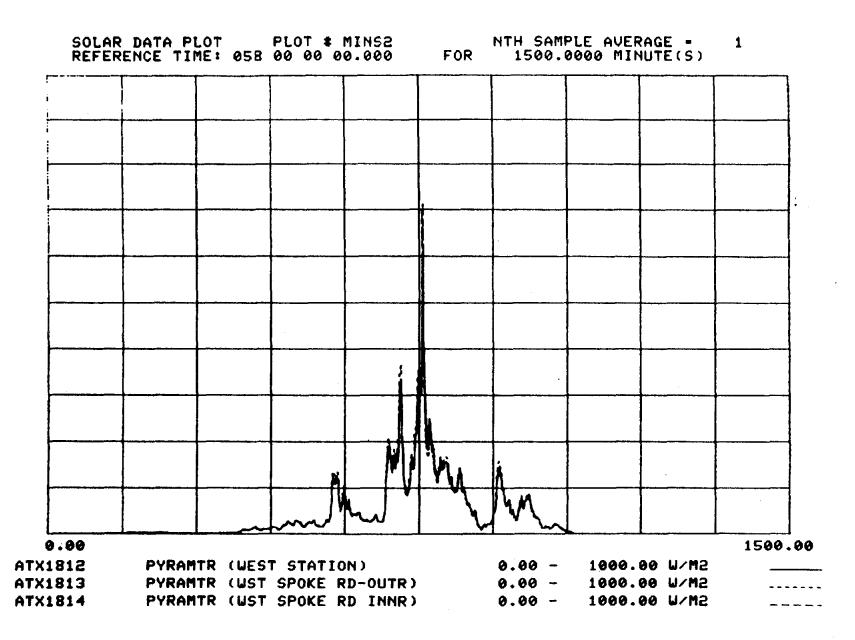


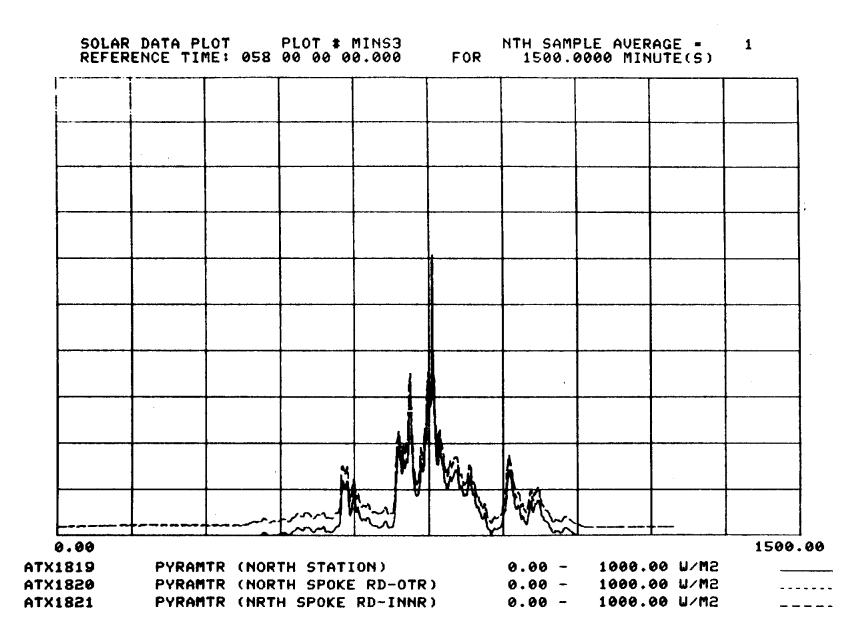


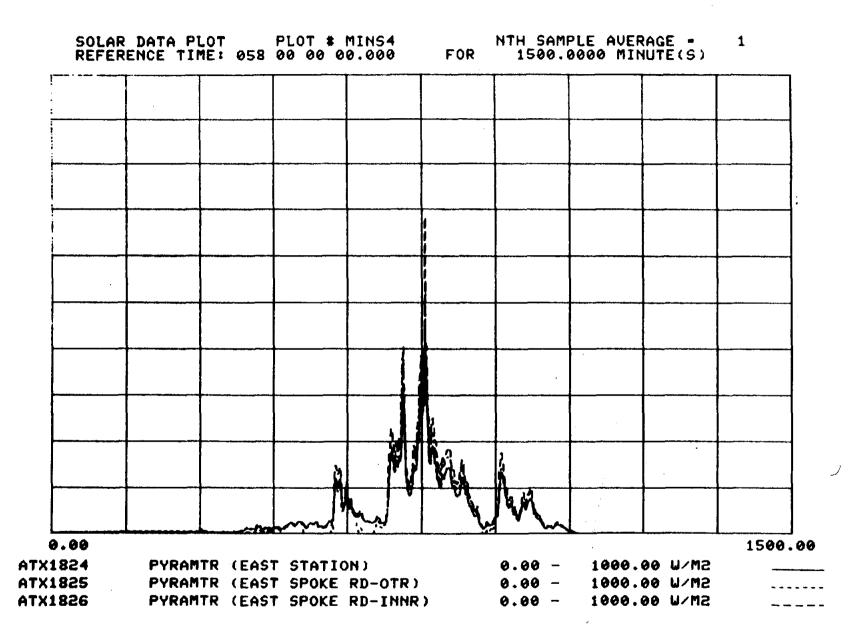


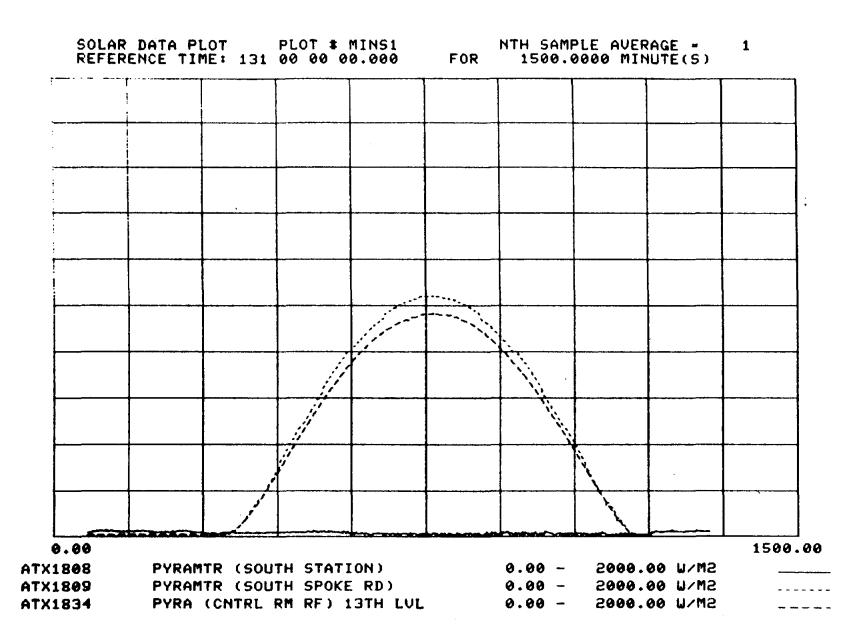


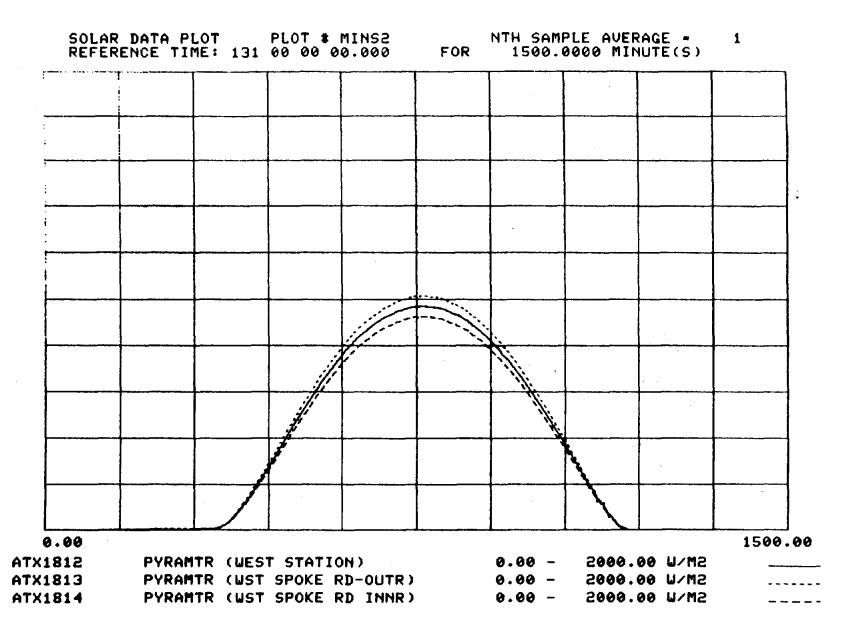


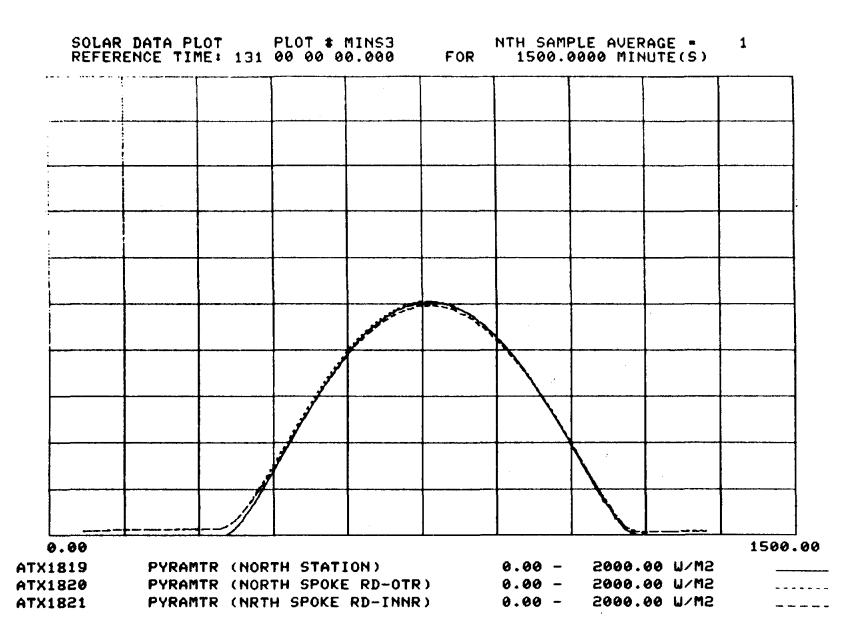


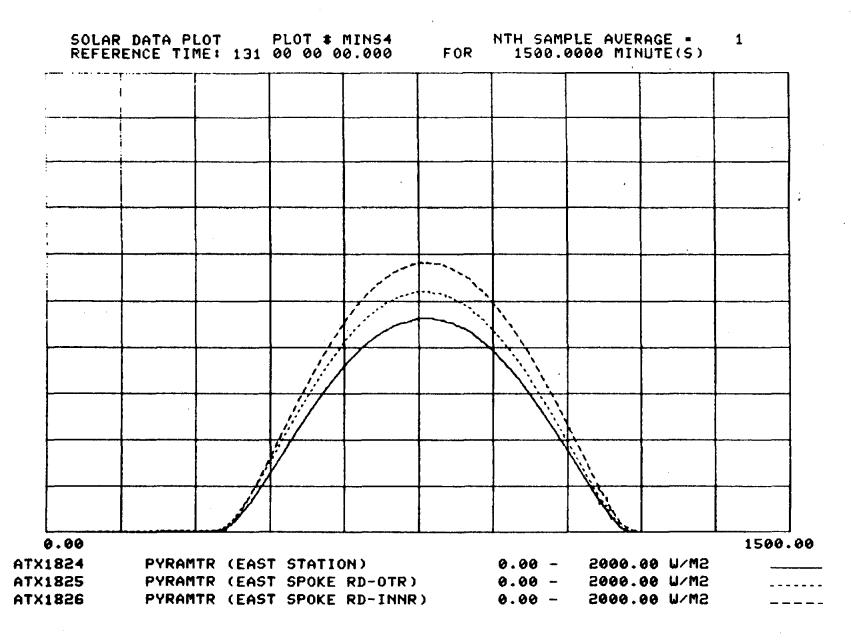


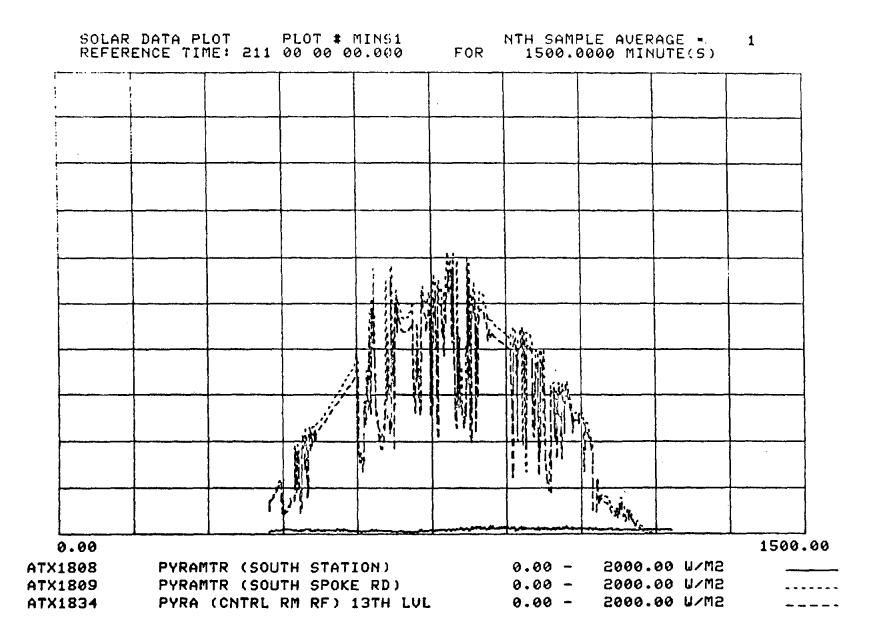


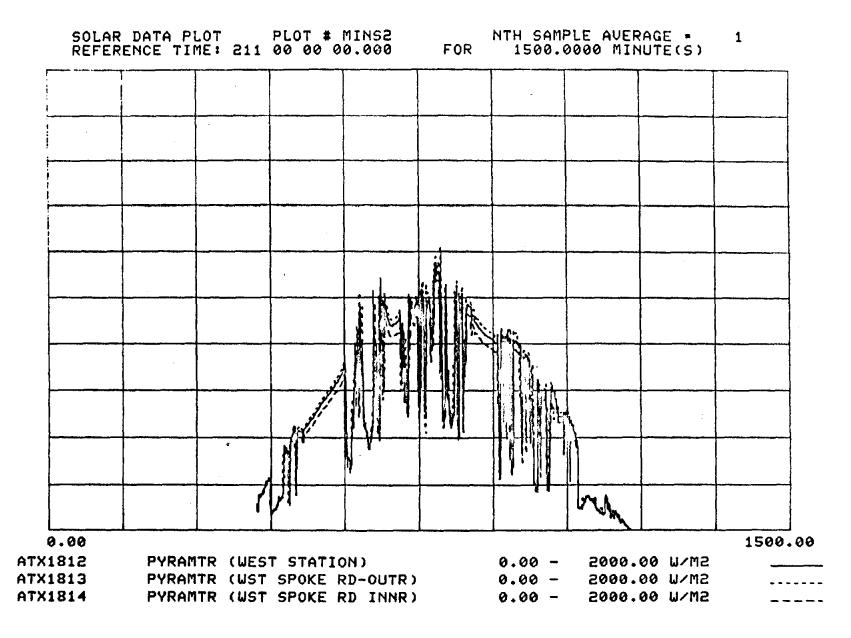


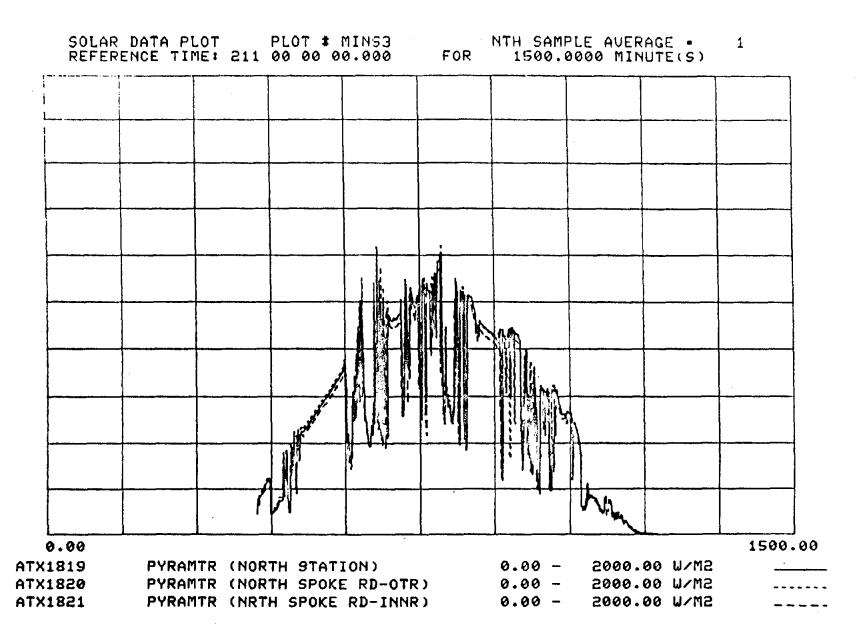


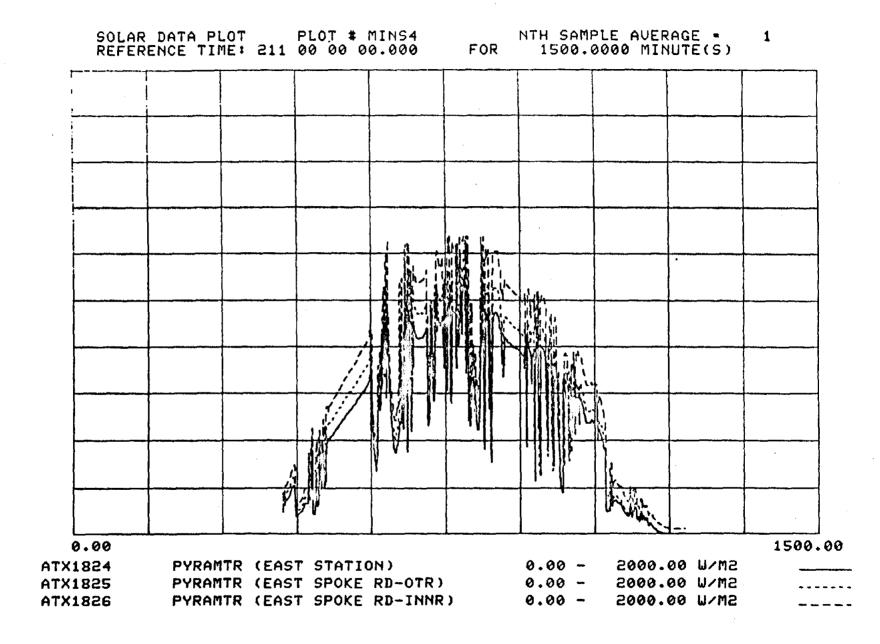


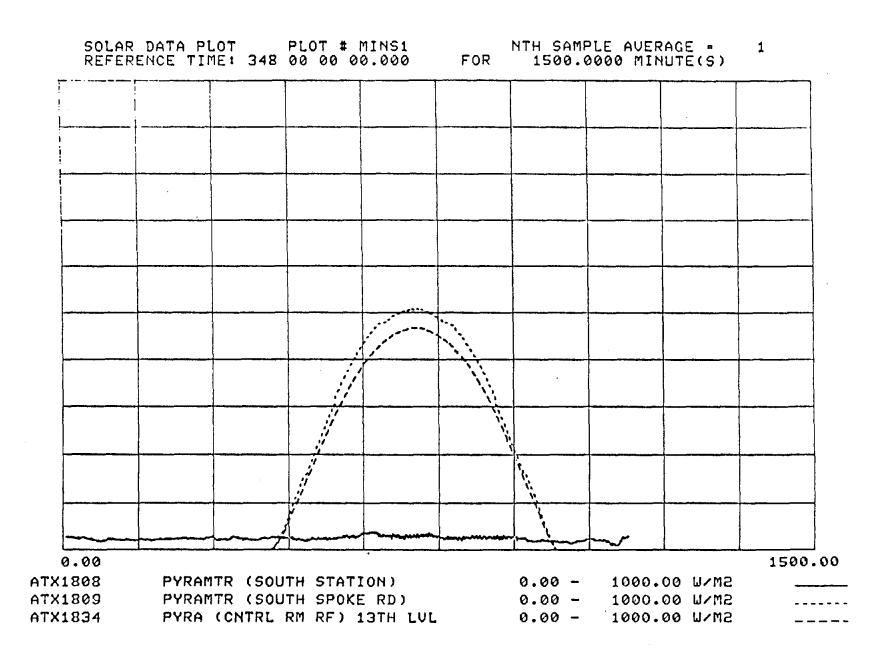


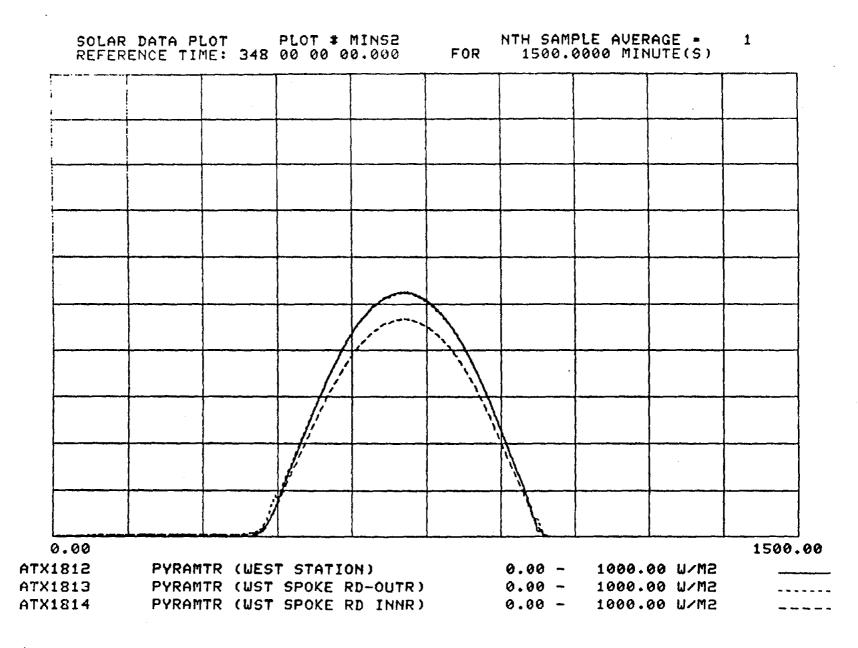


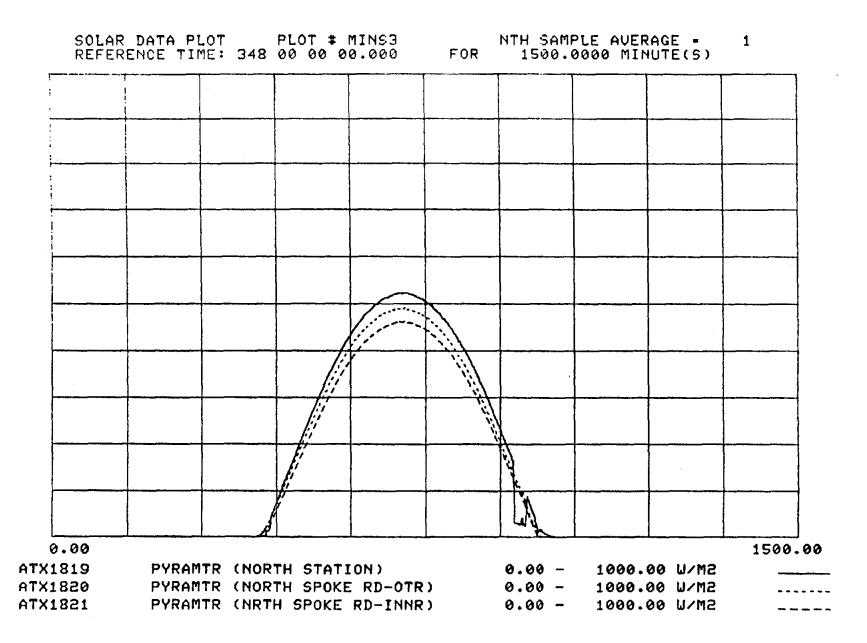


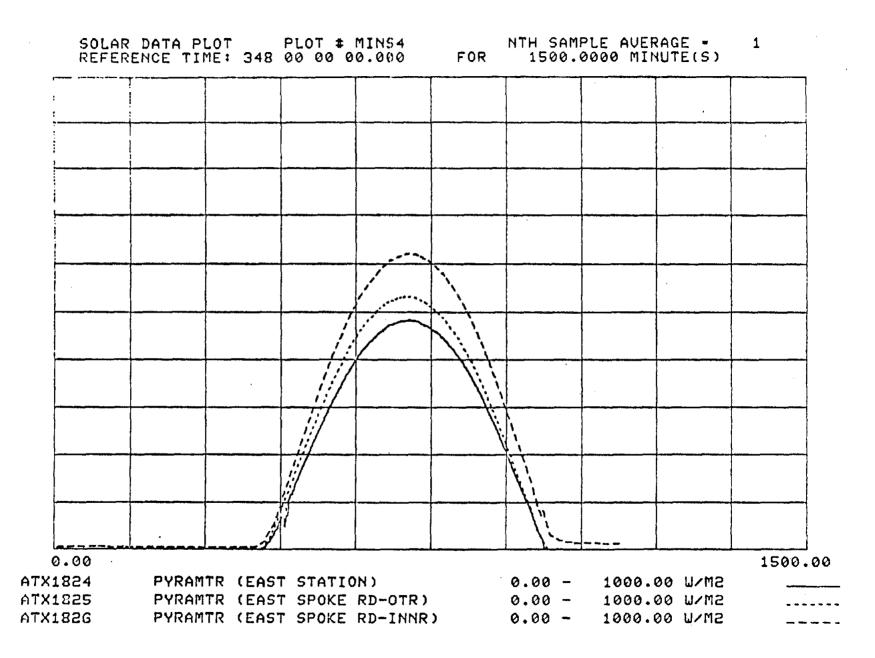


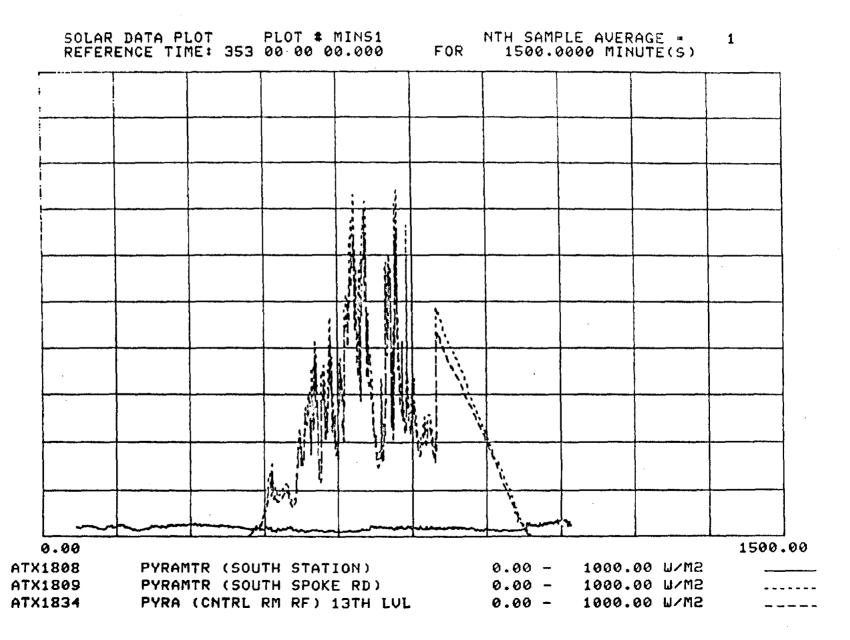


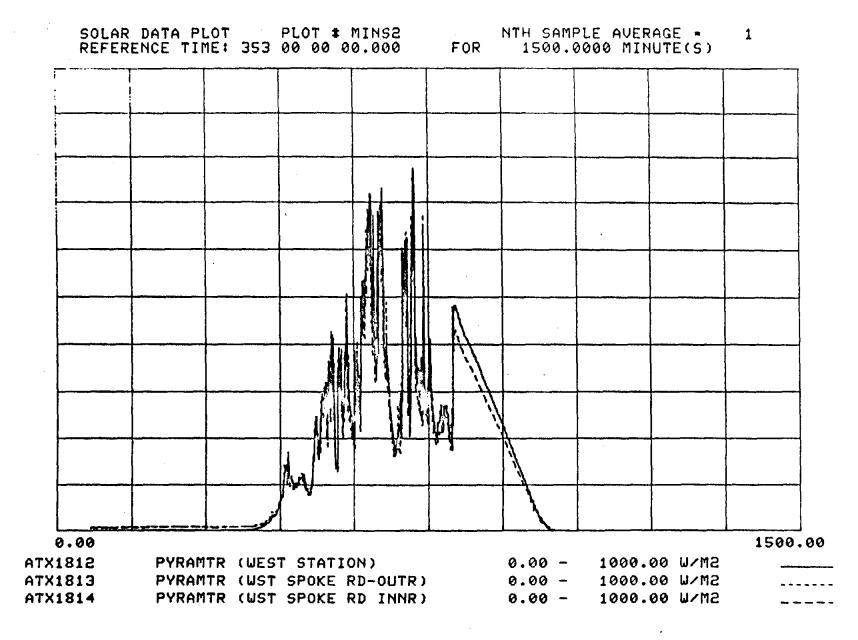


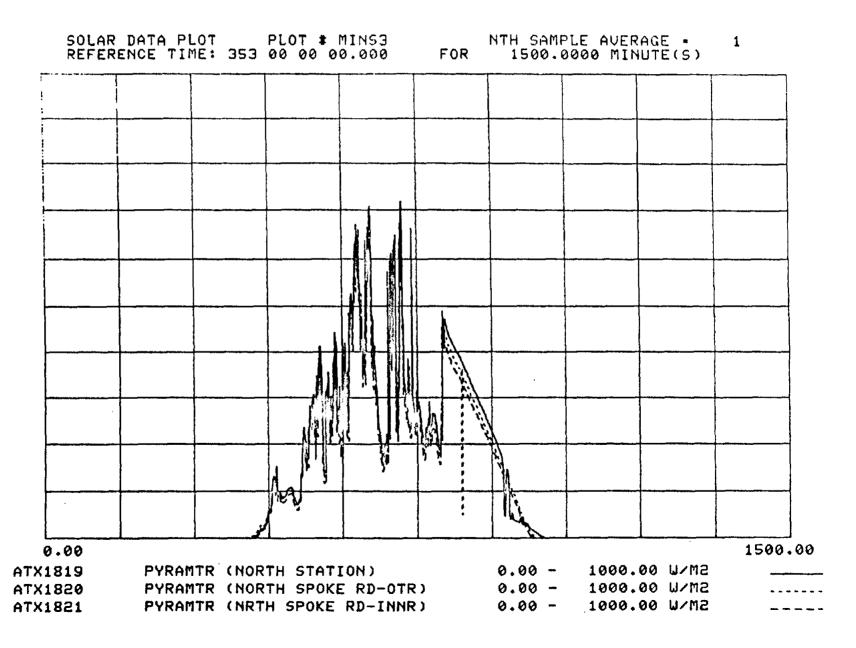


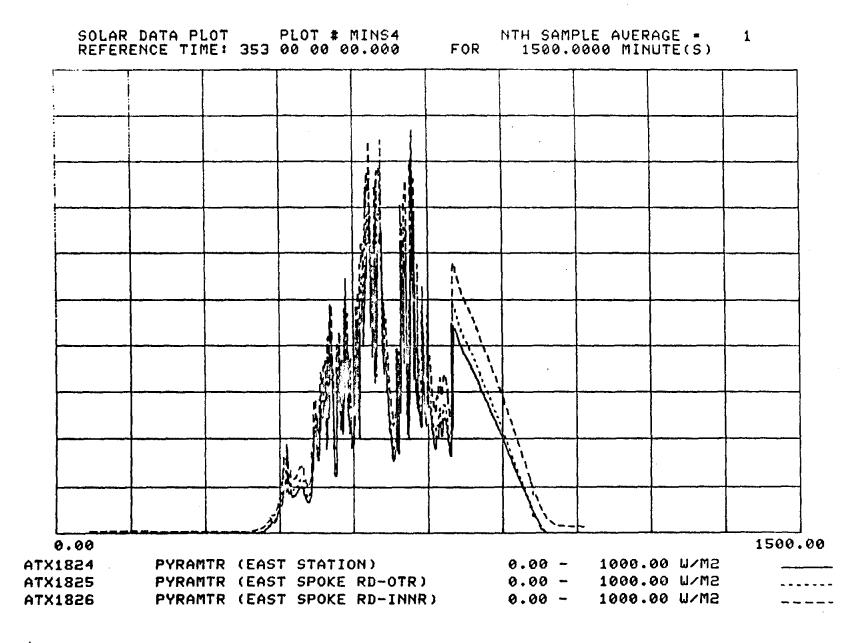


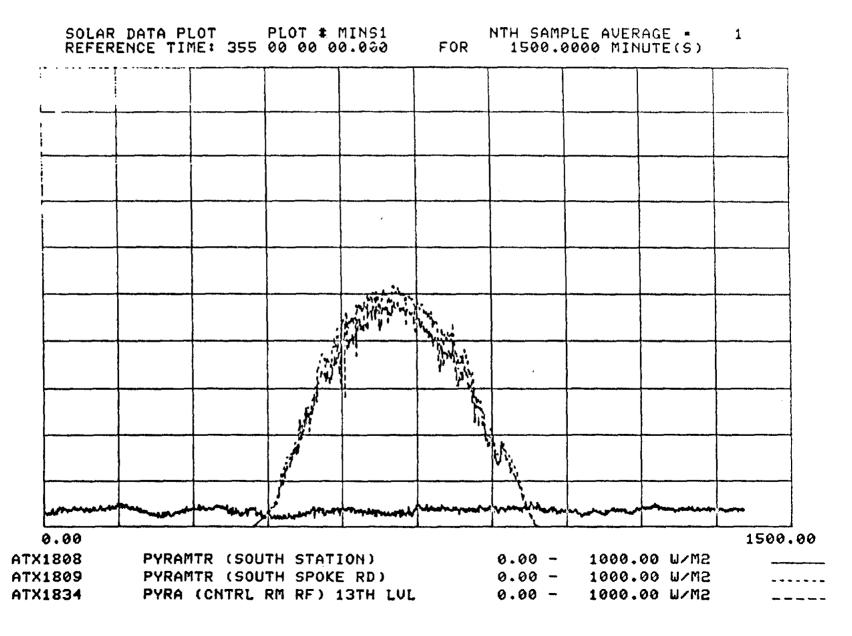


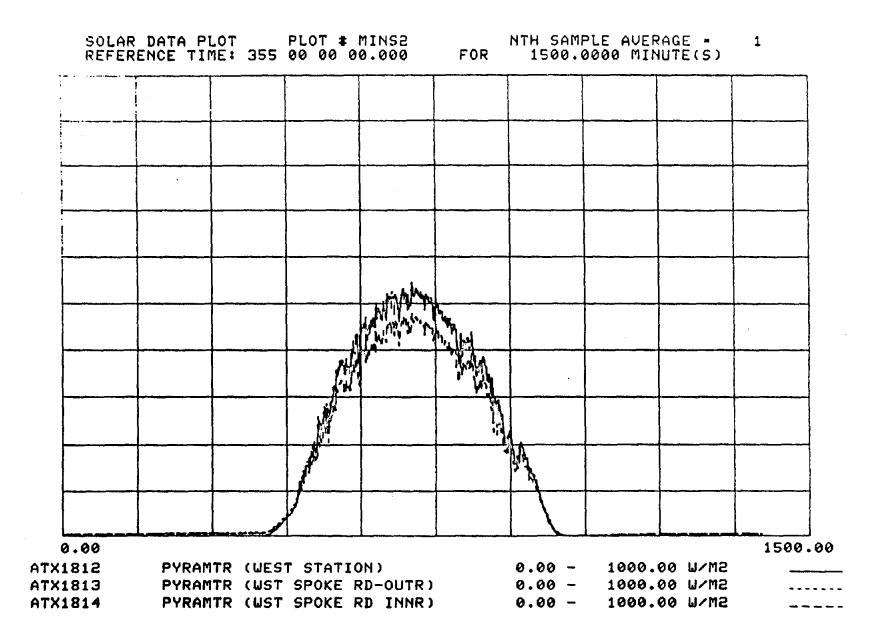


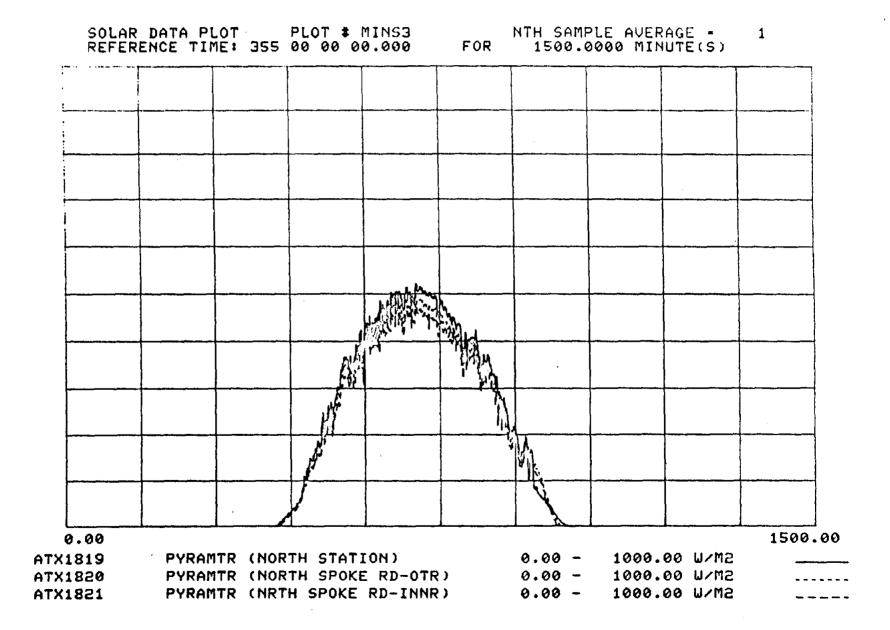


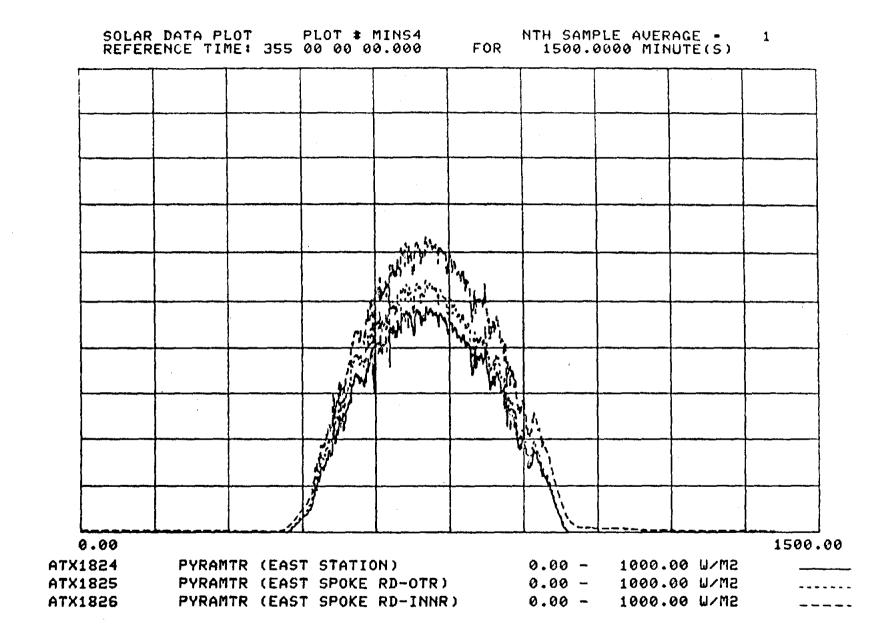


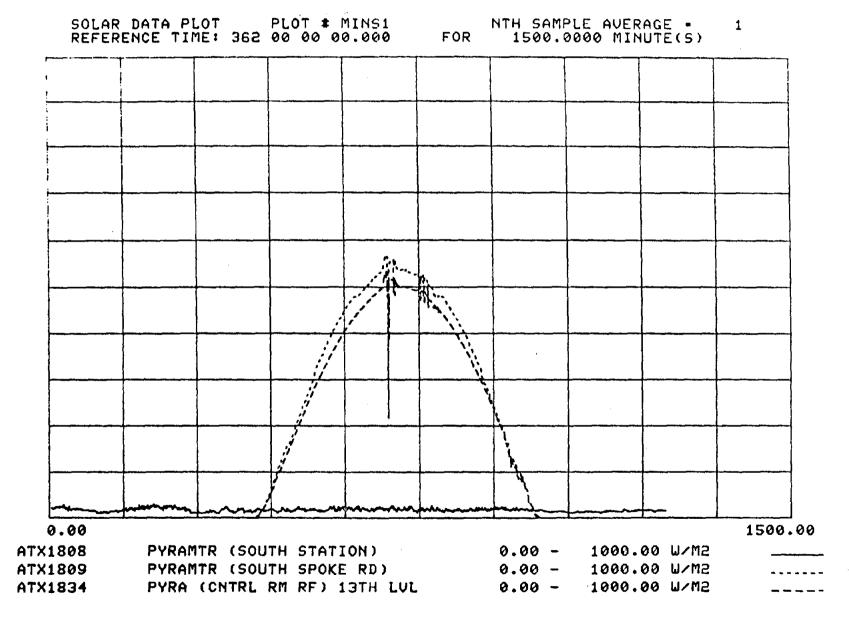


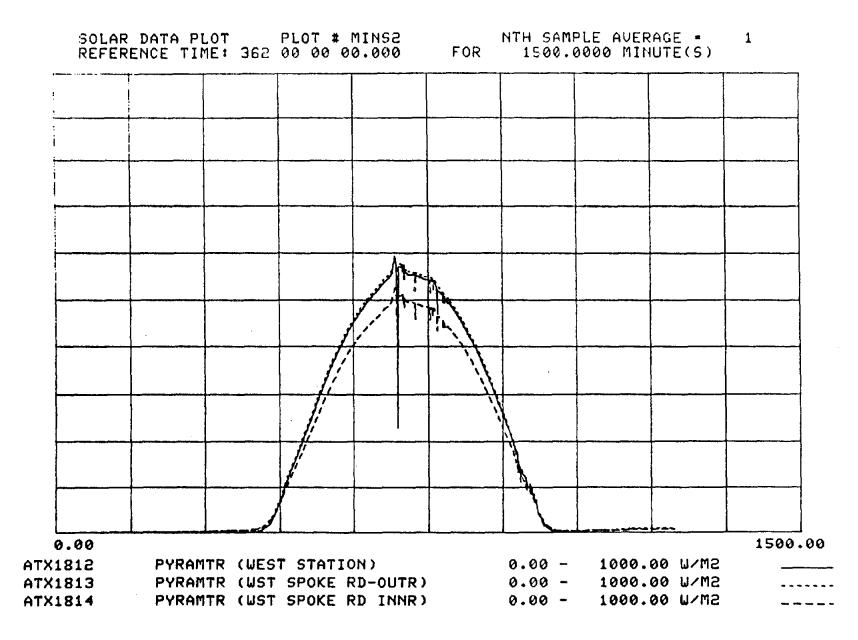


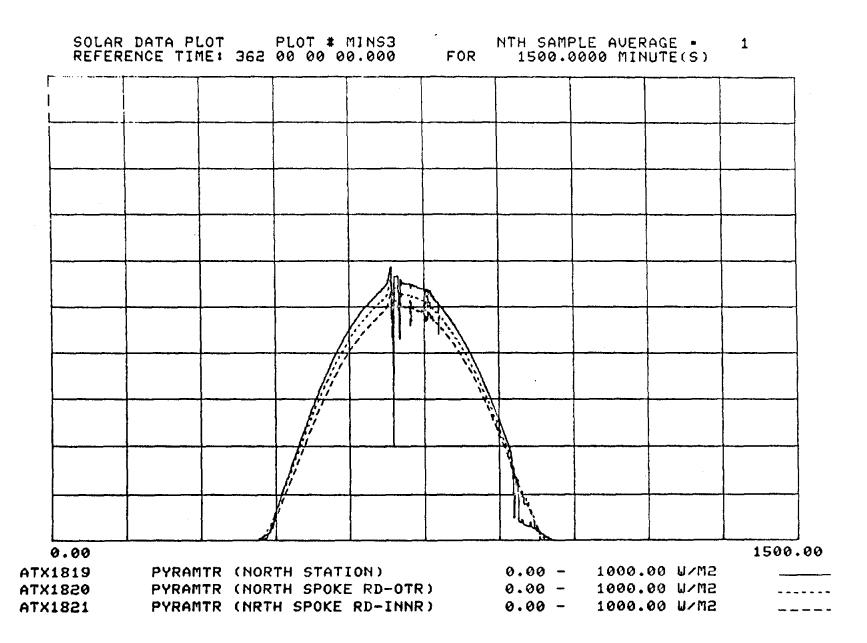


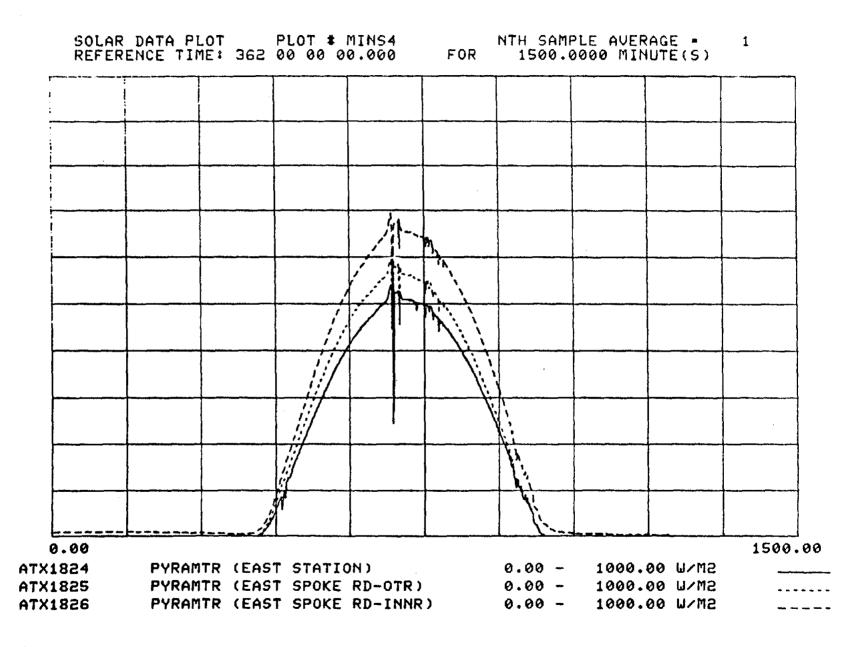




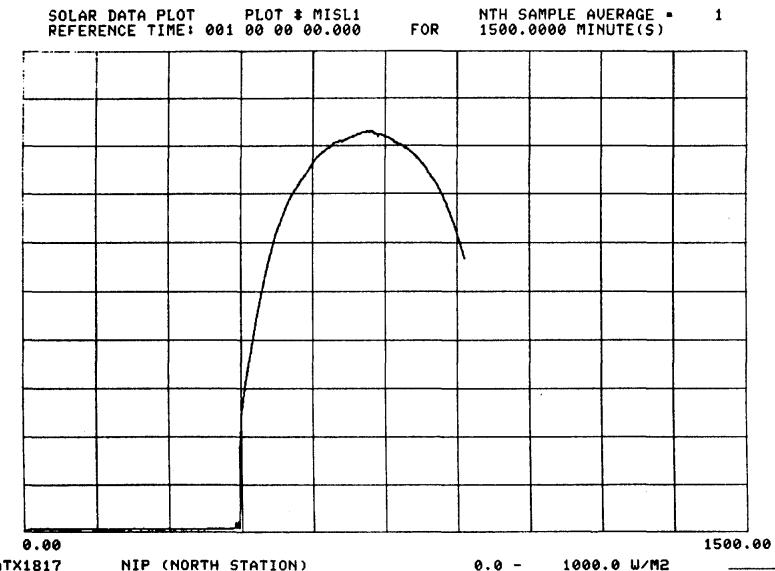




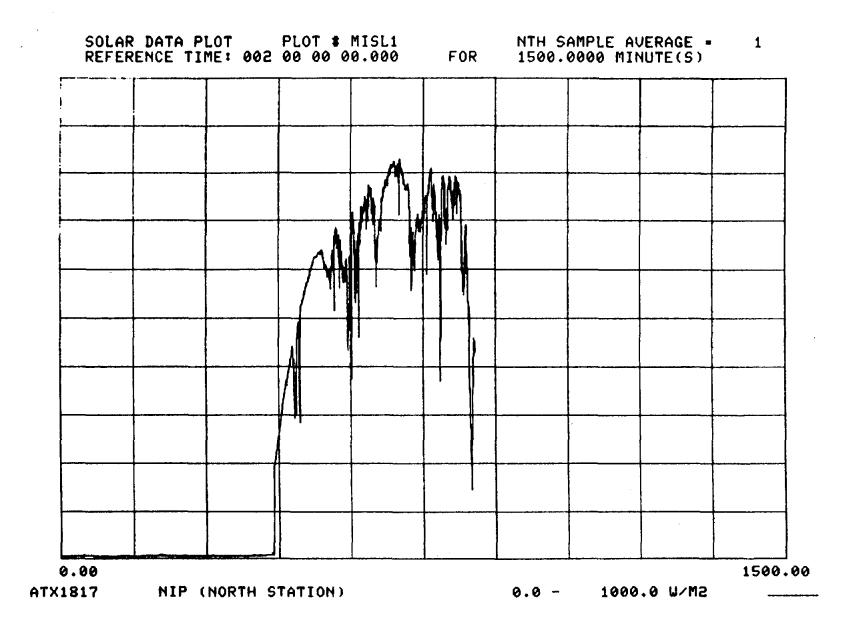


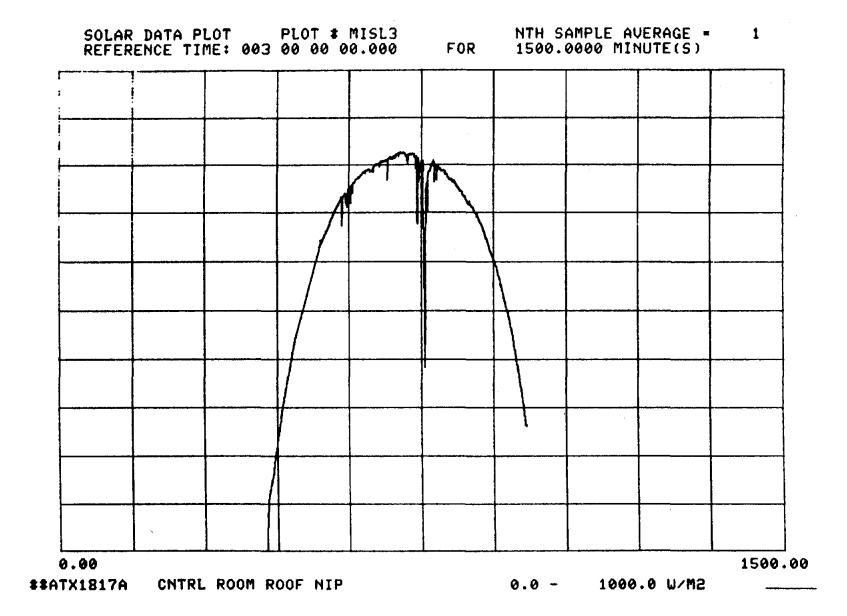


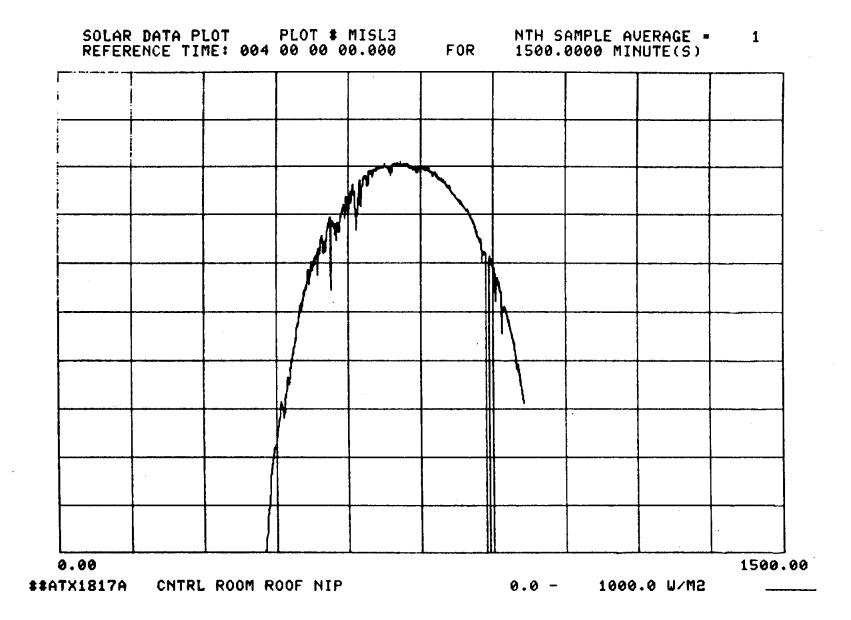
Direct normal insolation plots for one of the two normal incidence pyrheliometers (ATX 1817 at the north station, or ##ATX 1317A on the control room roof) are included on the following pages for each of the 289 days that were recorded with some NIP activity. The data include 104 clear days, 53 days with light cloud activity, and 132 days with heavy cloud activity. The data show that peaks of 900 watts/ $m^2$  occurred each month, but not very frequently. Moreover, this average peak values for each month are considerably lower than 900 watts/ $m^2$ . The reference time (start time) for each plot is shown on the top of each page, starting with the day of the year, followed by the time in hours, minutes, seconds, and milliseconds. For example, on the following page, the day is 001 (1 January), the start time is midnight, and the stop time is 1500 minutes (25 hours) later. The scale for the ordinate is 0.0 to 1000 watts/ $m^2$ .

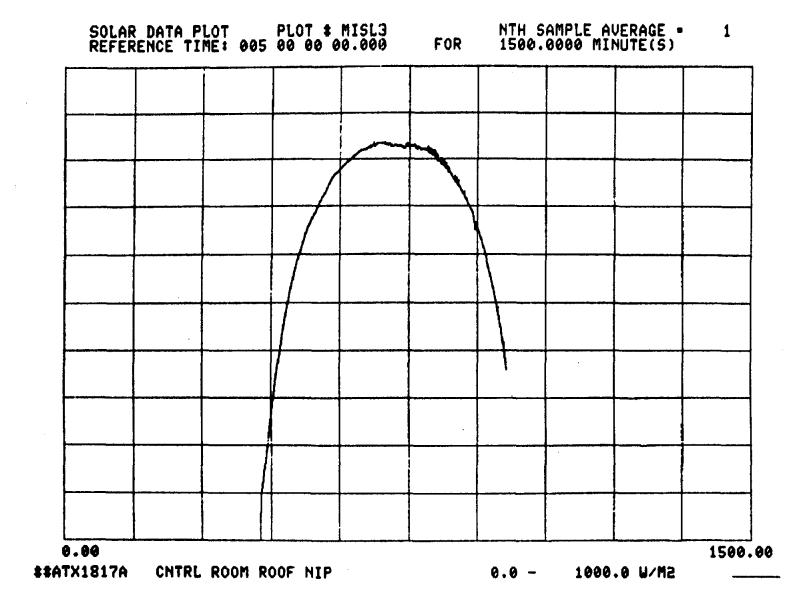


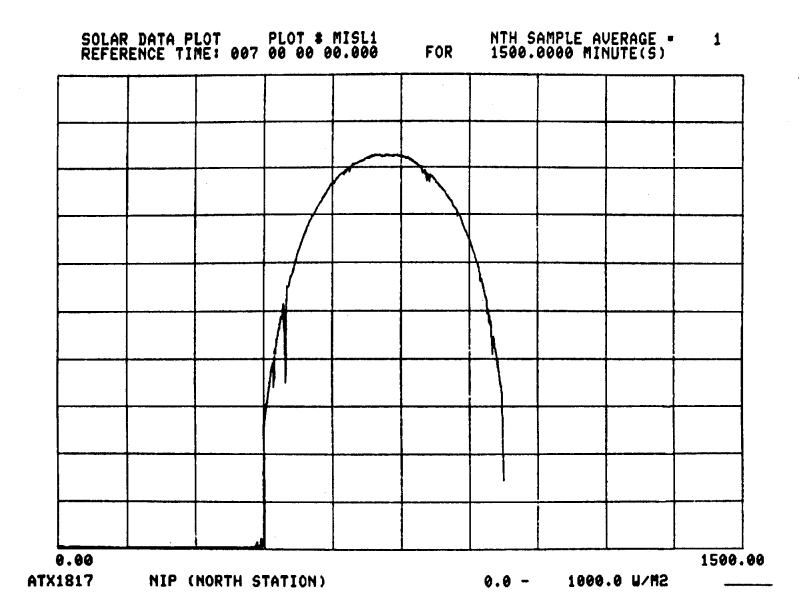
ATX1817

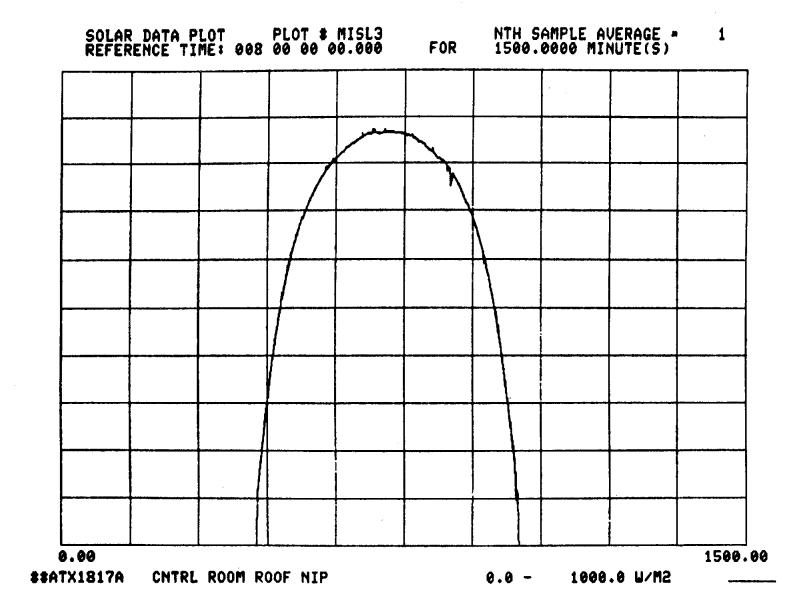


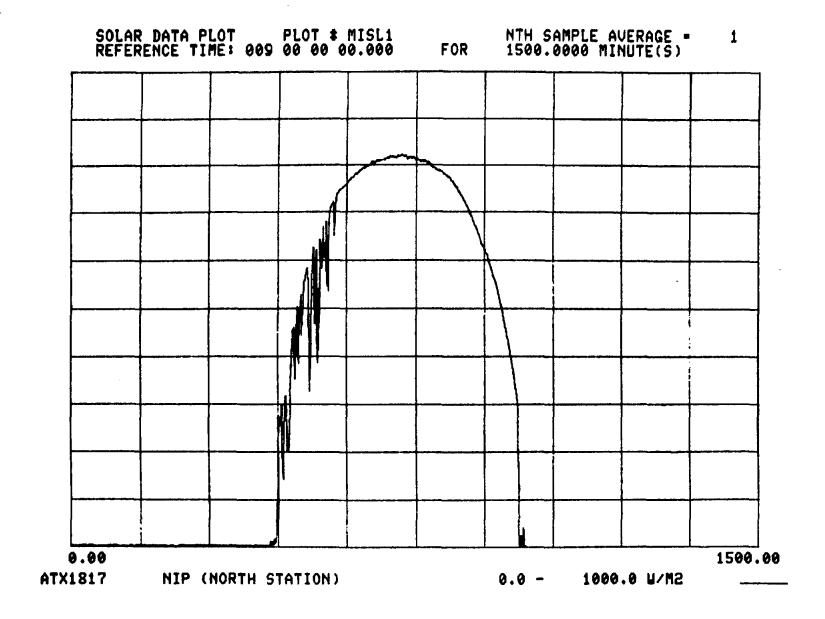


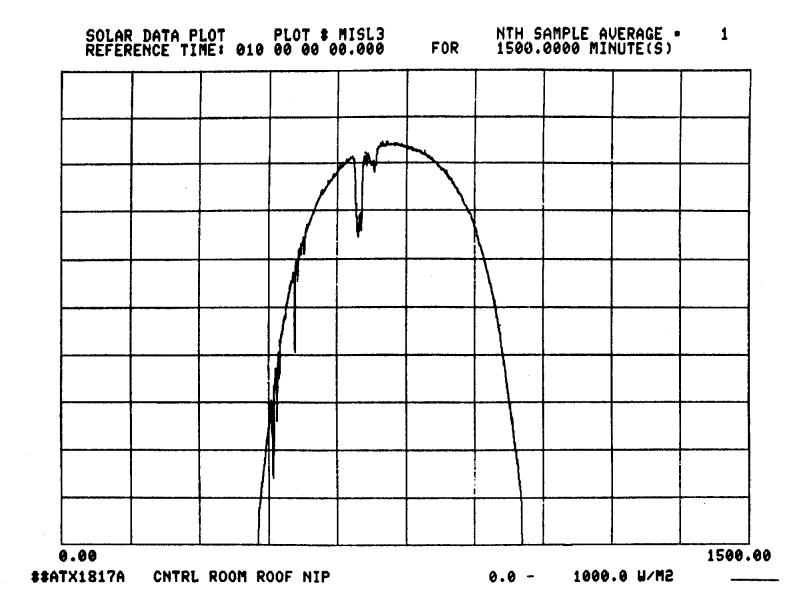


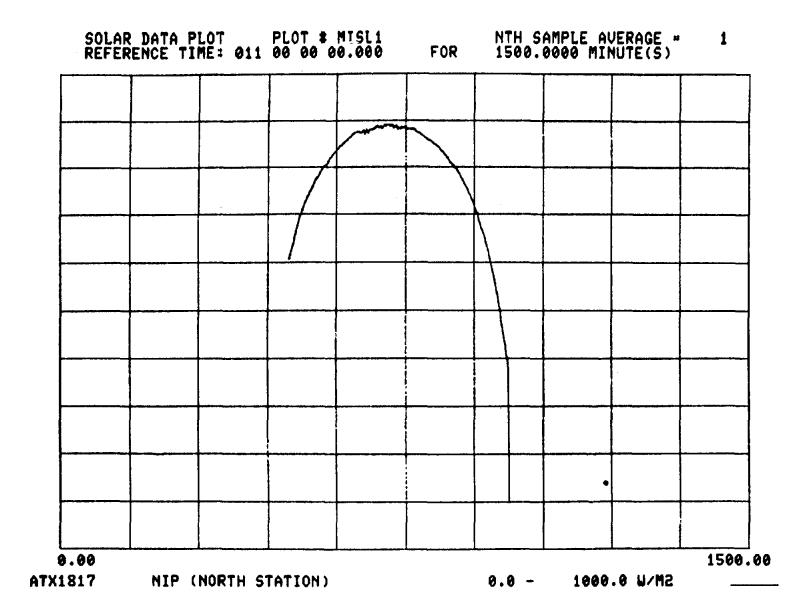


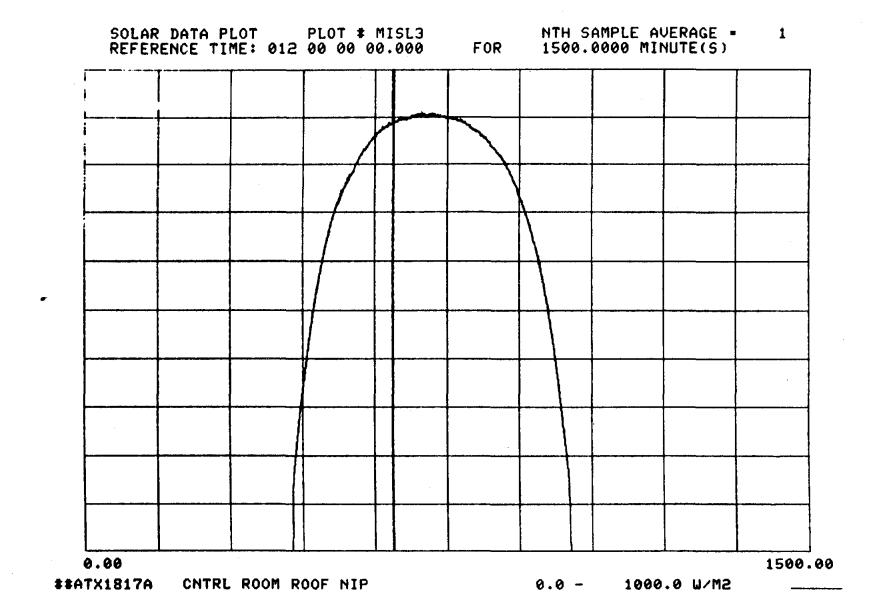


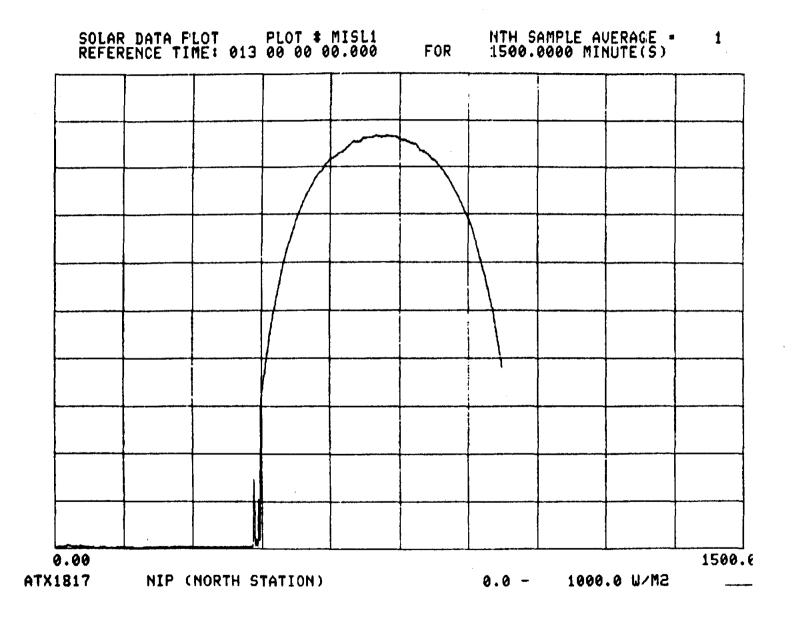


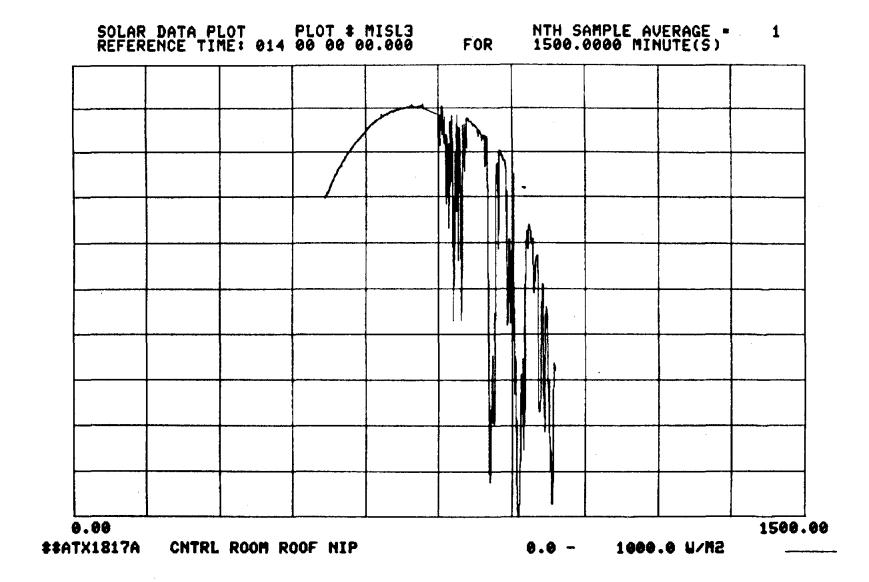


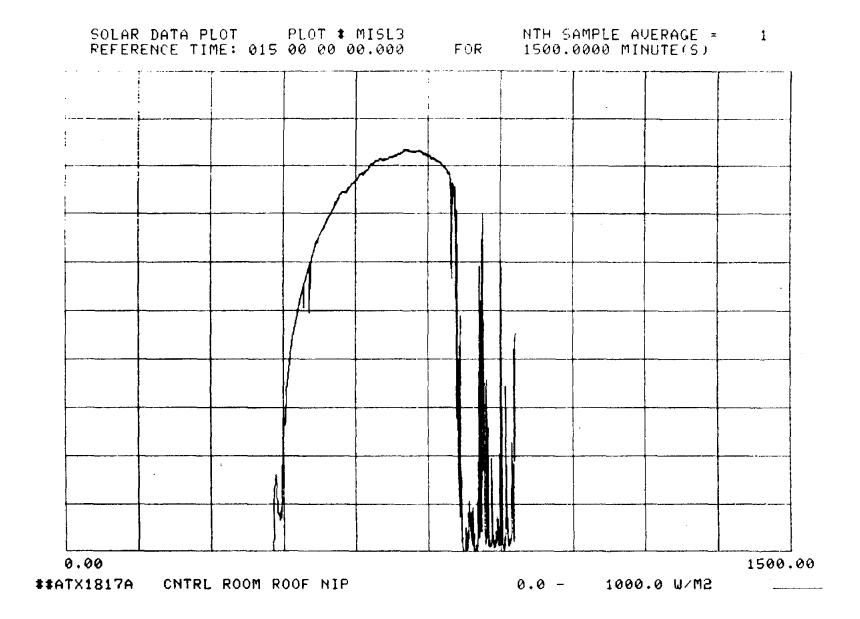


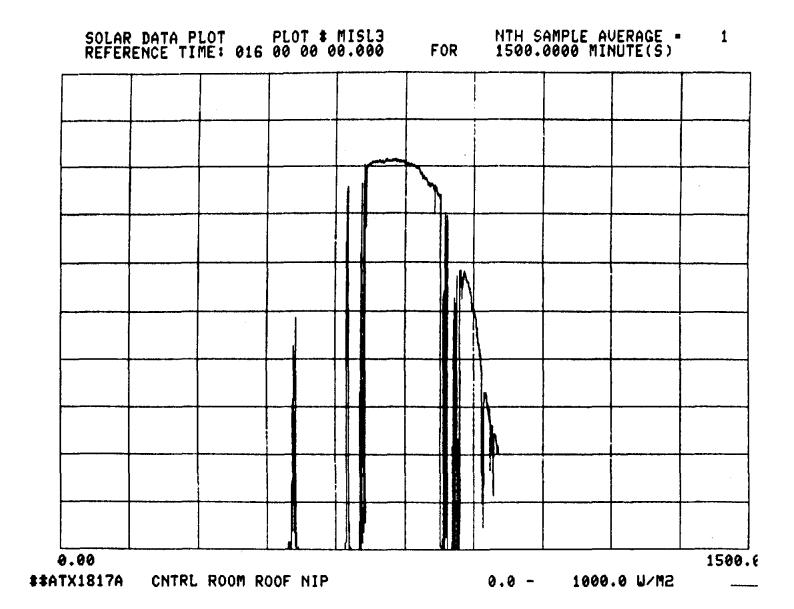


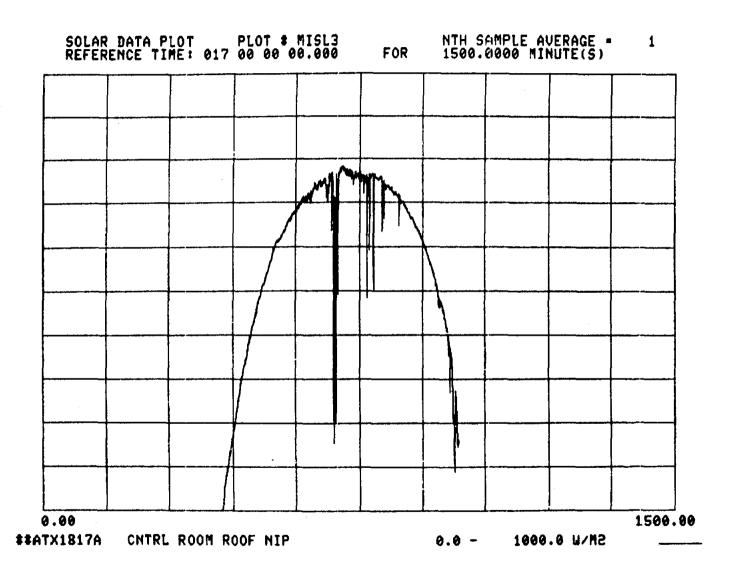


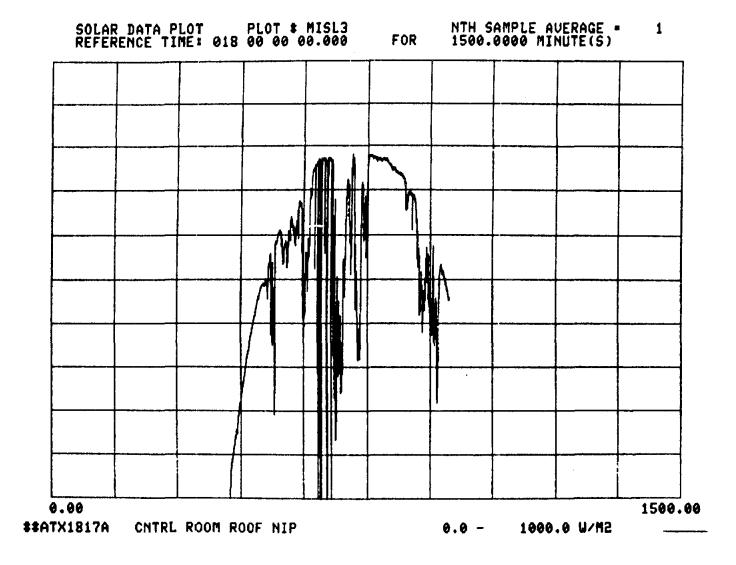


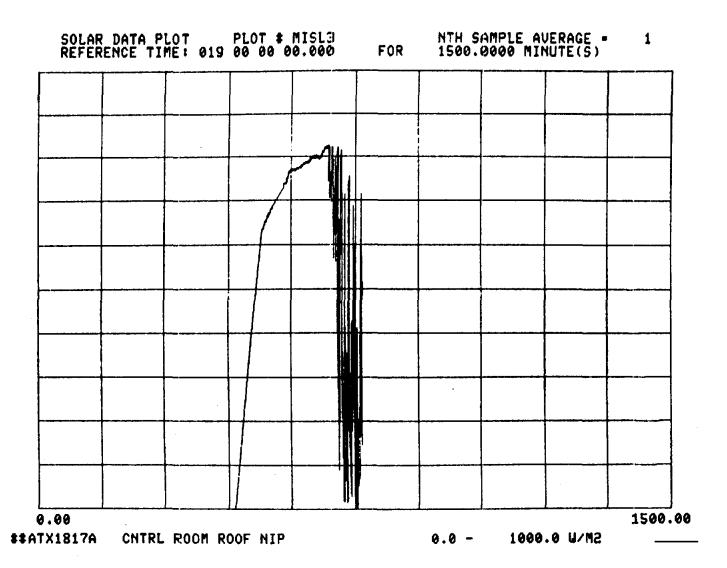


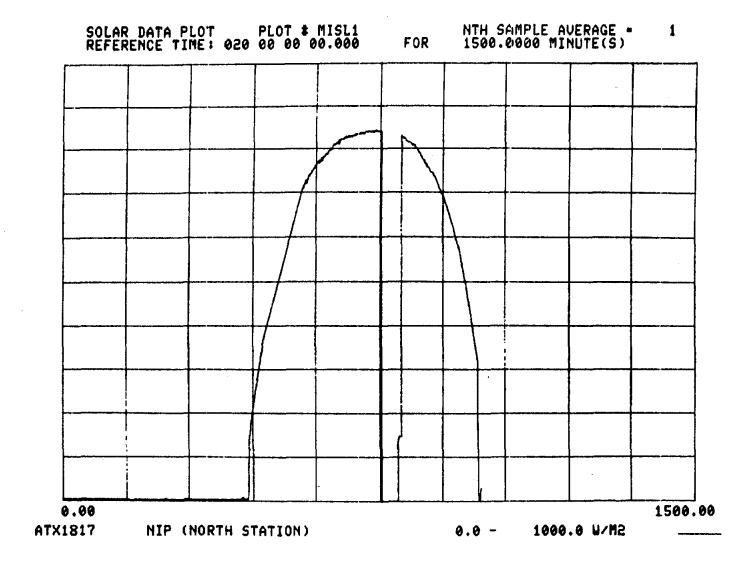


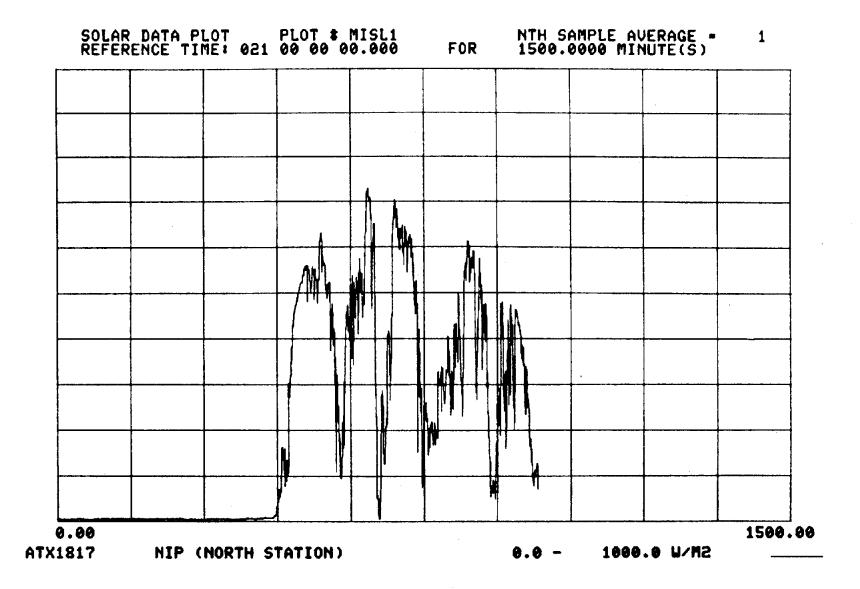


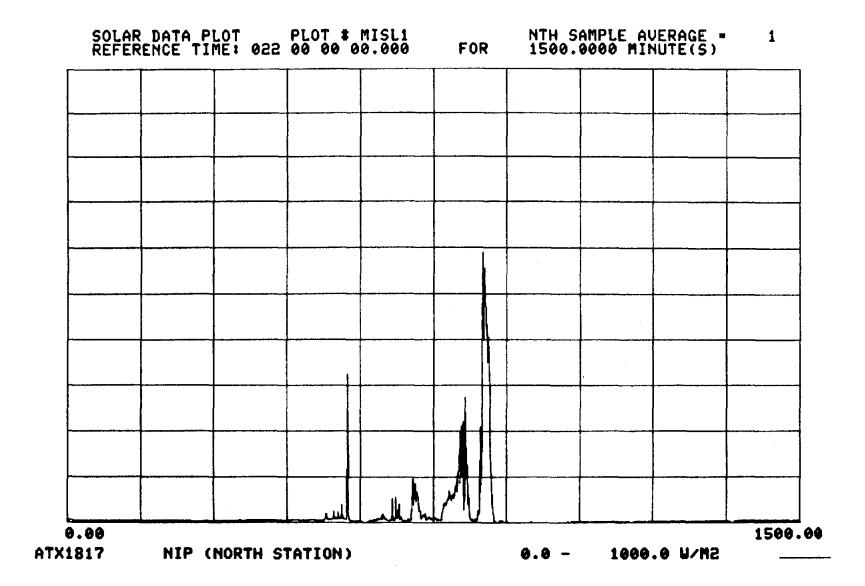


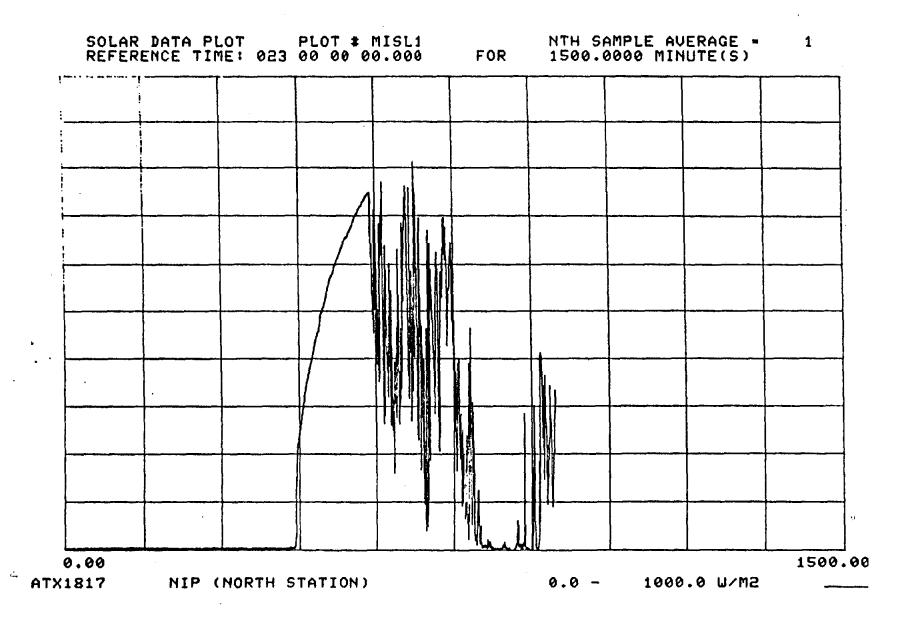


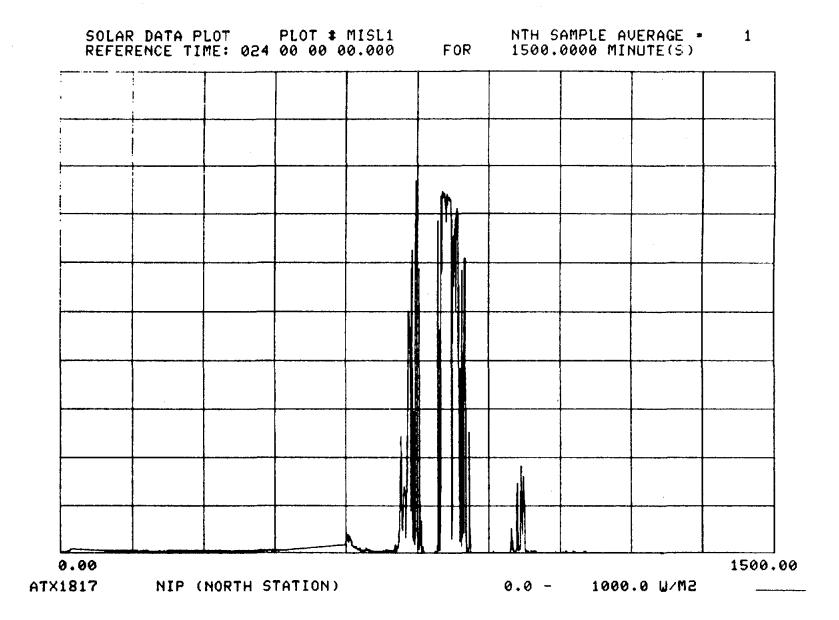


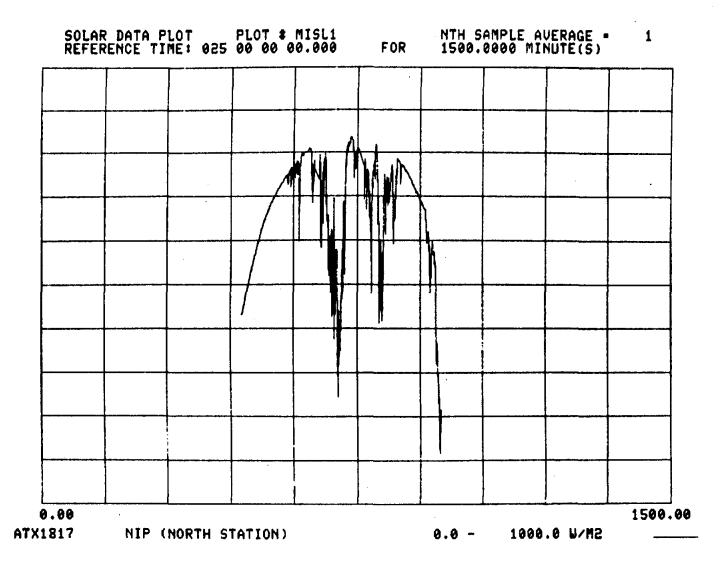


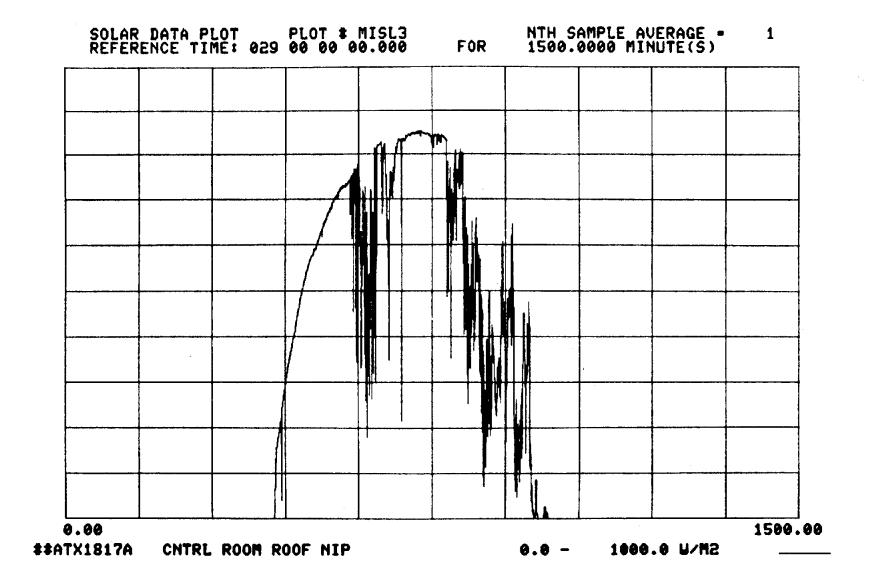


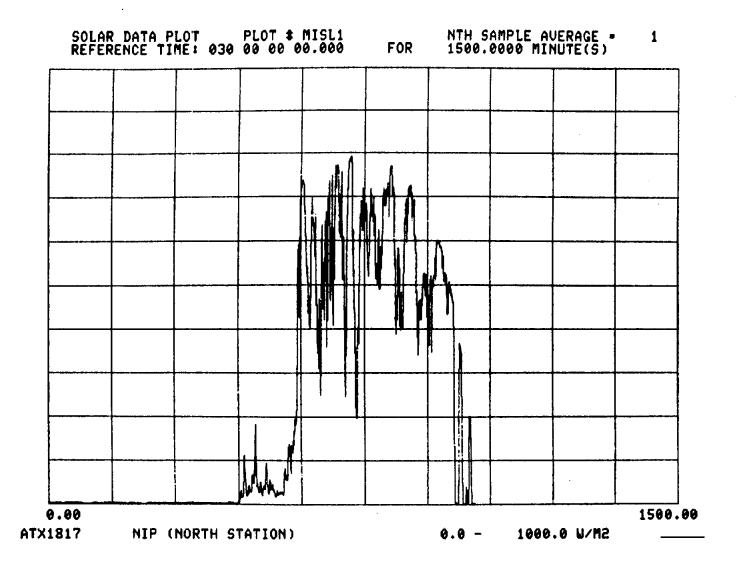


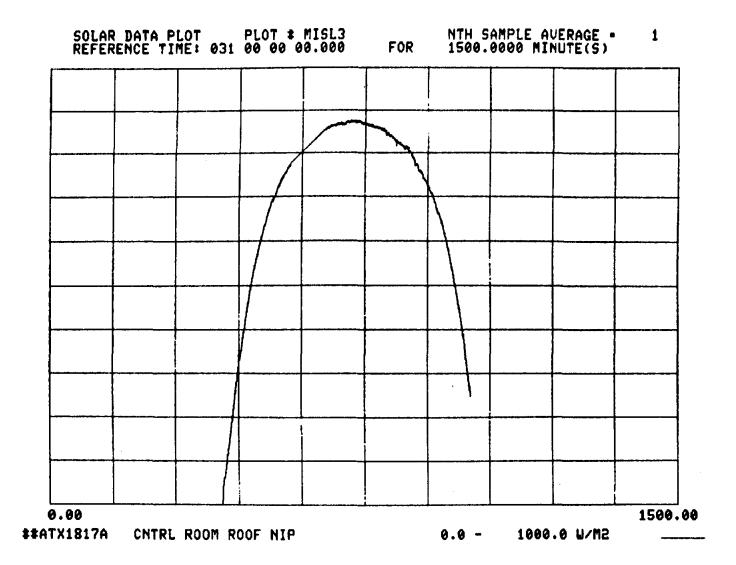


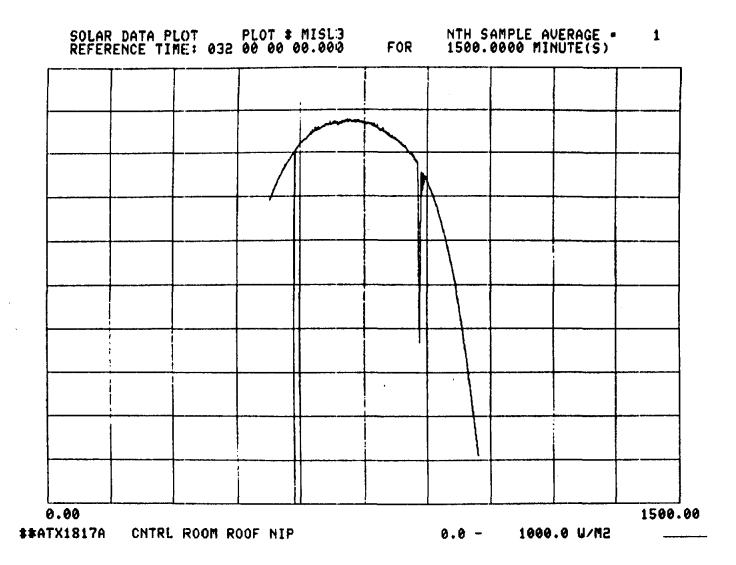


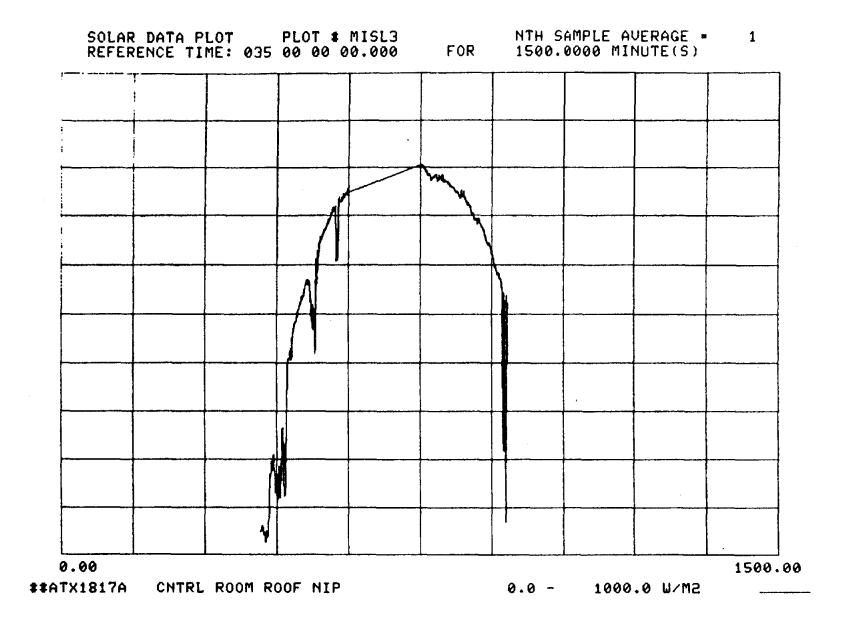


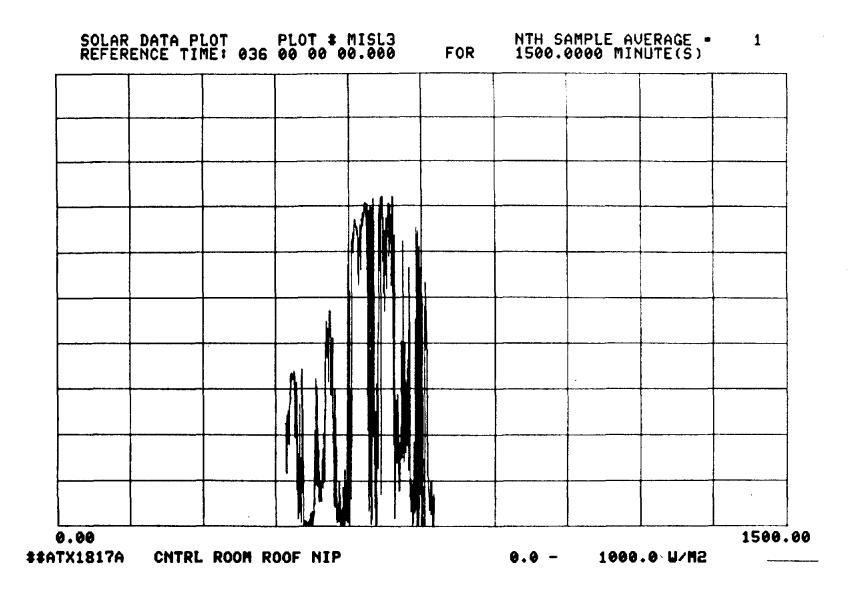


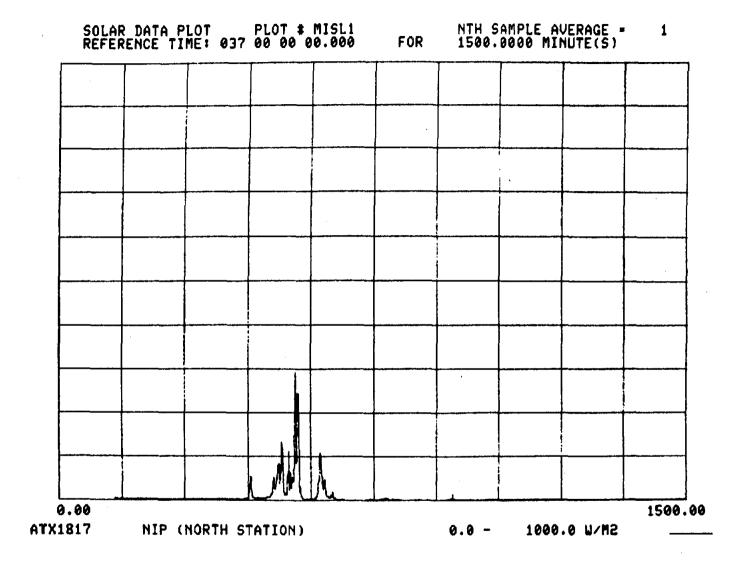


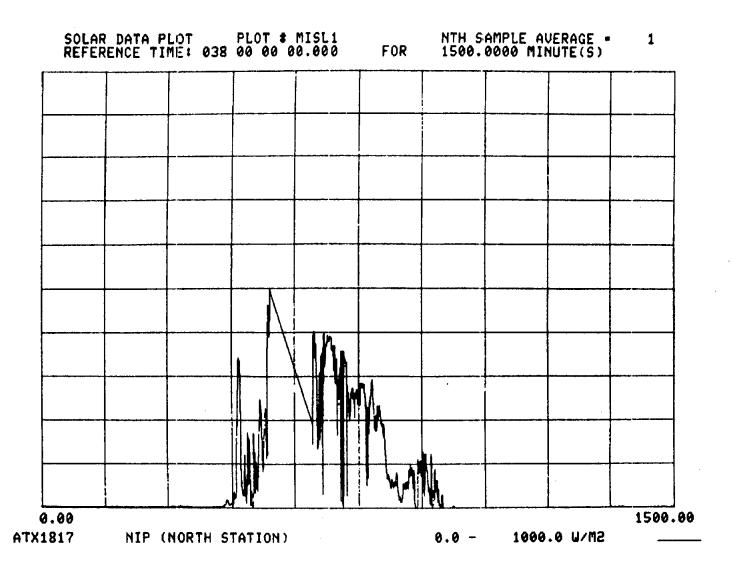


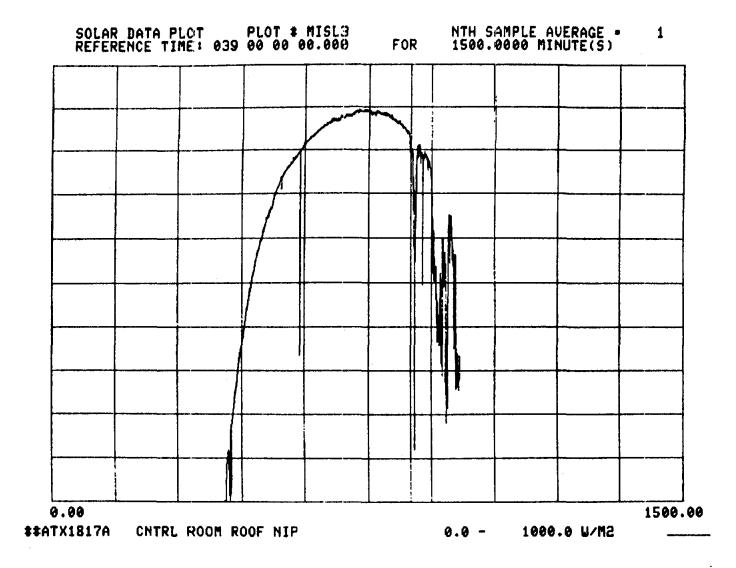


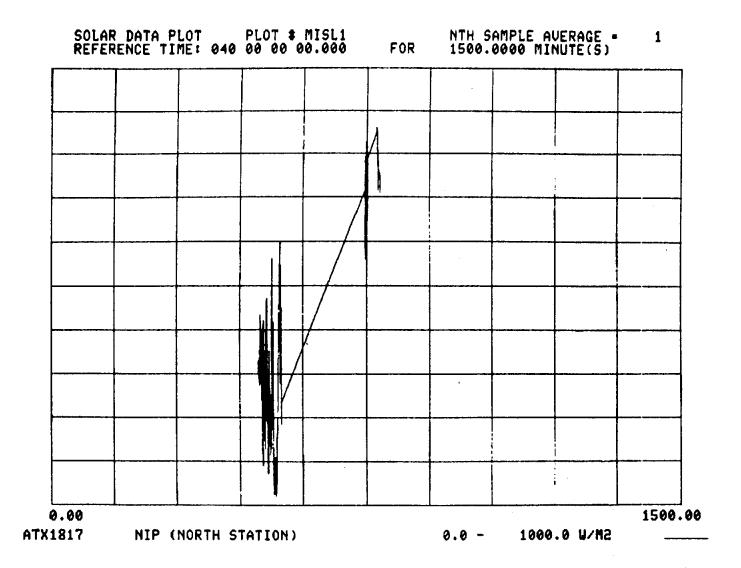


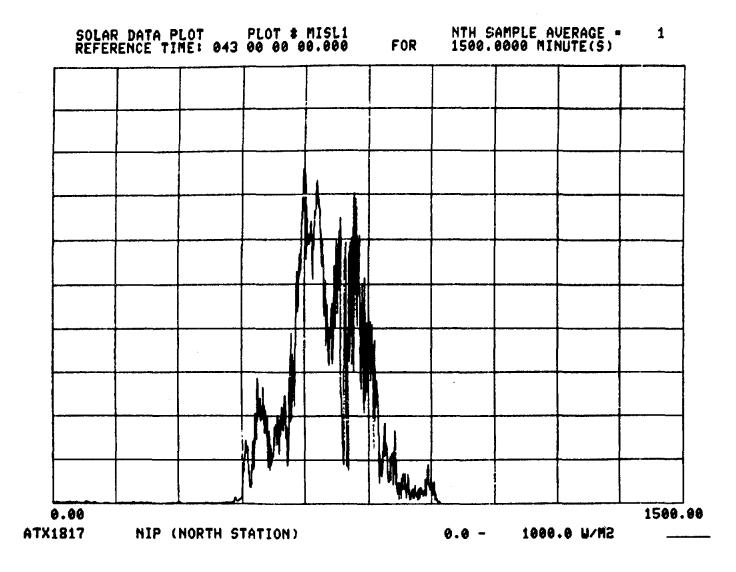


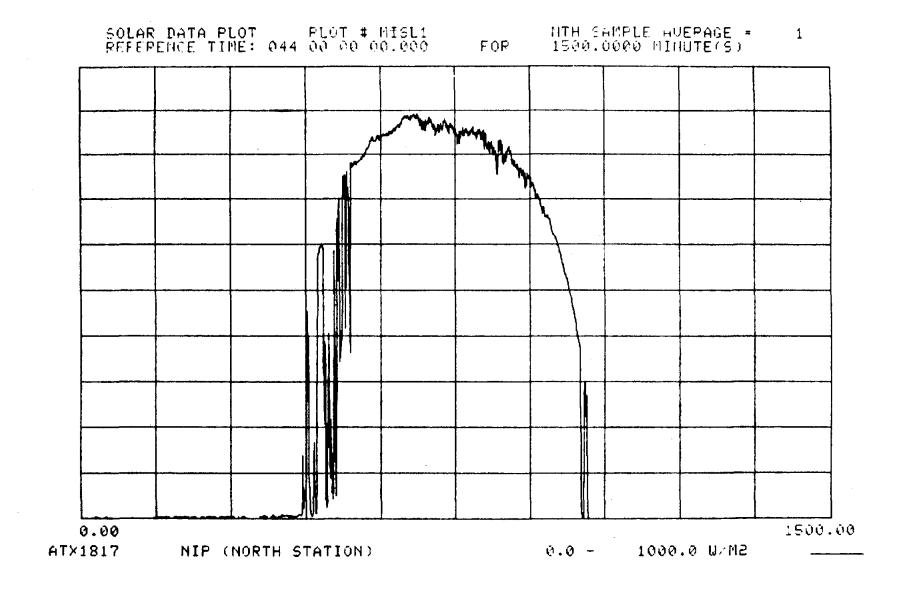


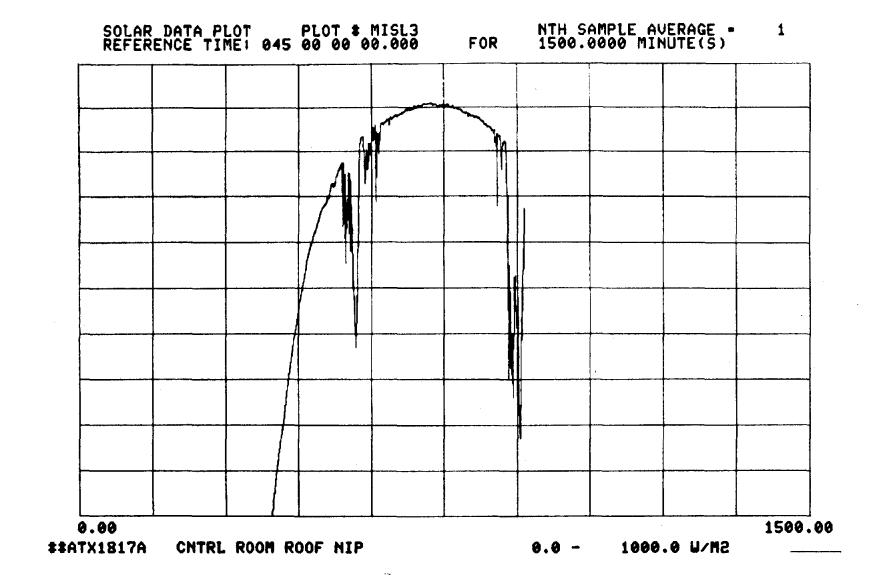


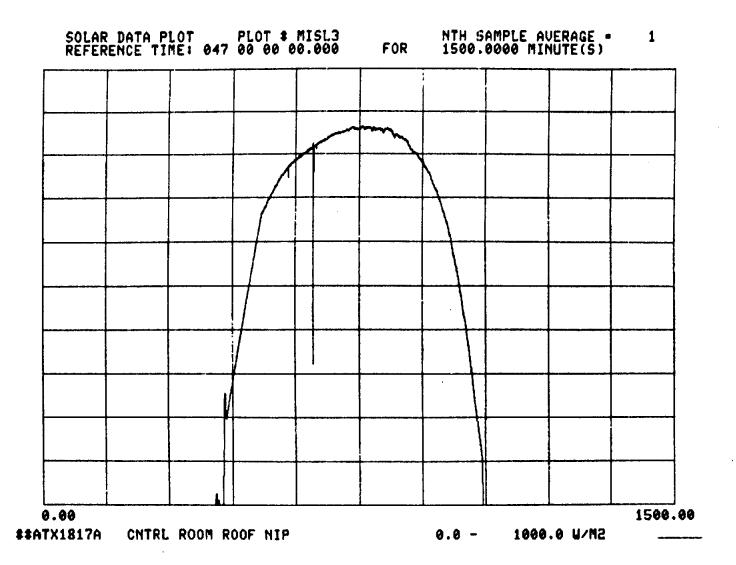


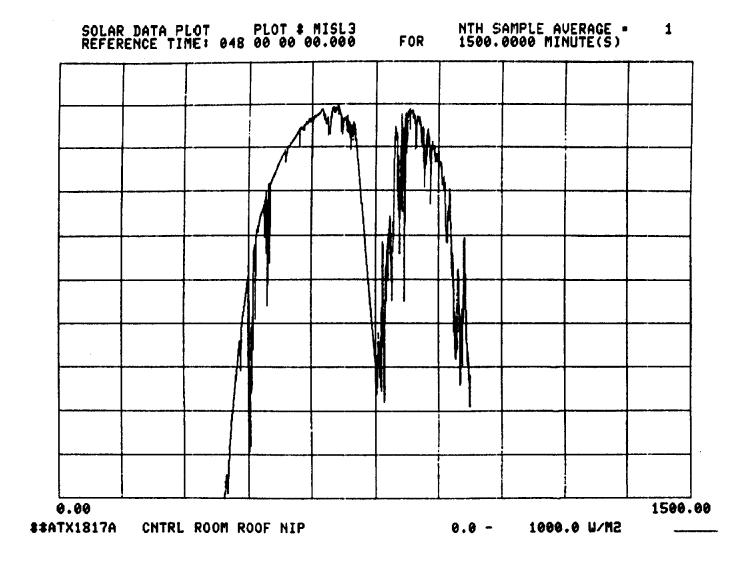


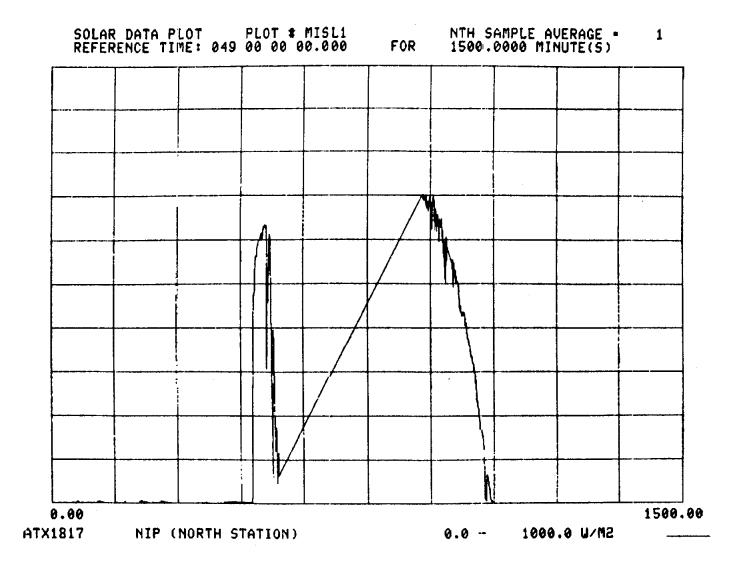


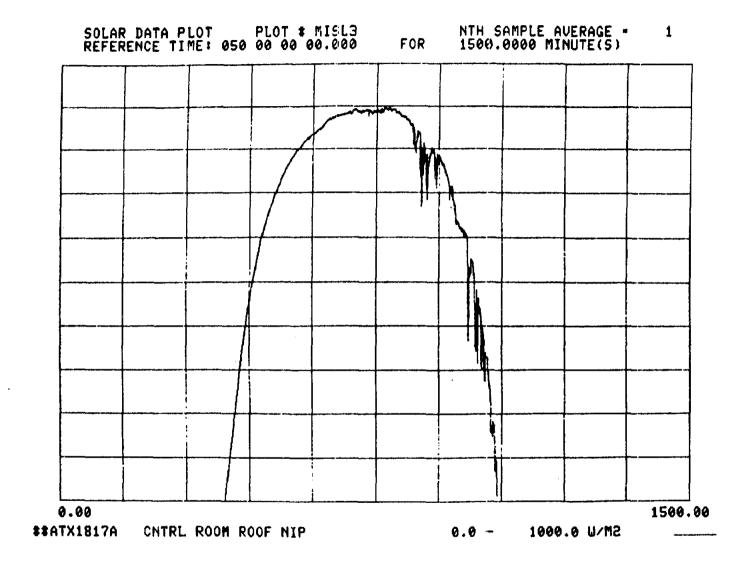


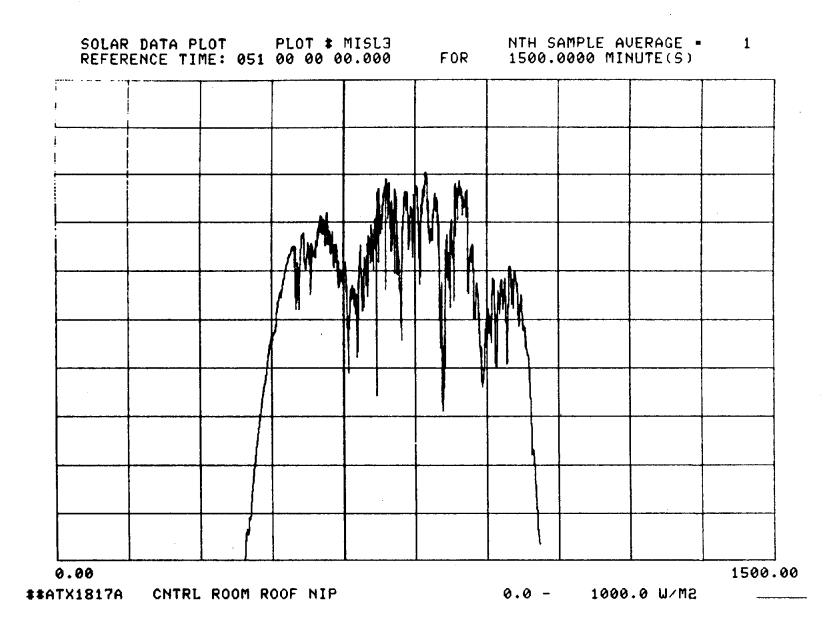


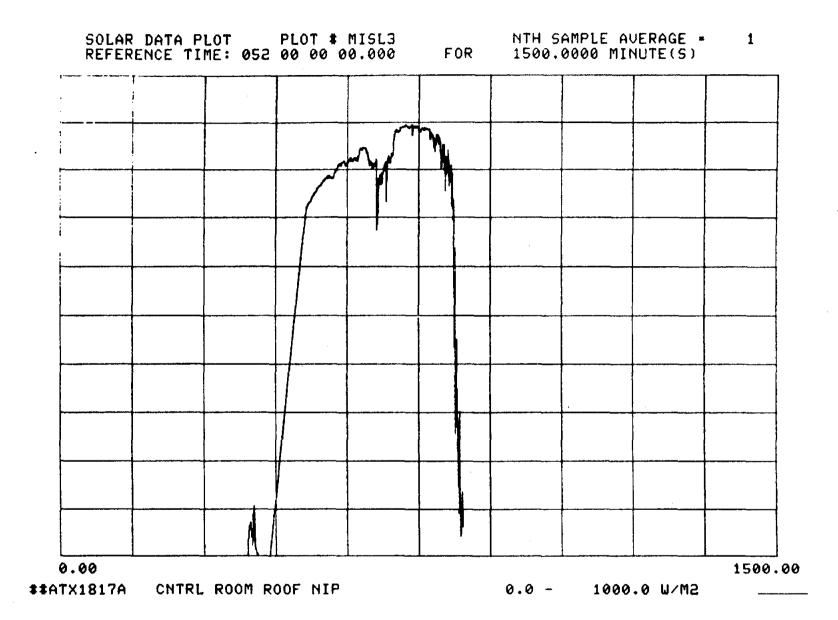


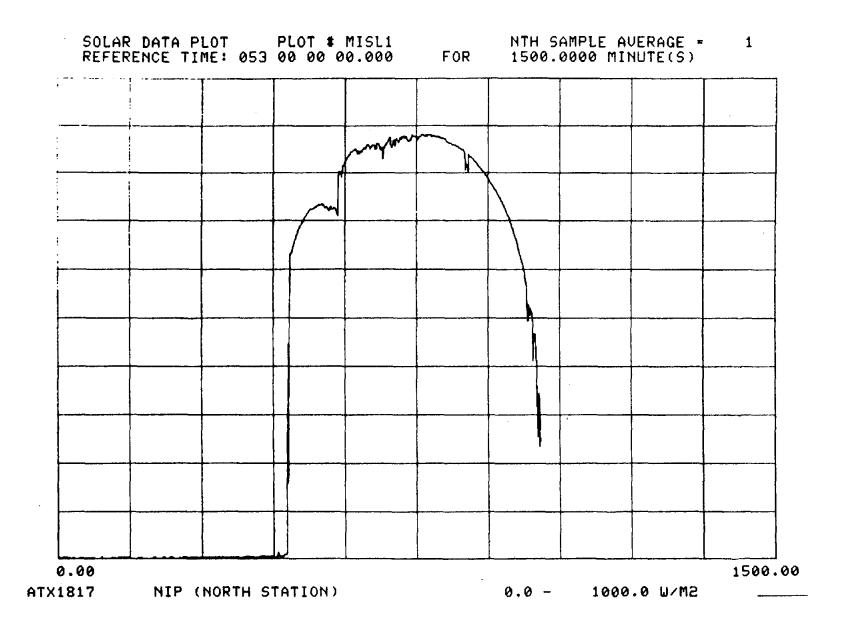


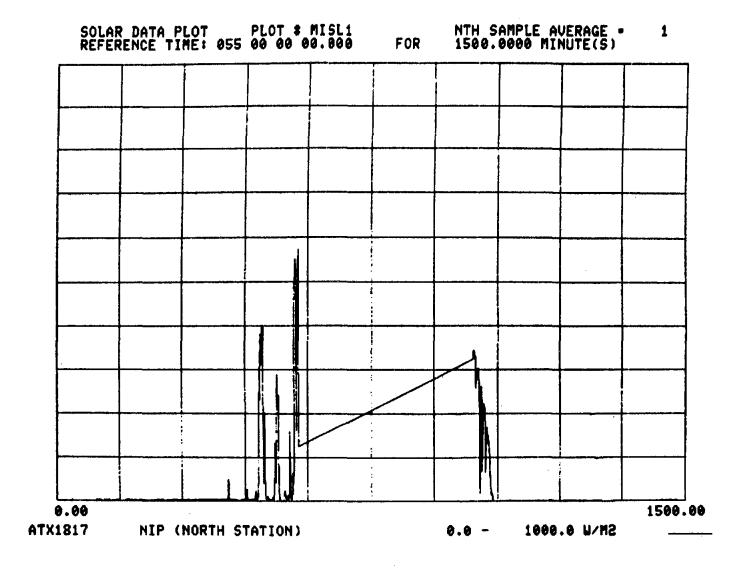


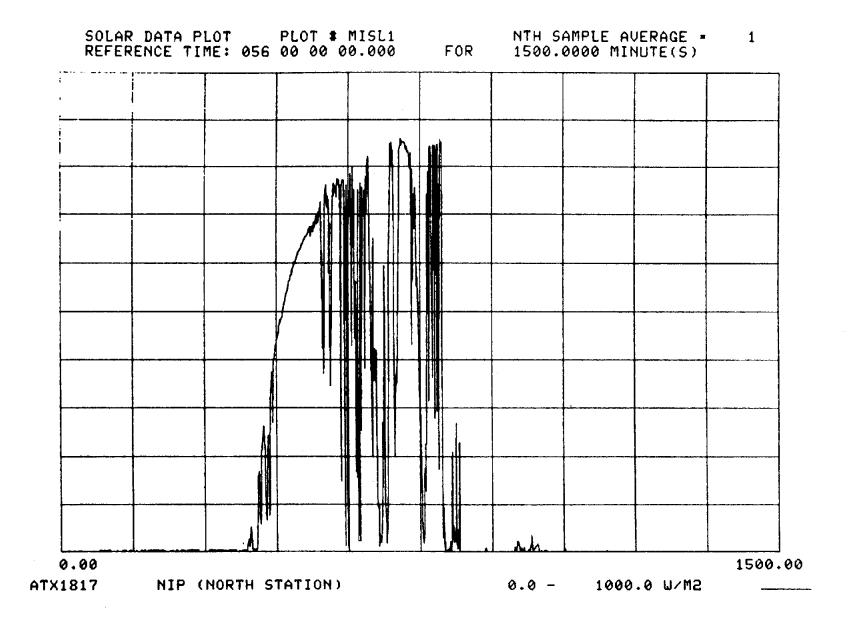


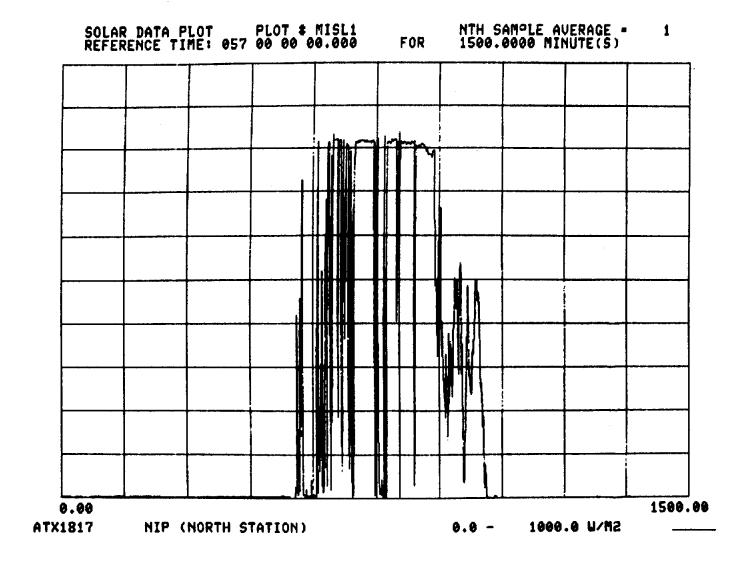


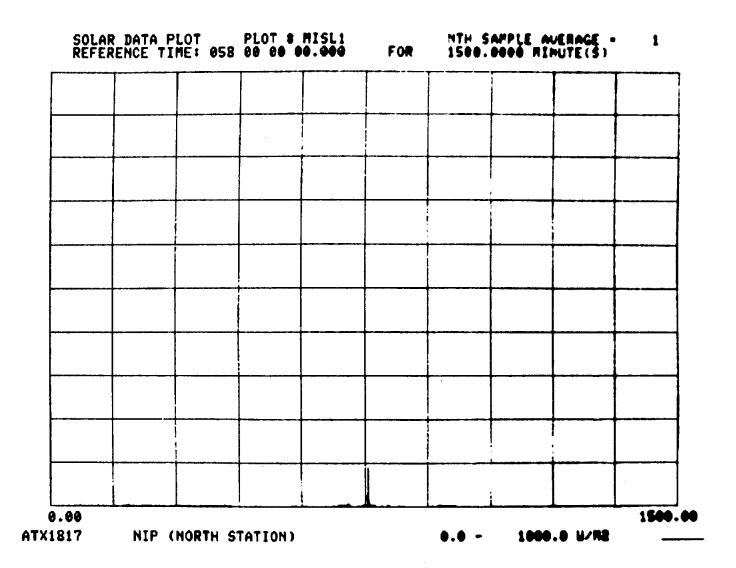


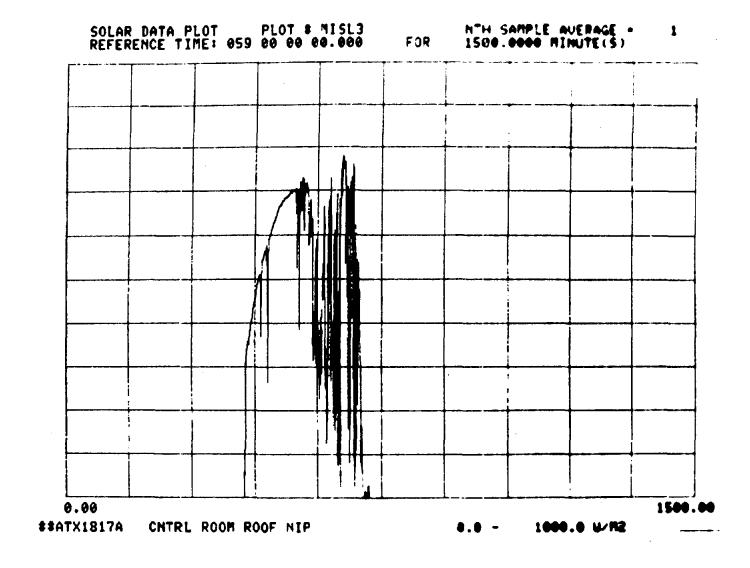


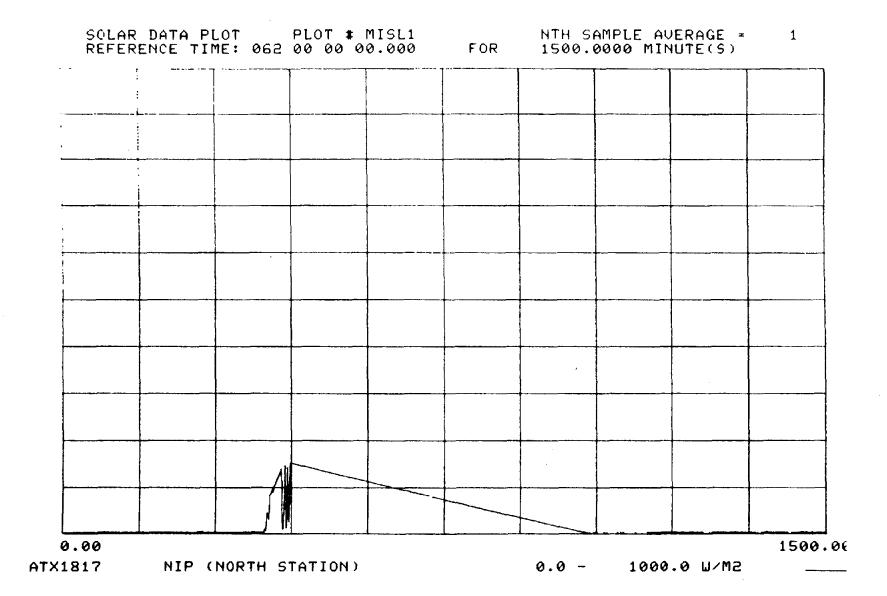


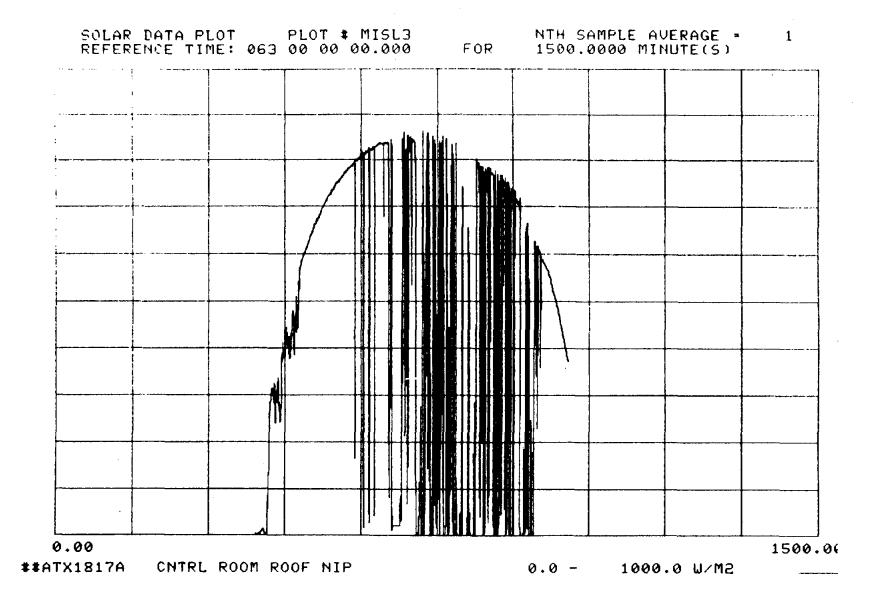


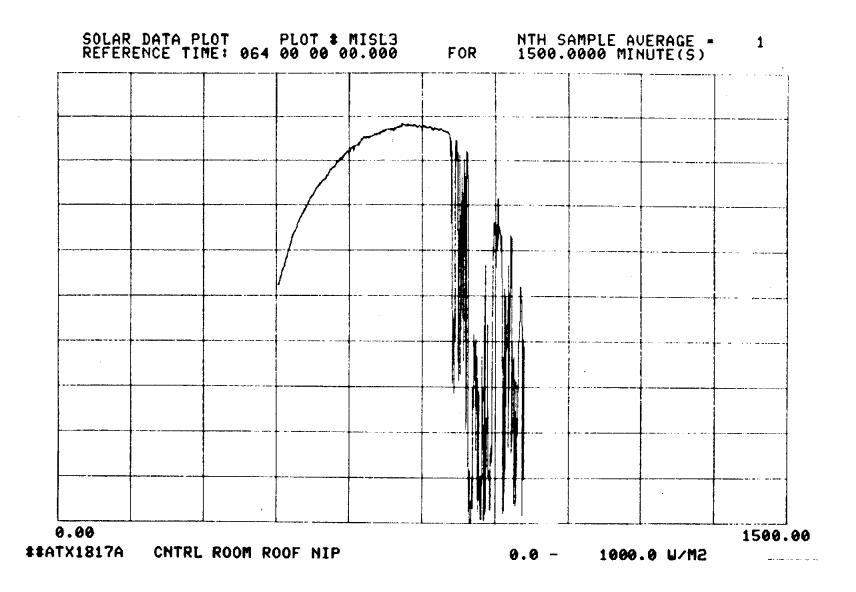


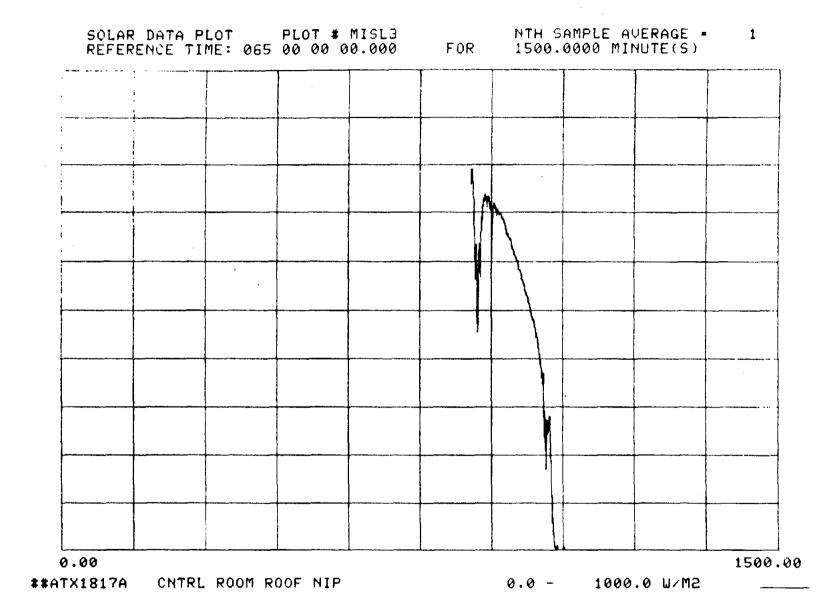


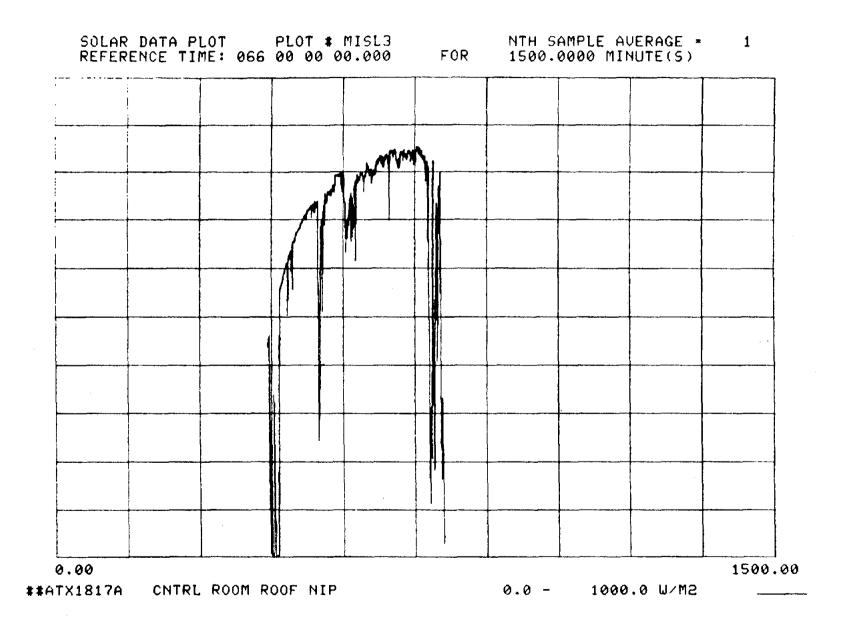


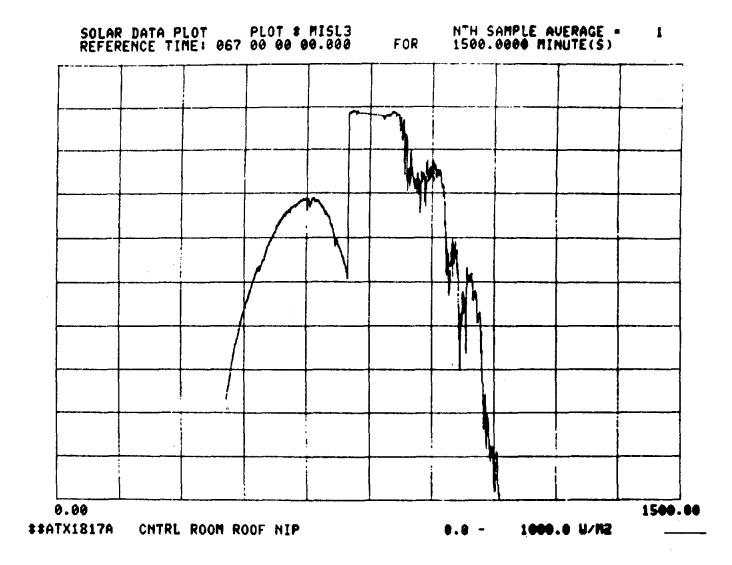


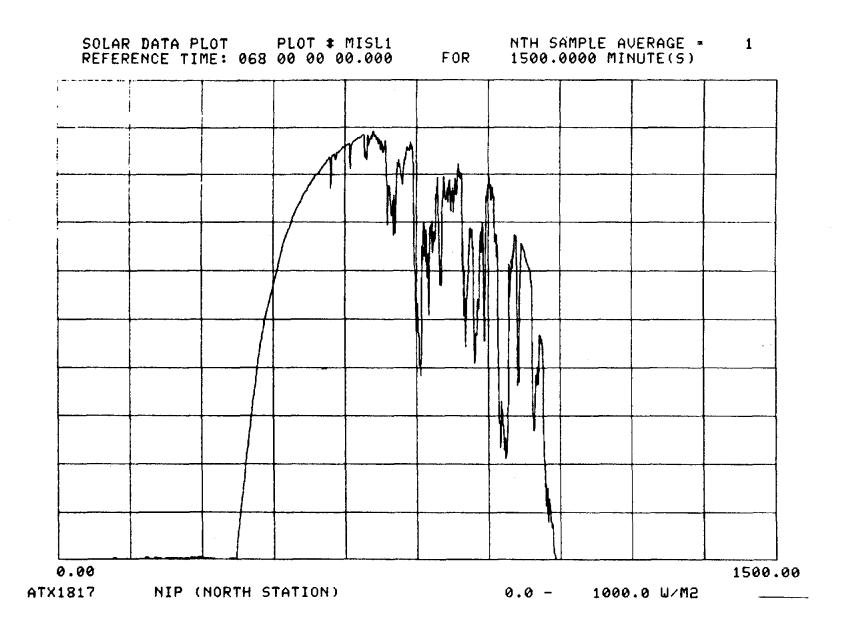


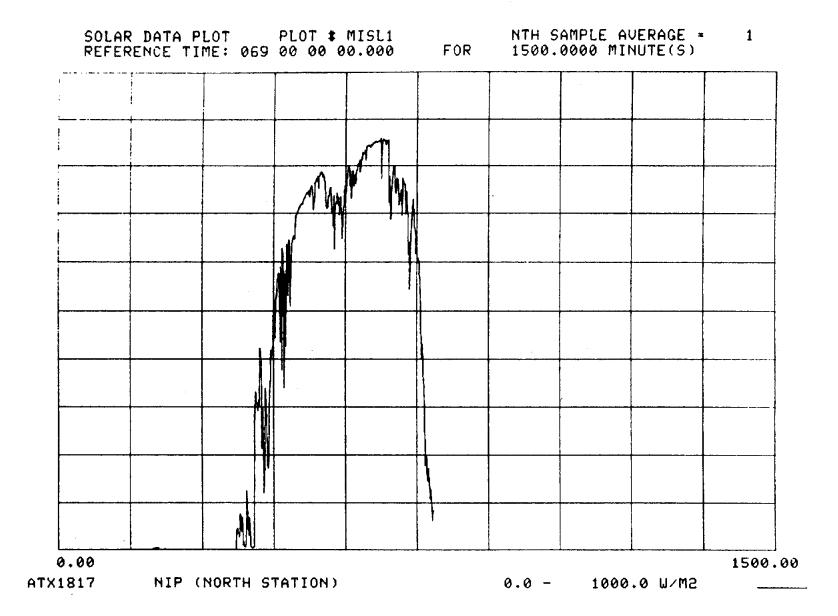


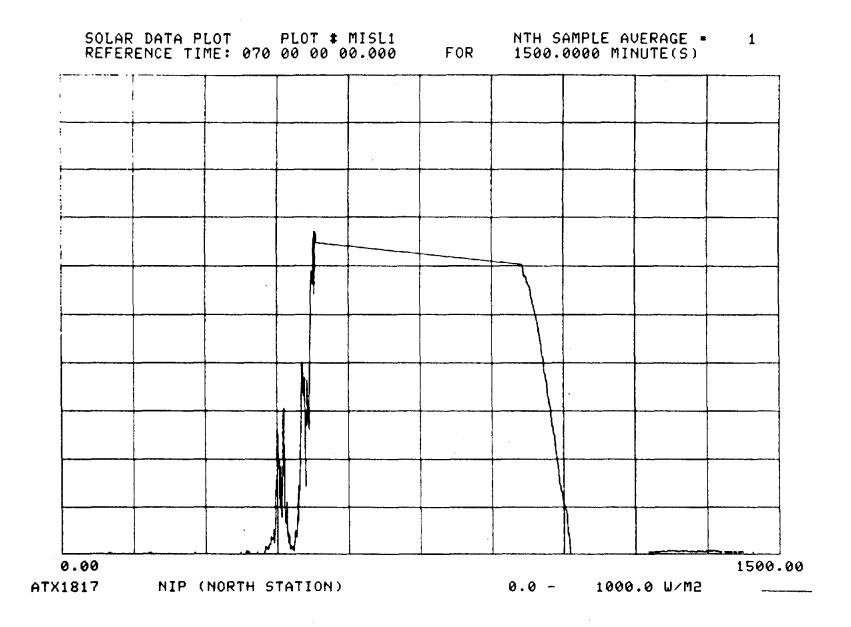


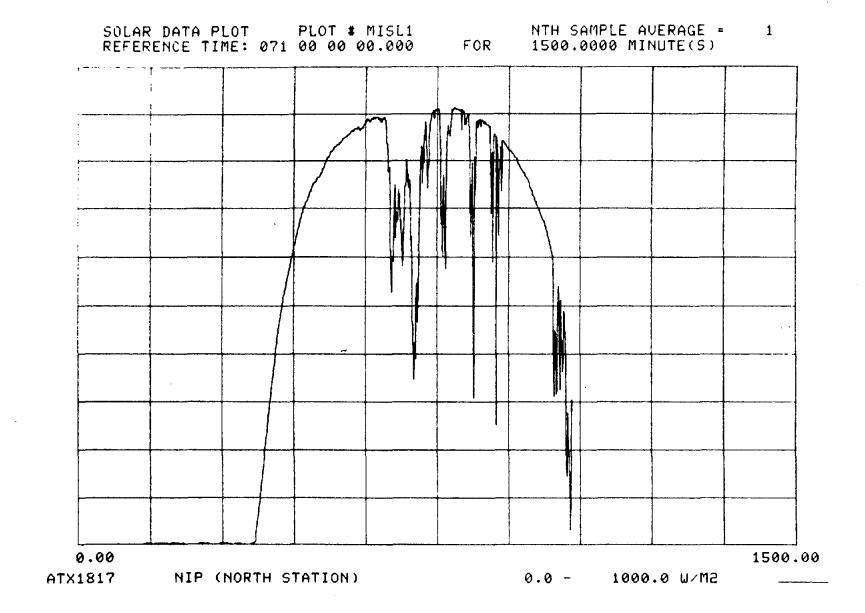


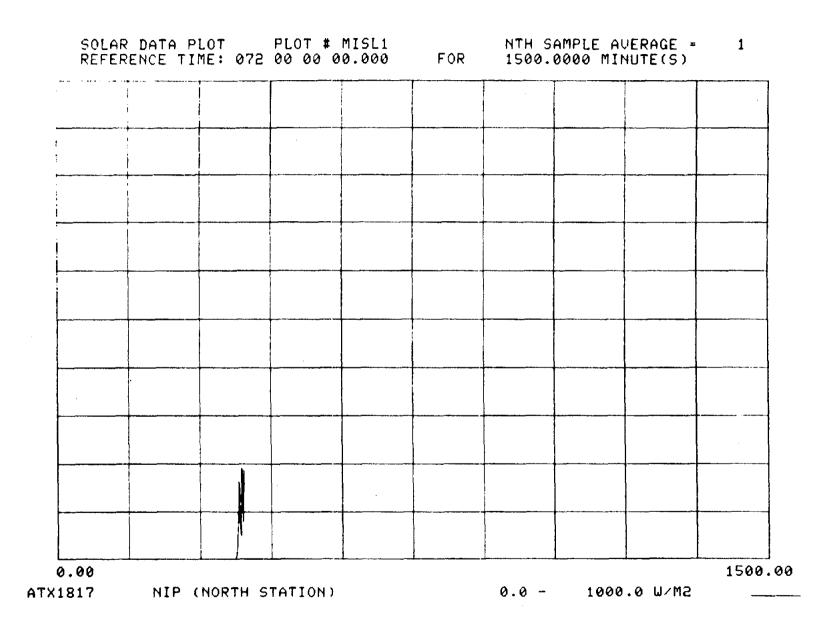


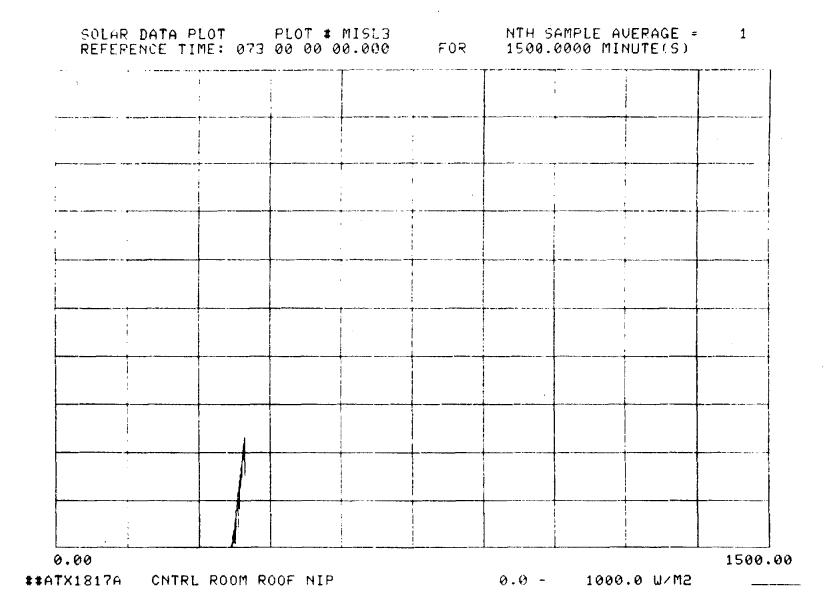


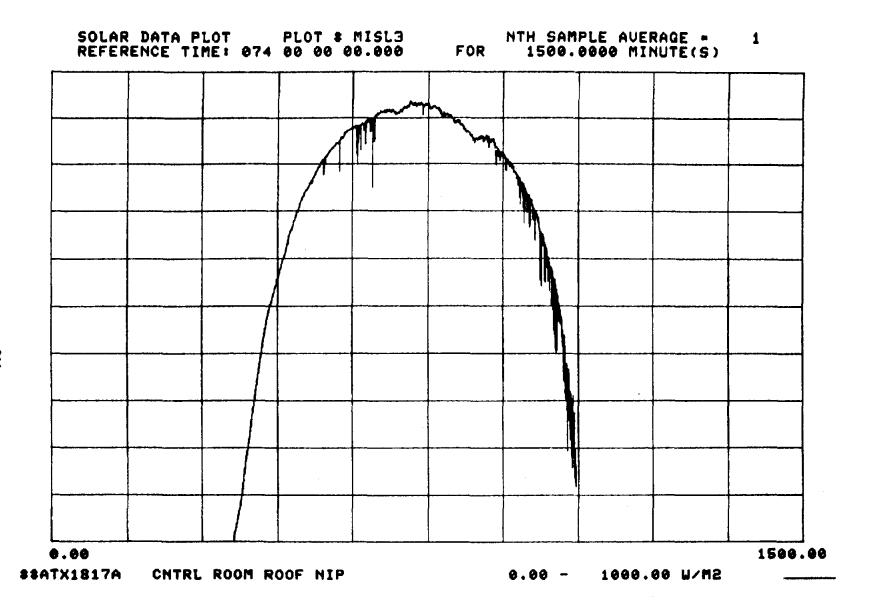


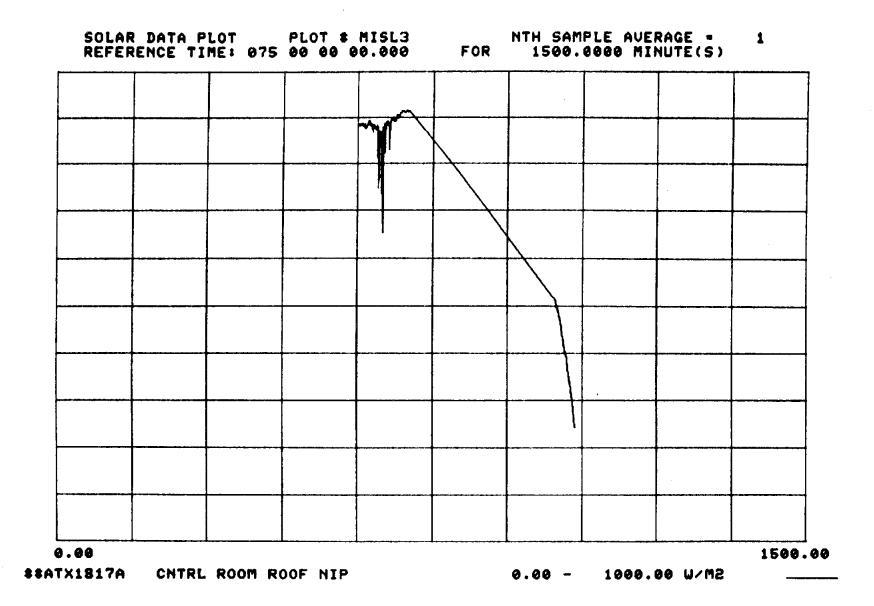


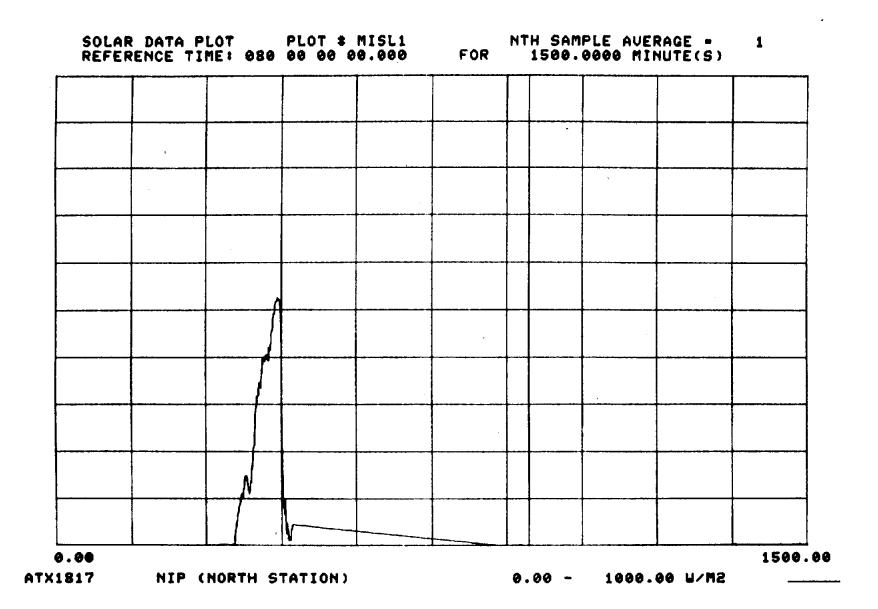


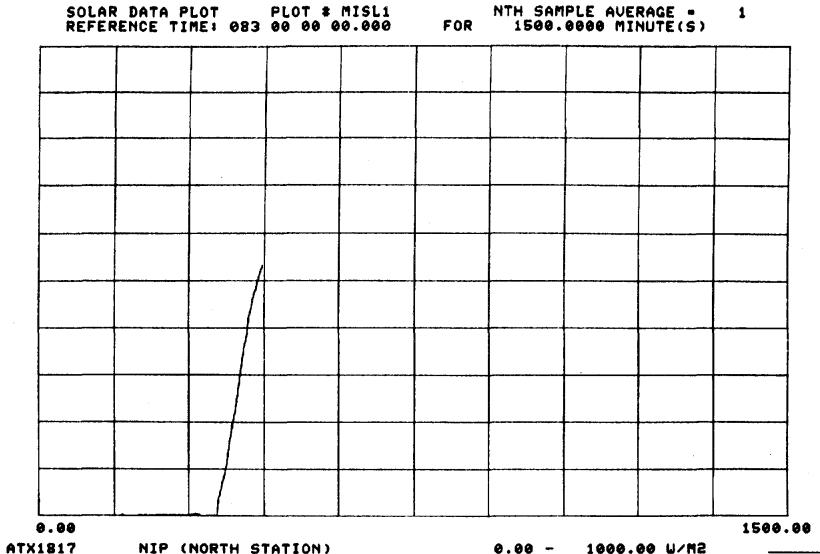


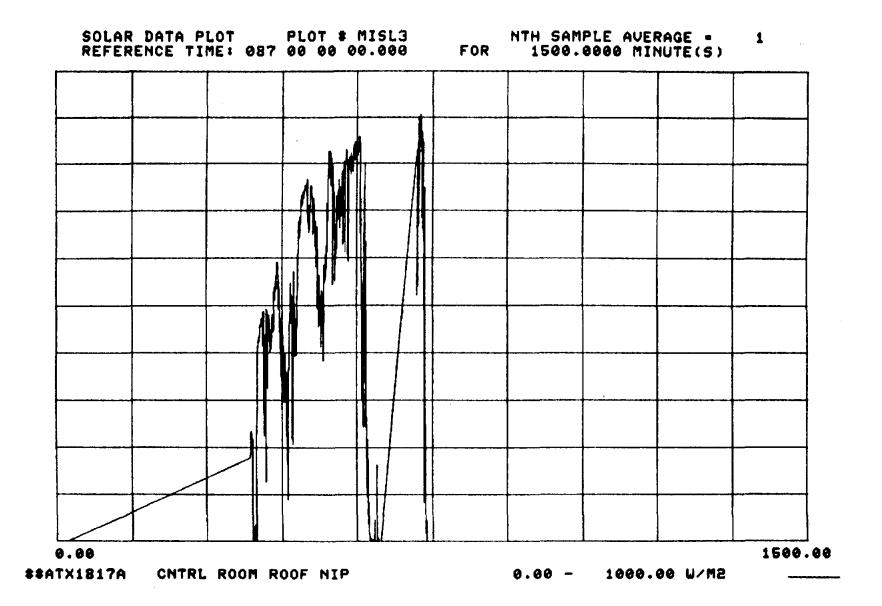


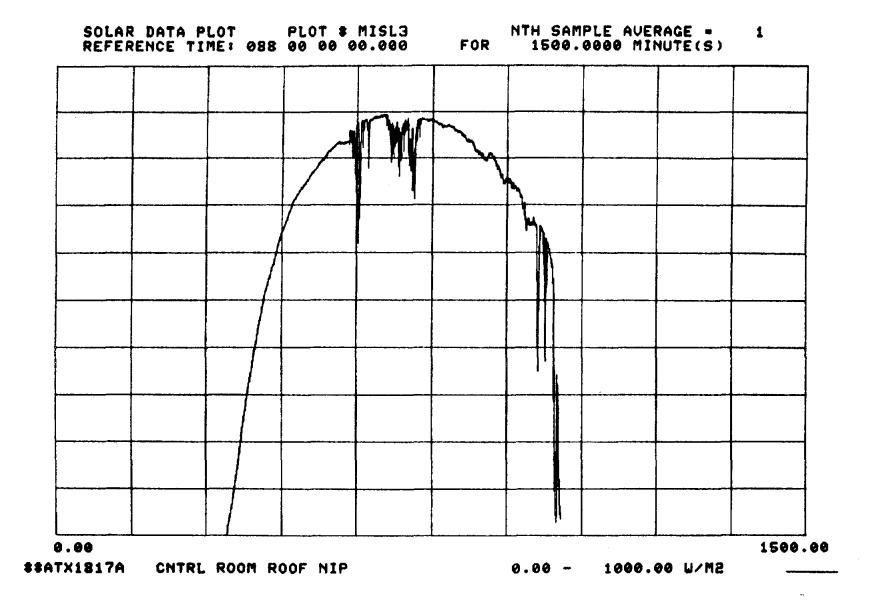


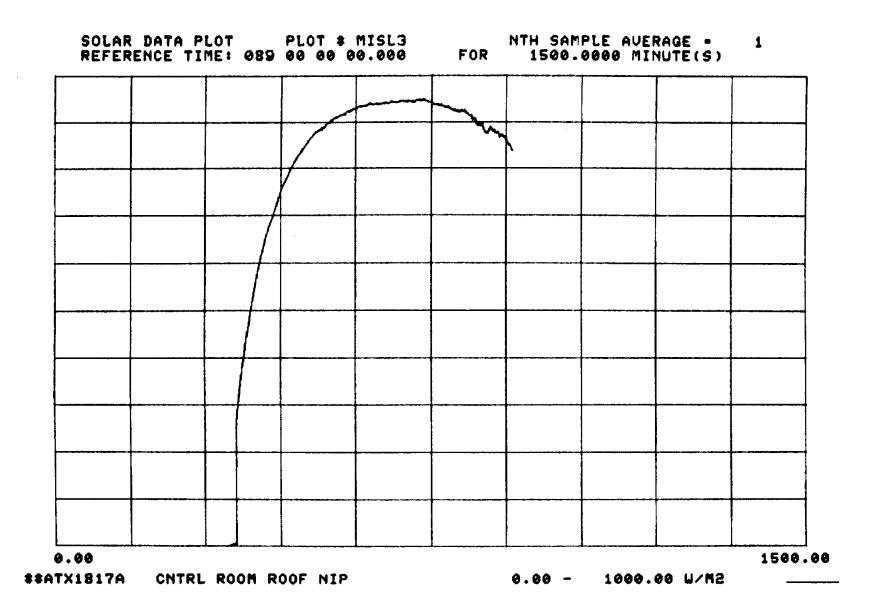


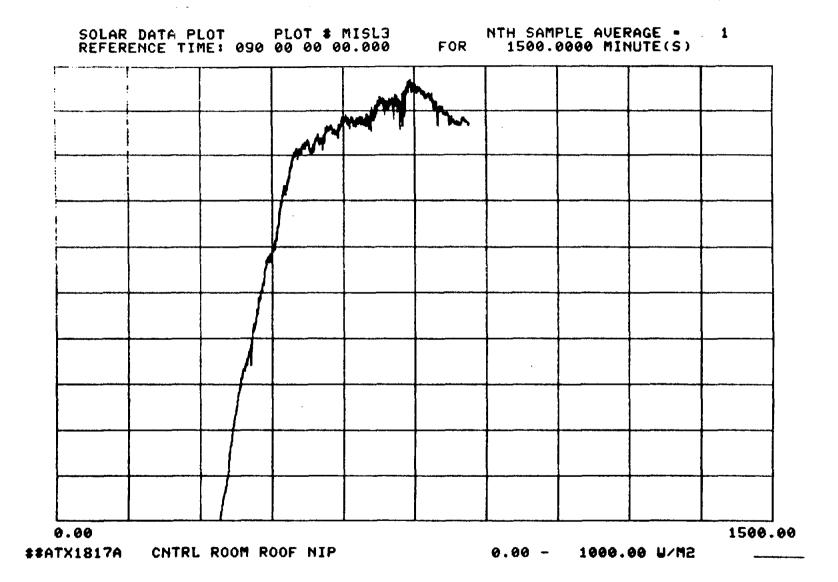


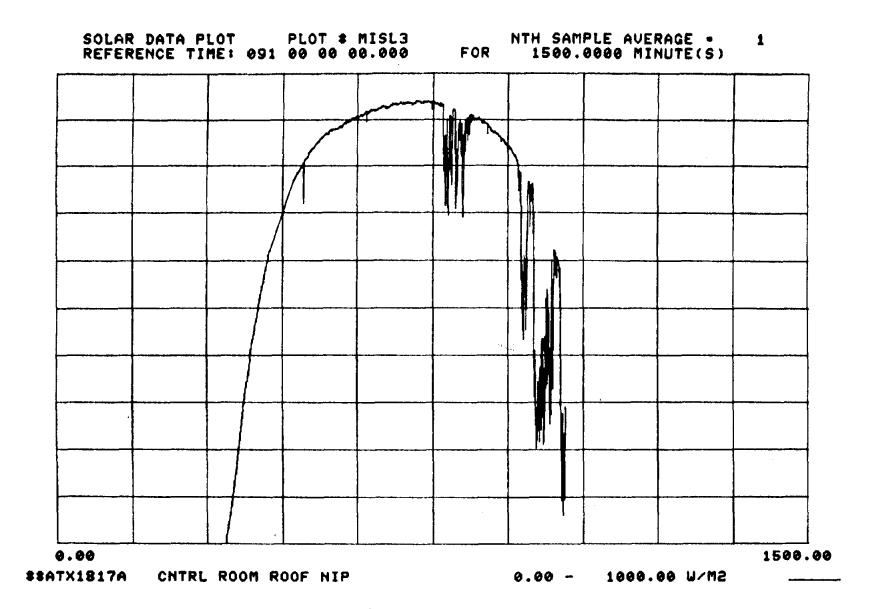


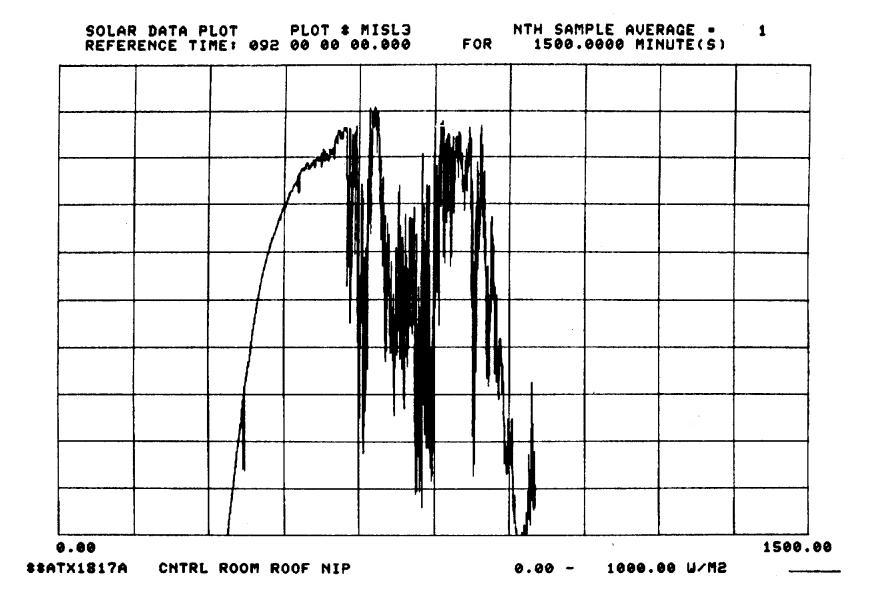


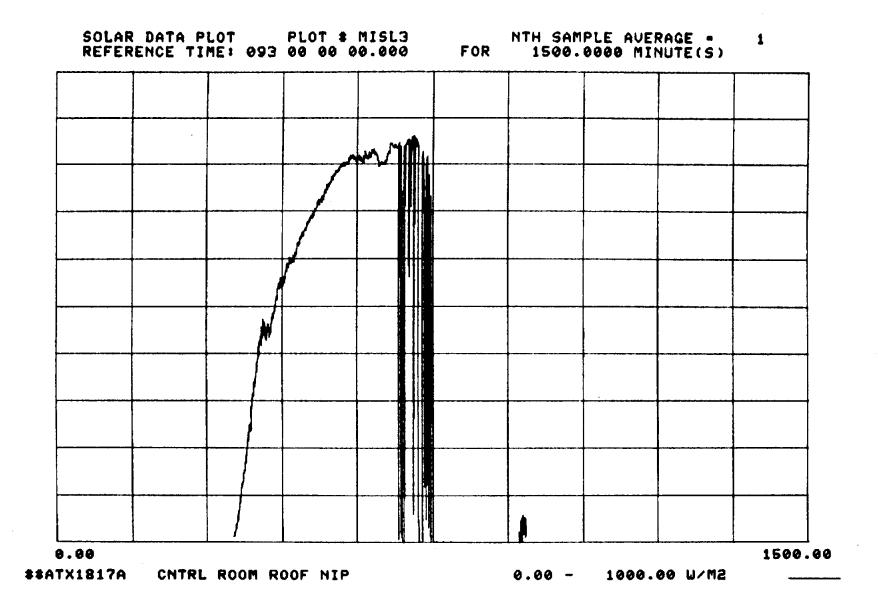


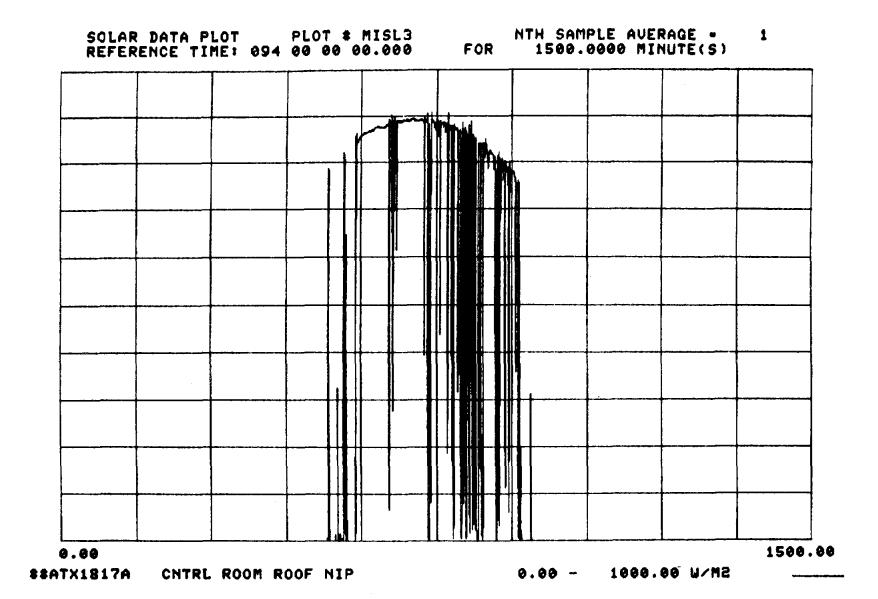


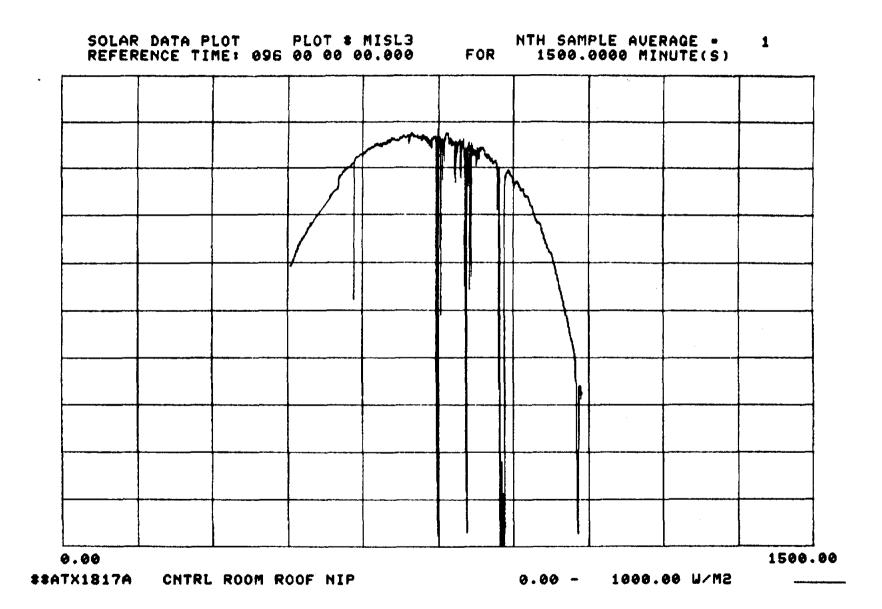


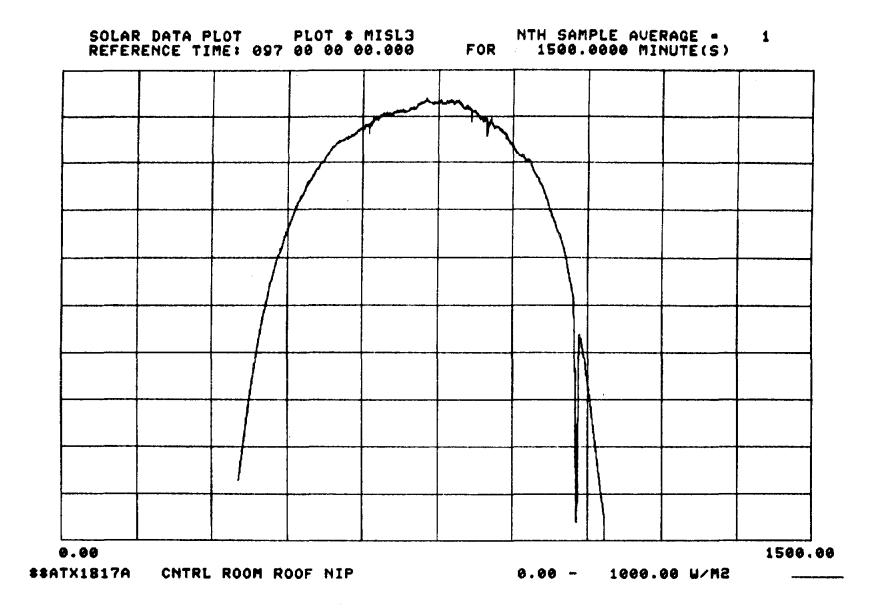


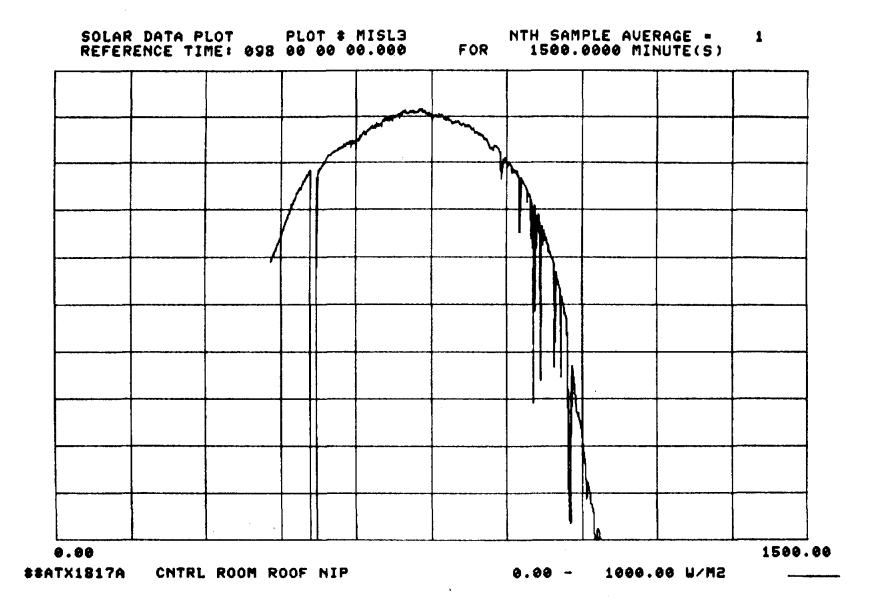


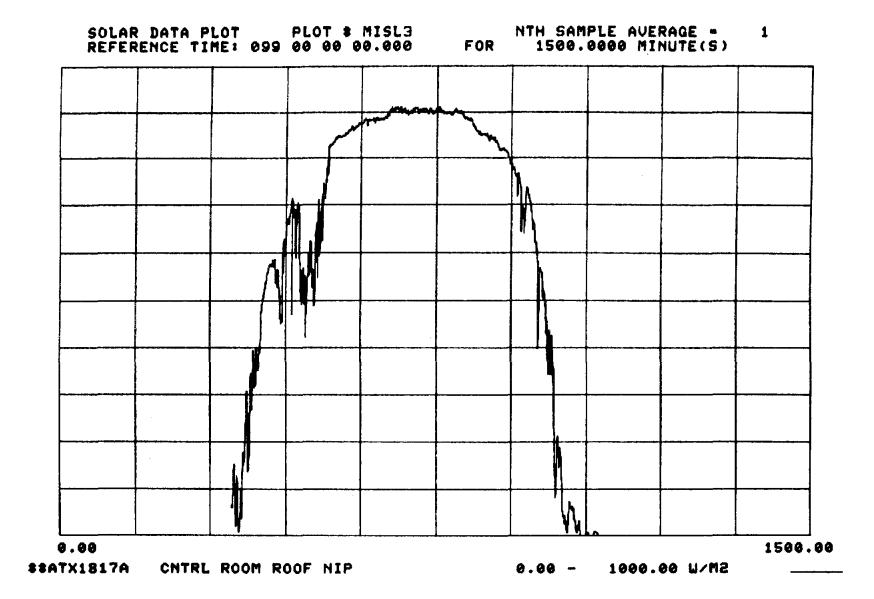


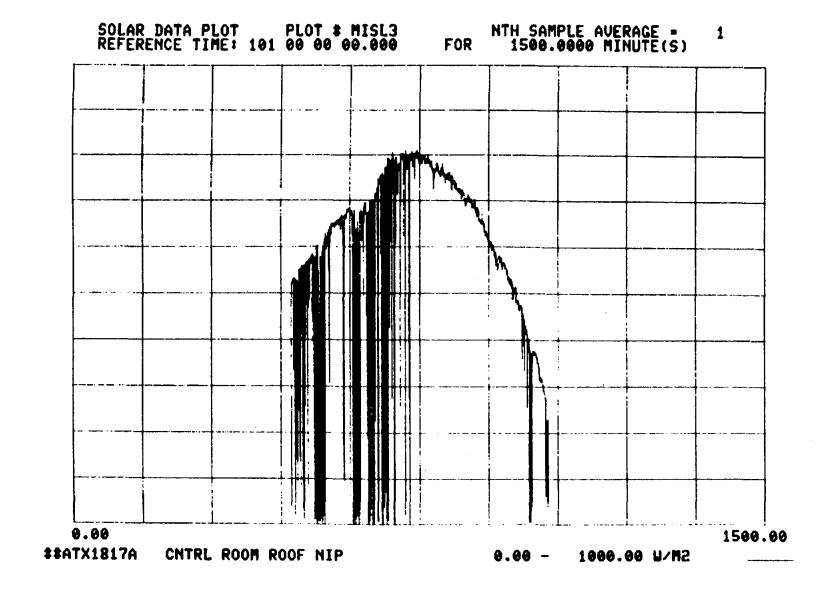


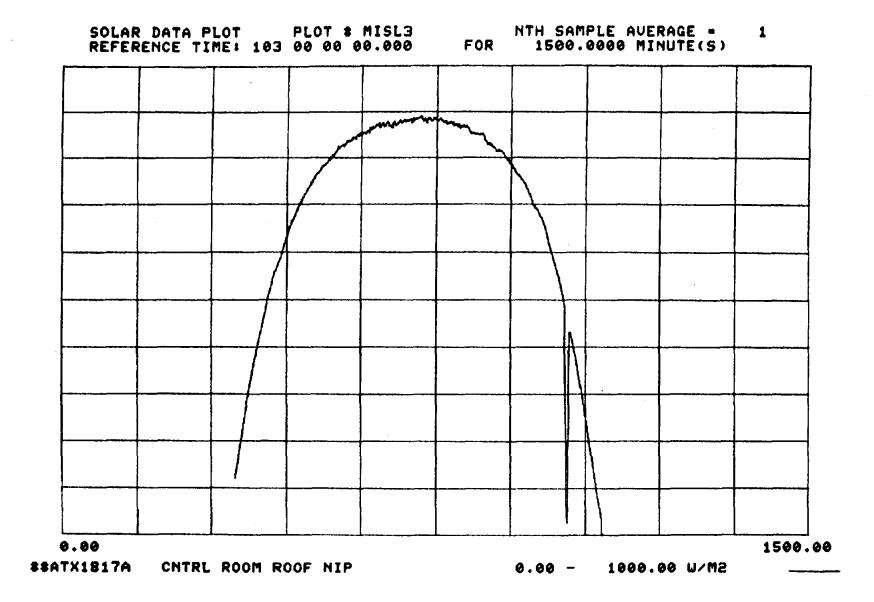


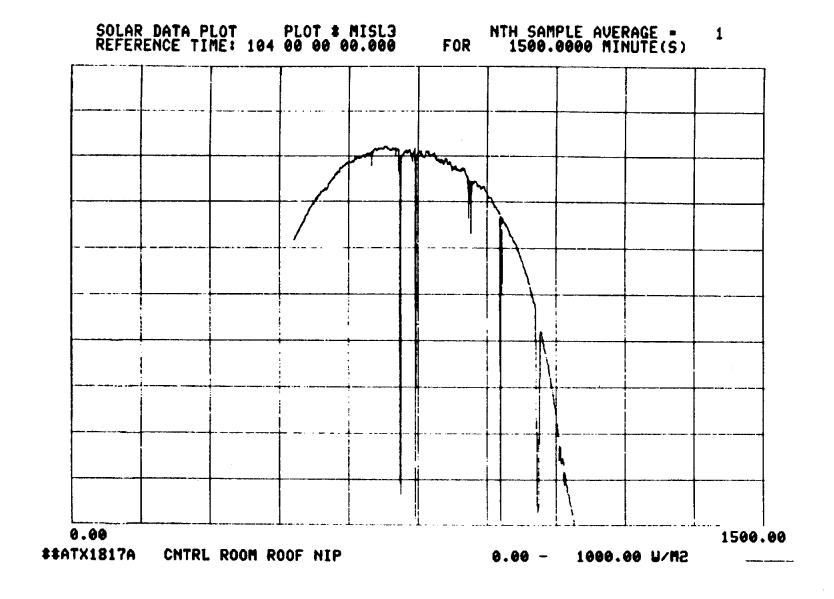


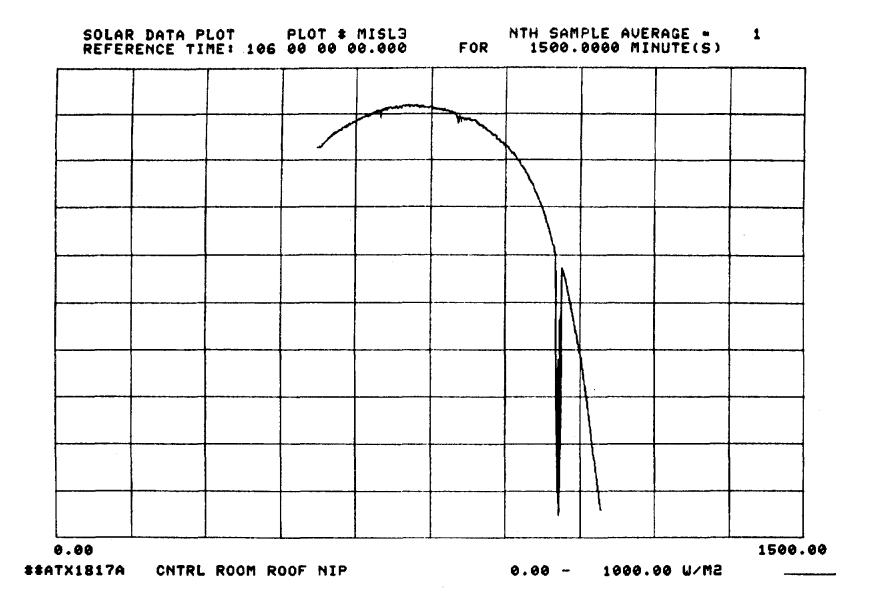


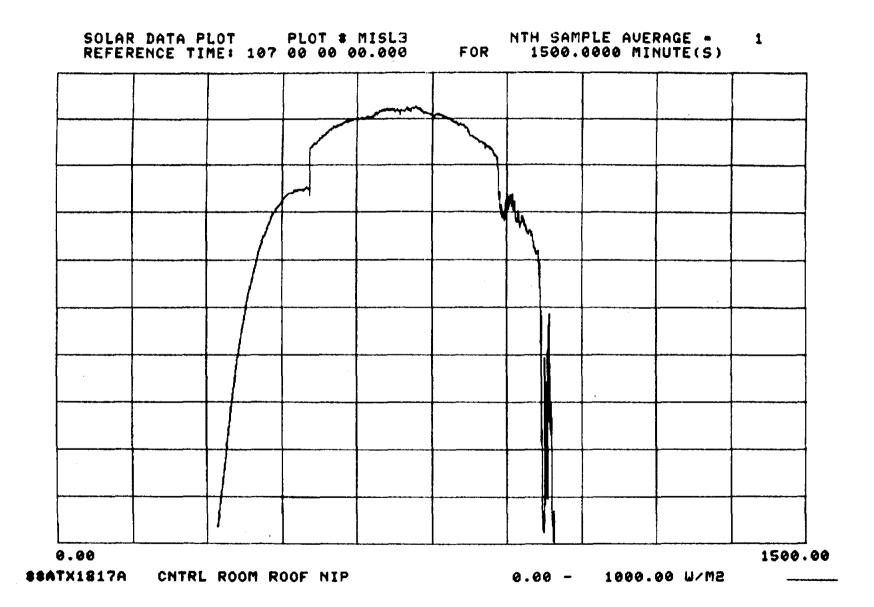


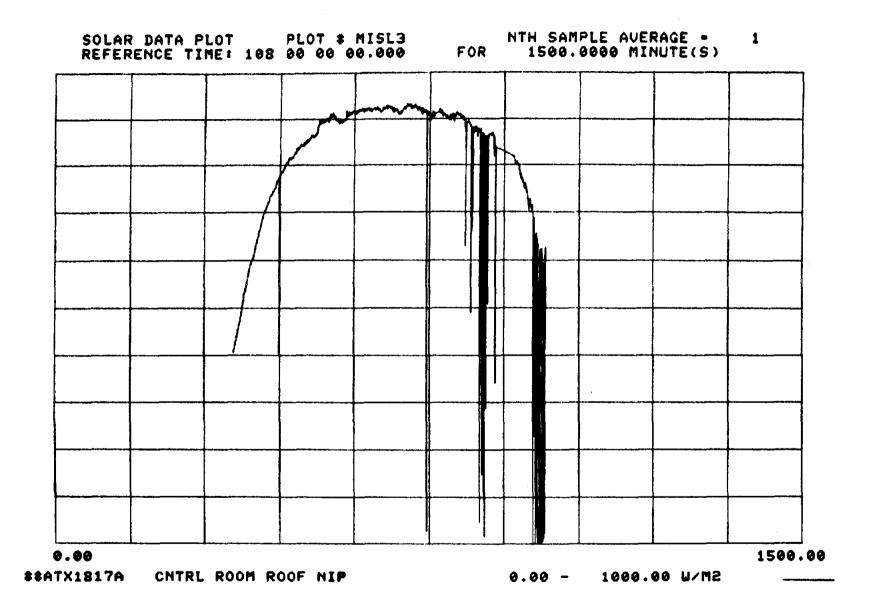


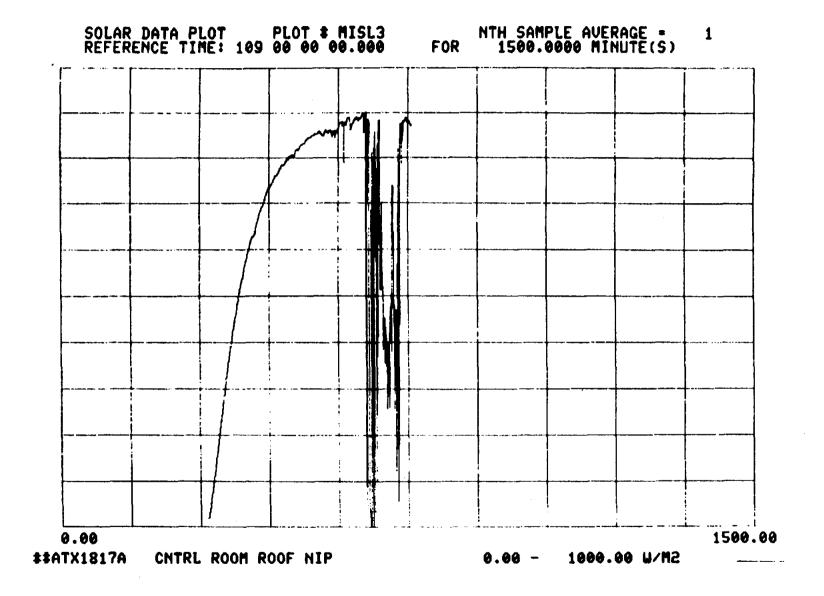


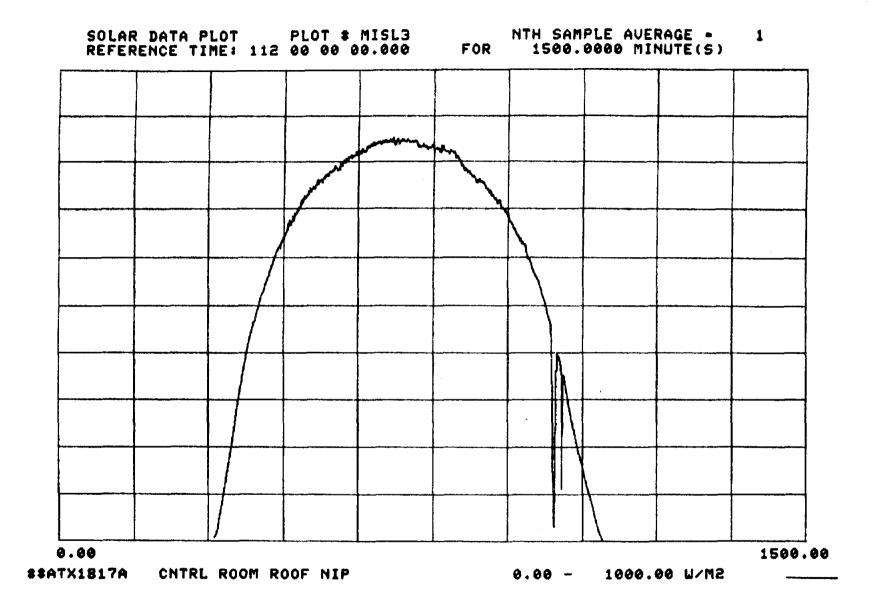


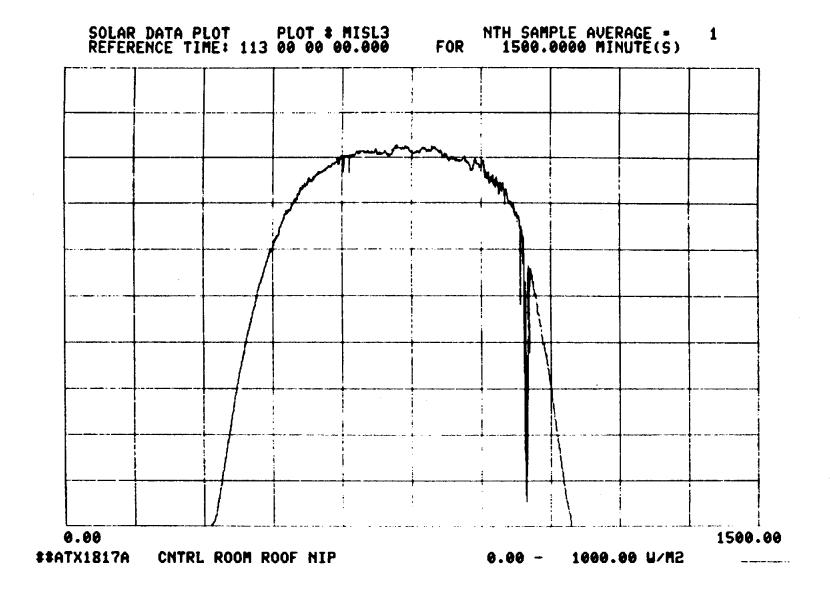


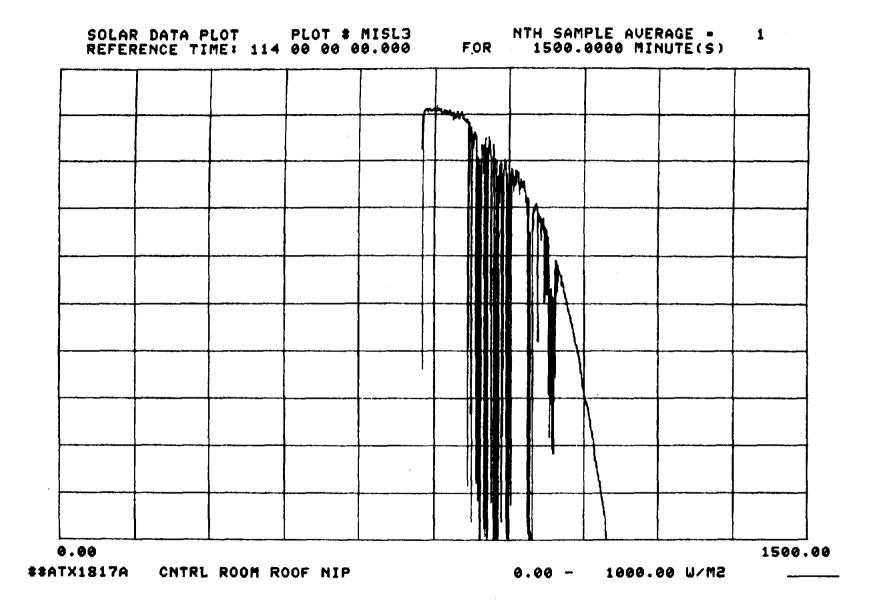


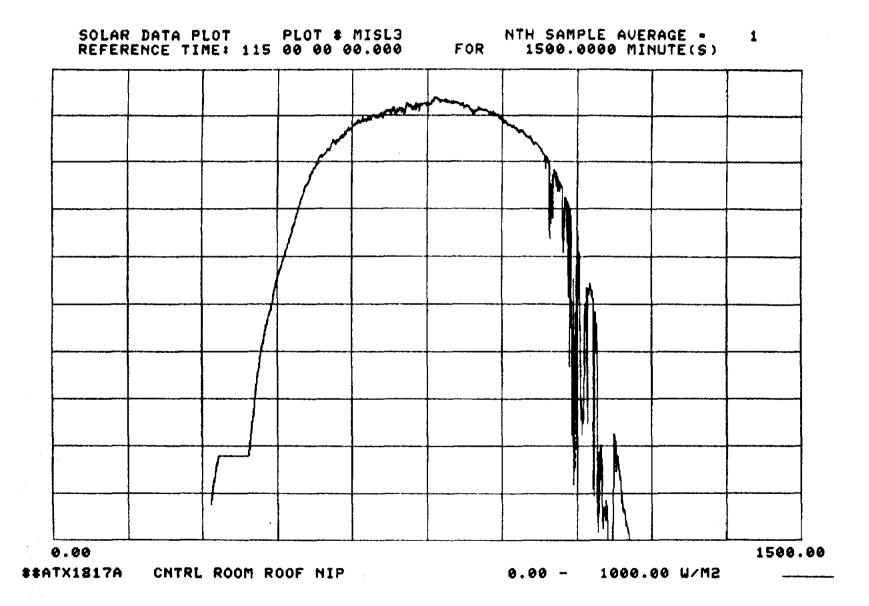


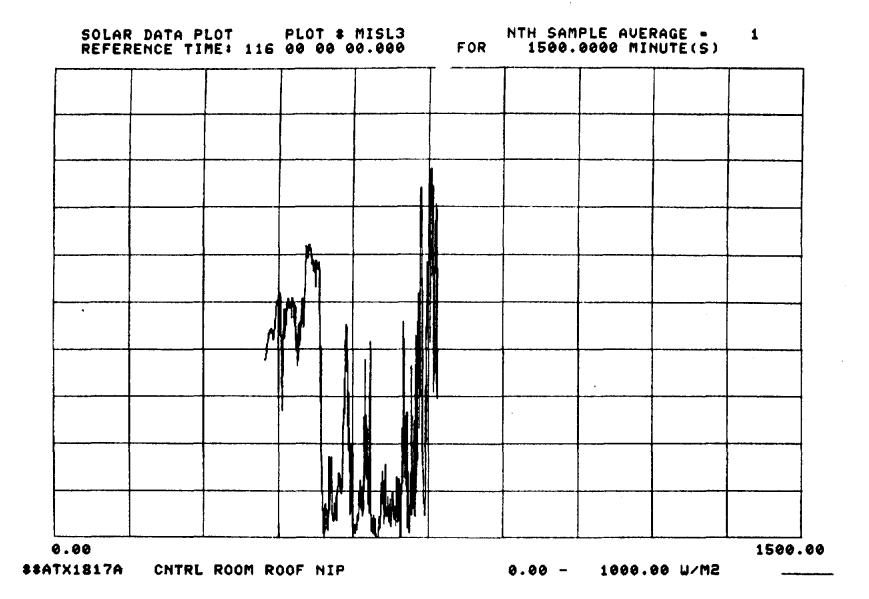


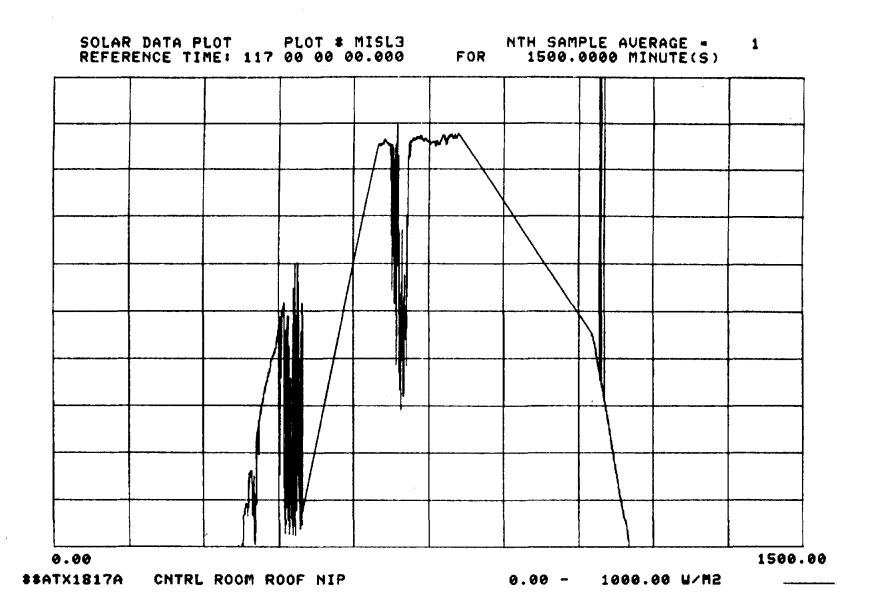


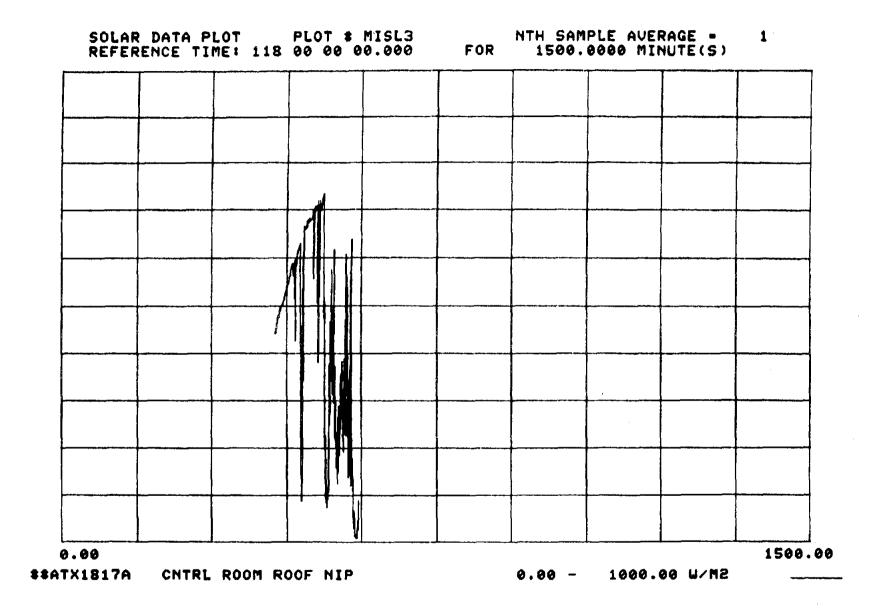


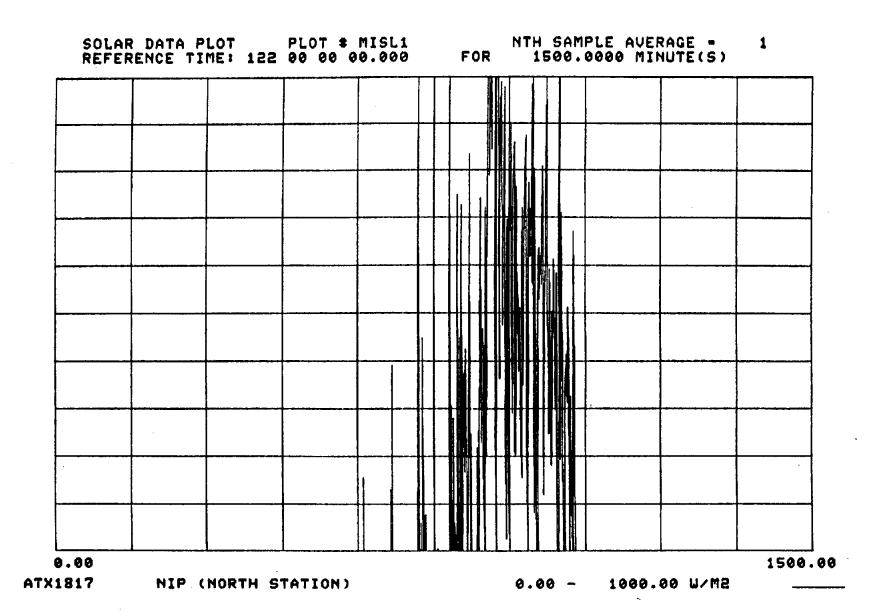


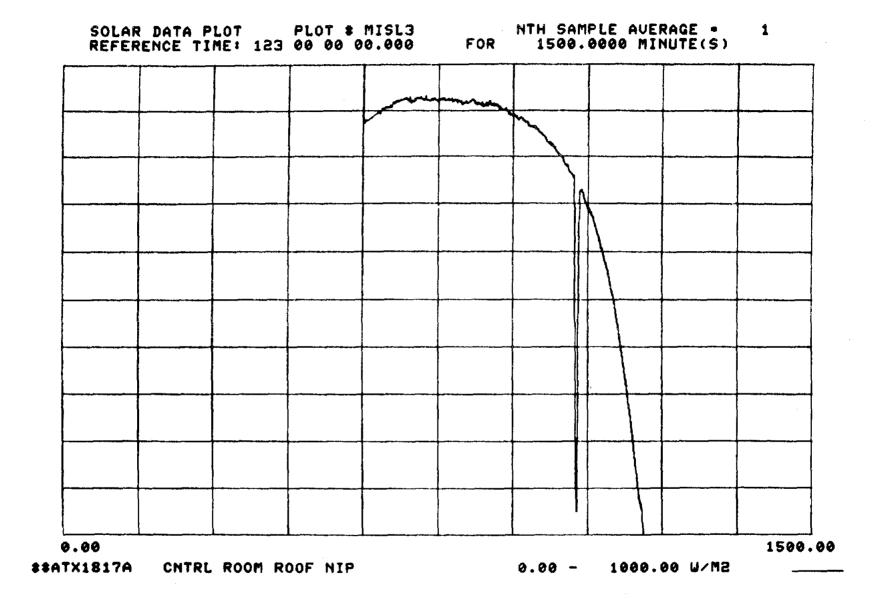


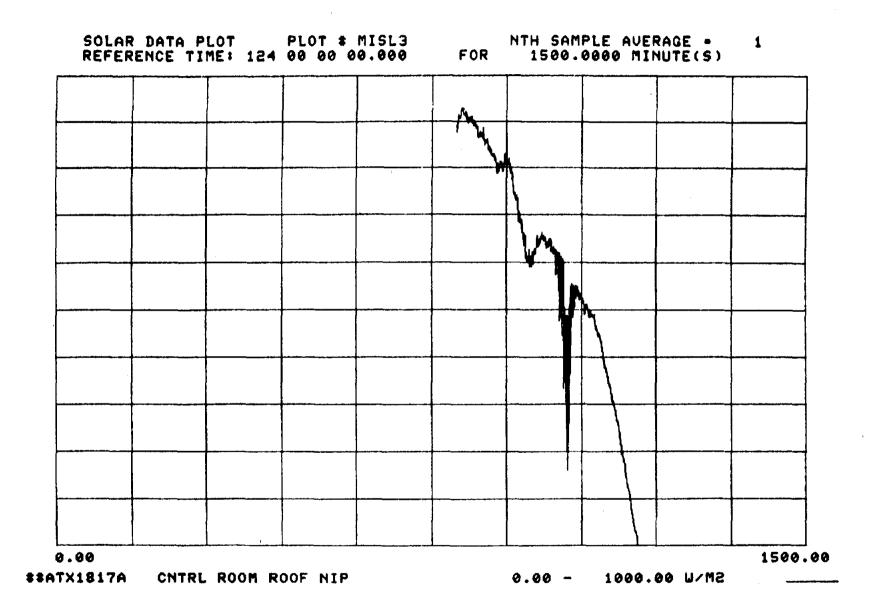


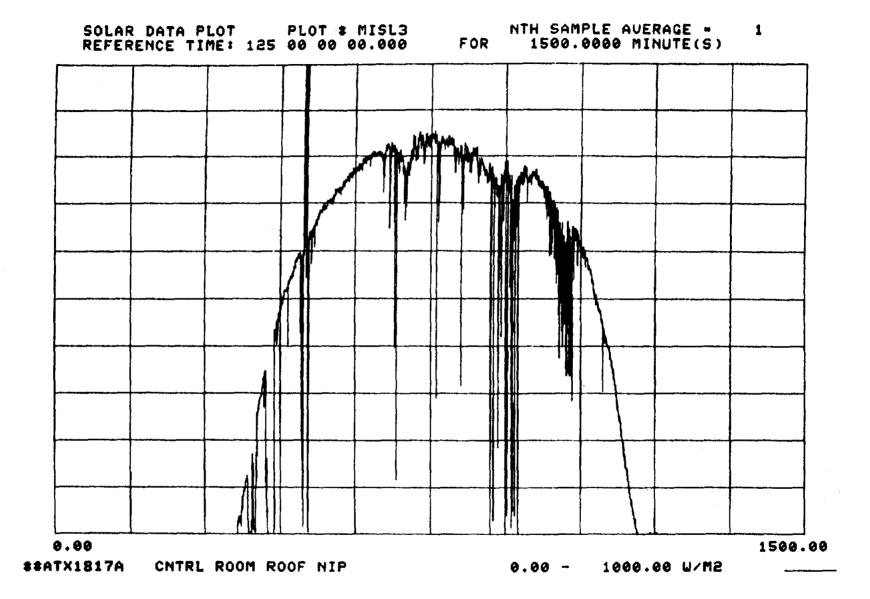


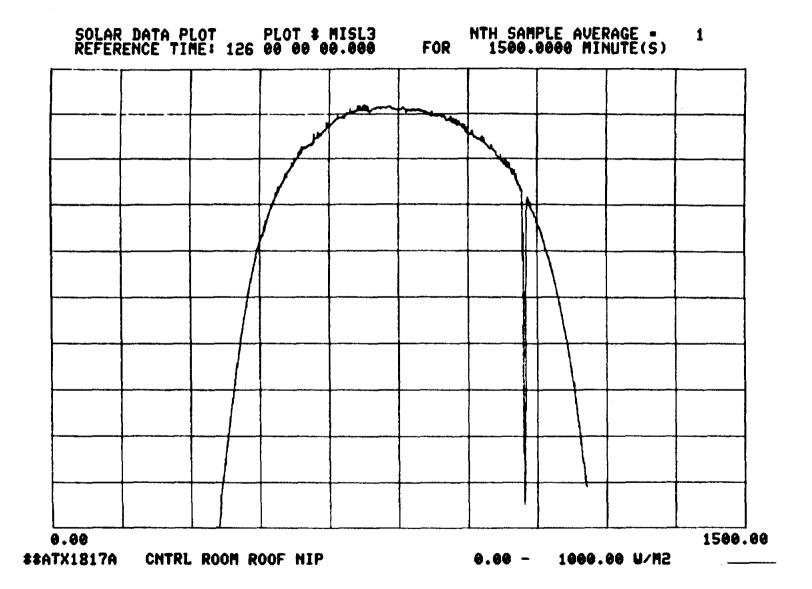


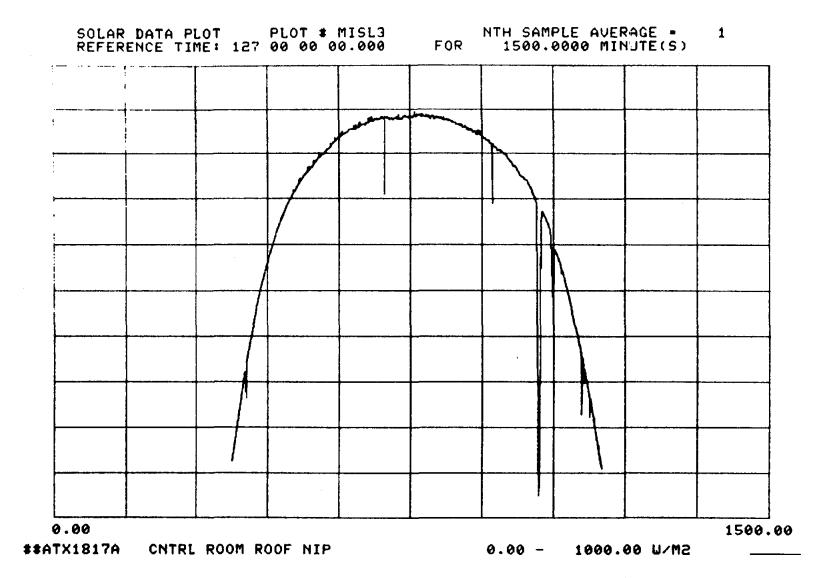


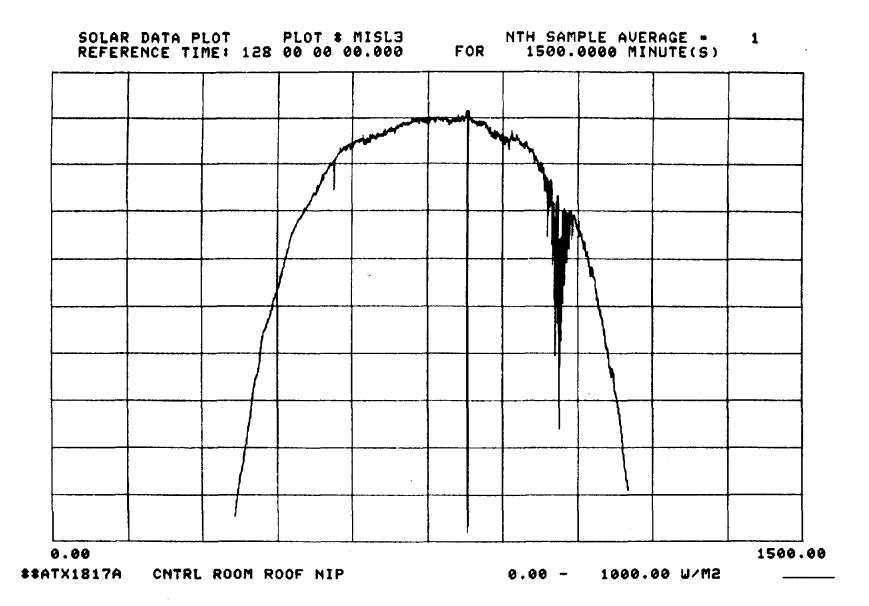


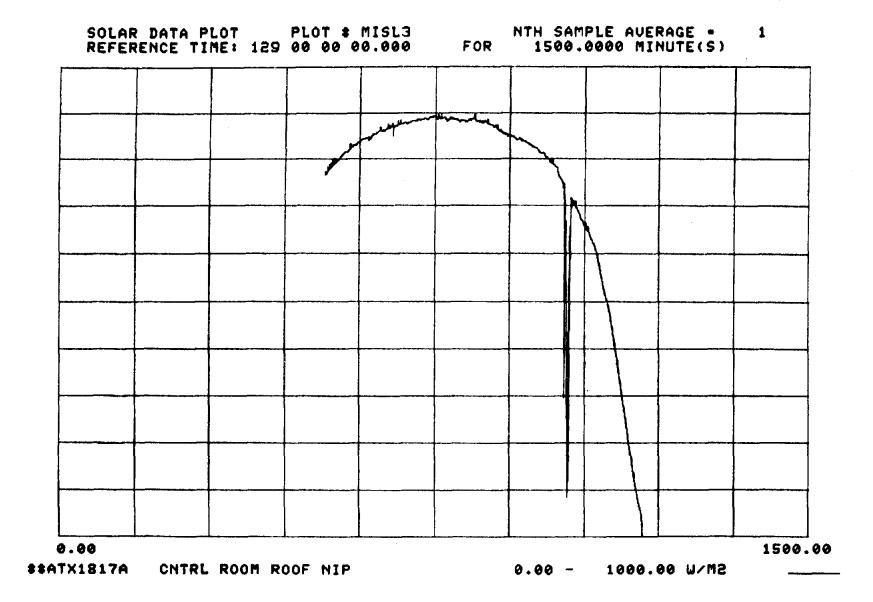


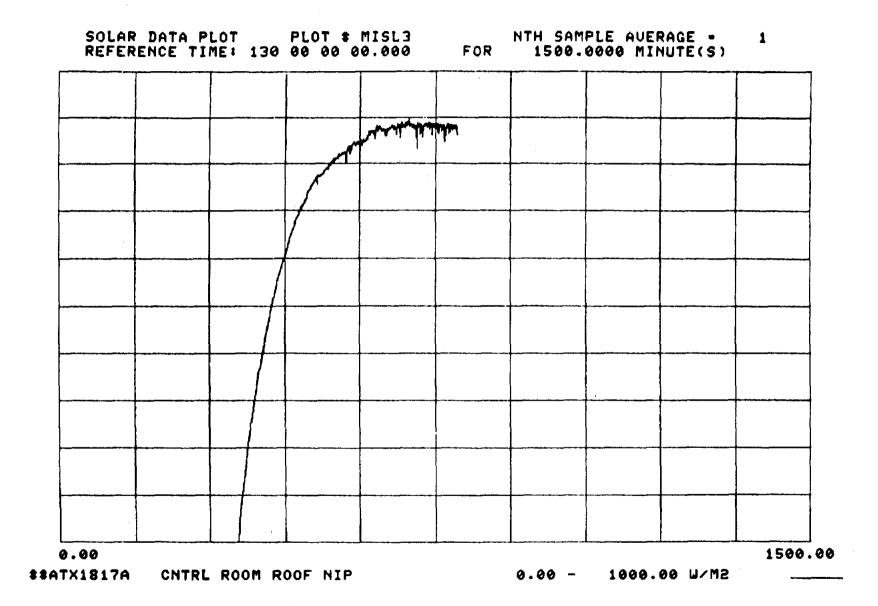


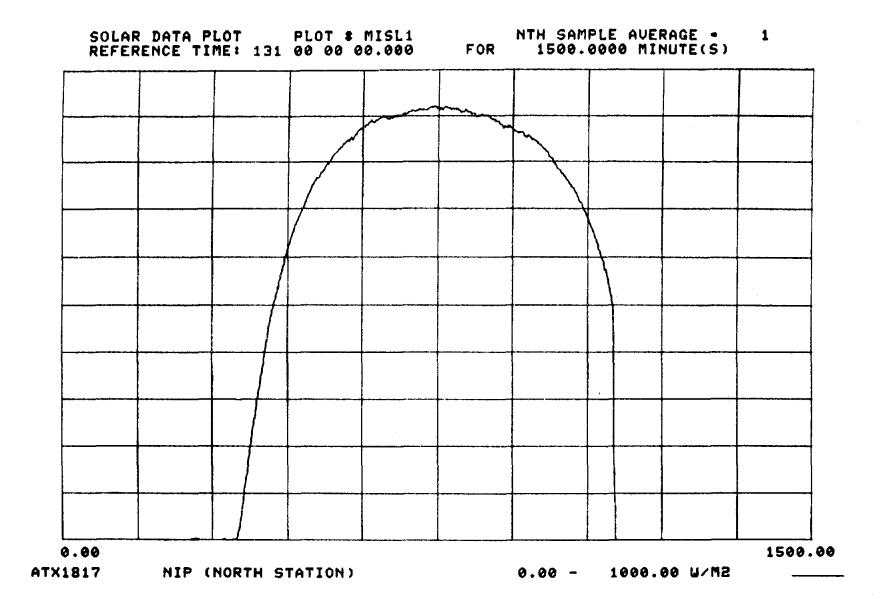


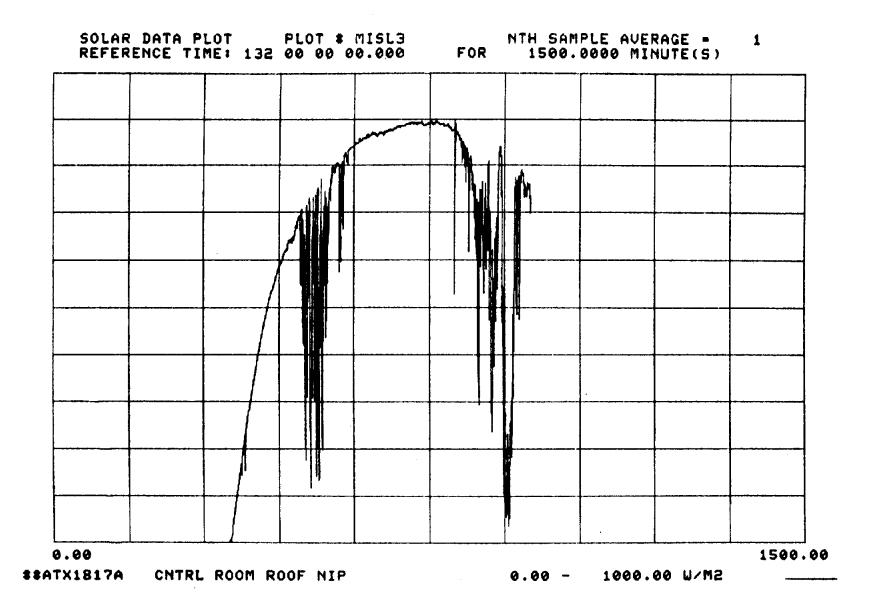


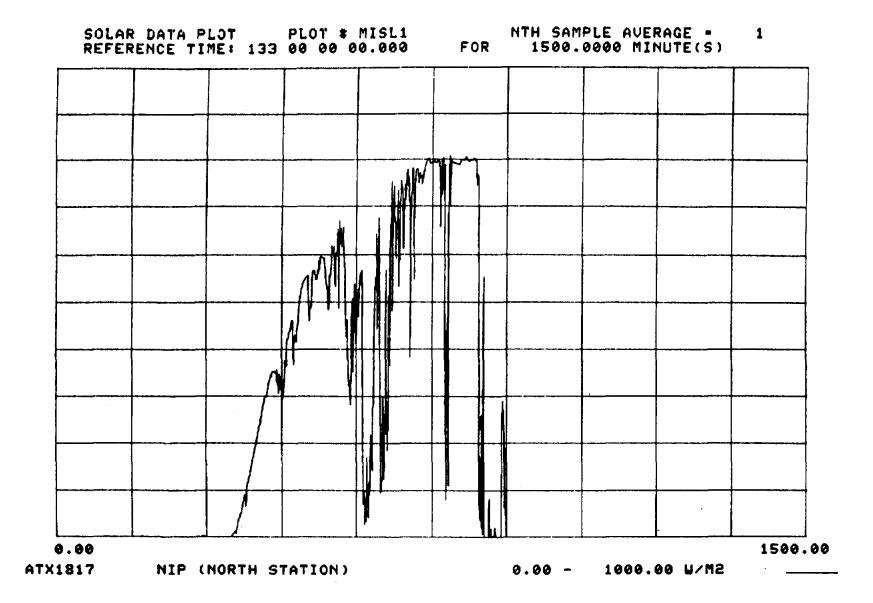


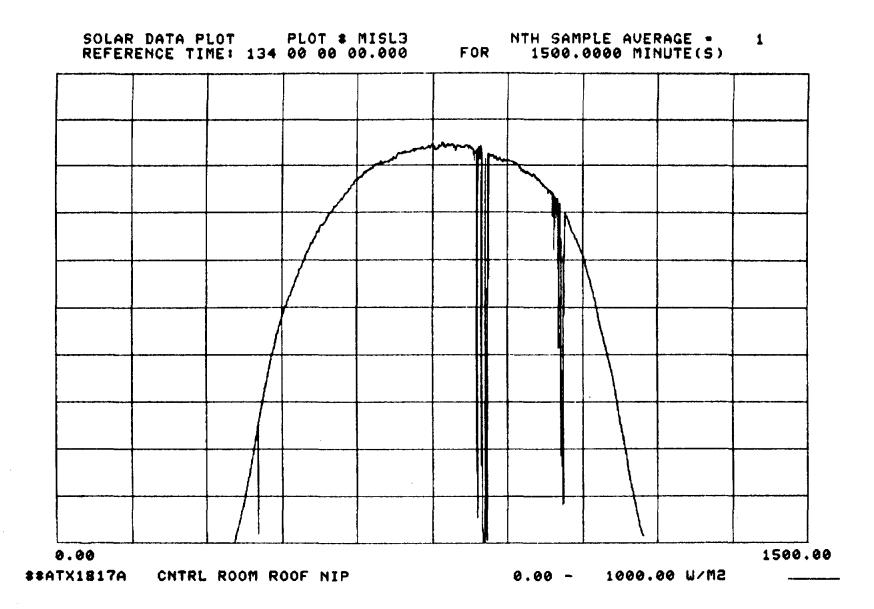


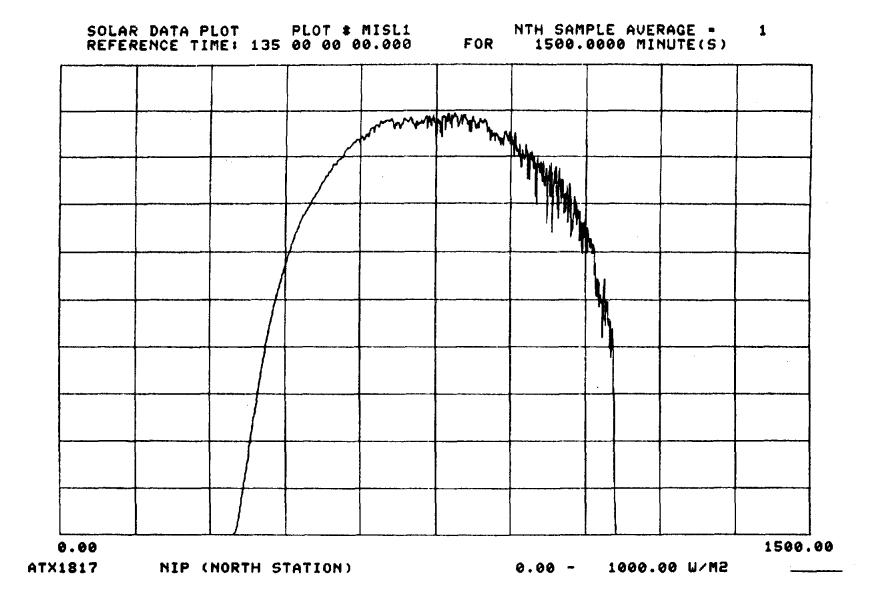


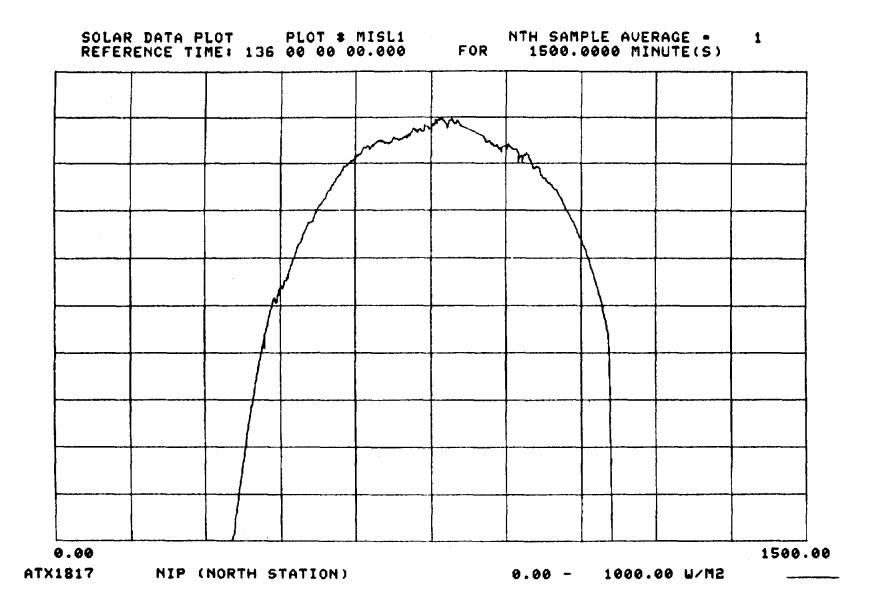


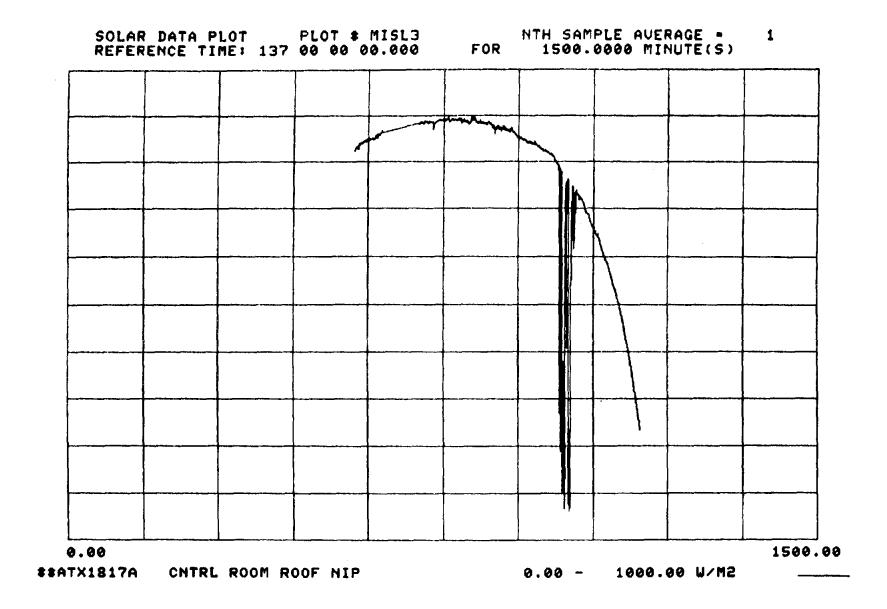


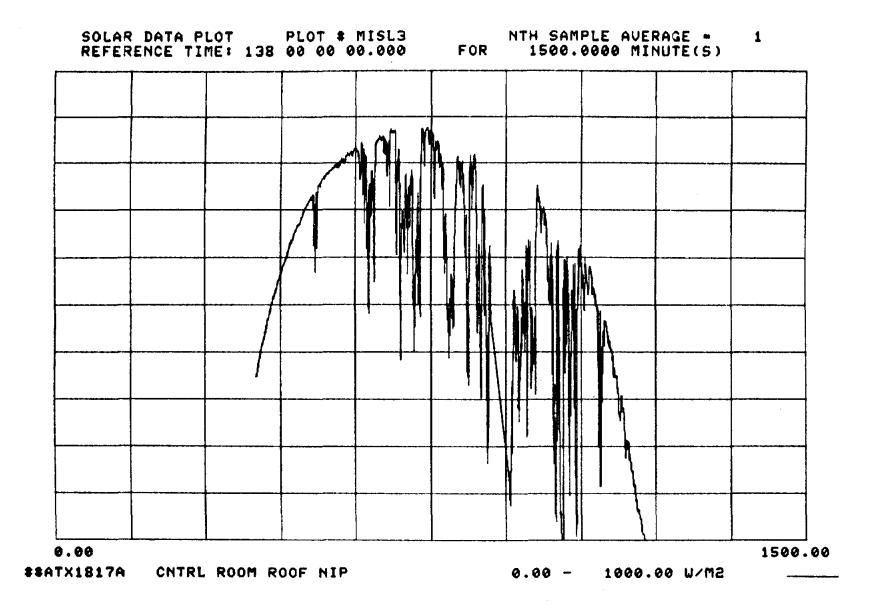


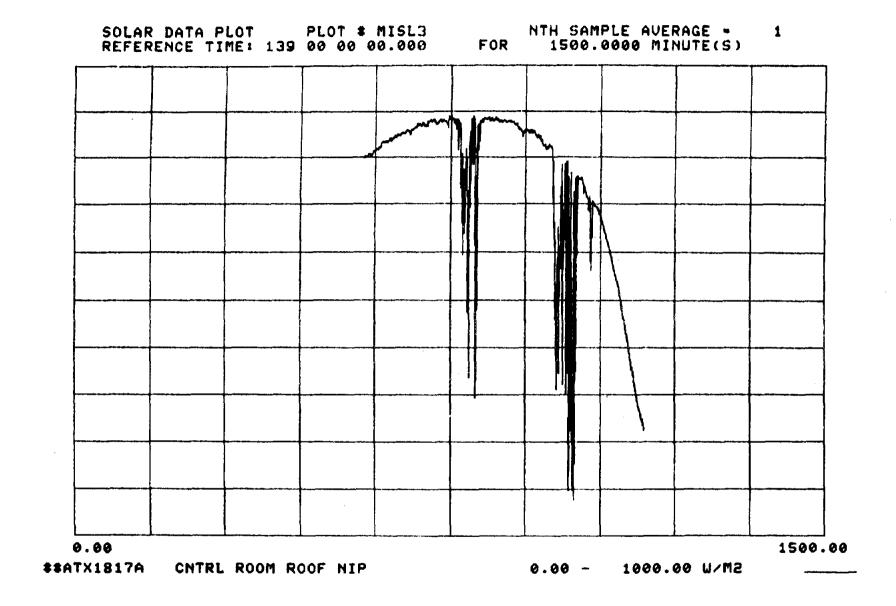


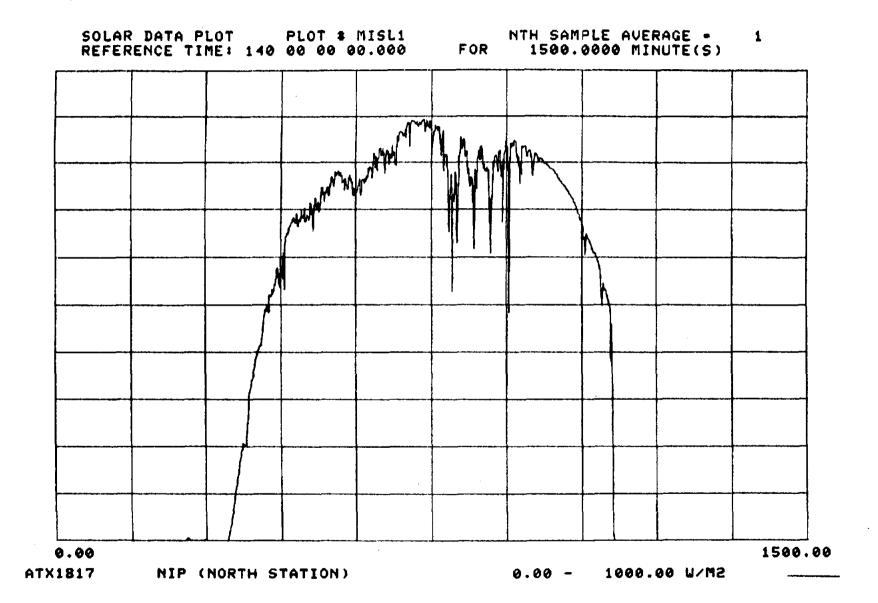


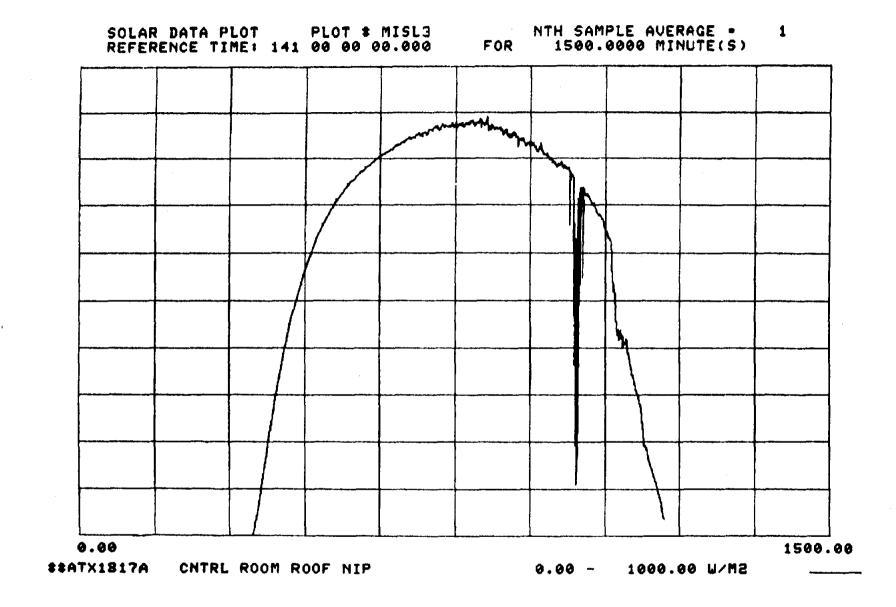


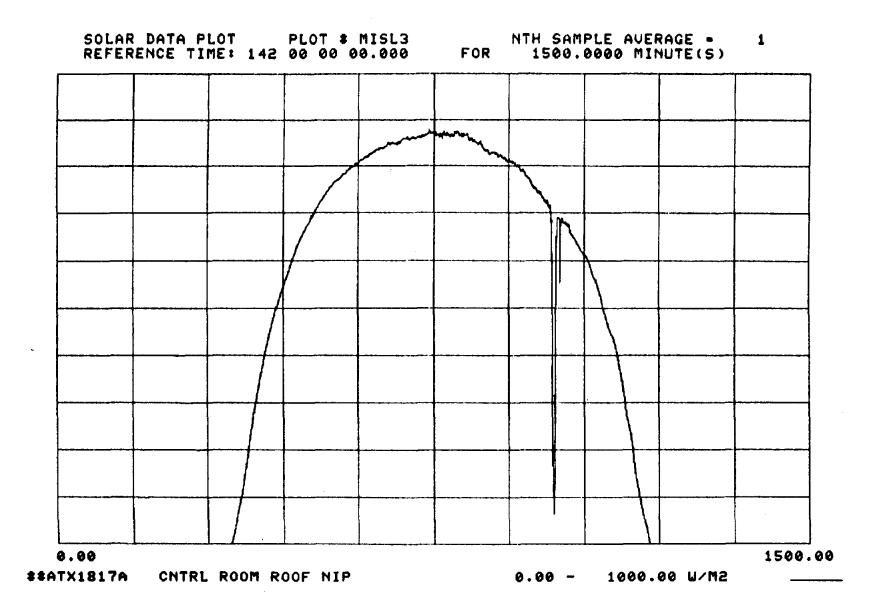


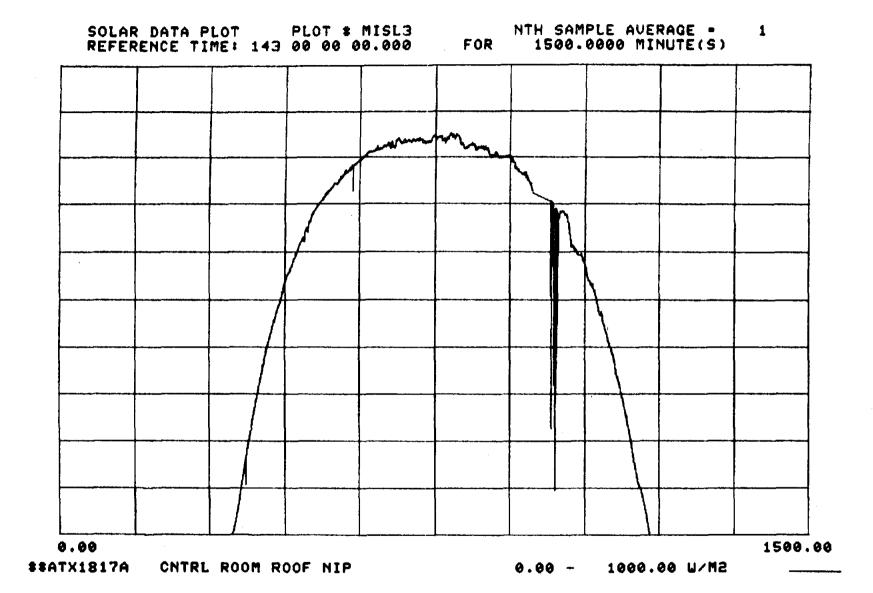


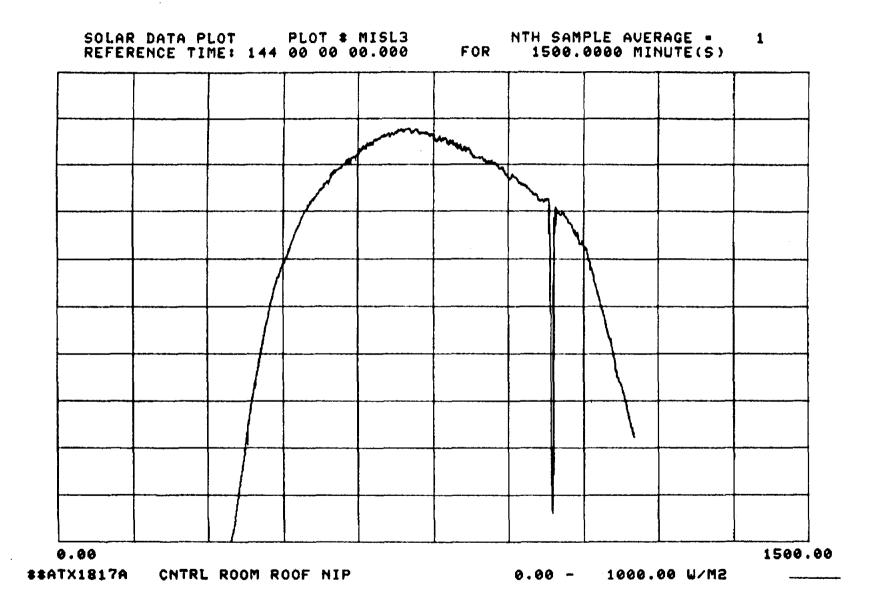


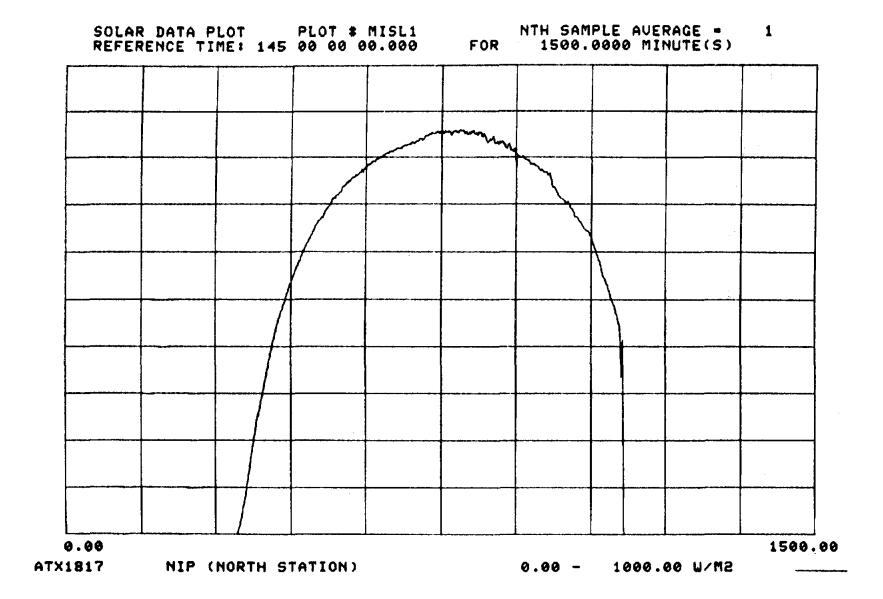


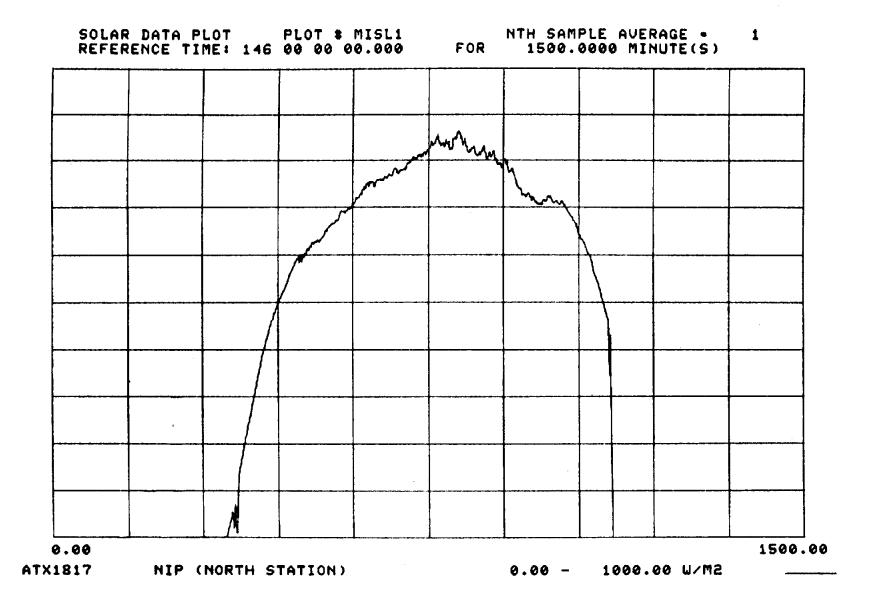


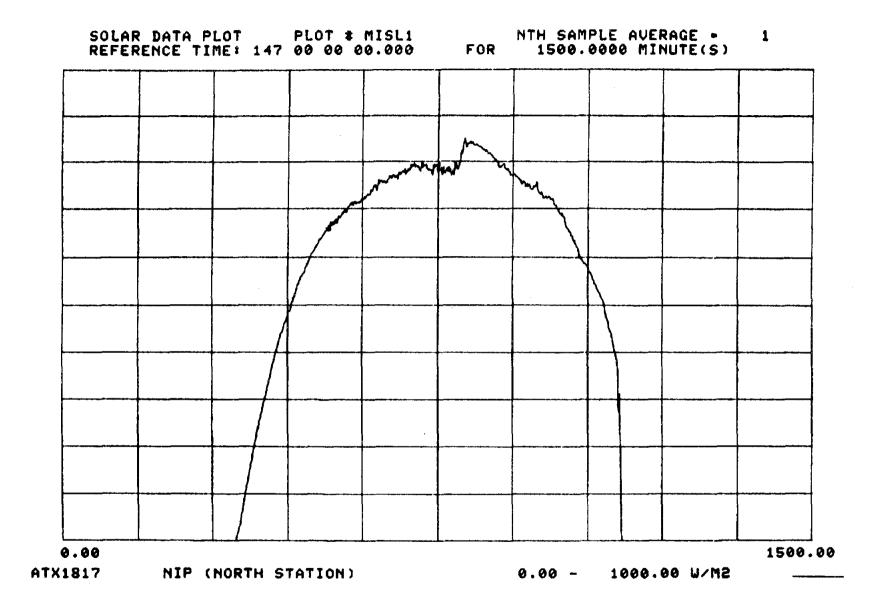


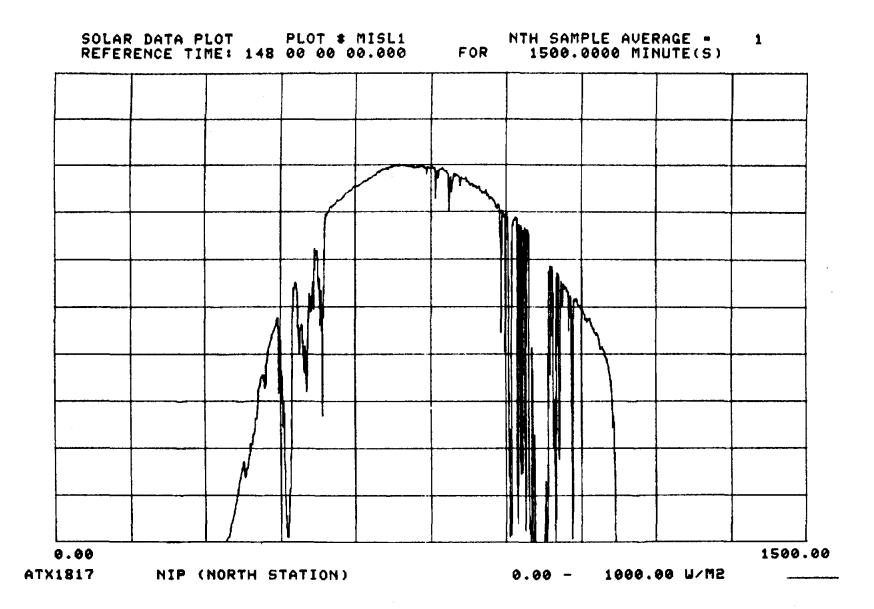


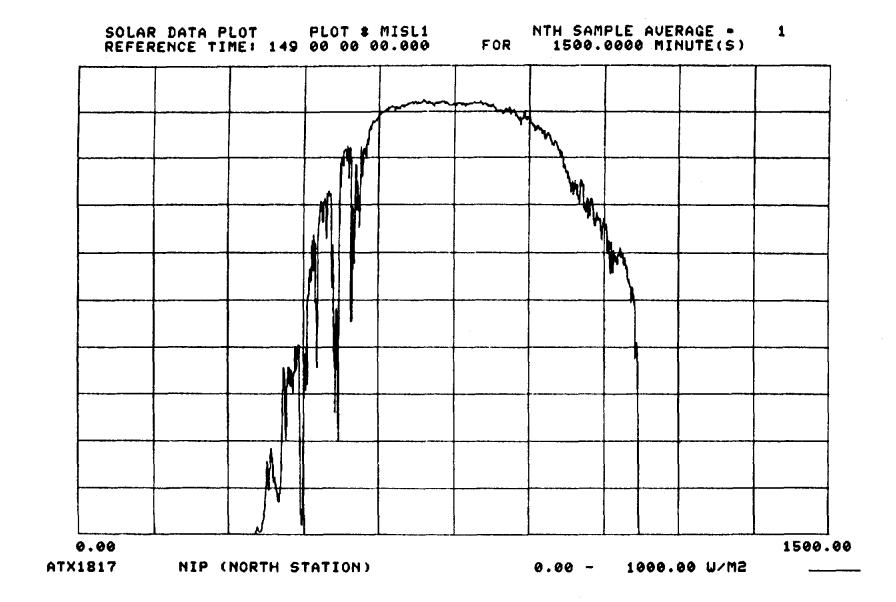


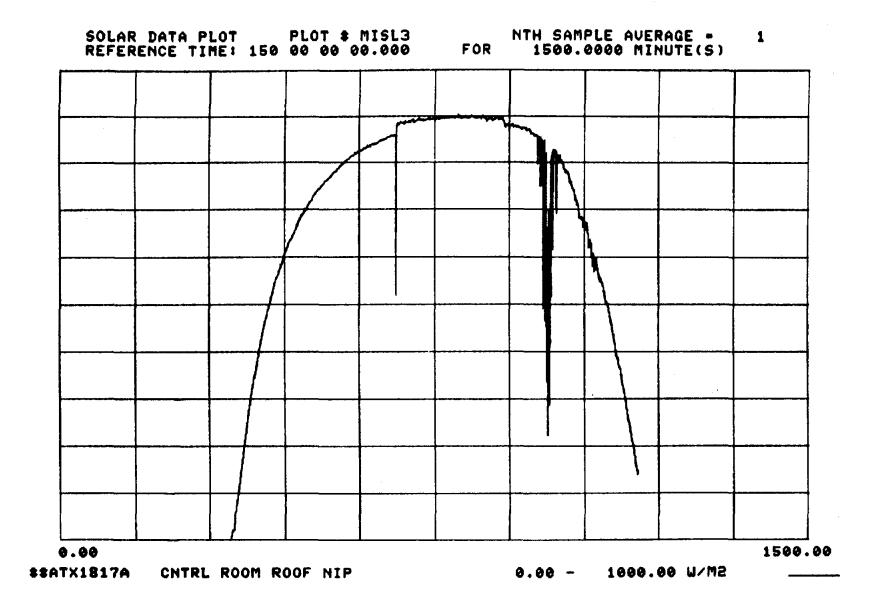


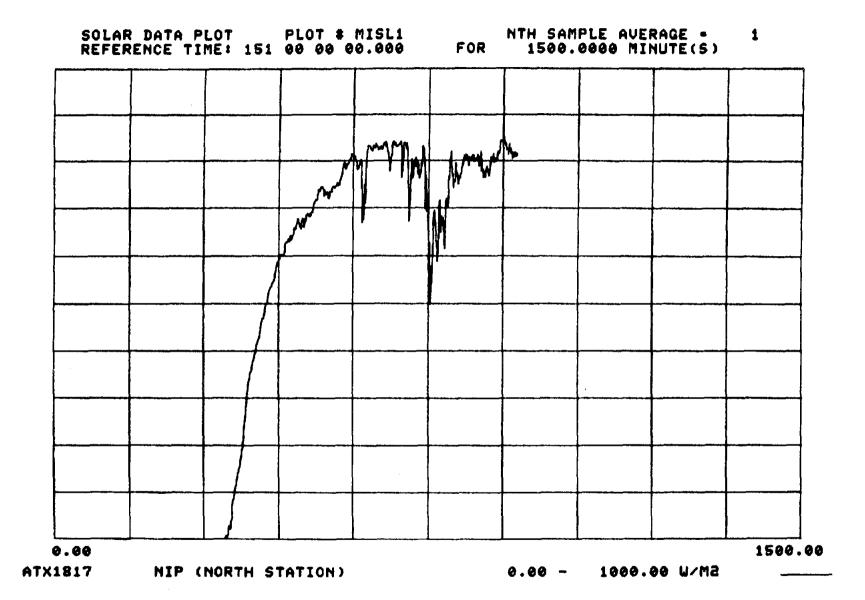


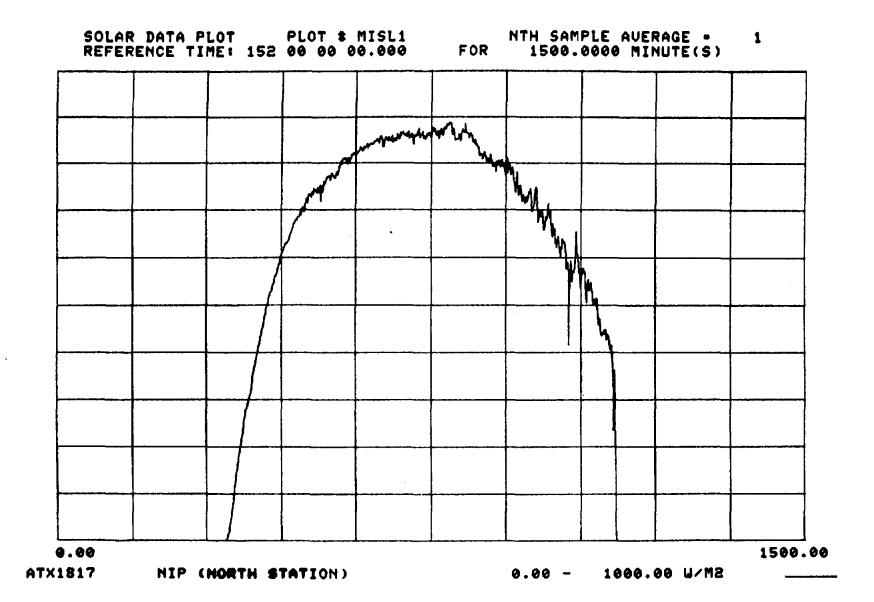


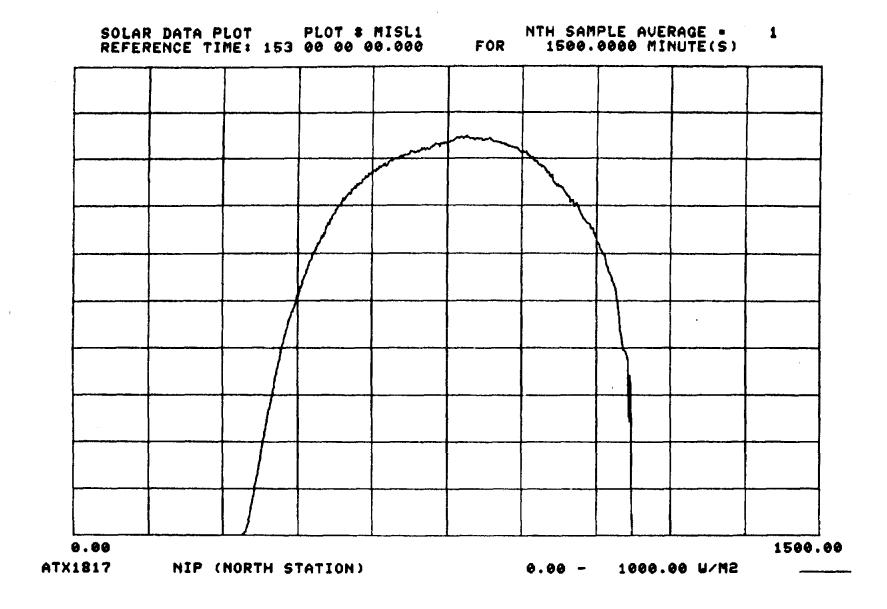


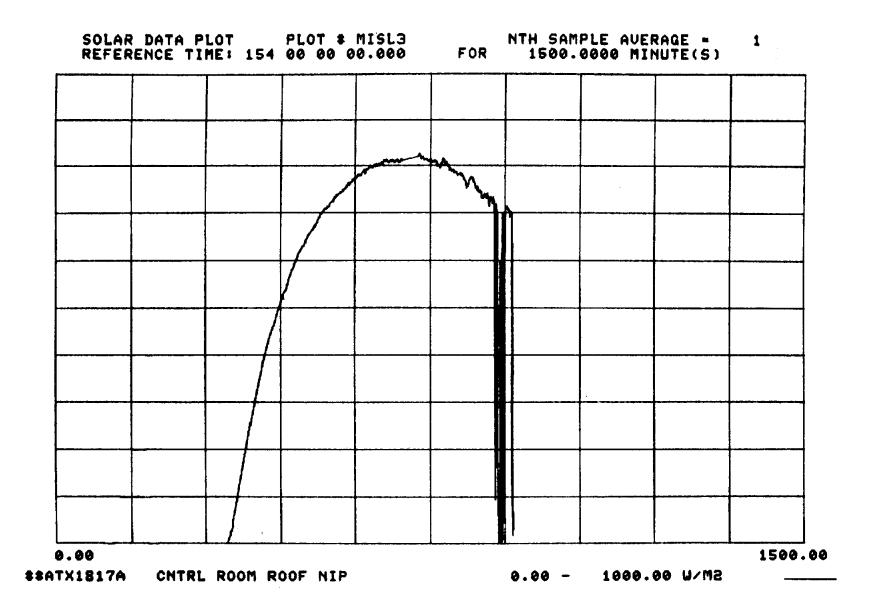


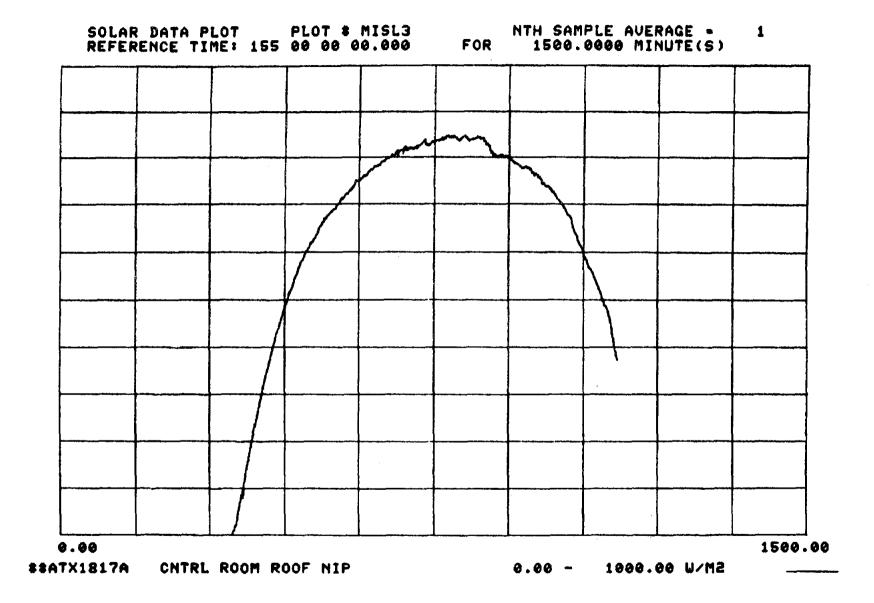


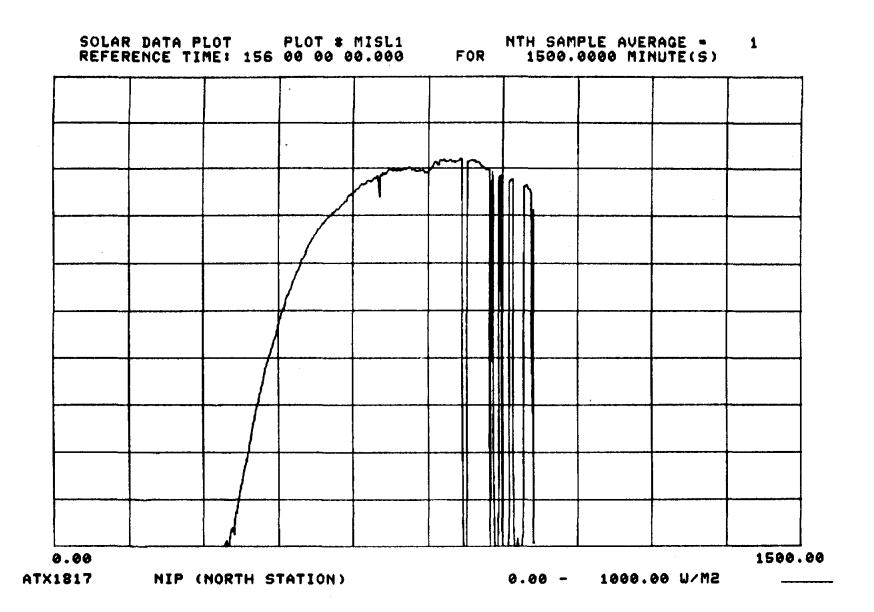


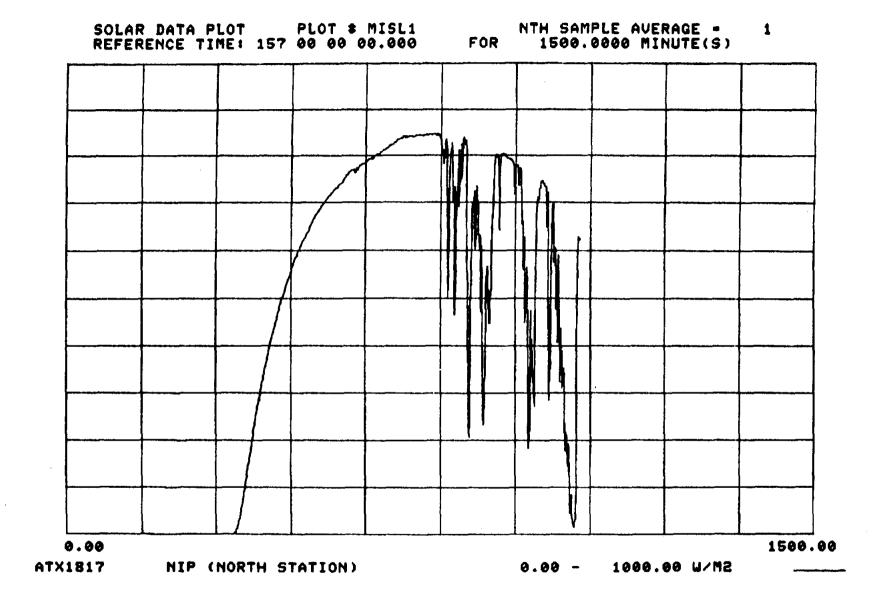


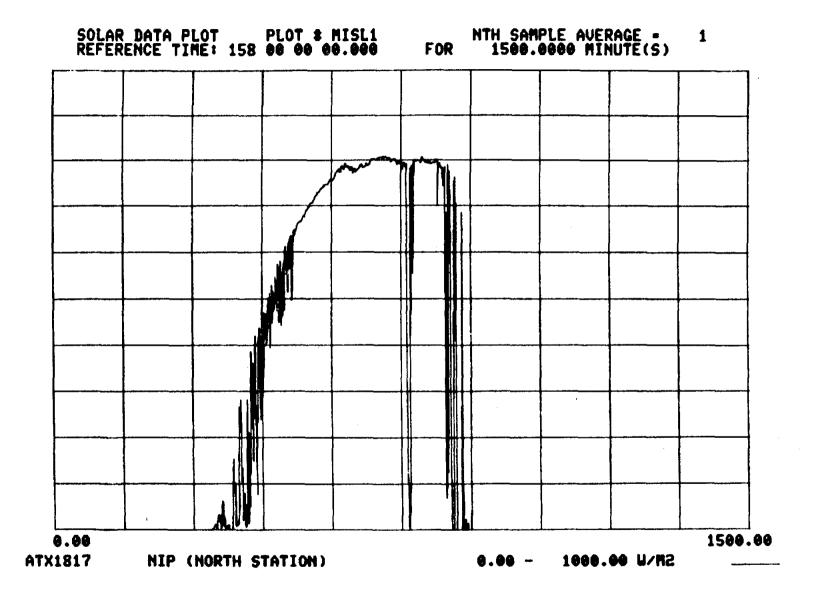


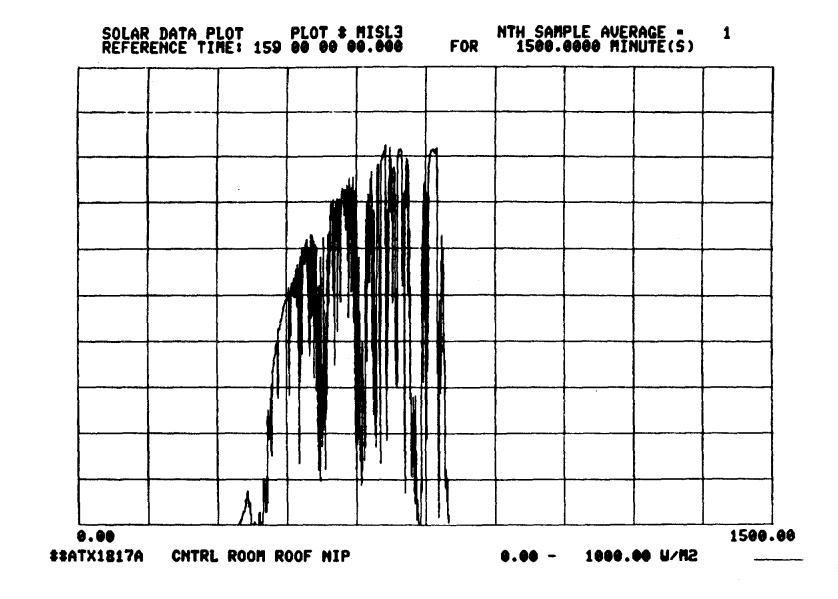


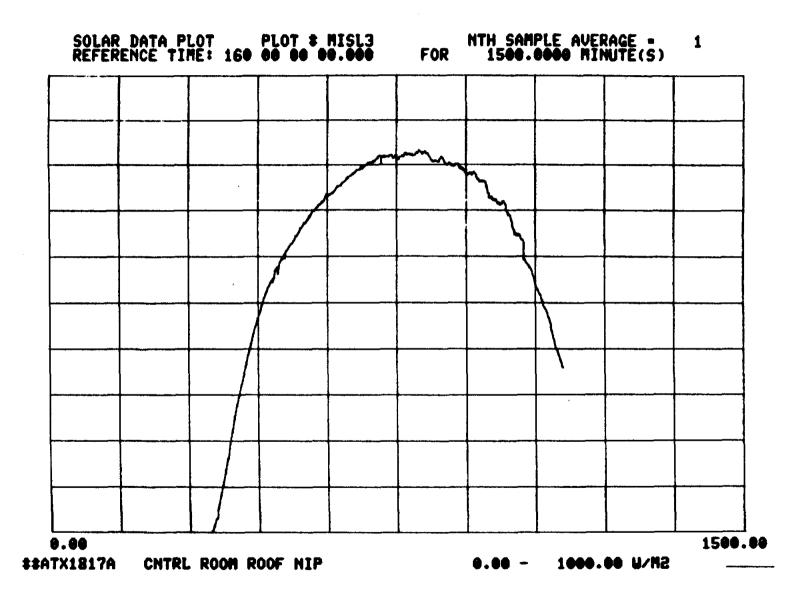


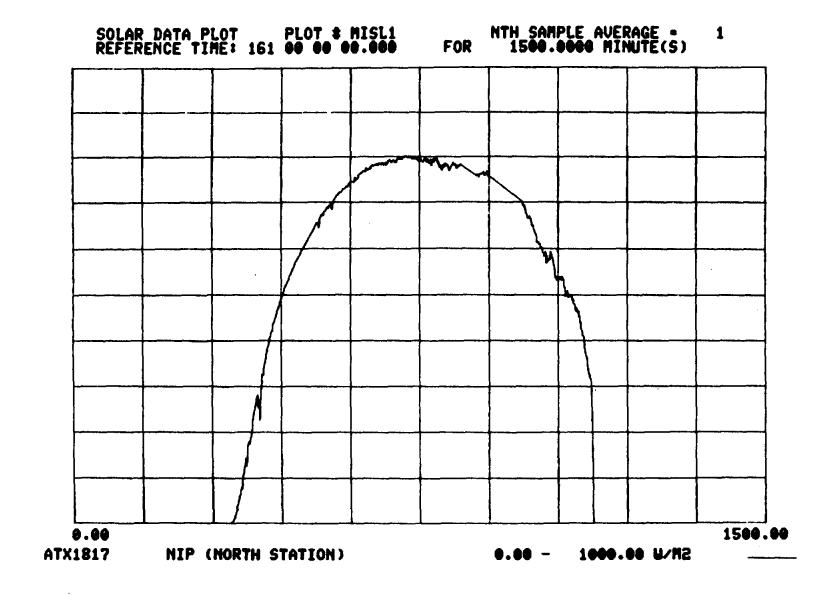


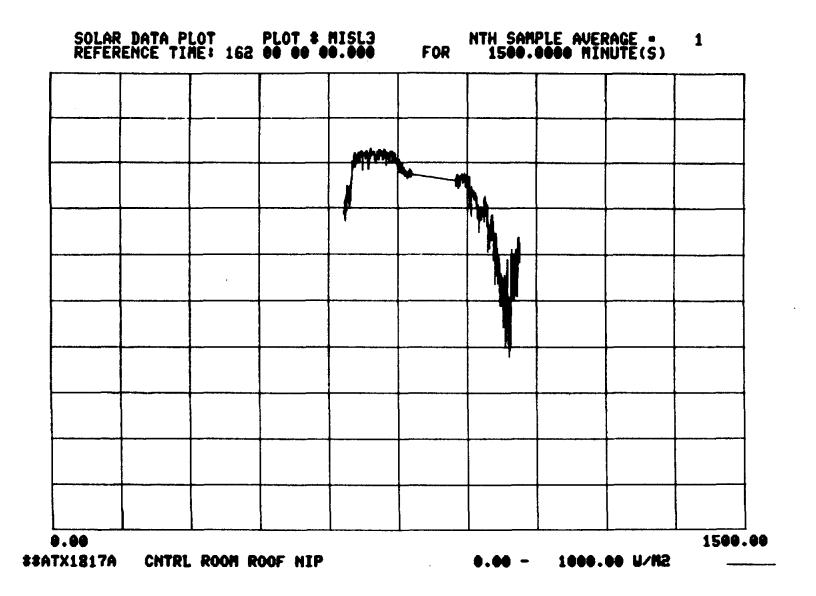


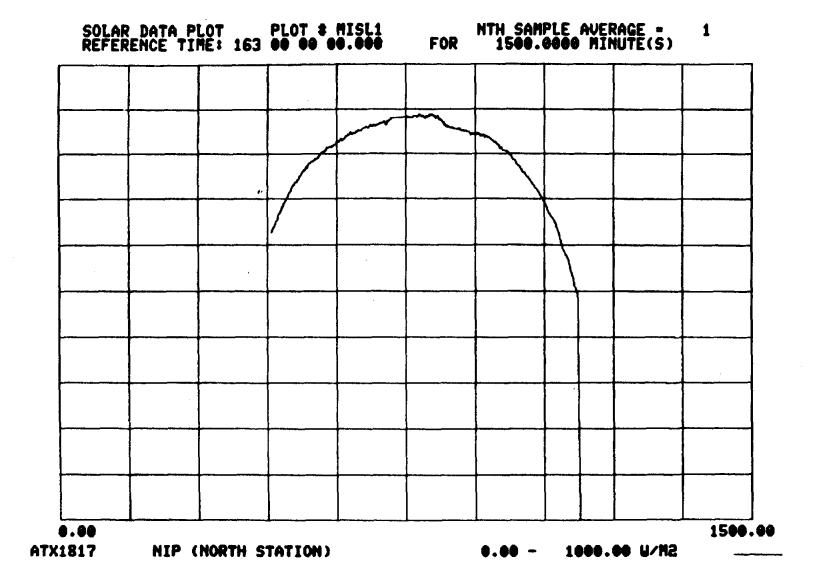


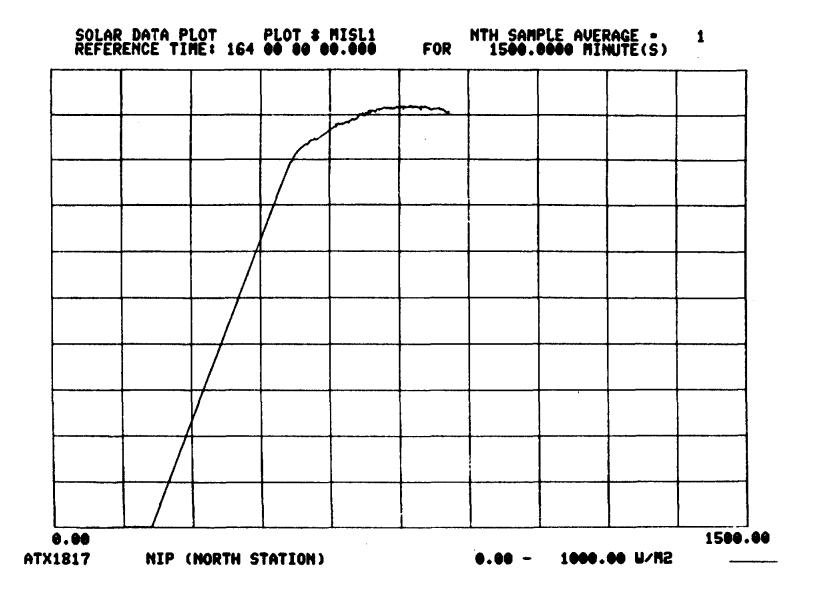


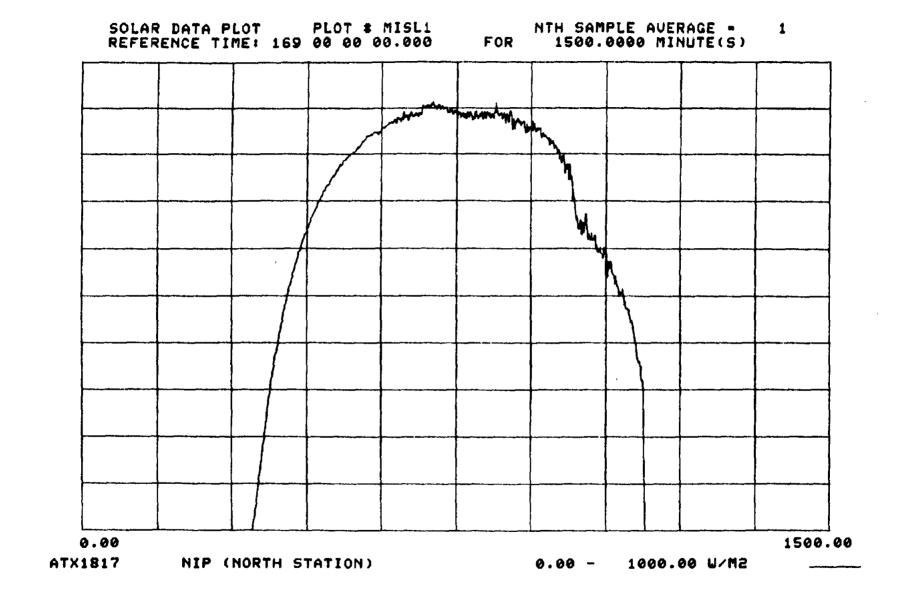


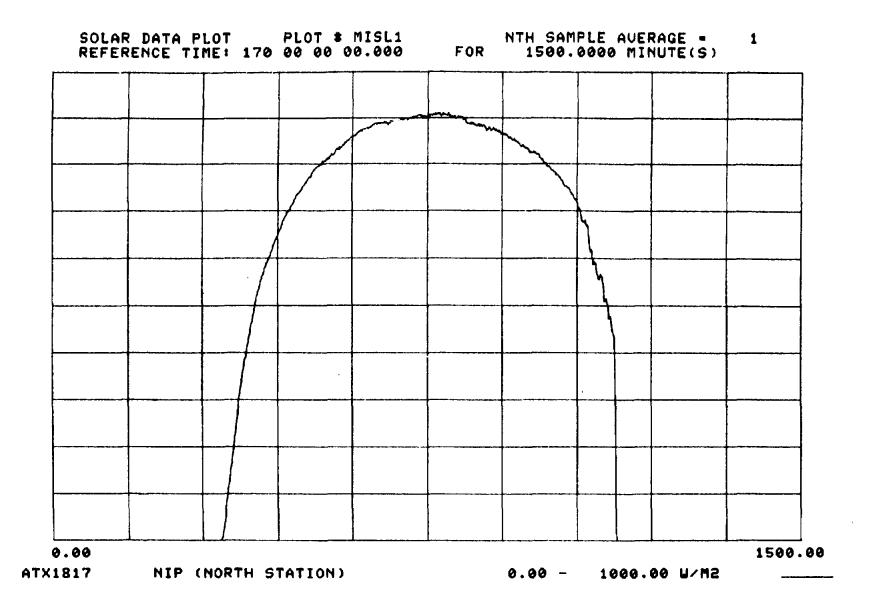


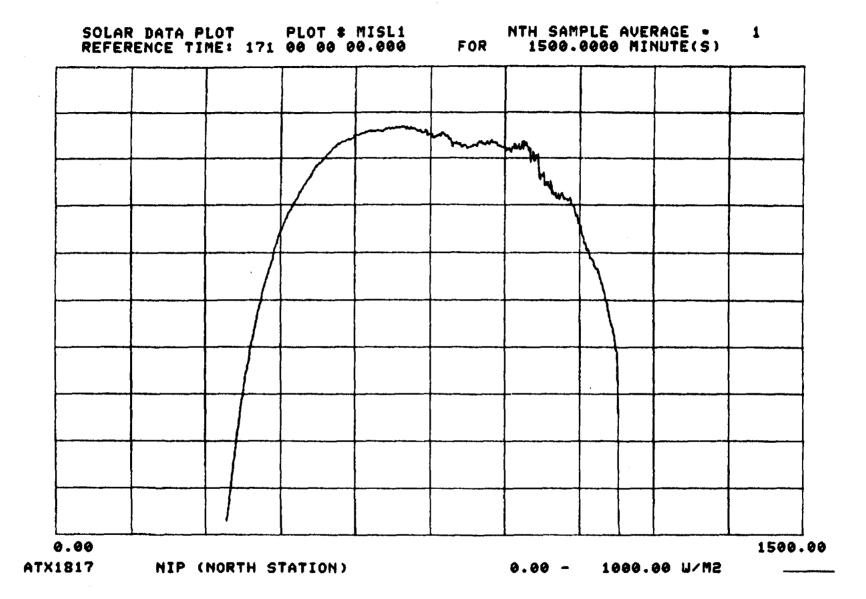


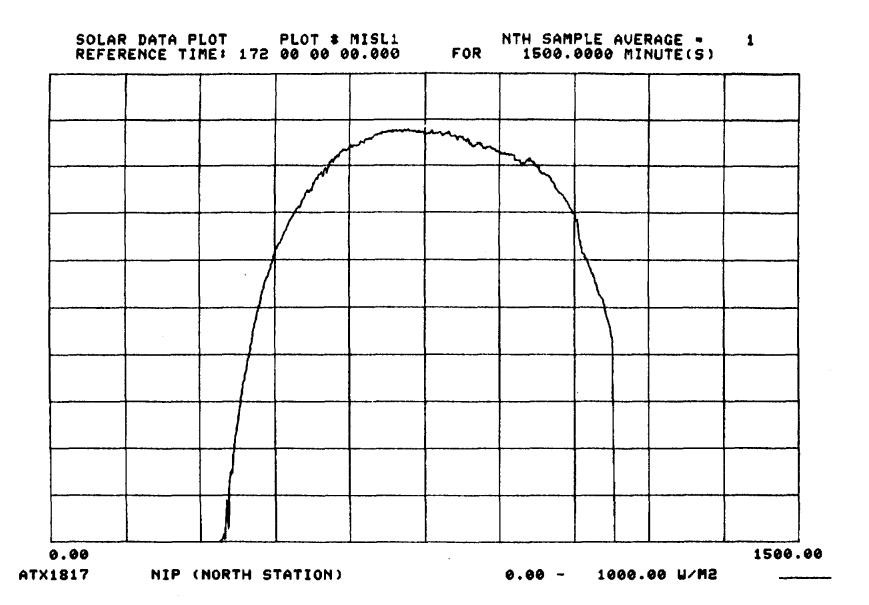


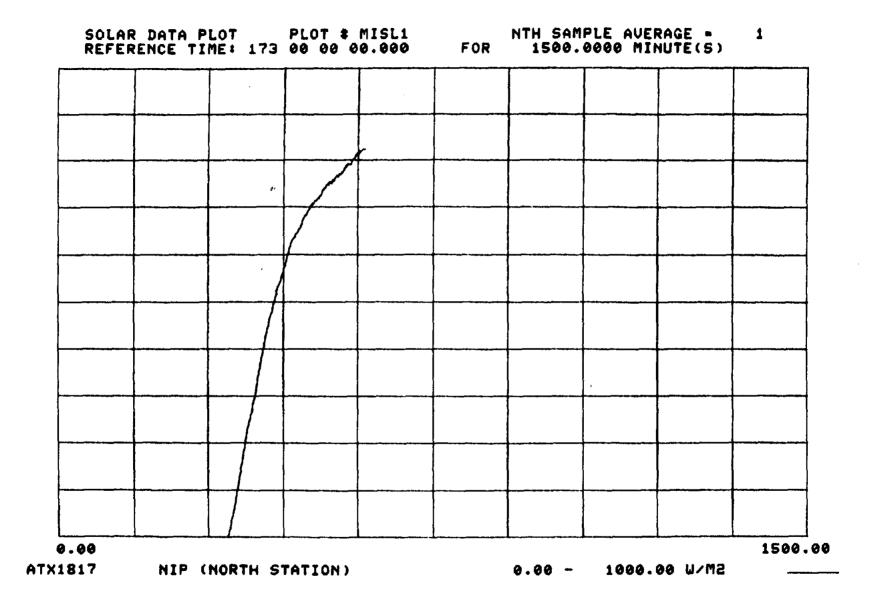


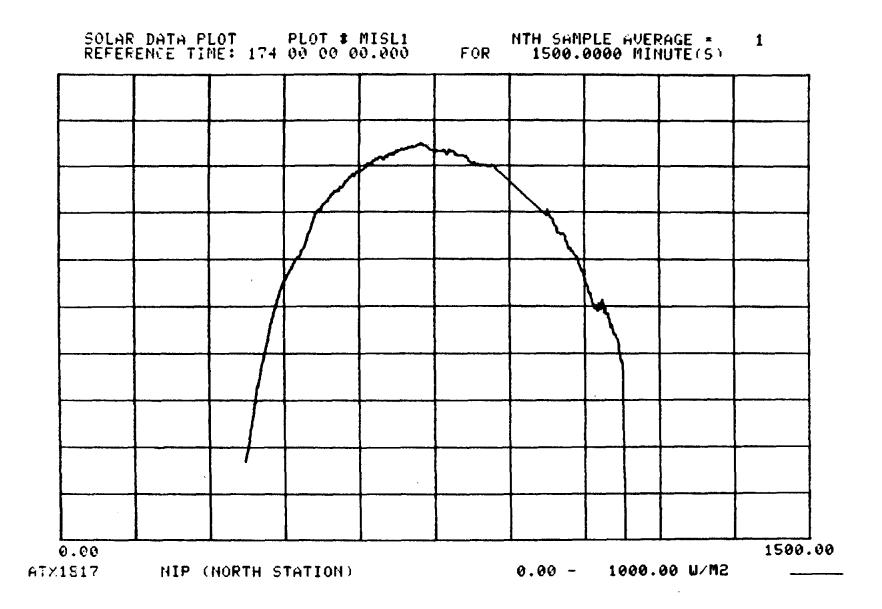


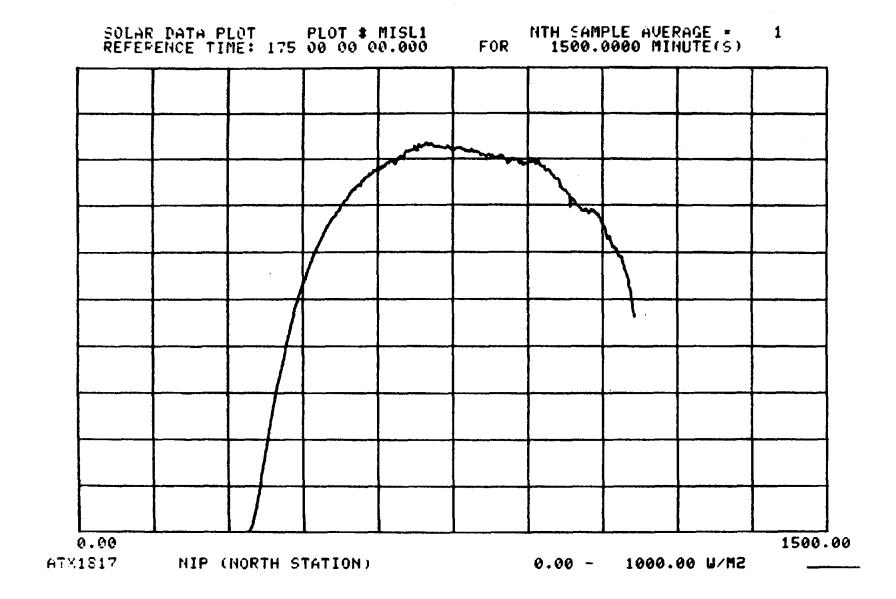


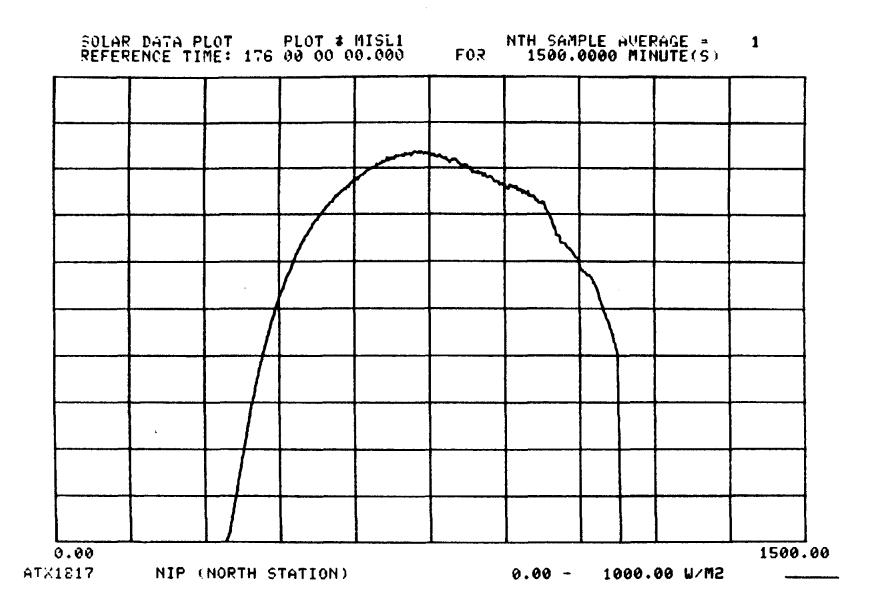


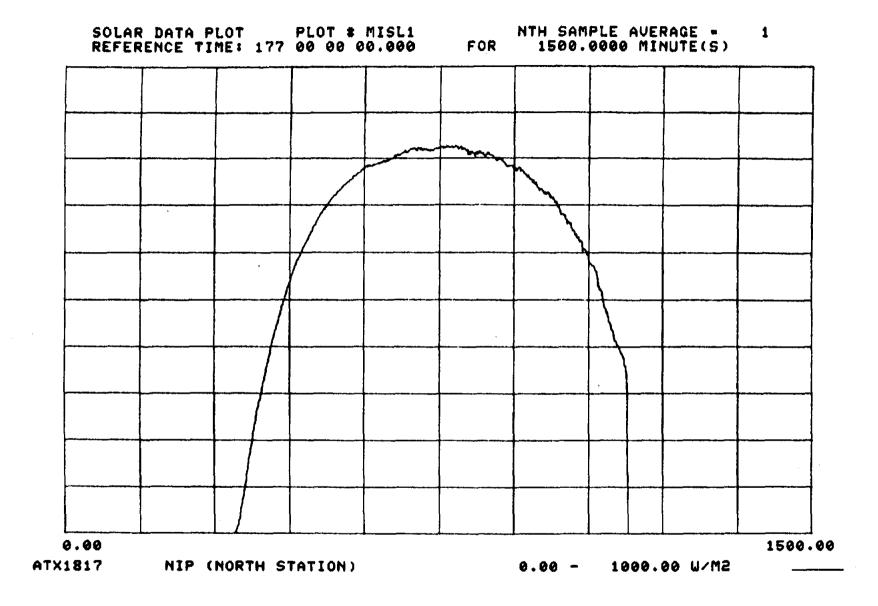


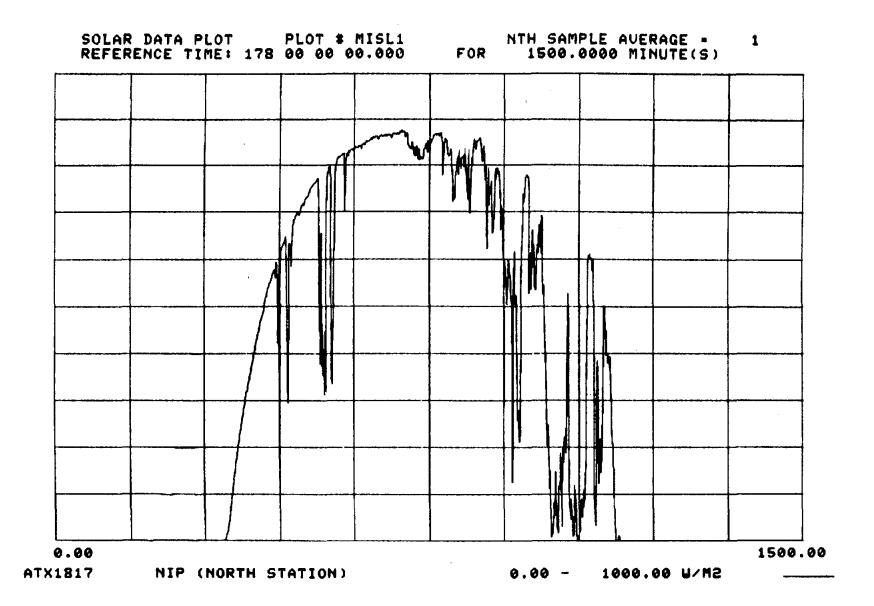


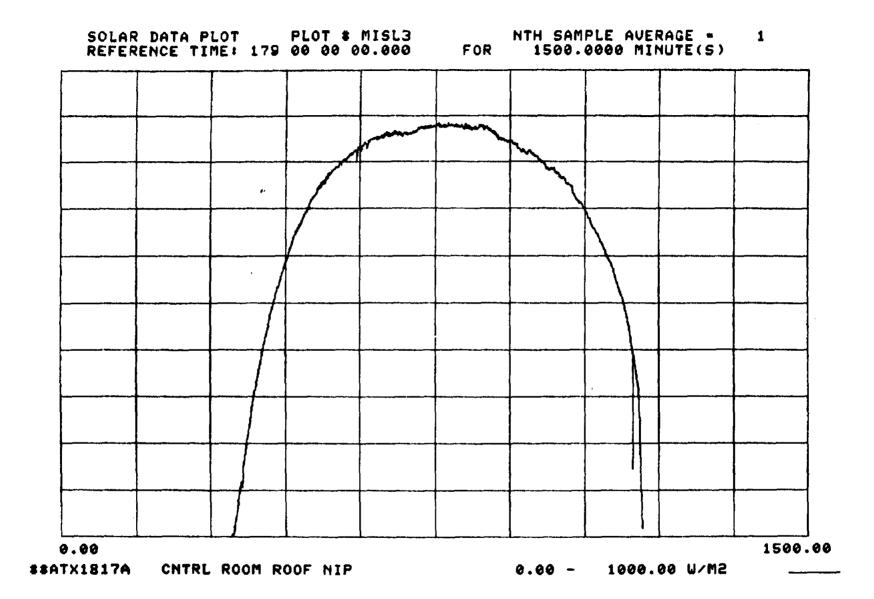


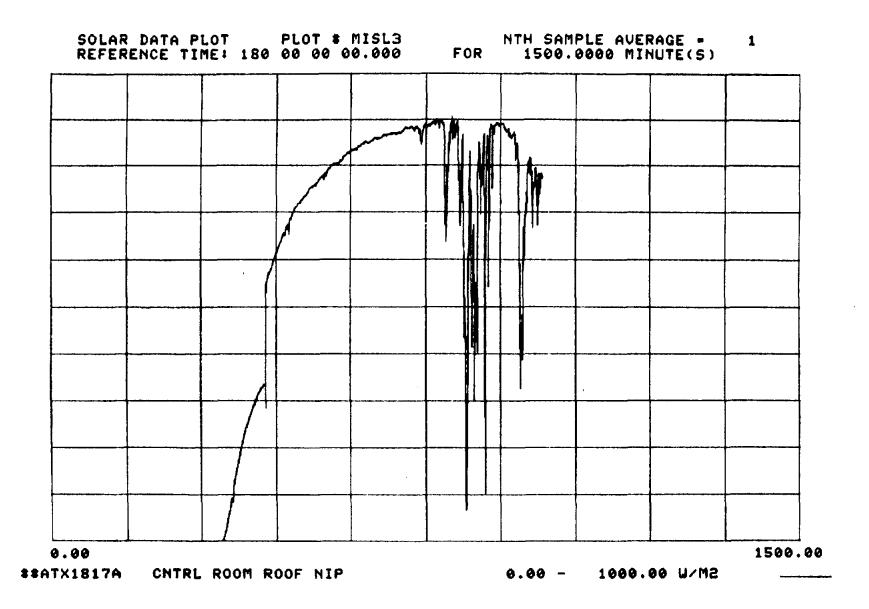


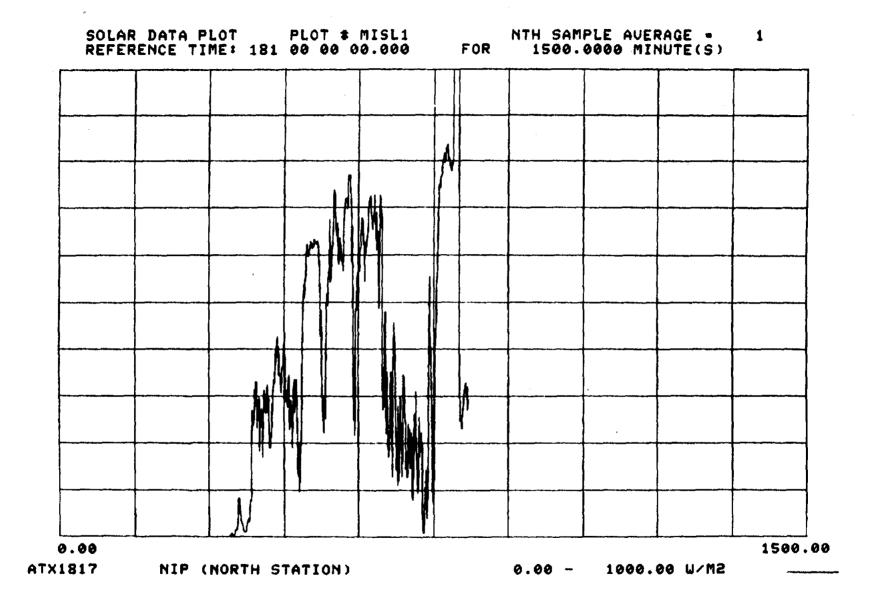


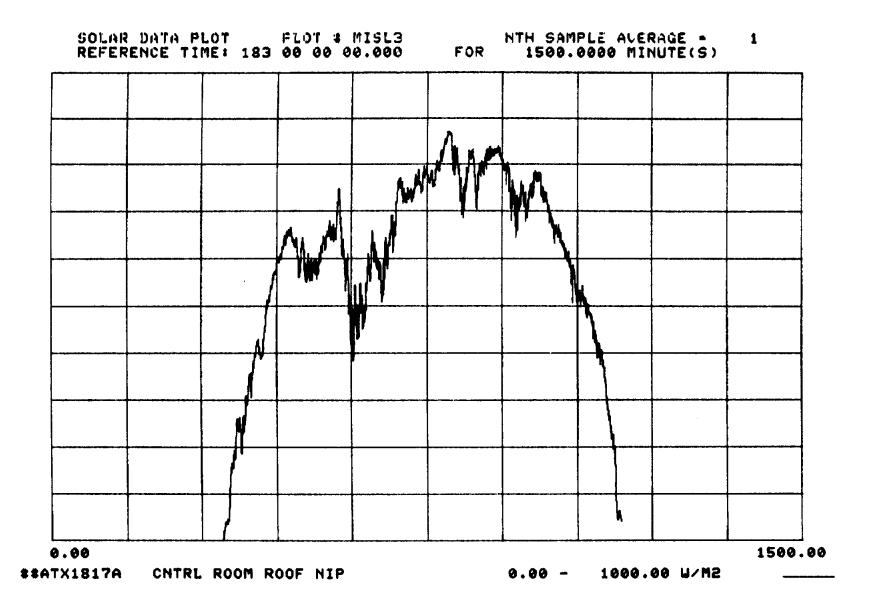


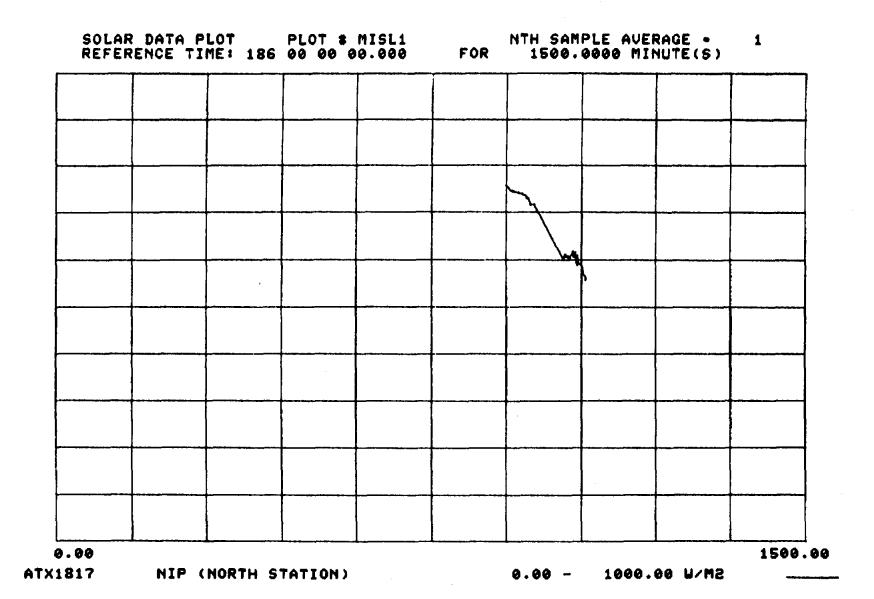


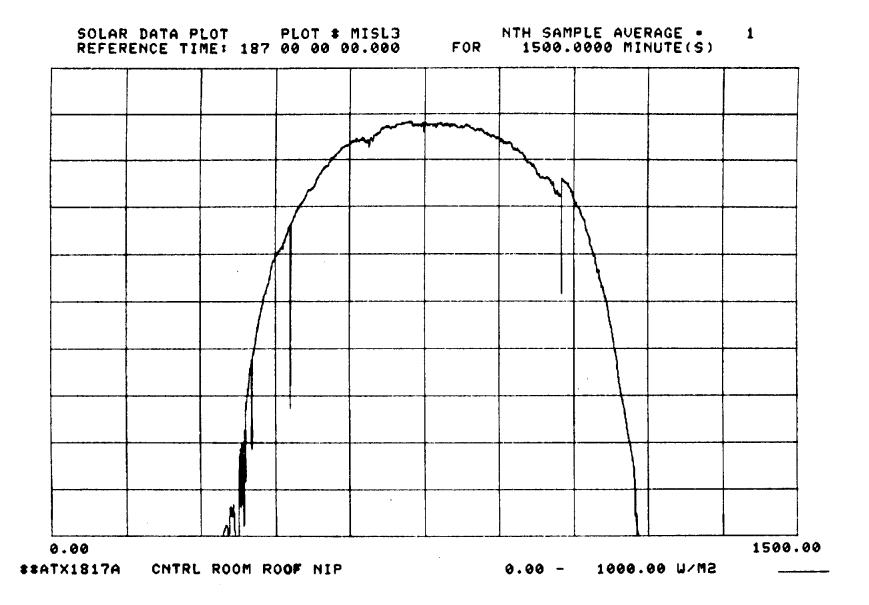


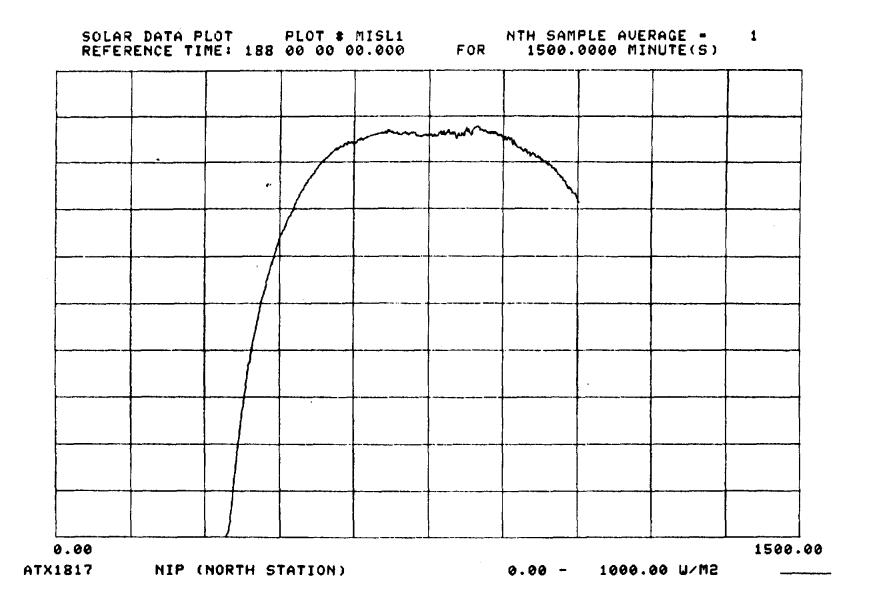


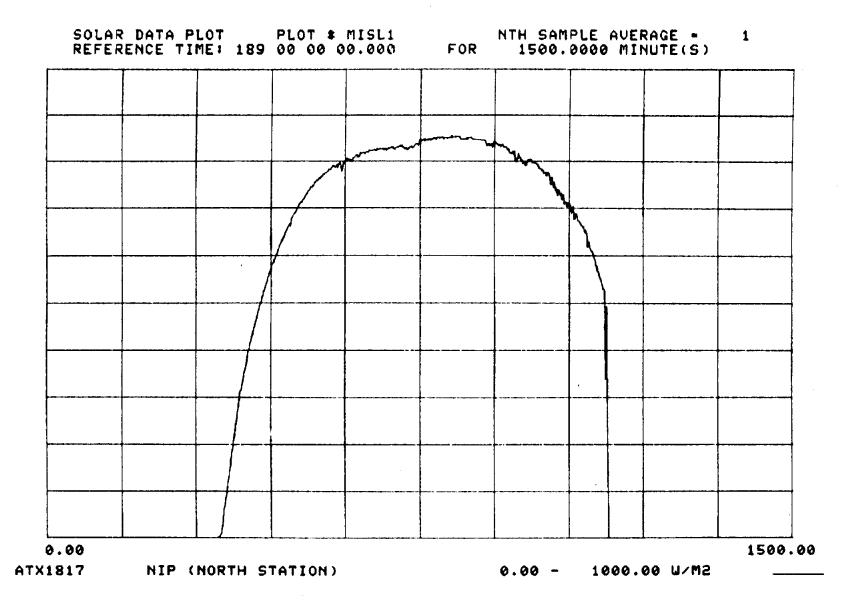


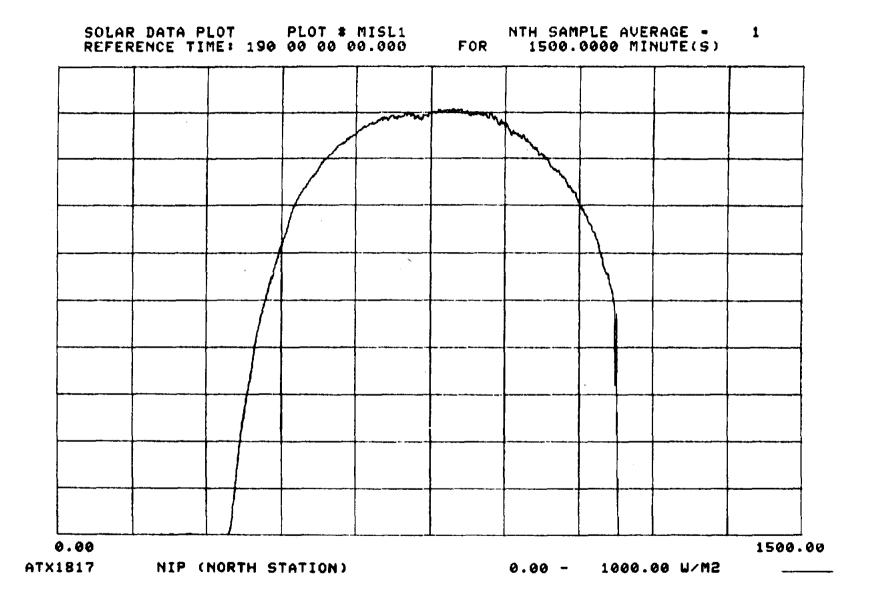


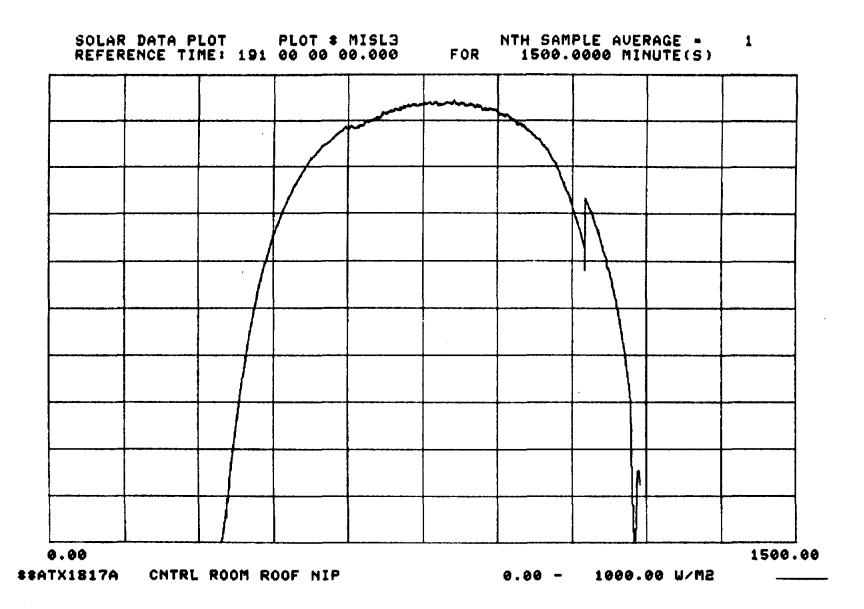


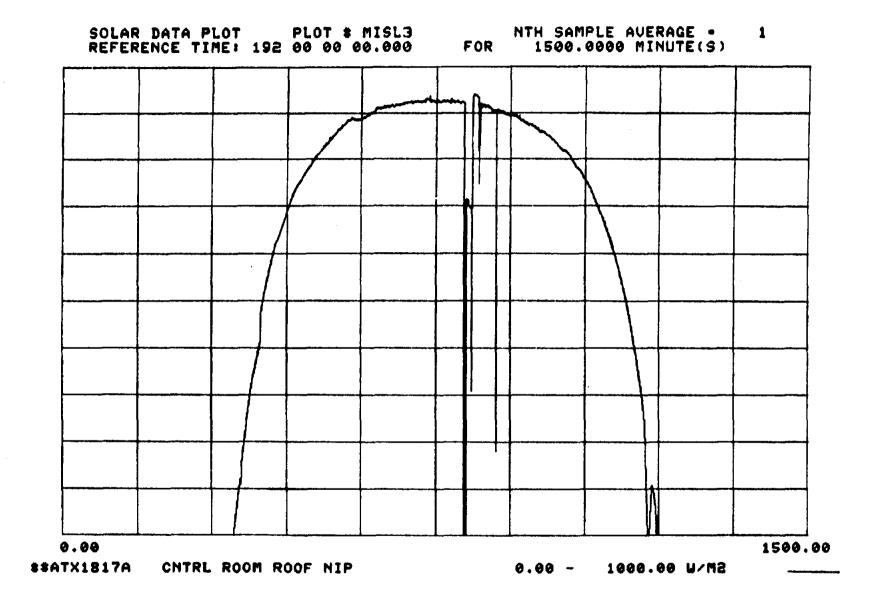


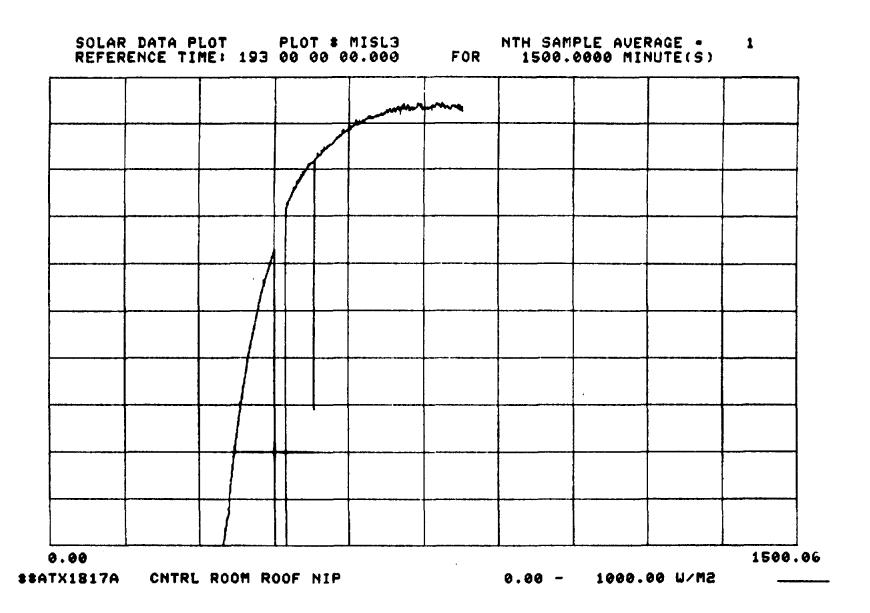


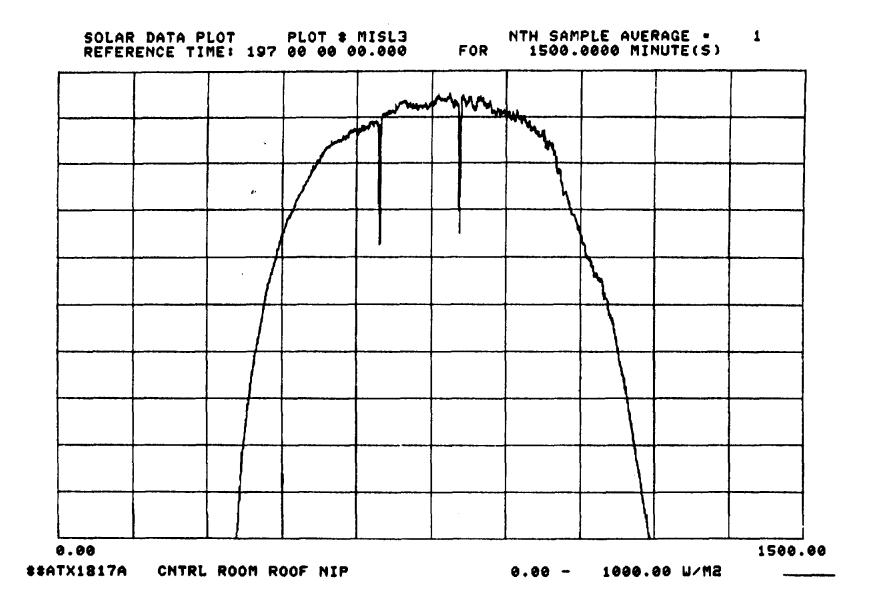


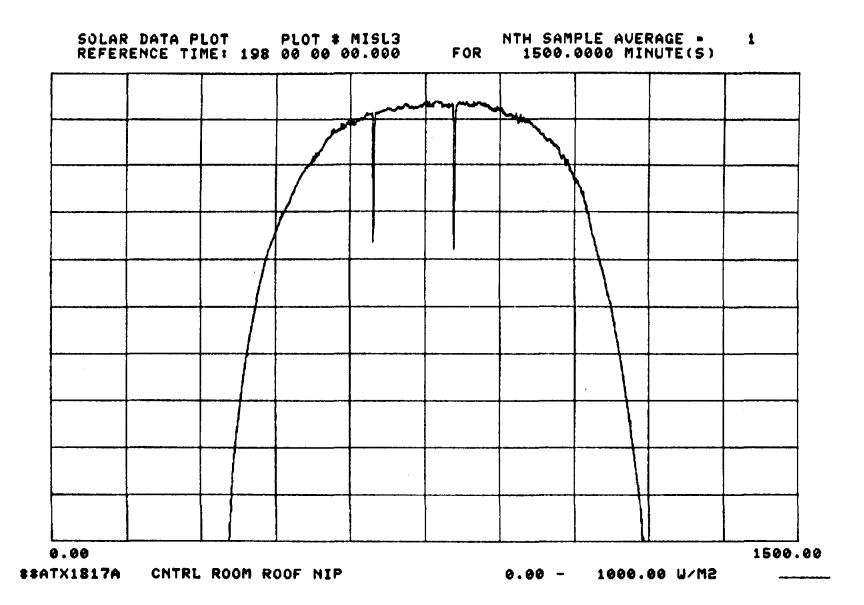


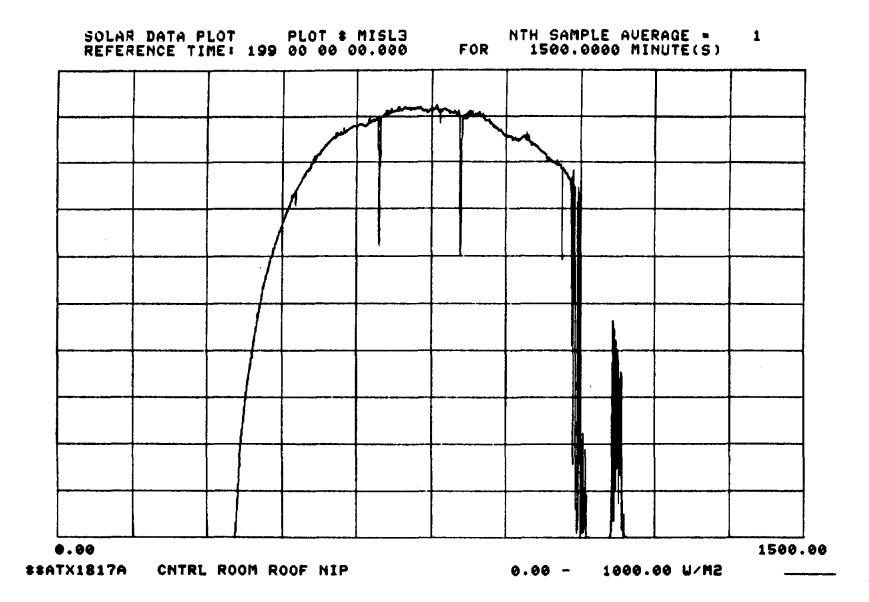


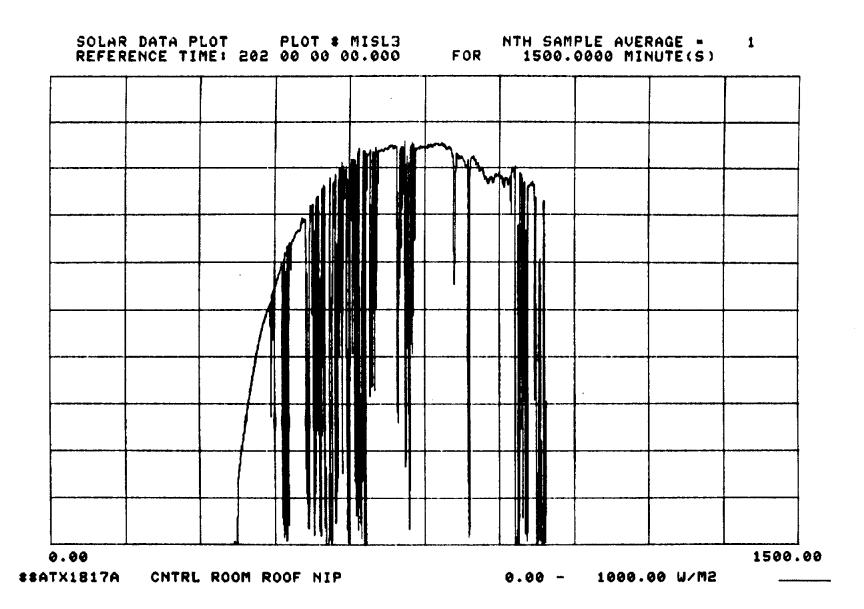


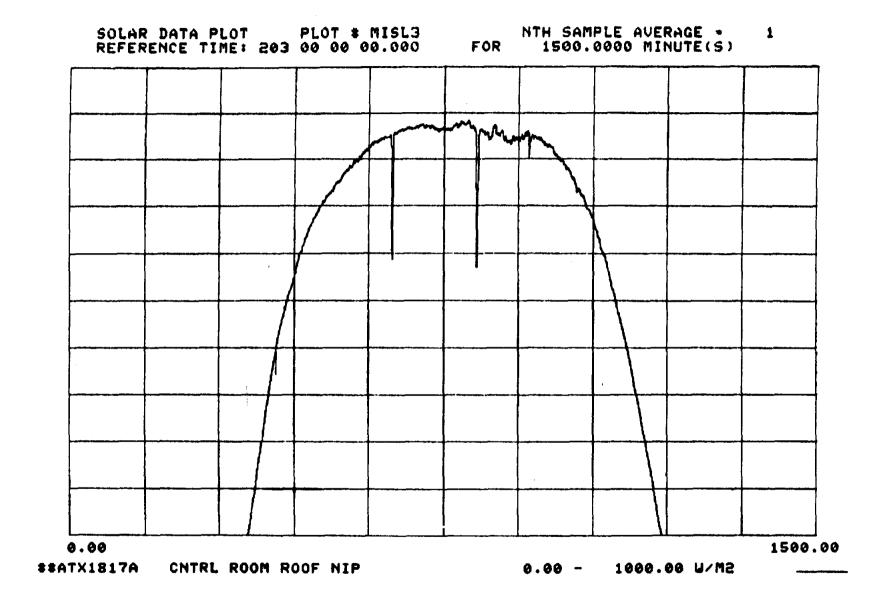


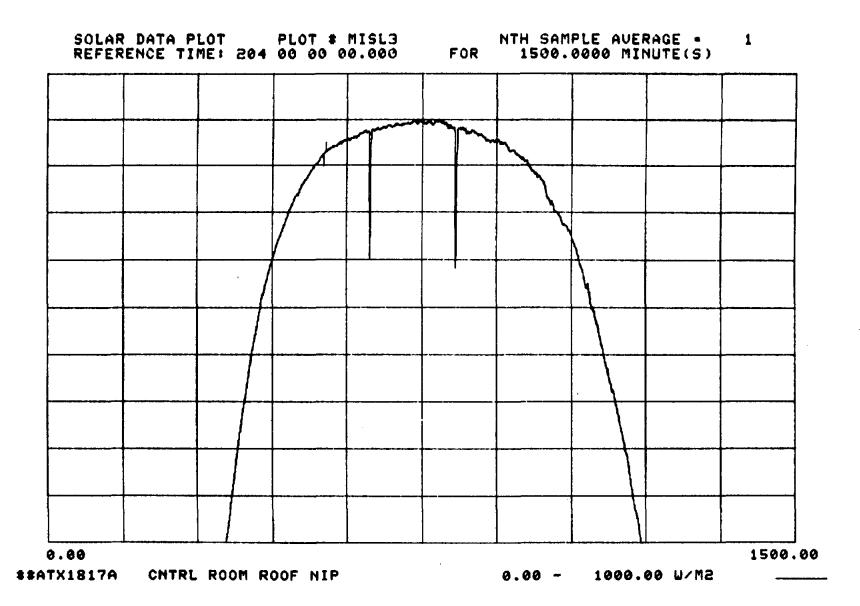


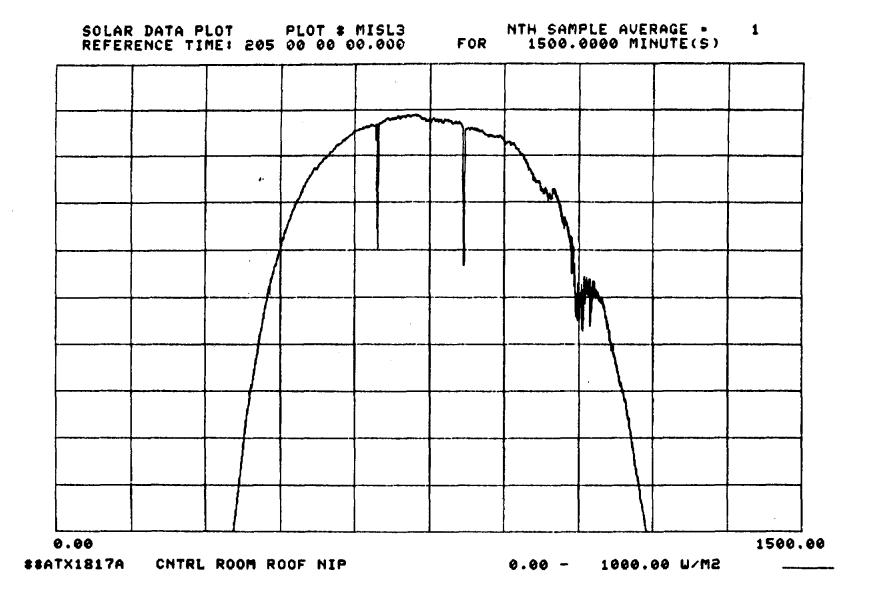


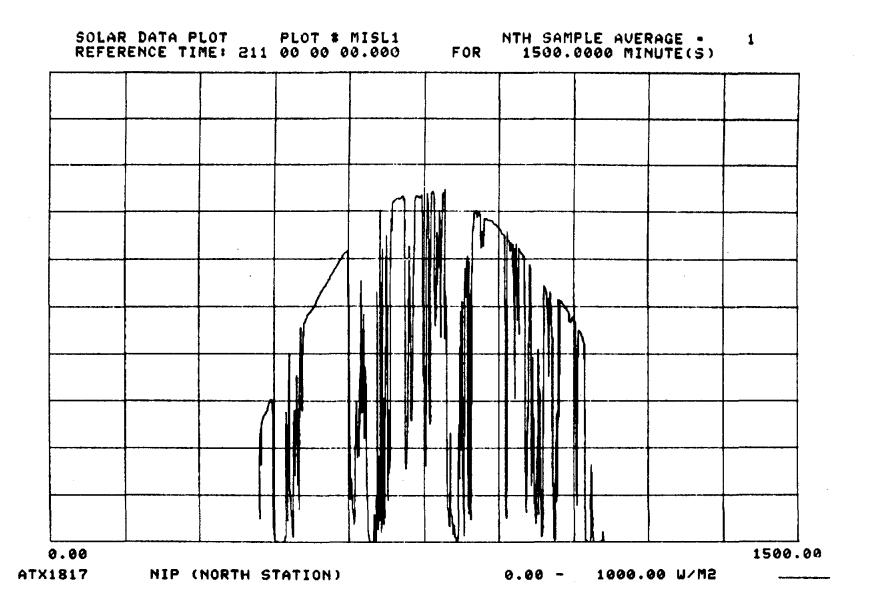


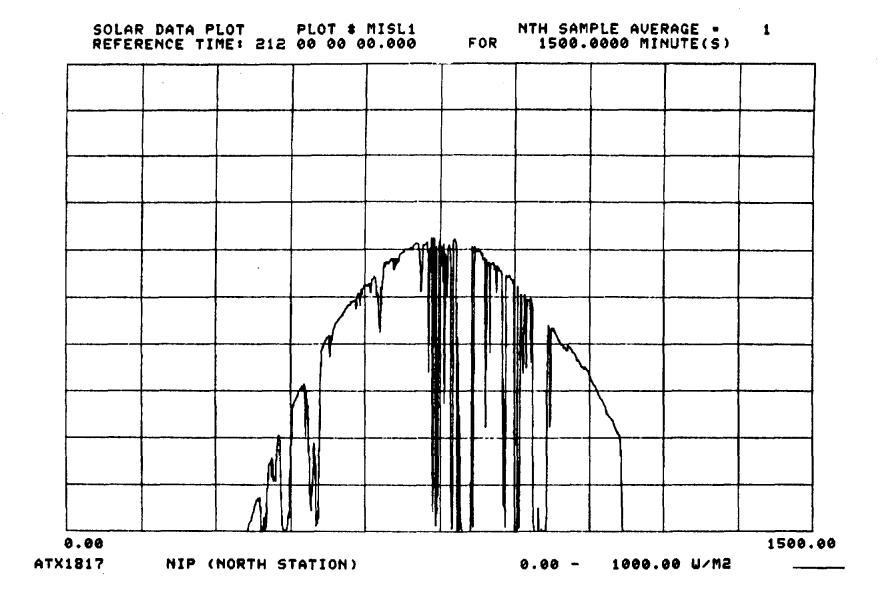


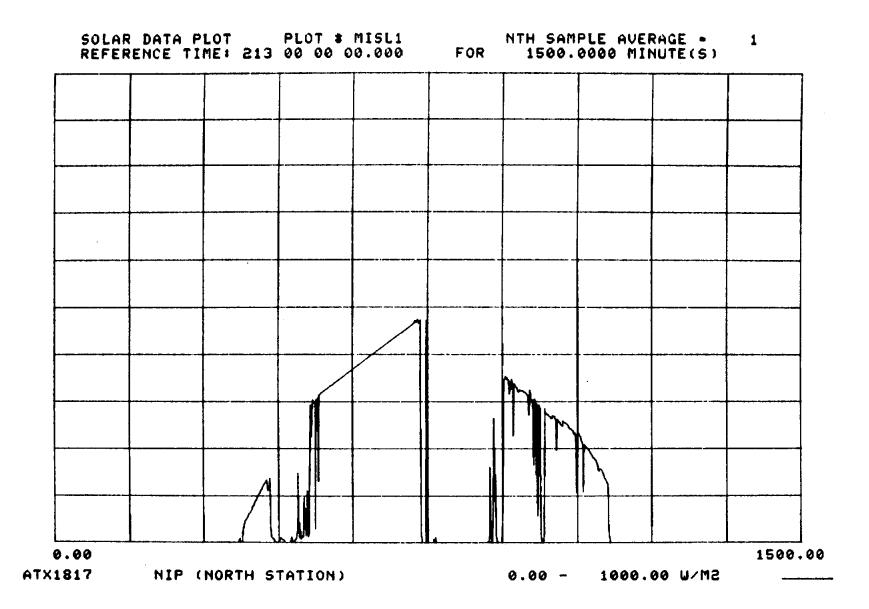


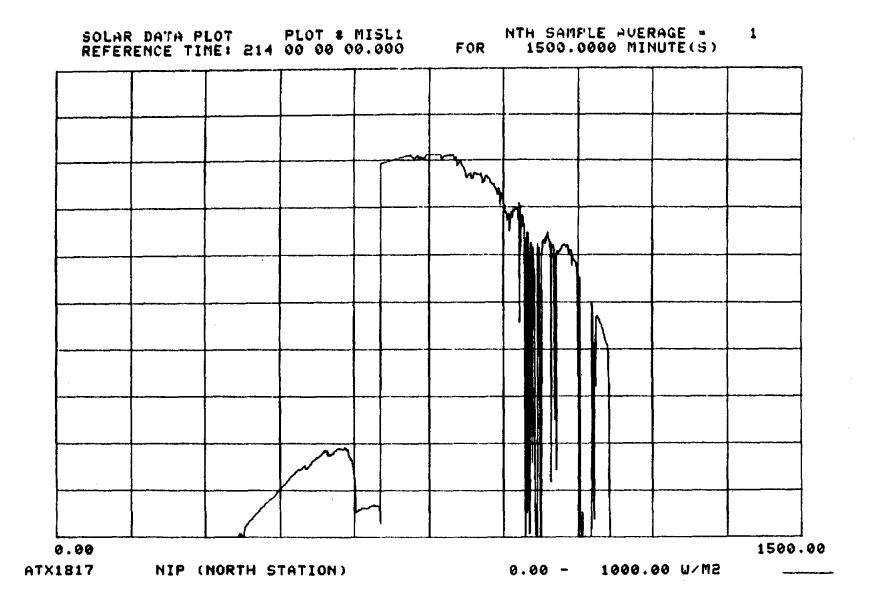


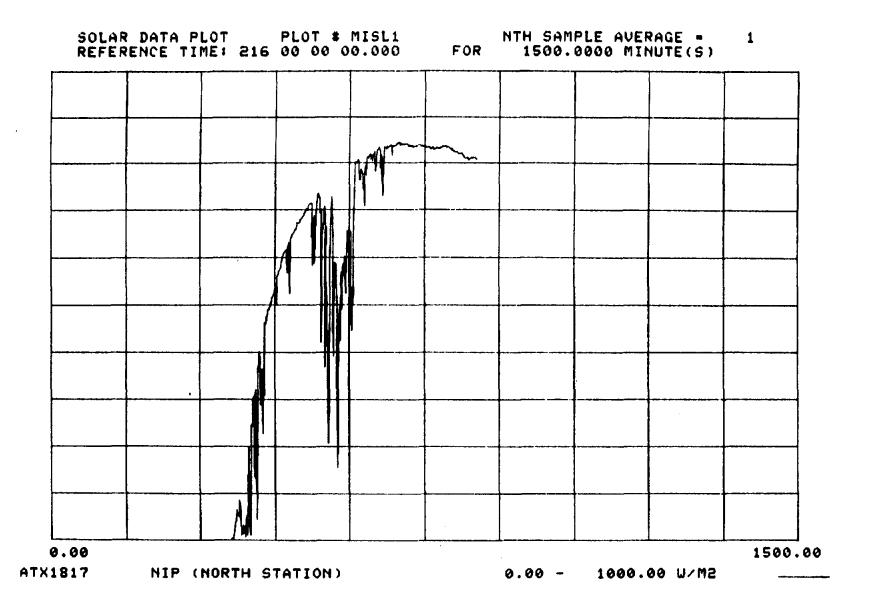


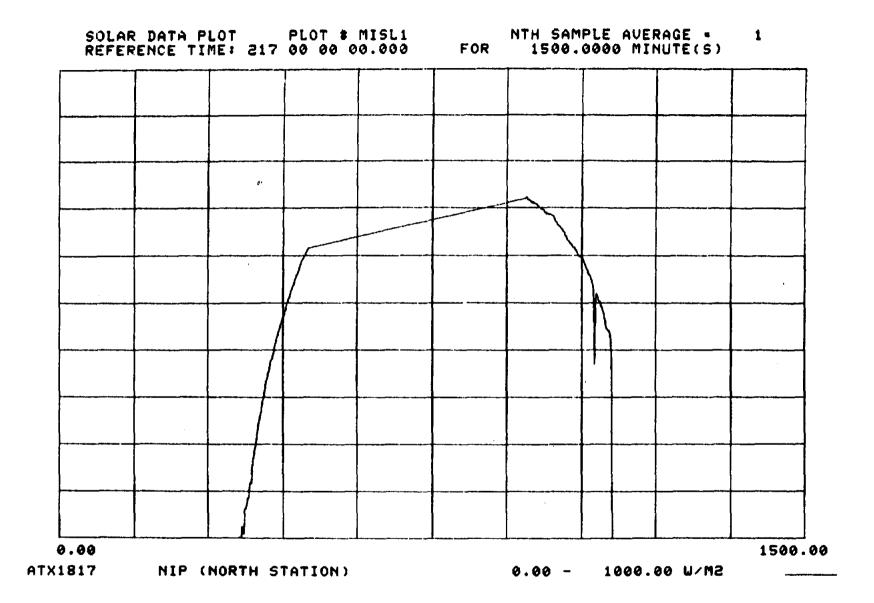


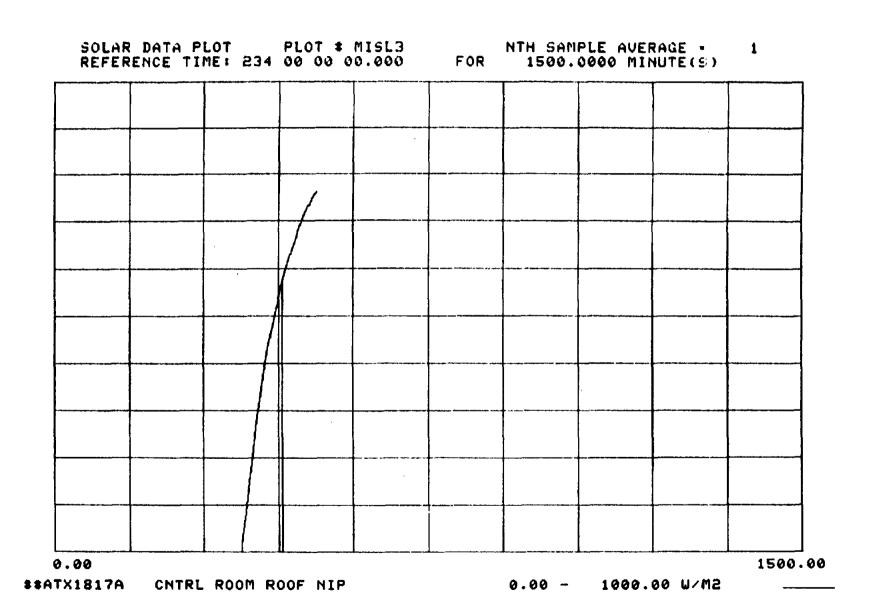


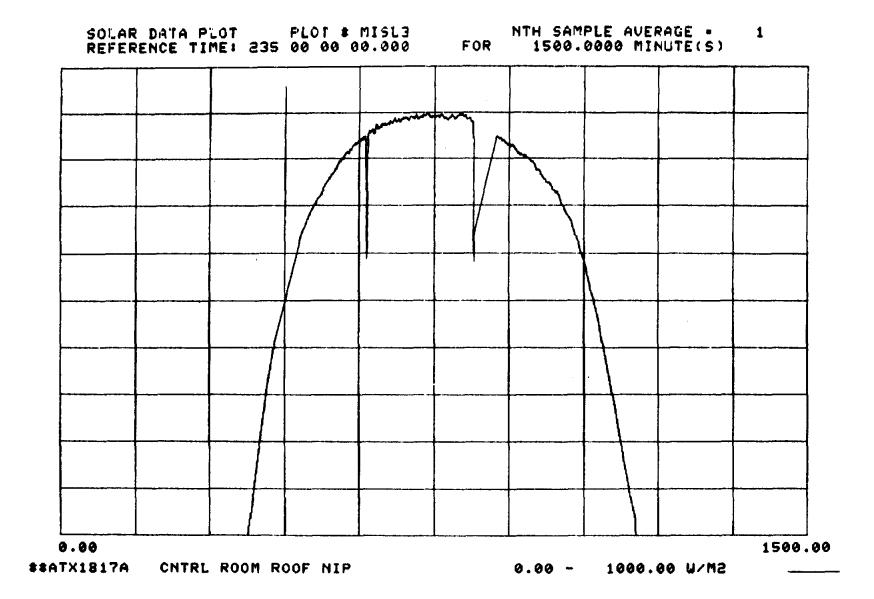


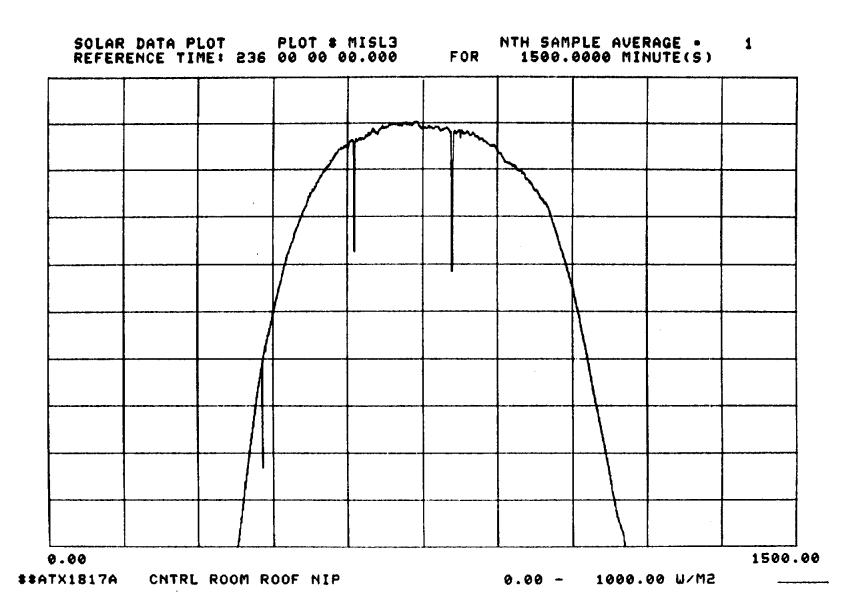


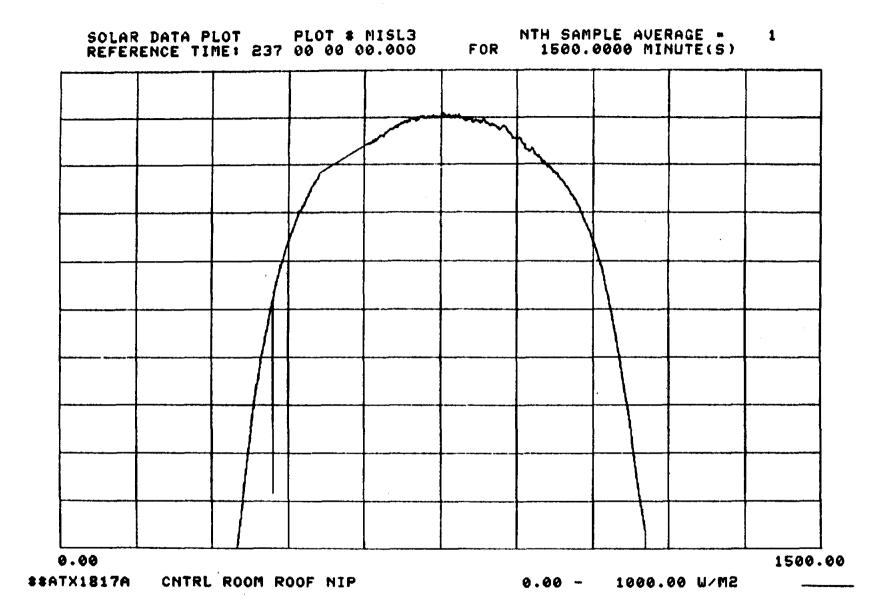


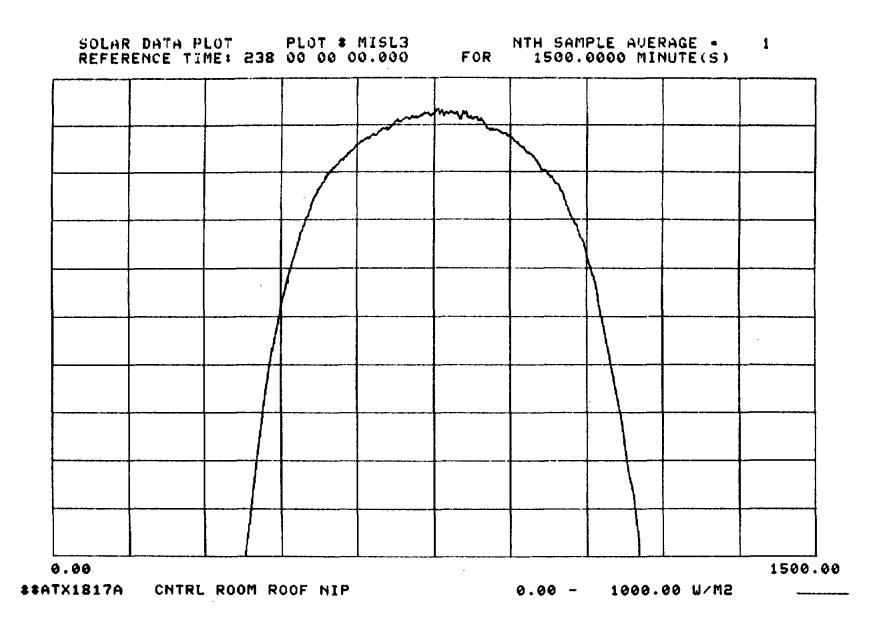


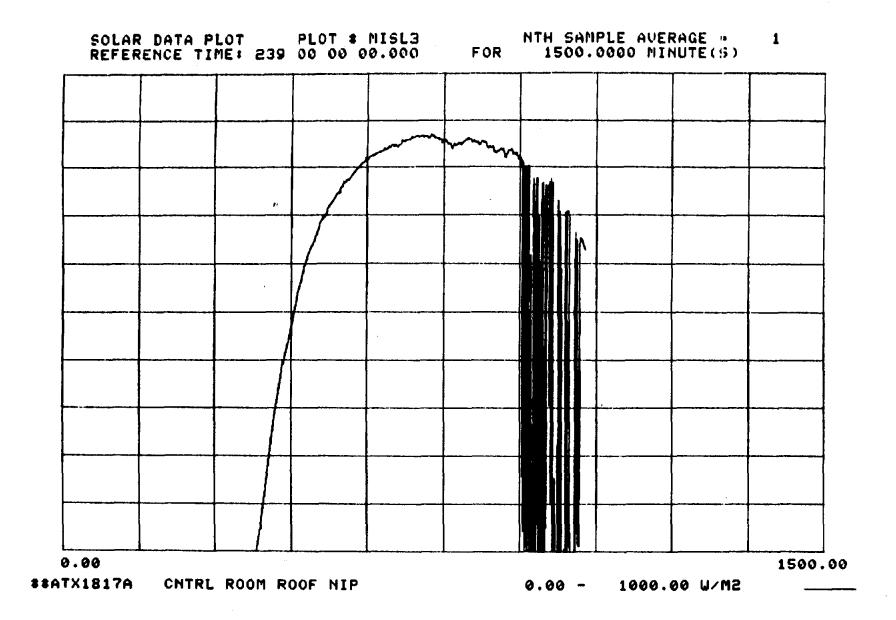


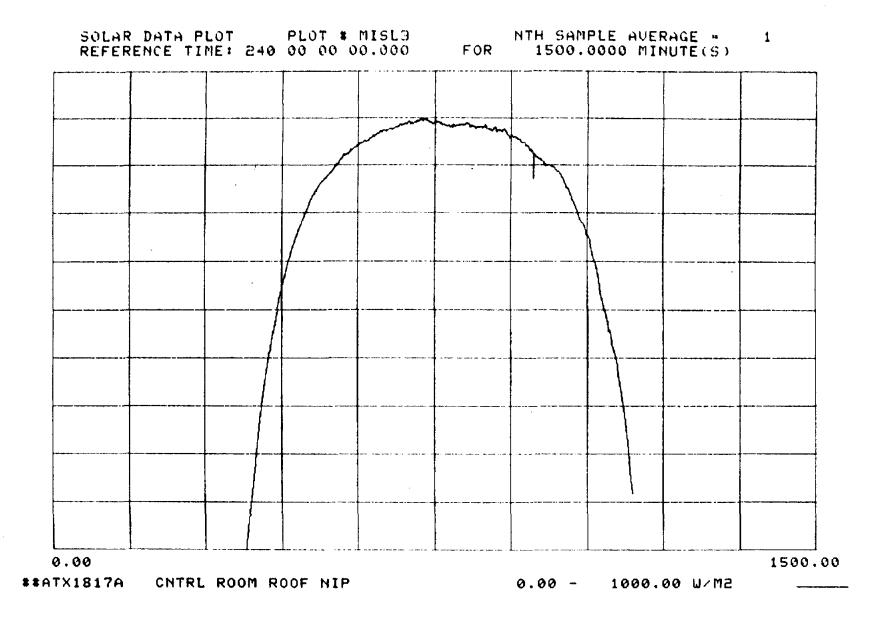


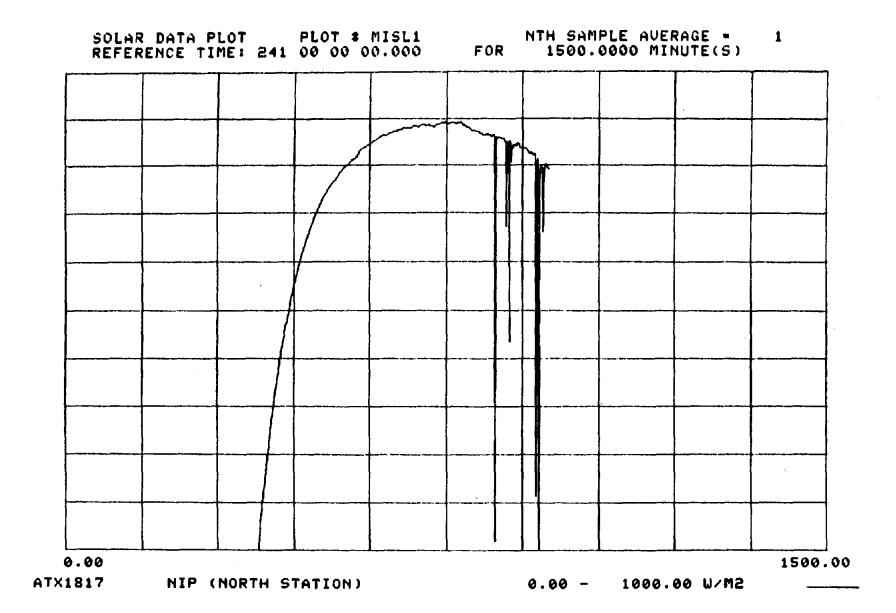


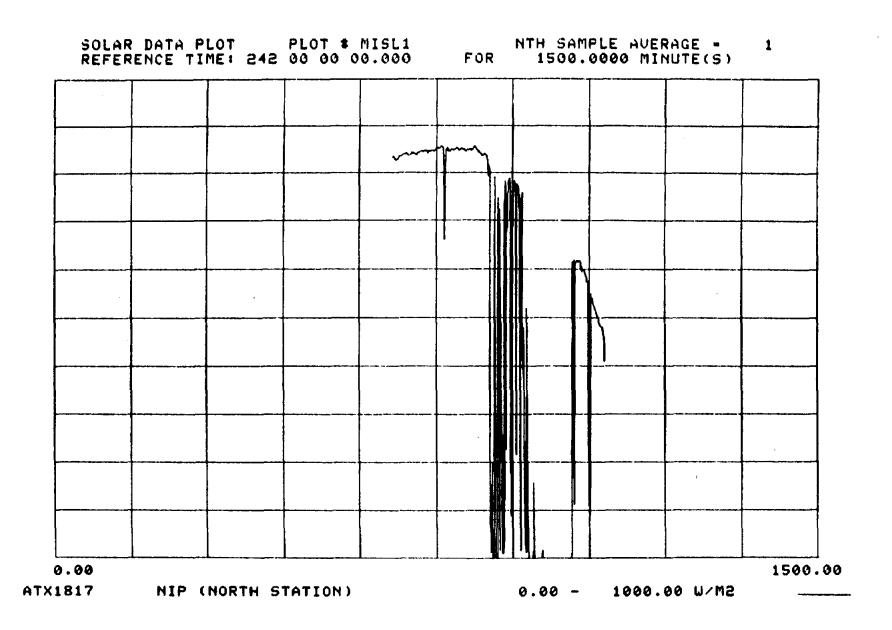


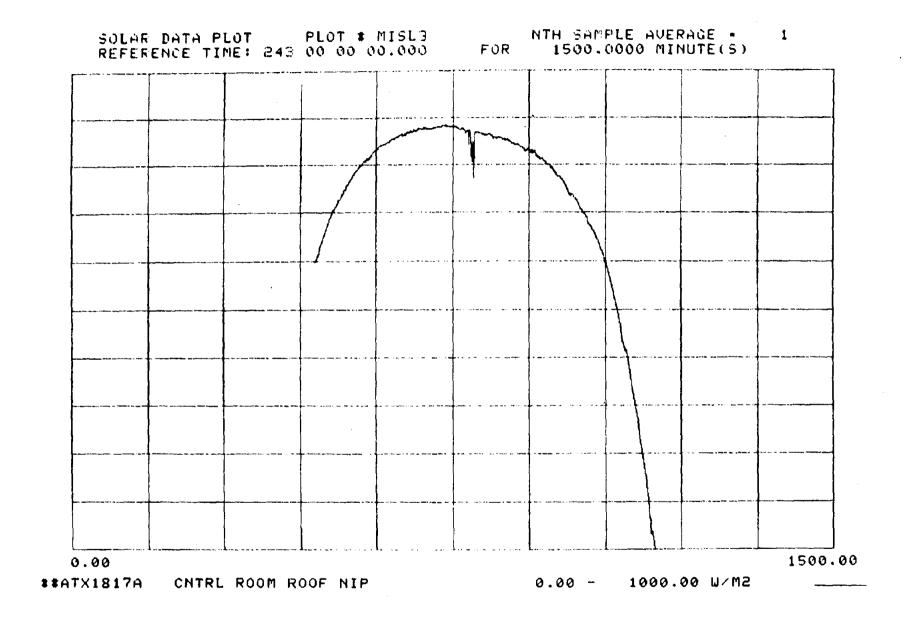


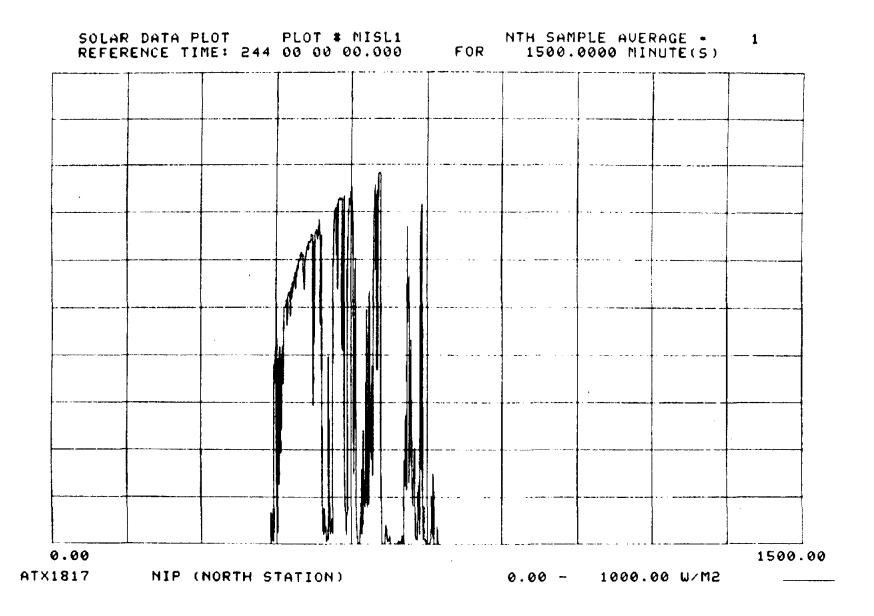


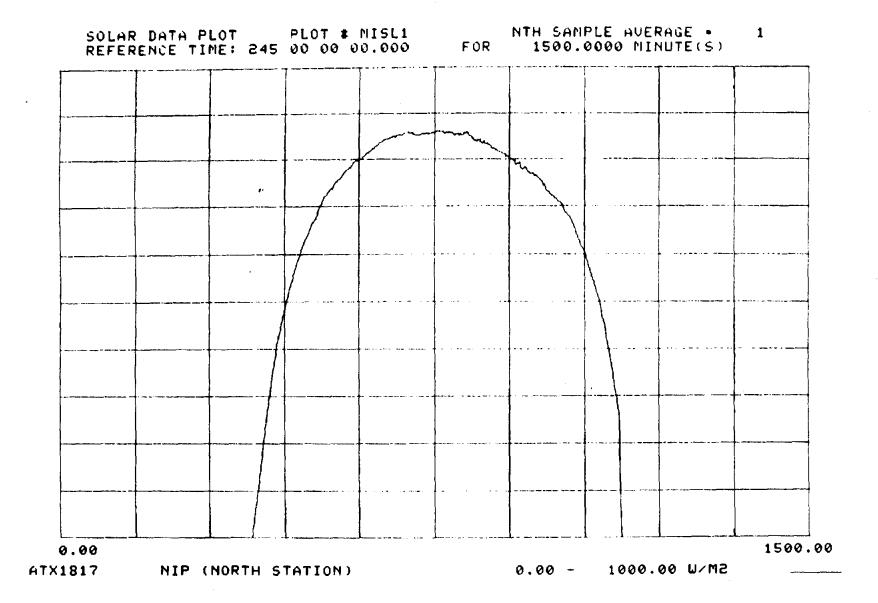


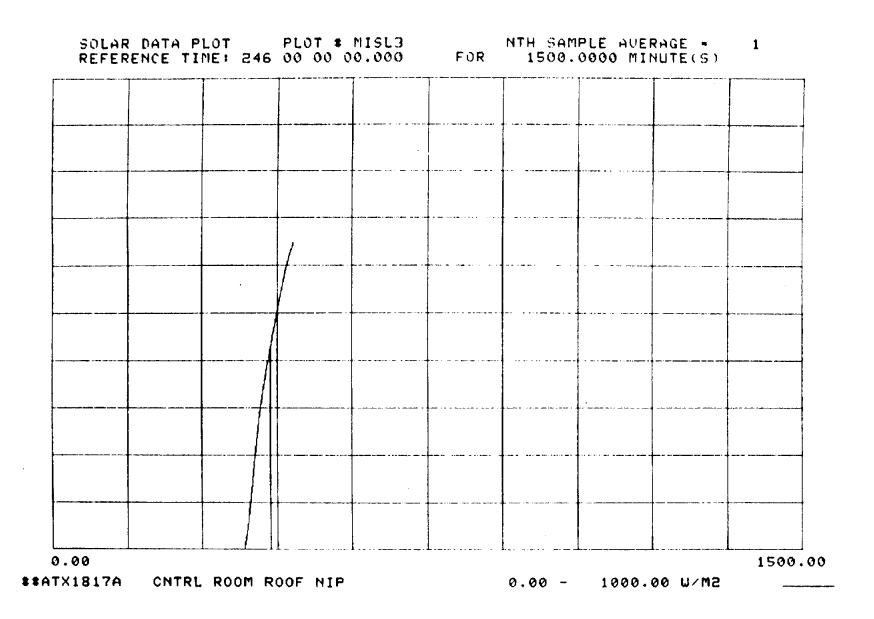


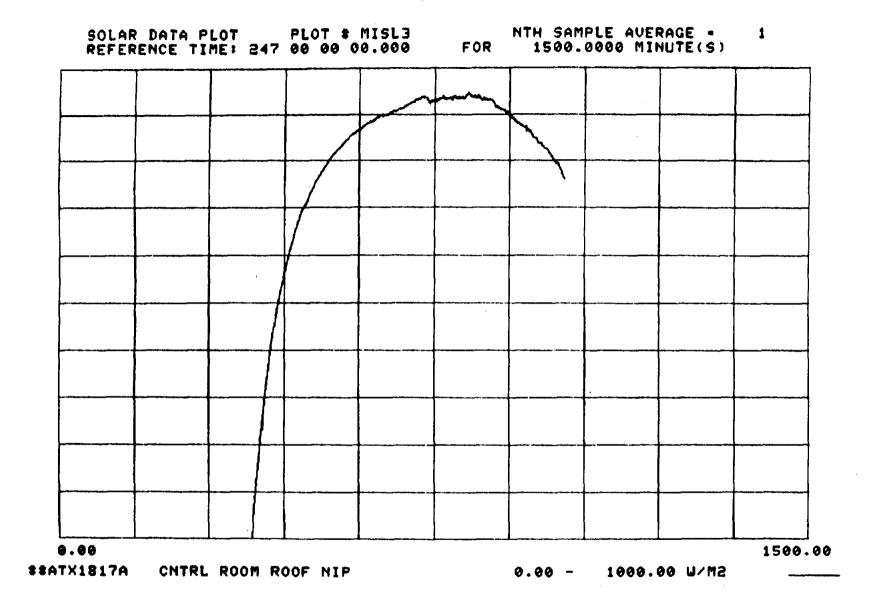


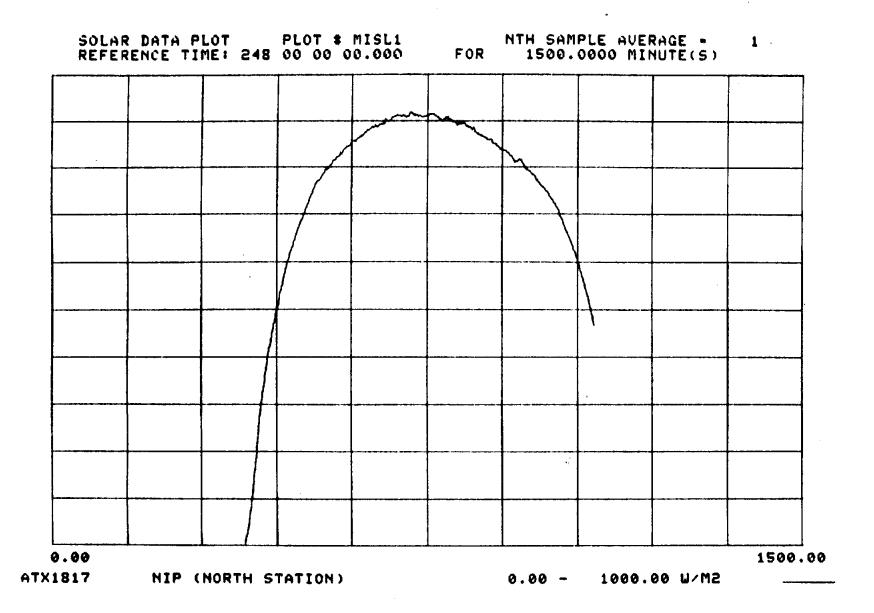


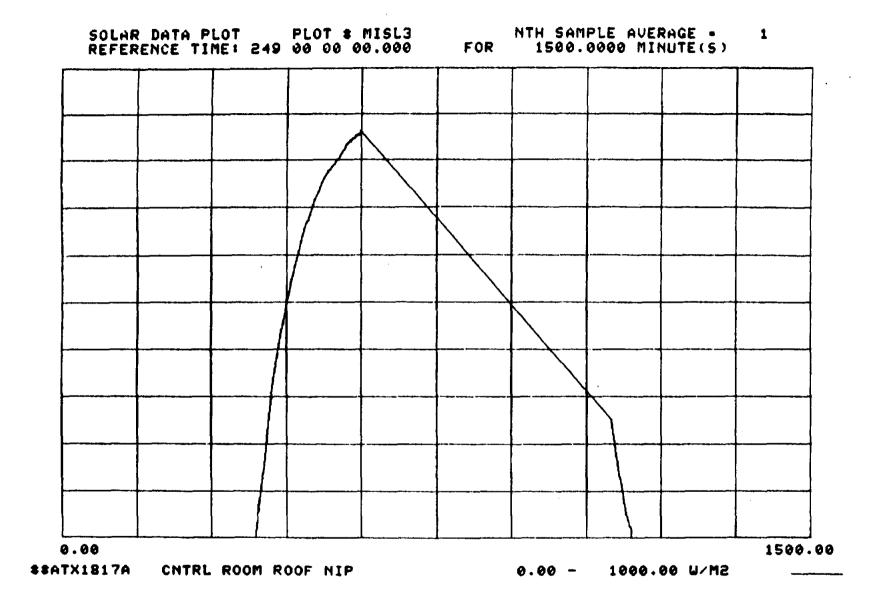


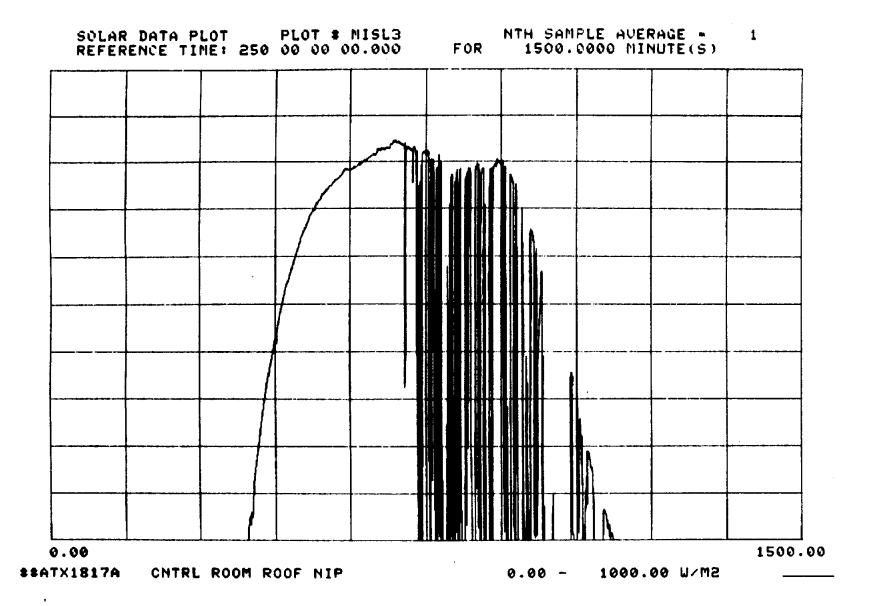


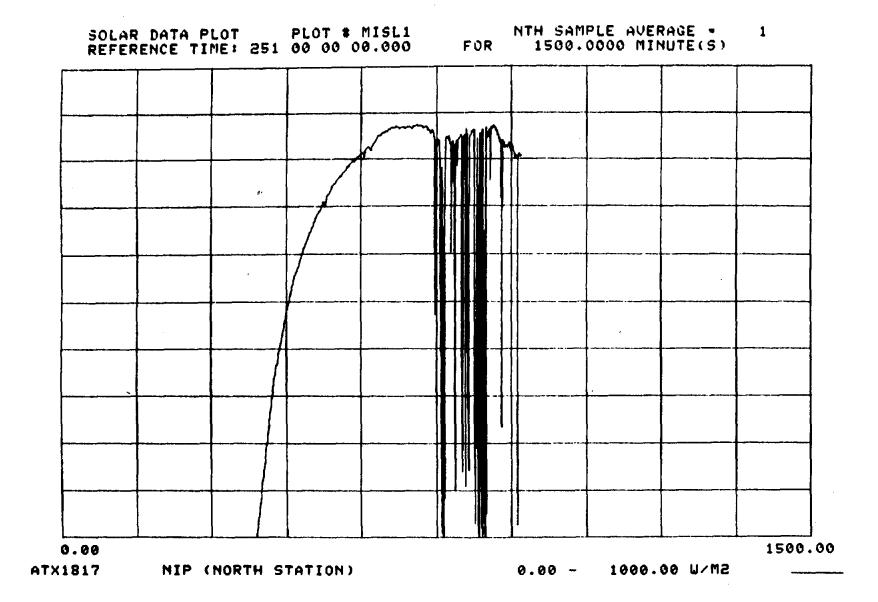


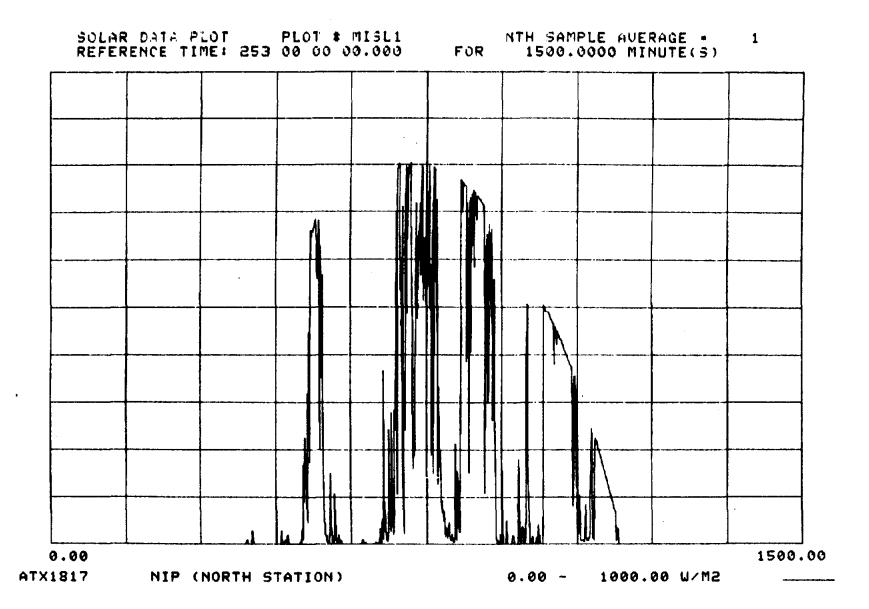


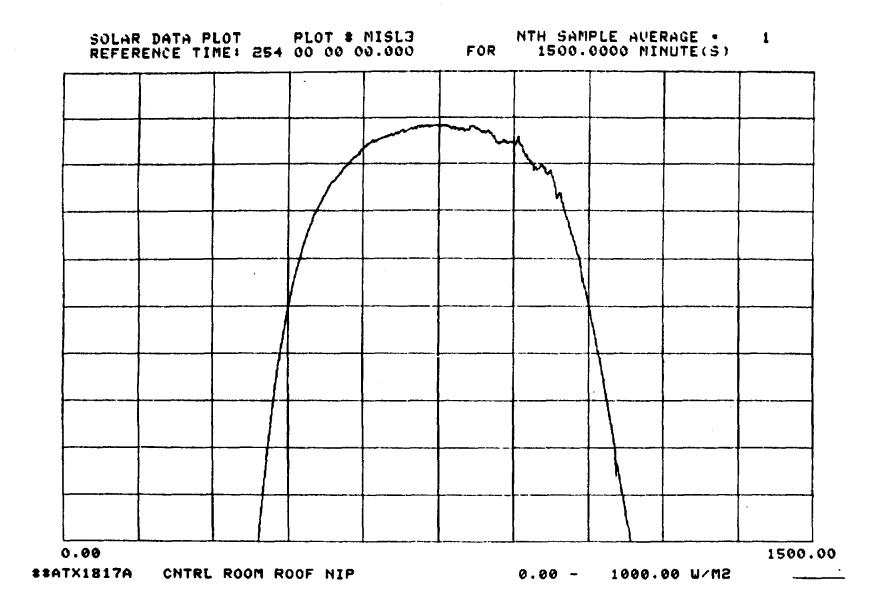


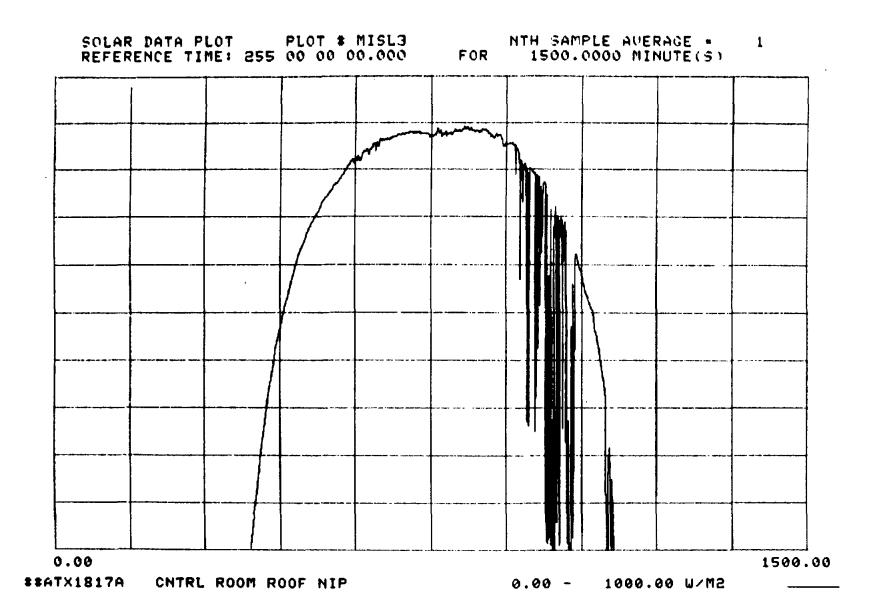


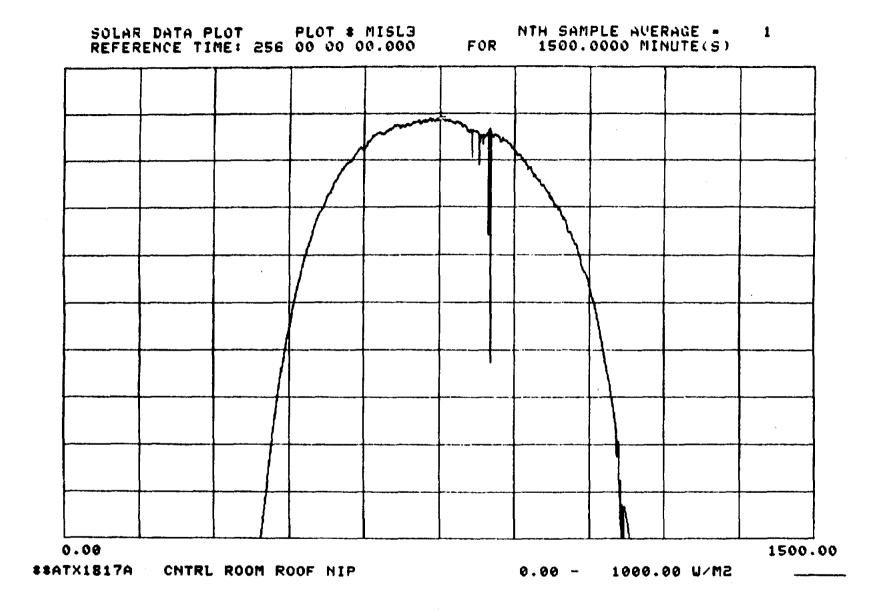


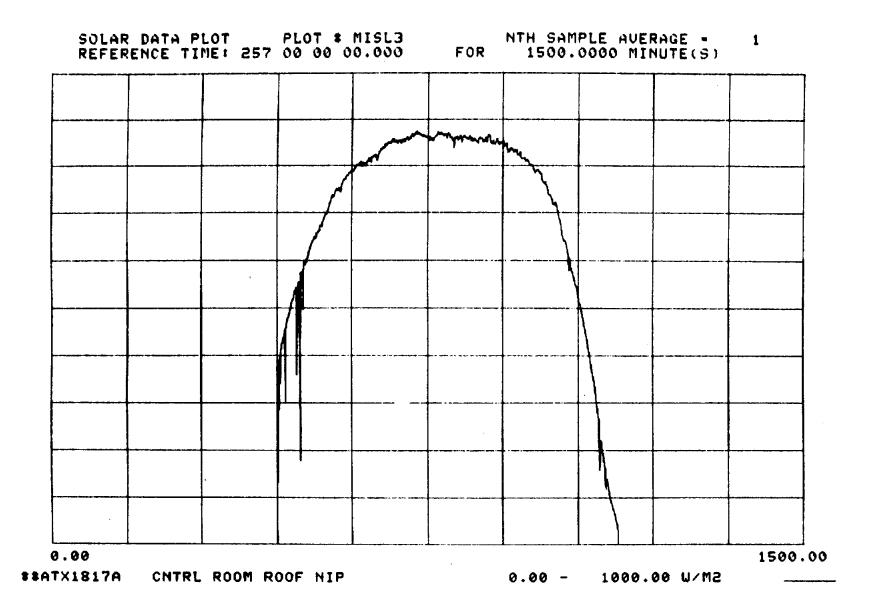


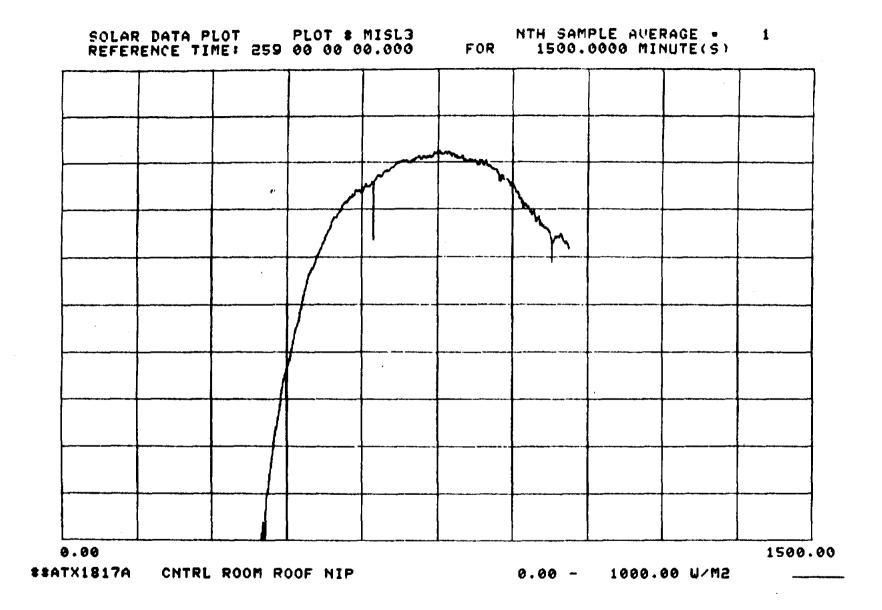


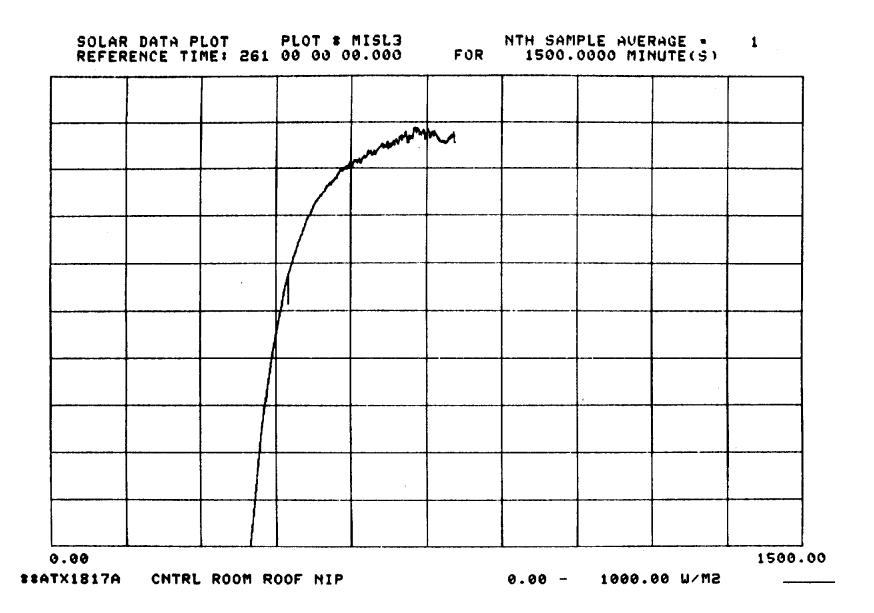


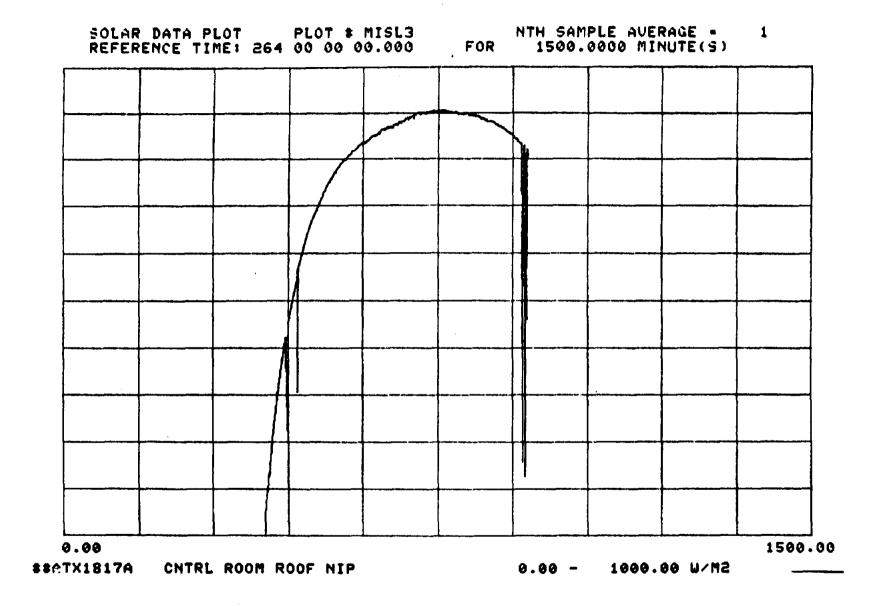


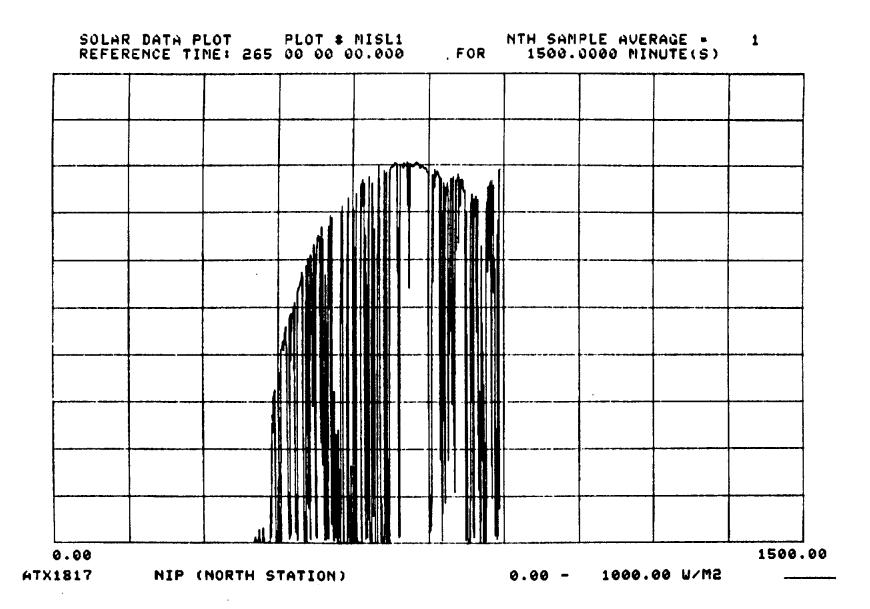


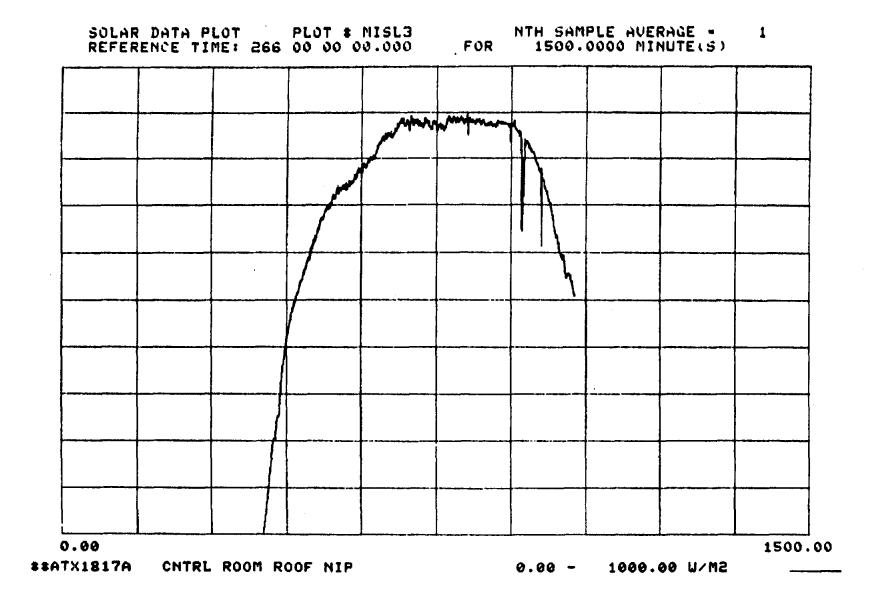


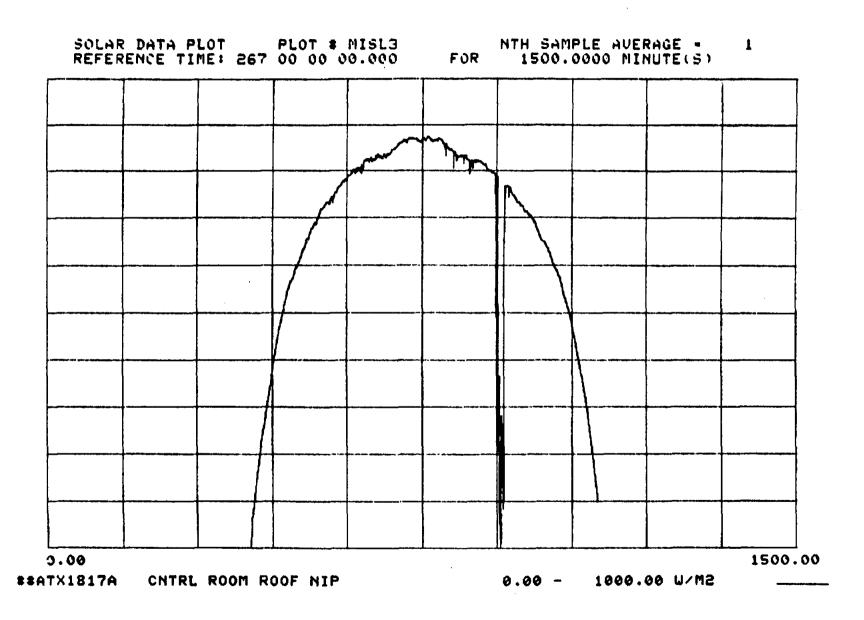


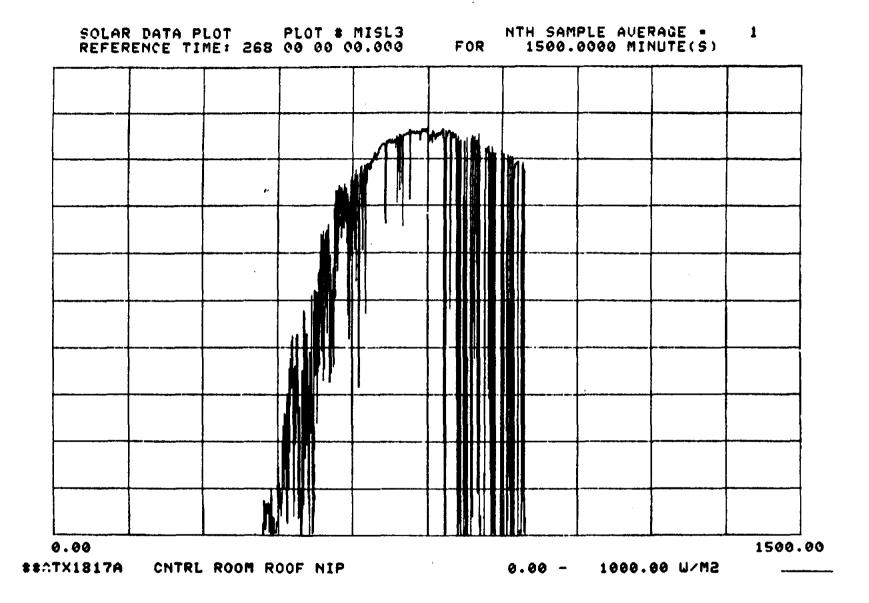


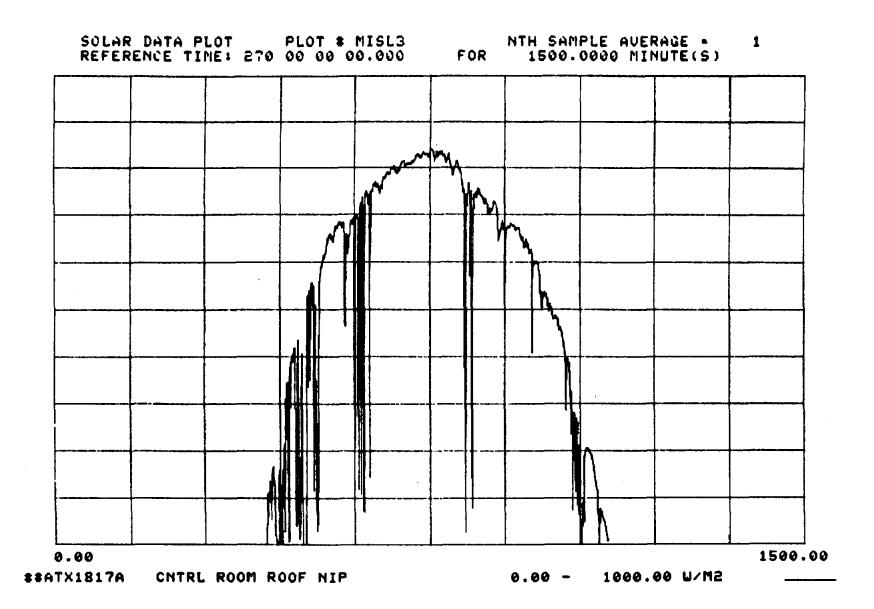


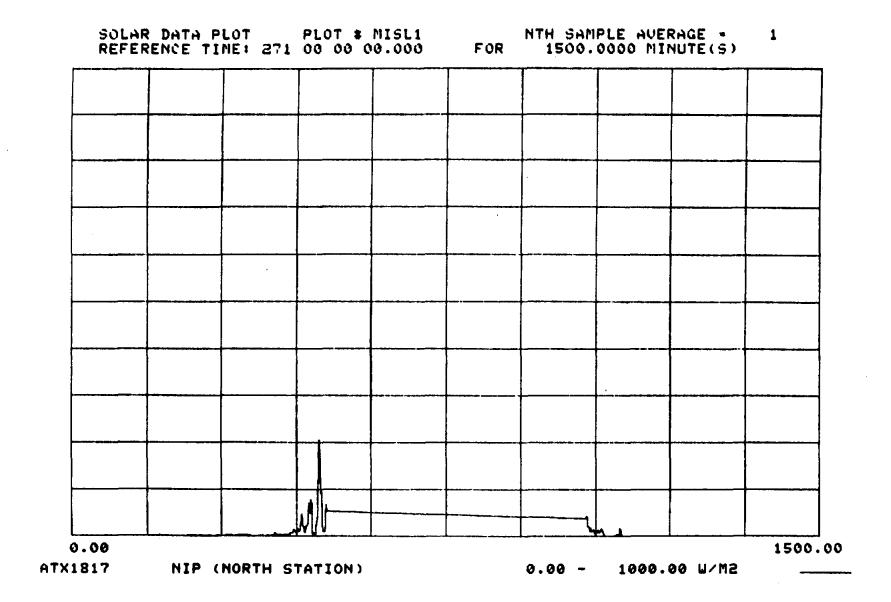


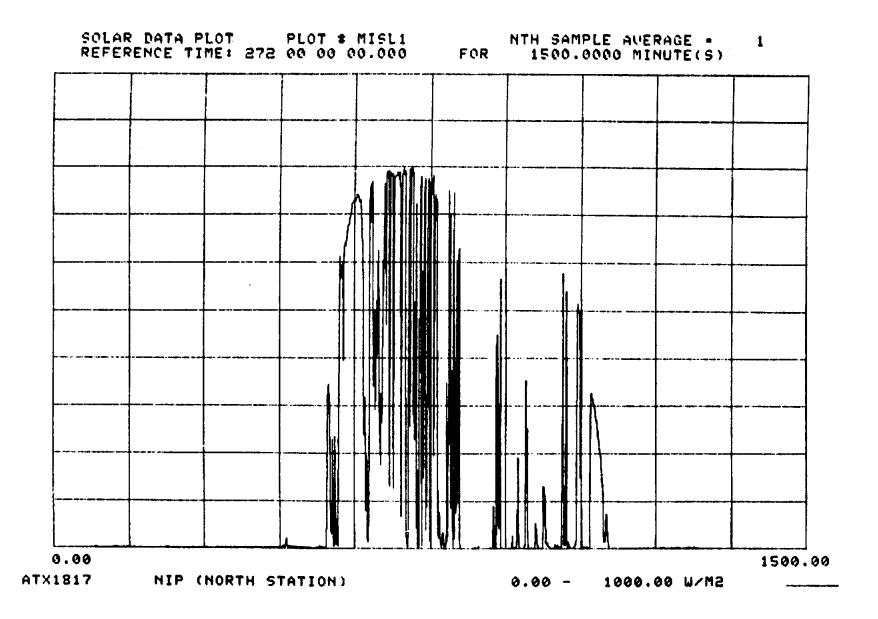


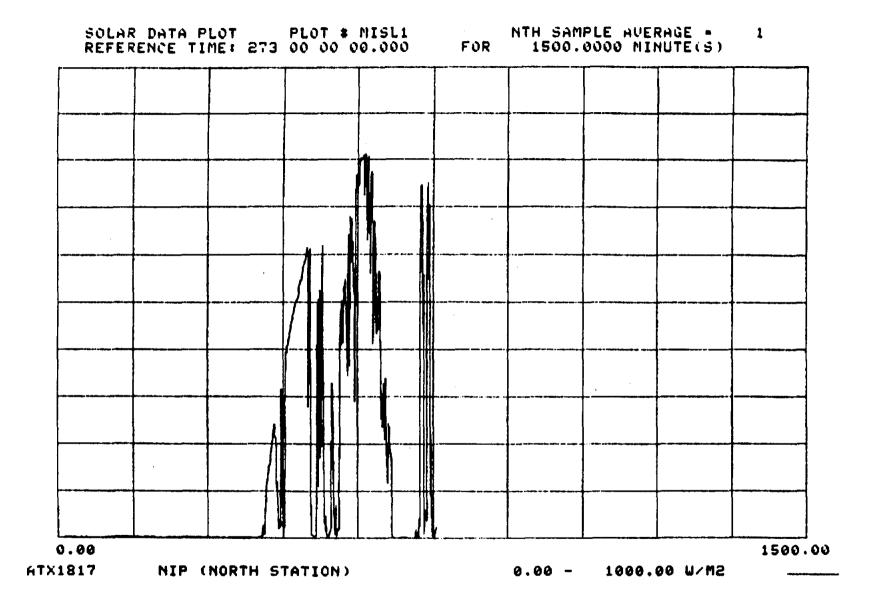


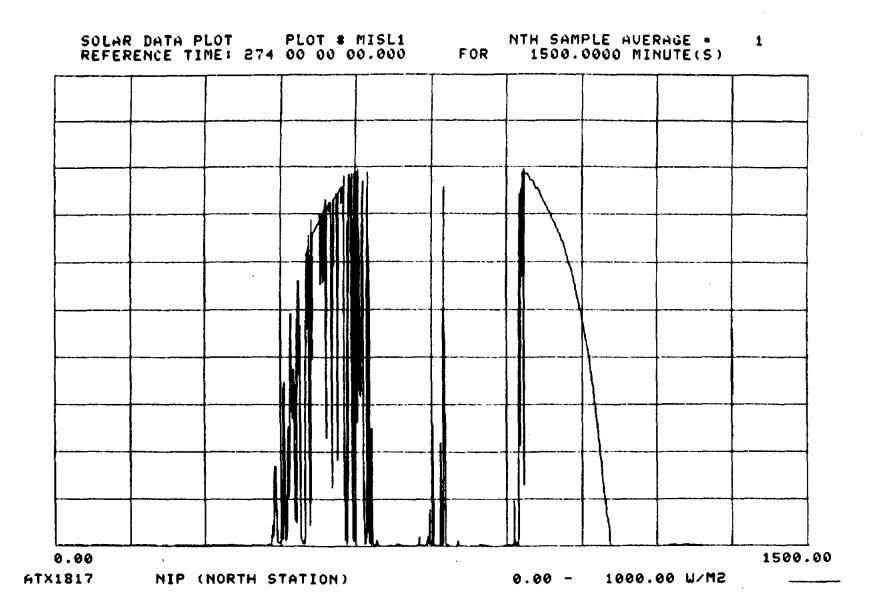


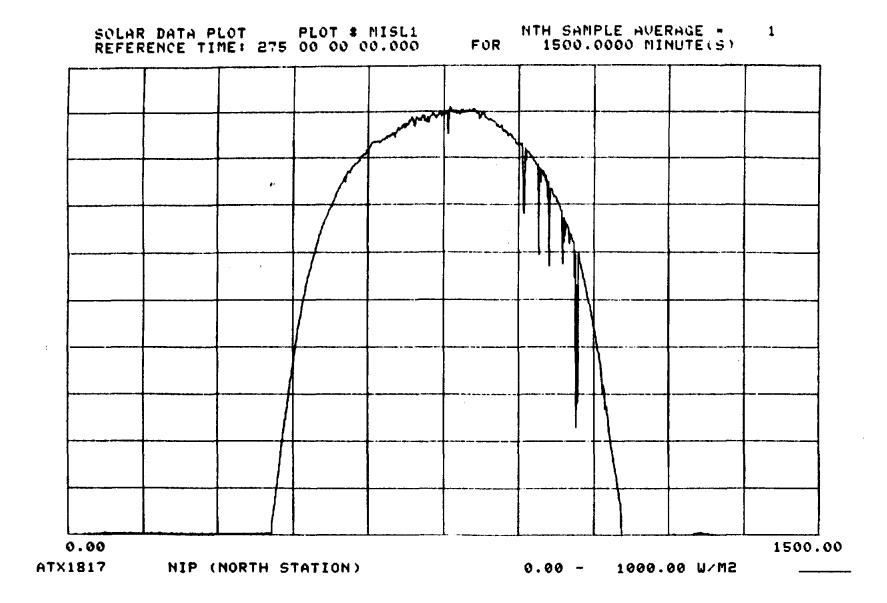


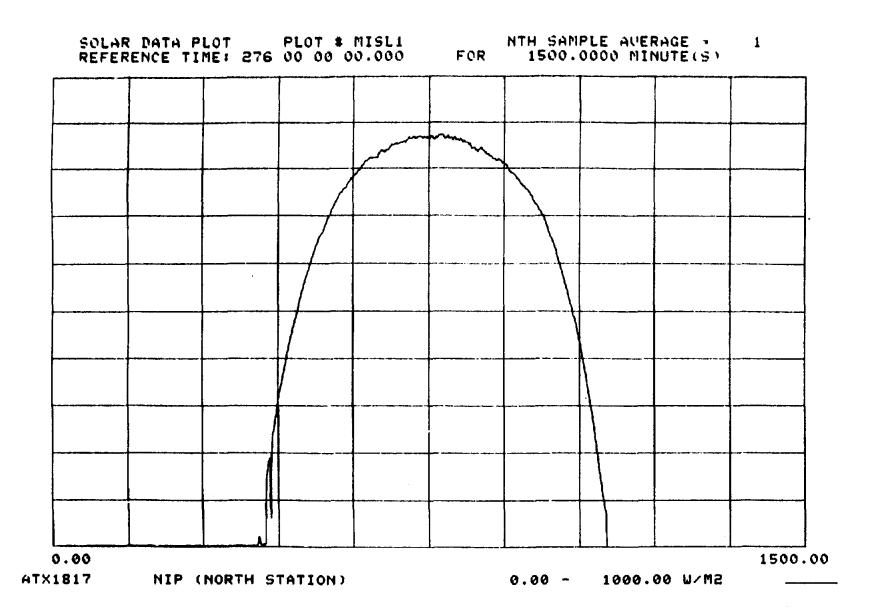


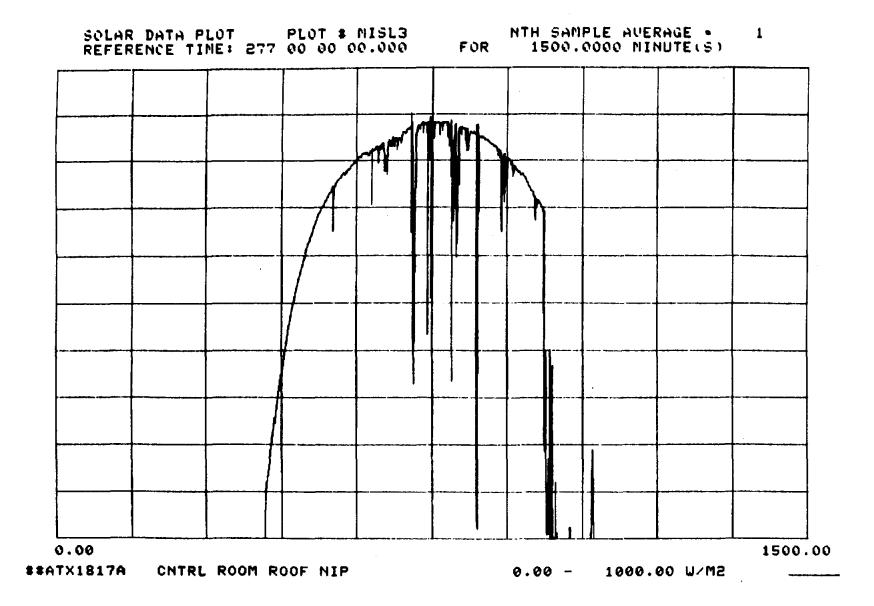


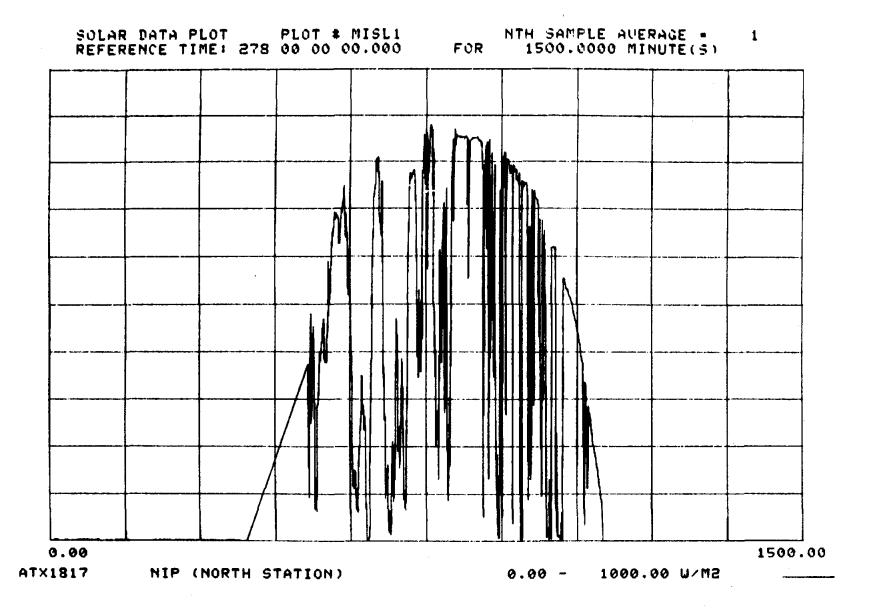


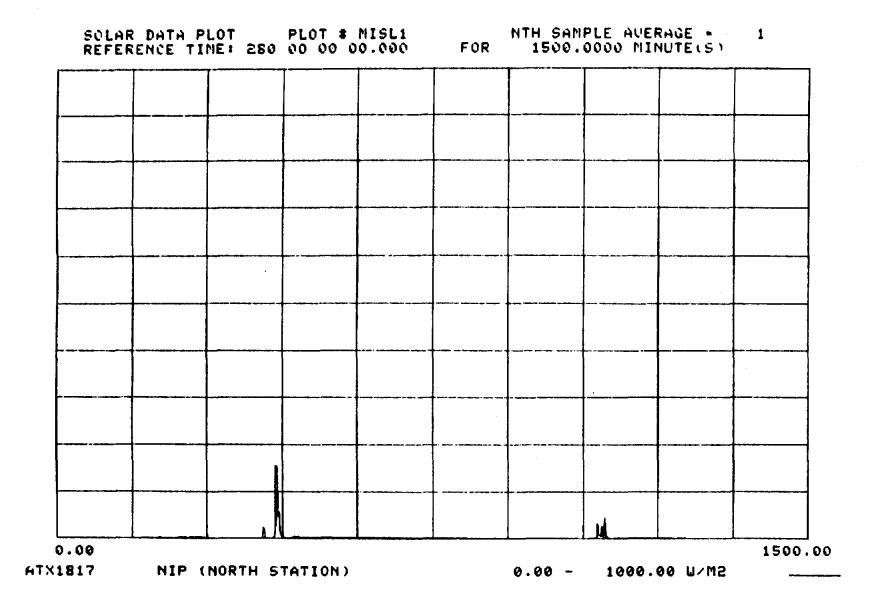


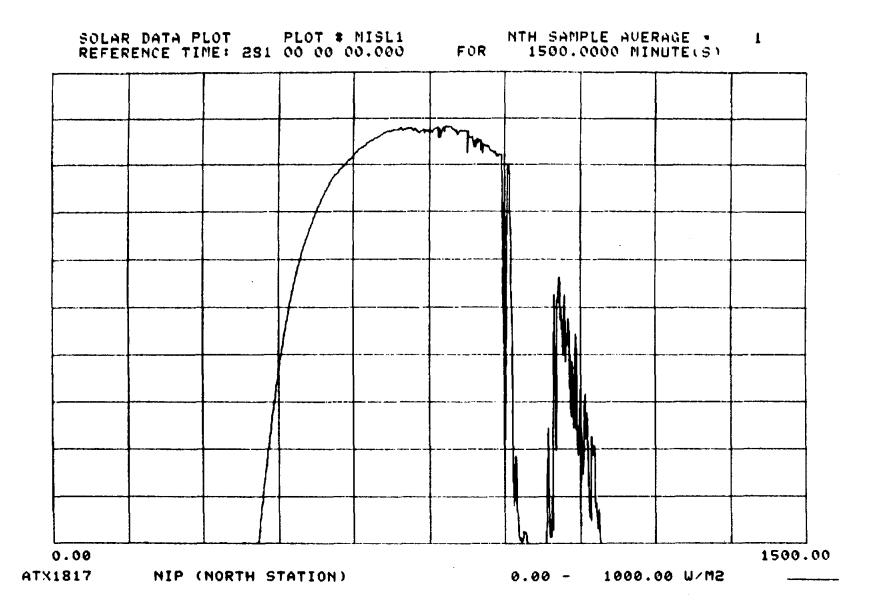


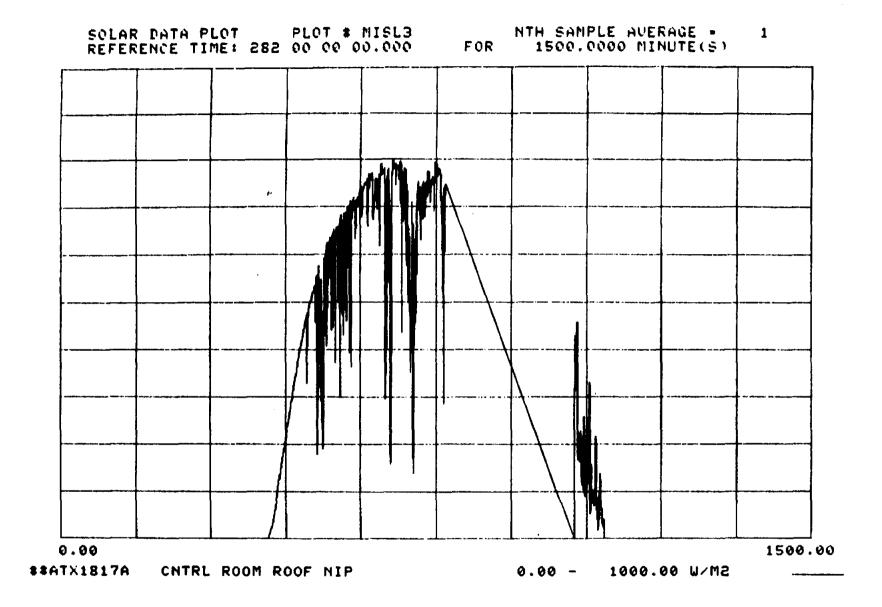


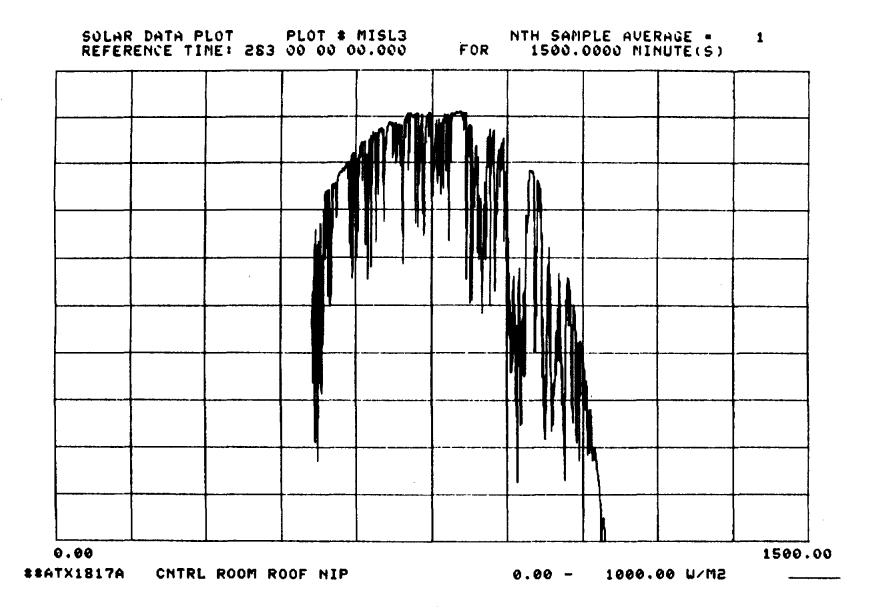


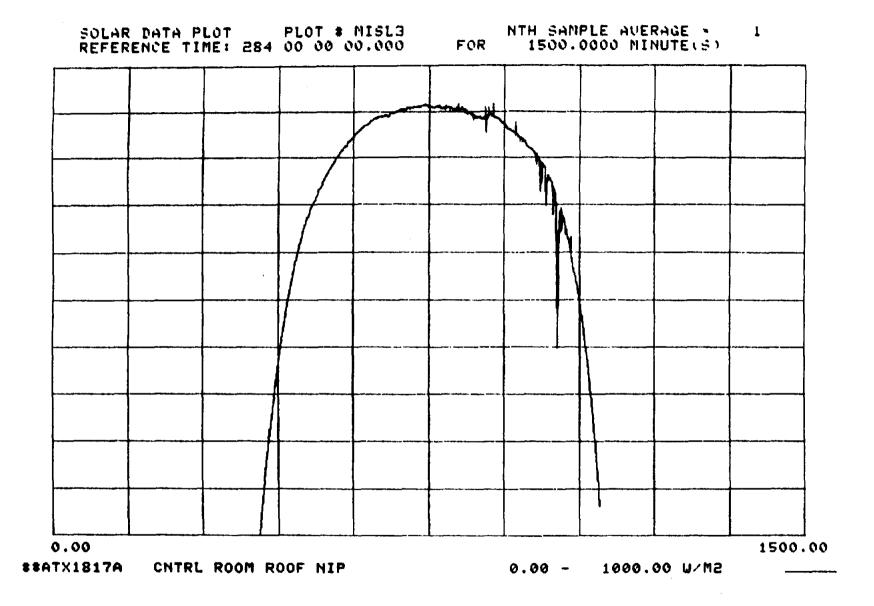


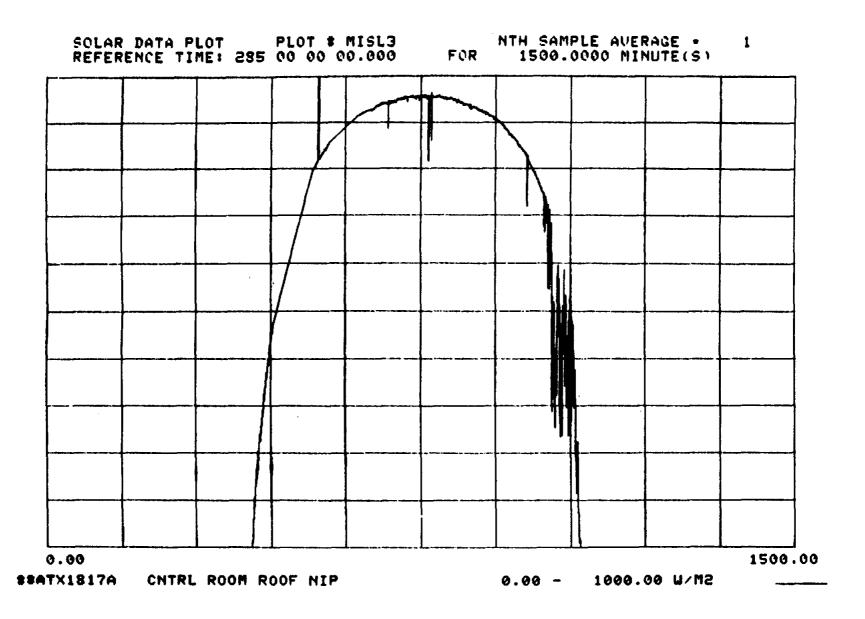


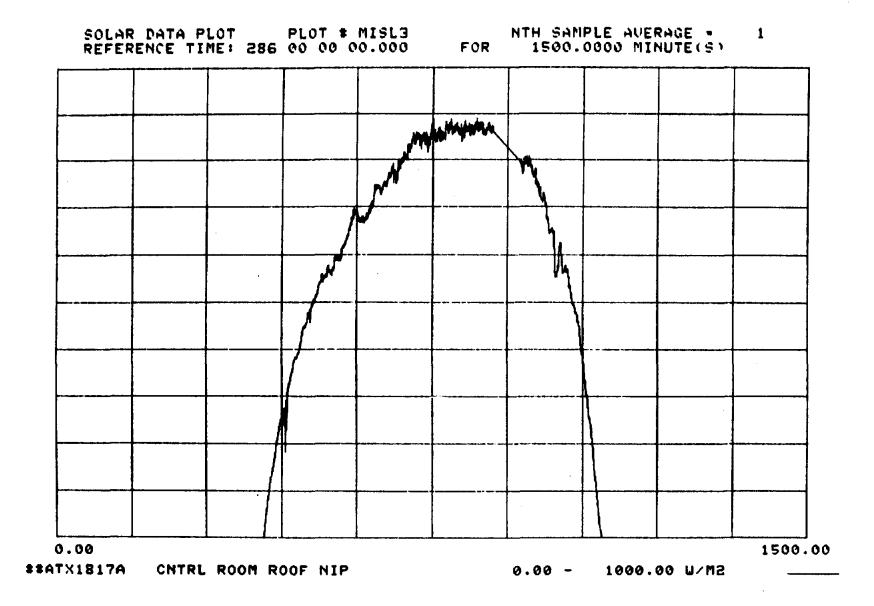


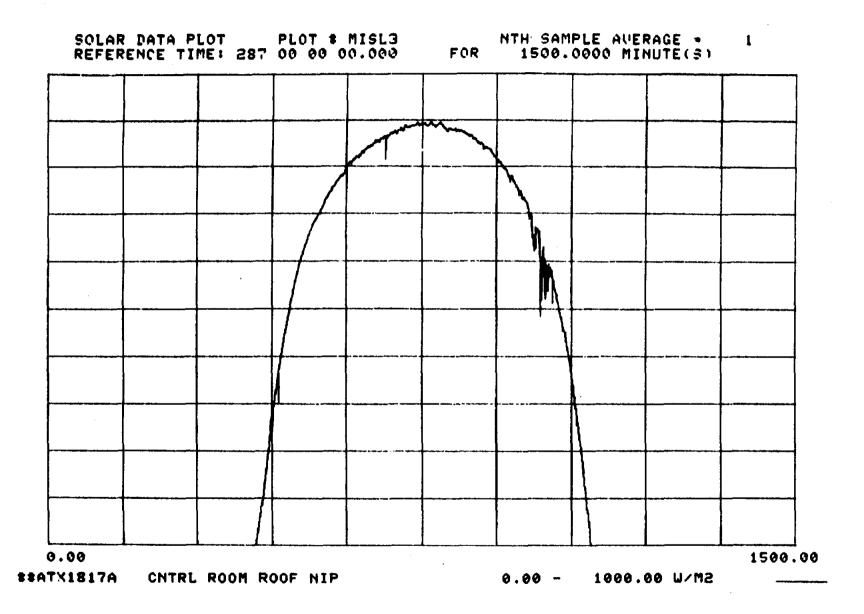


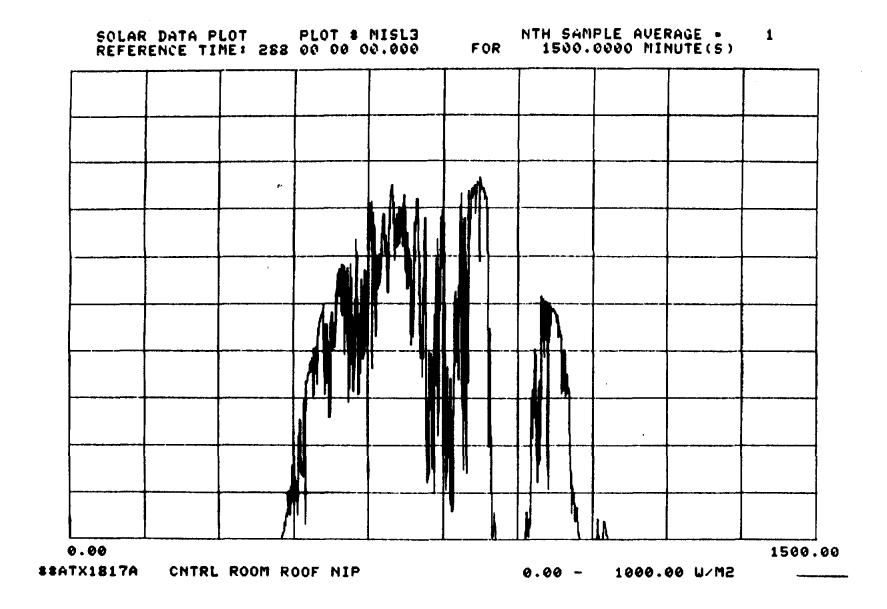


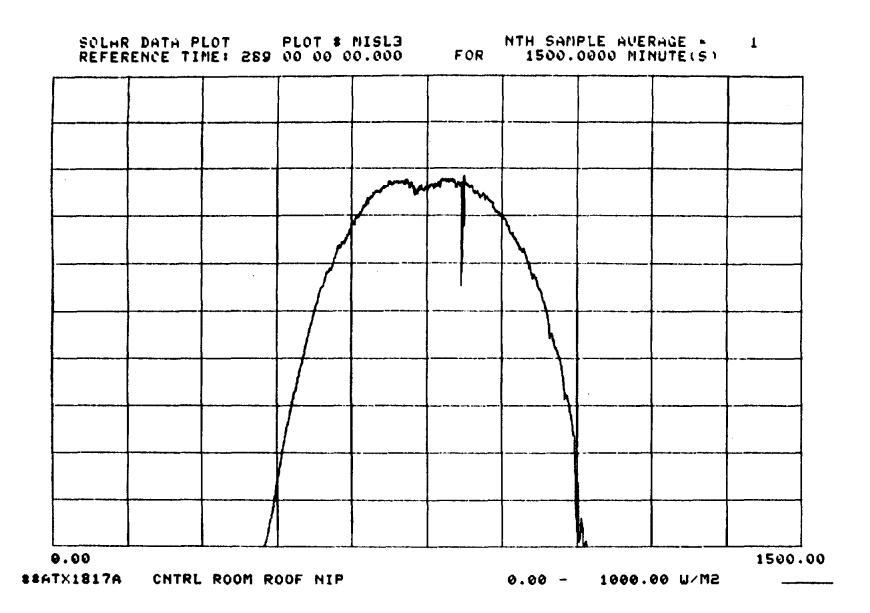


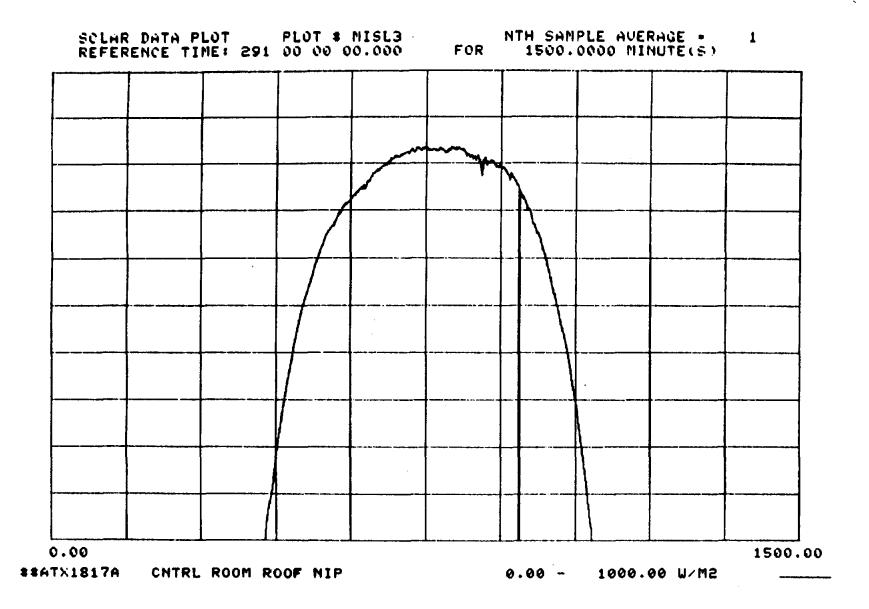


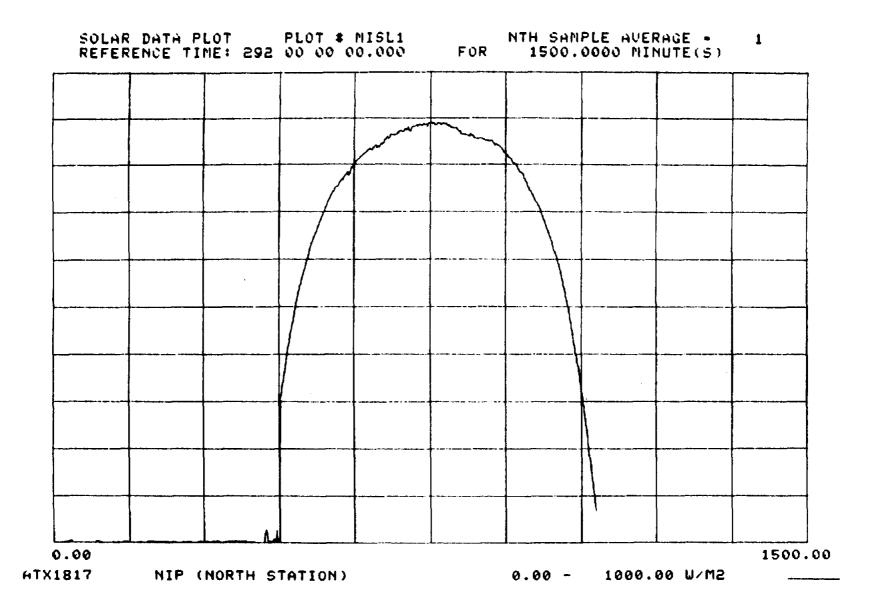


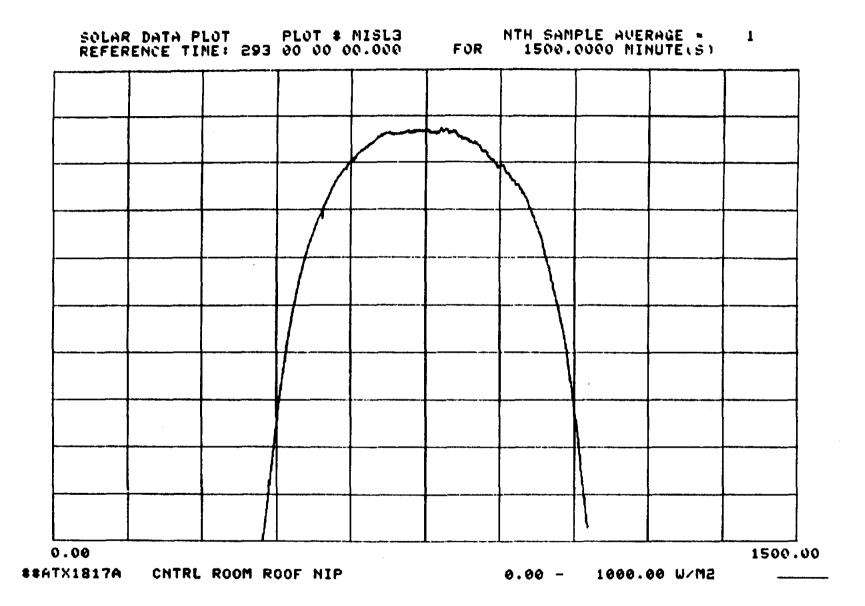


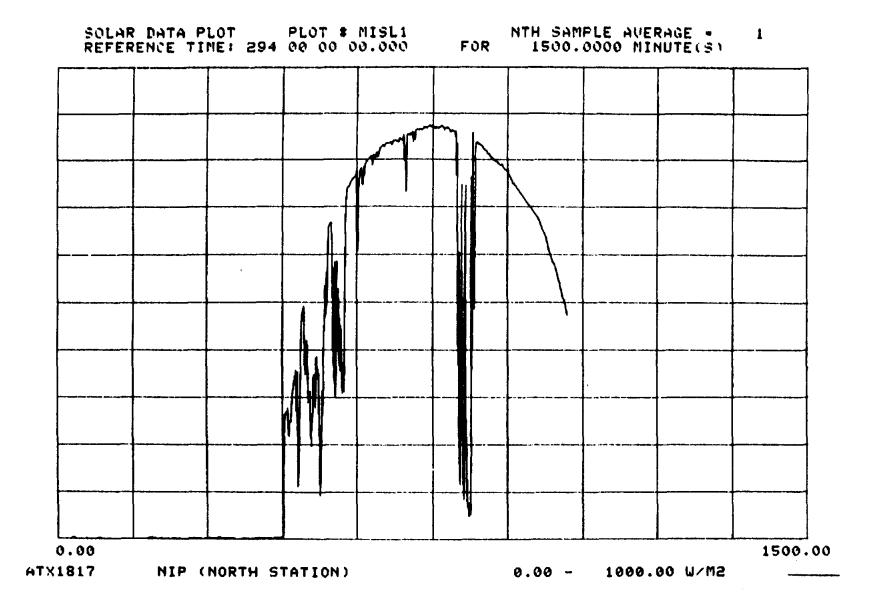


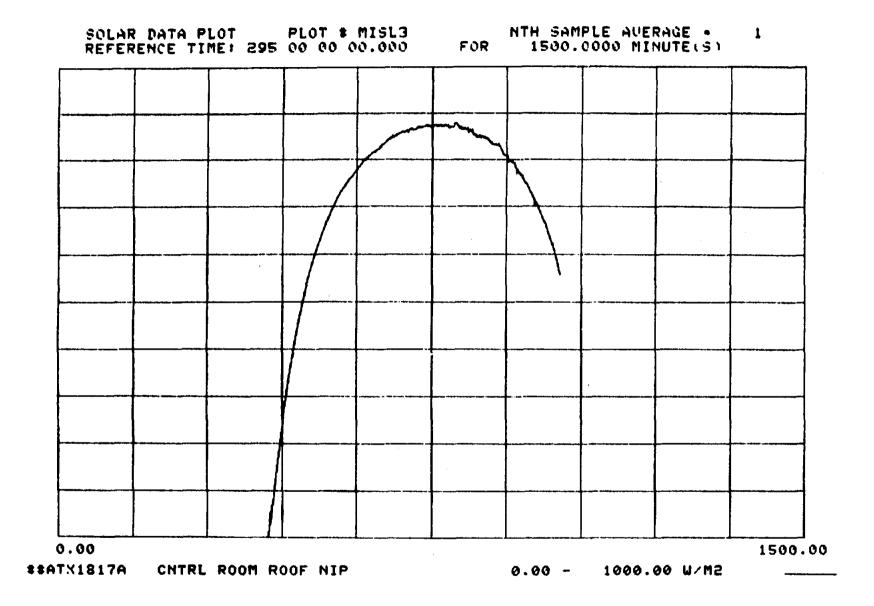


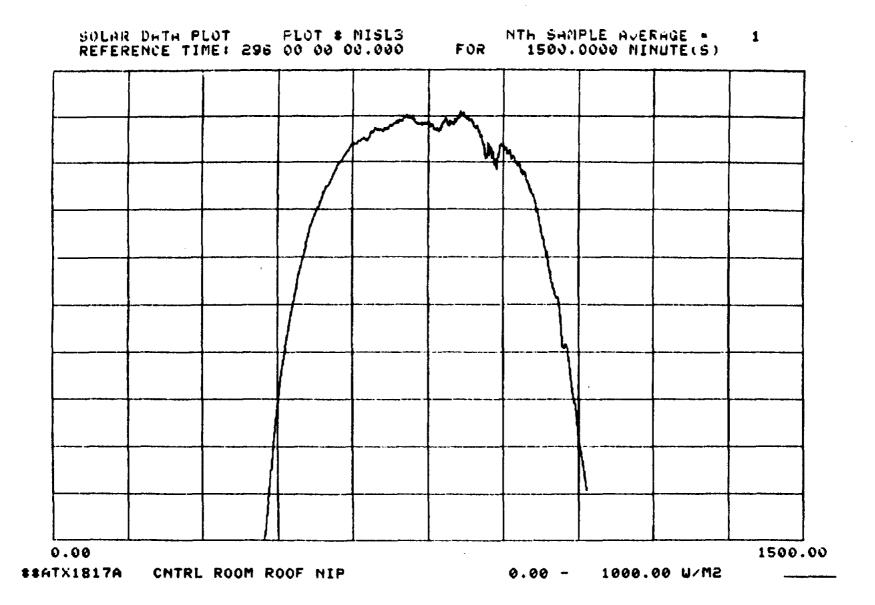


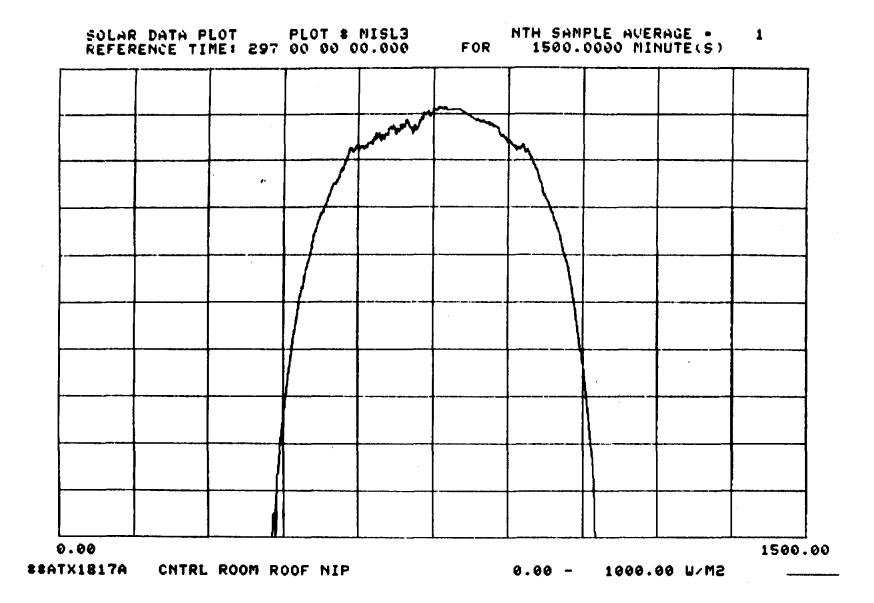


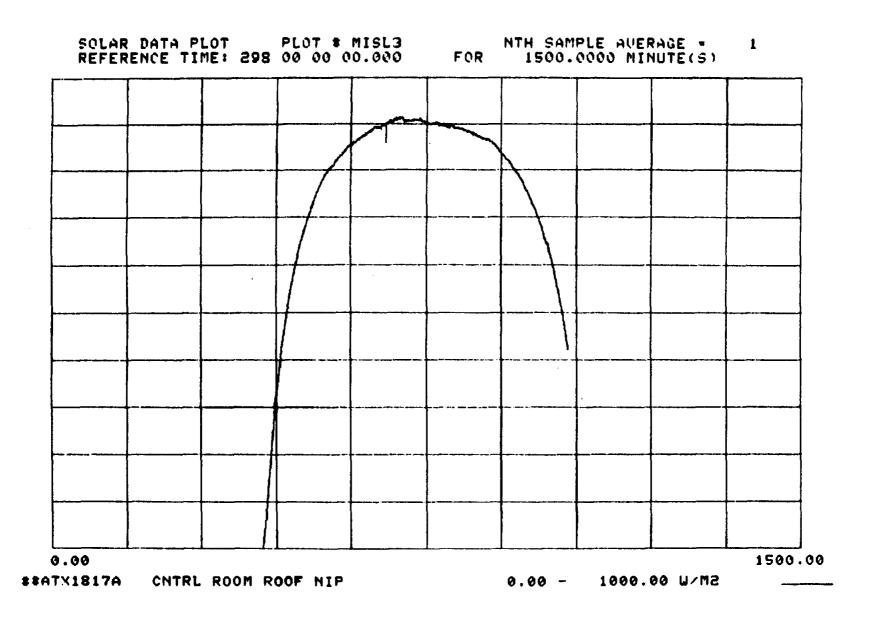


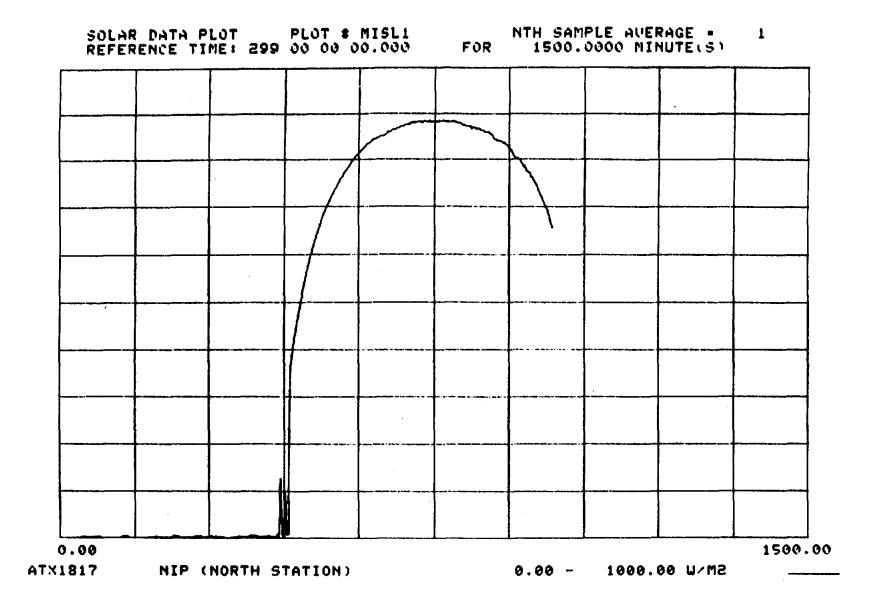


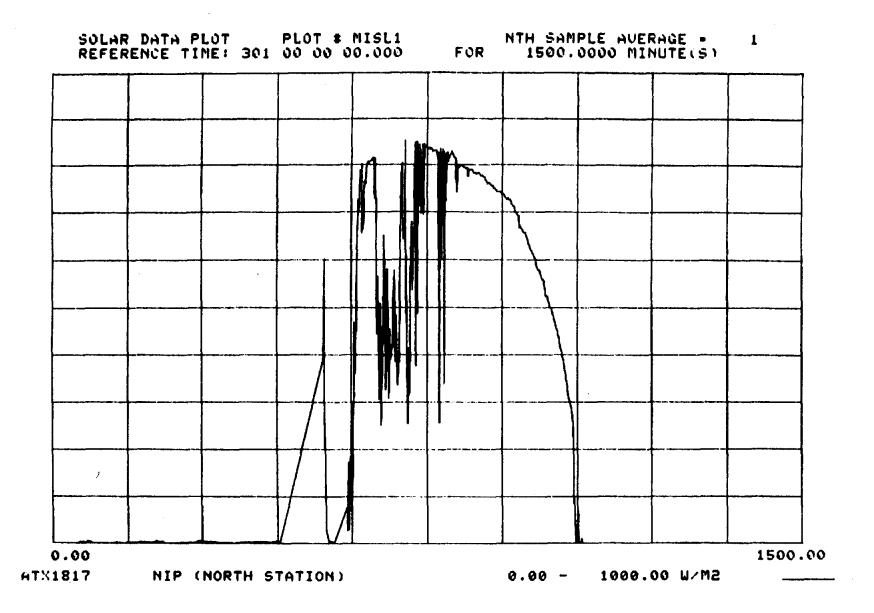


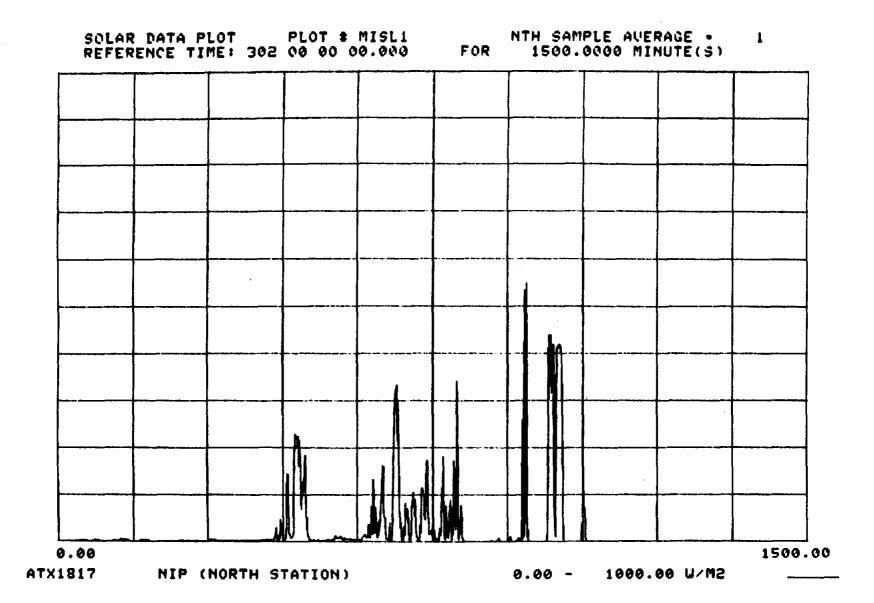


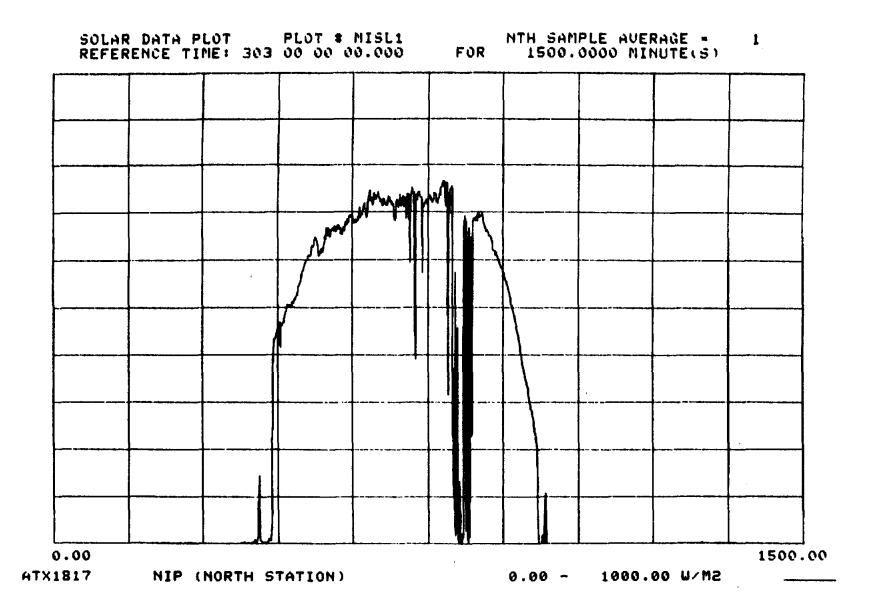


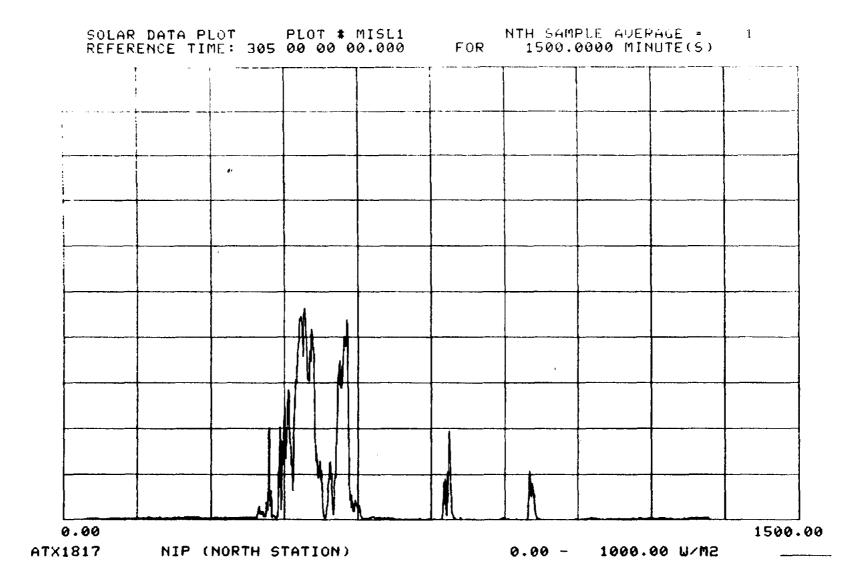


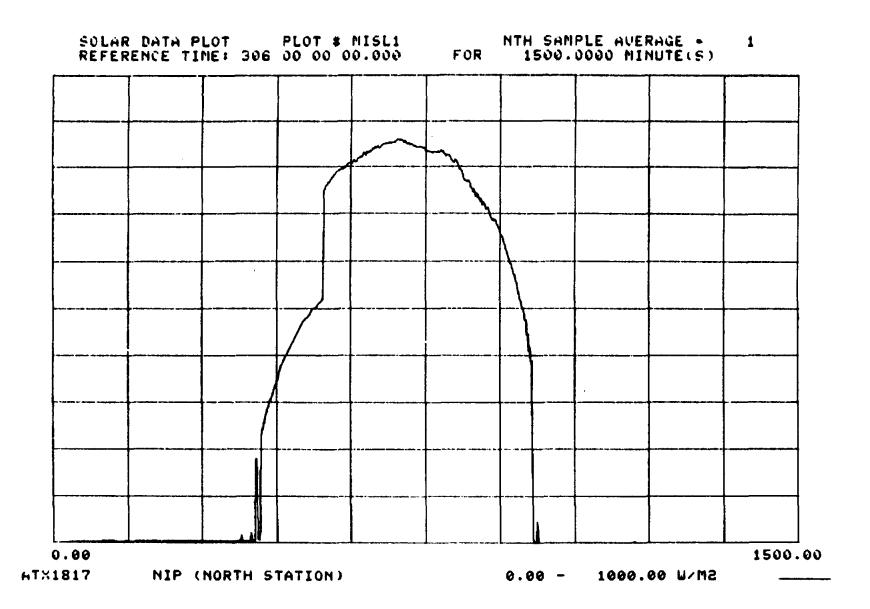


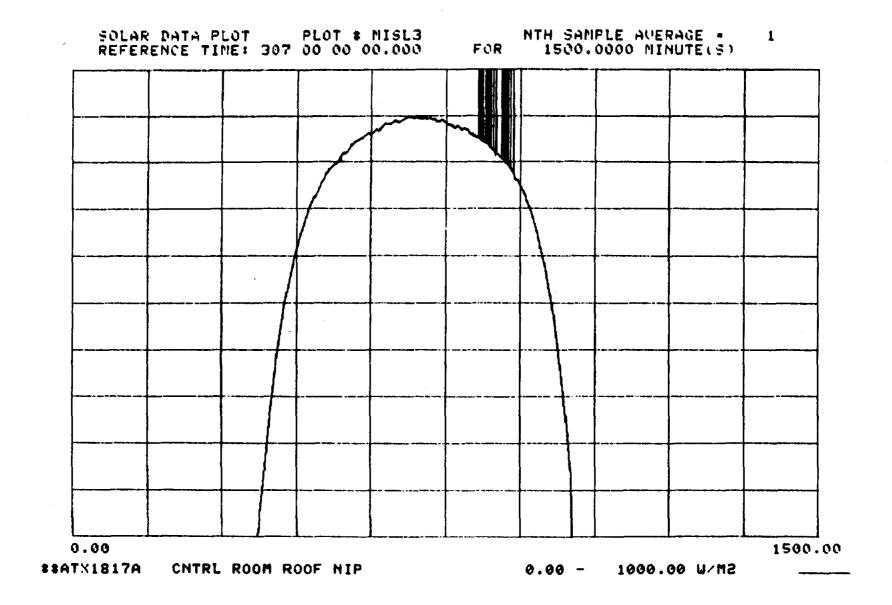


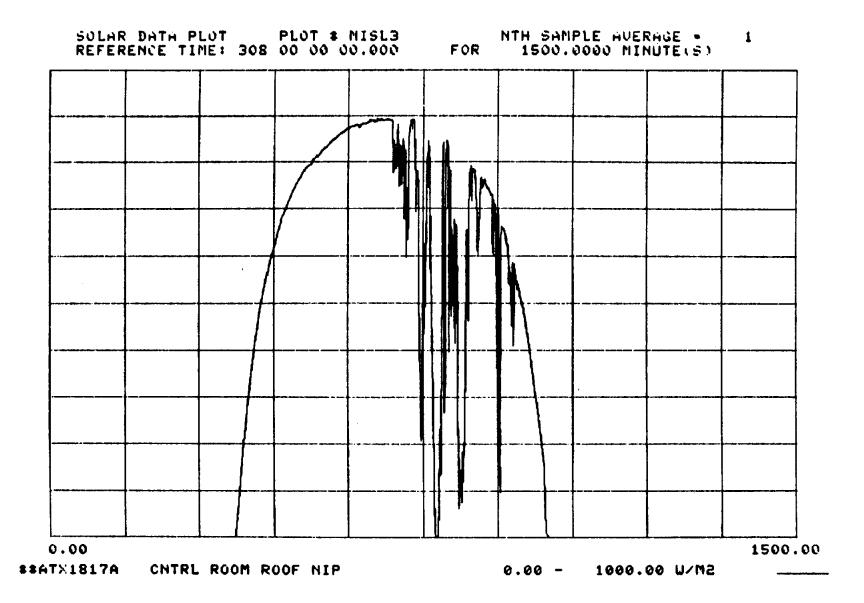


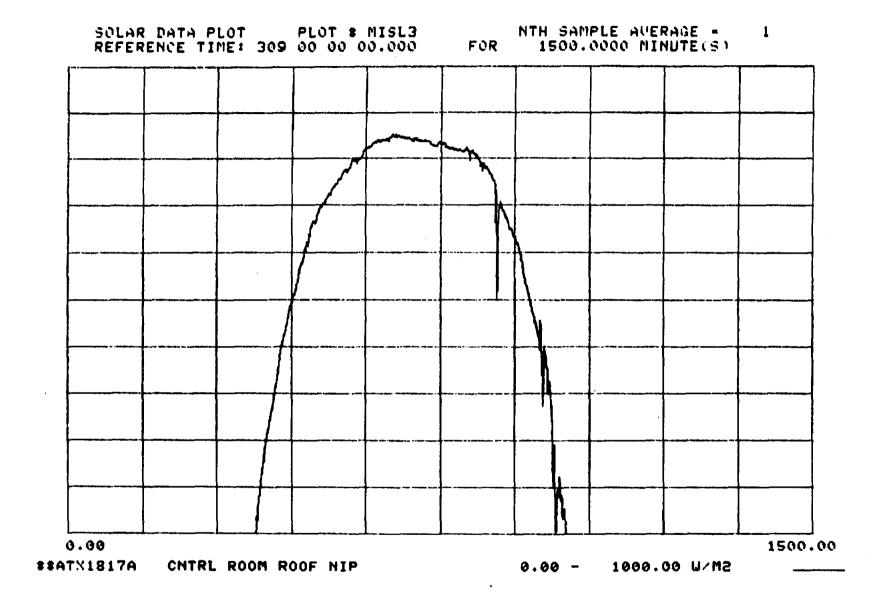


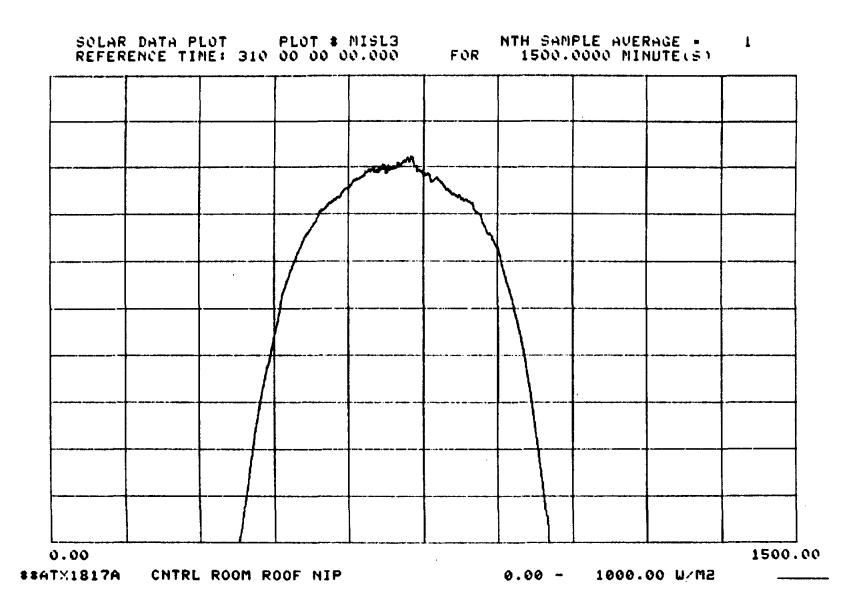


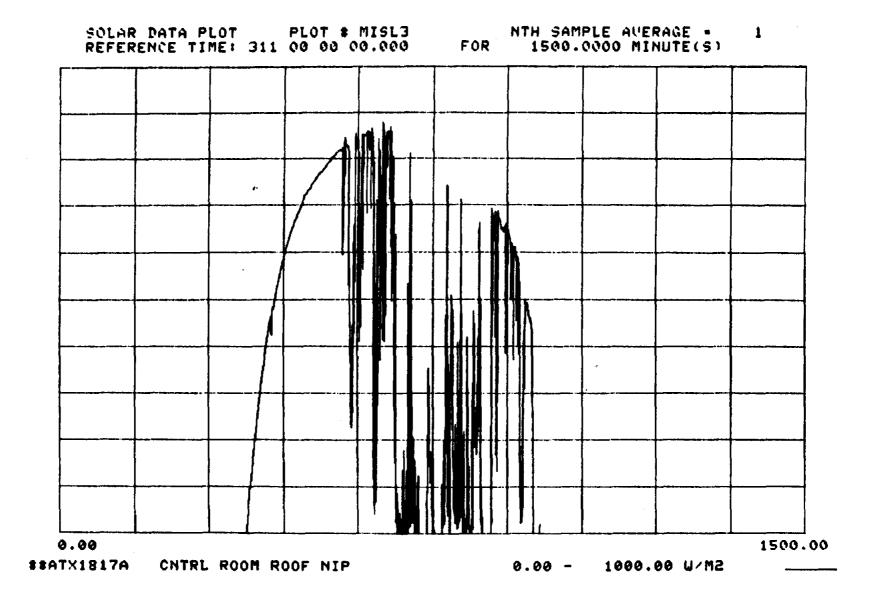


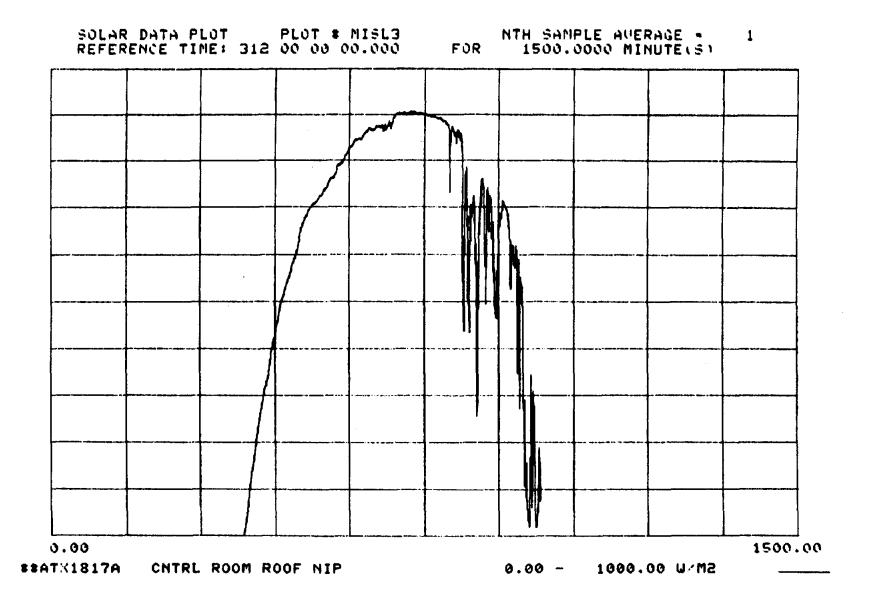


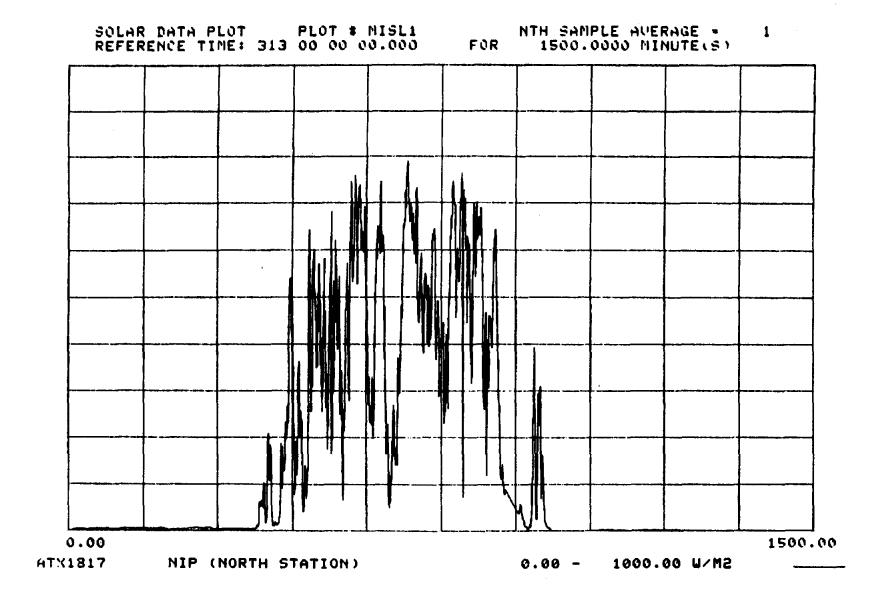


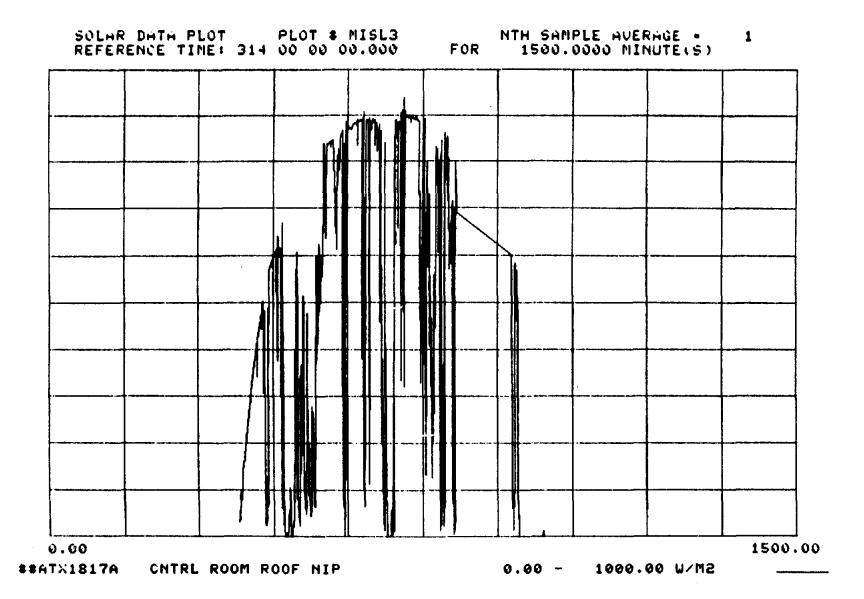


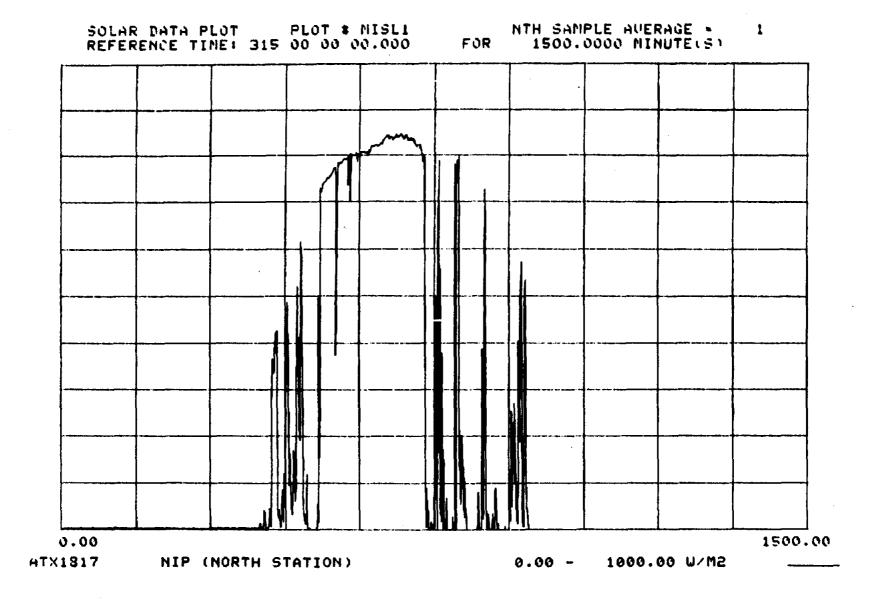


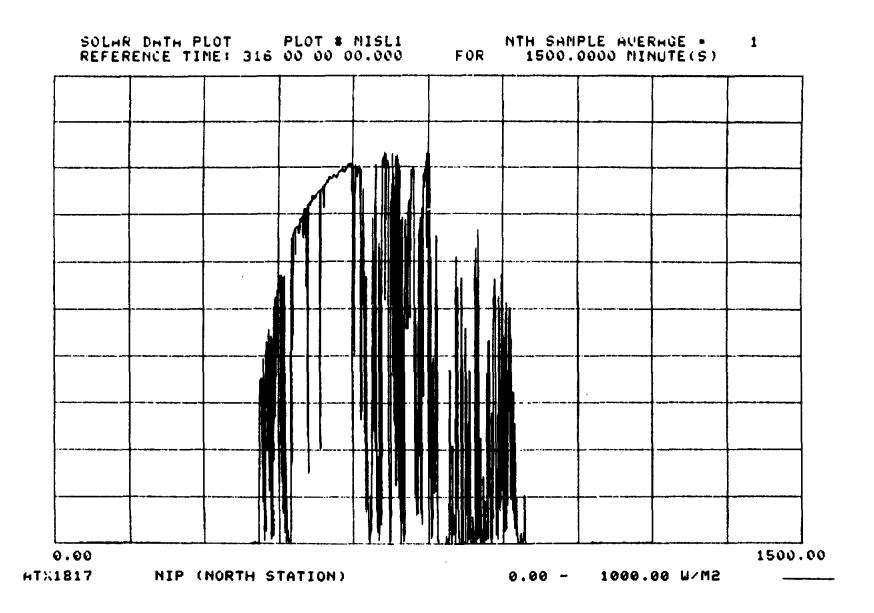


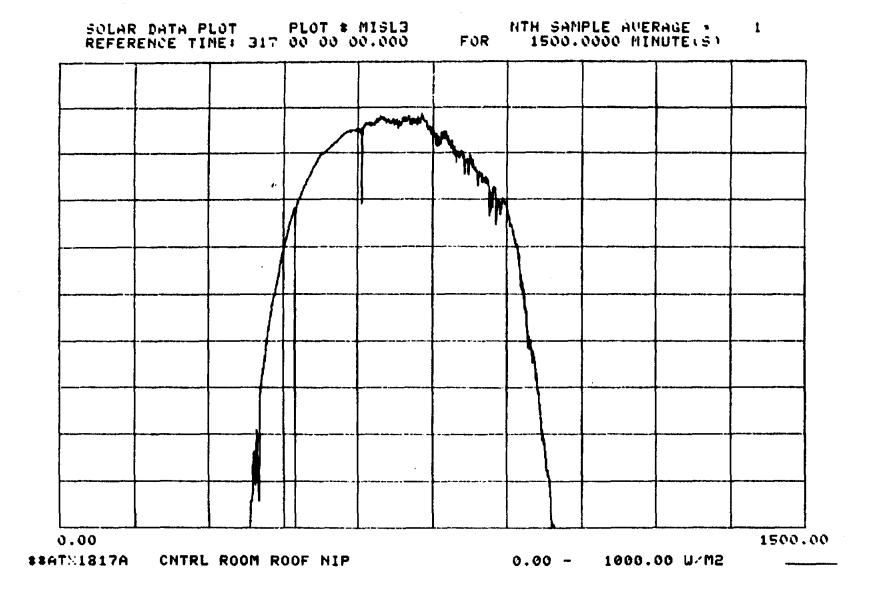


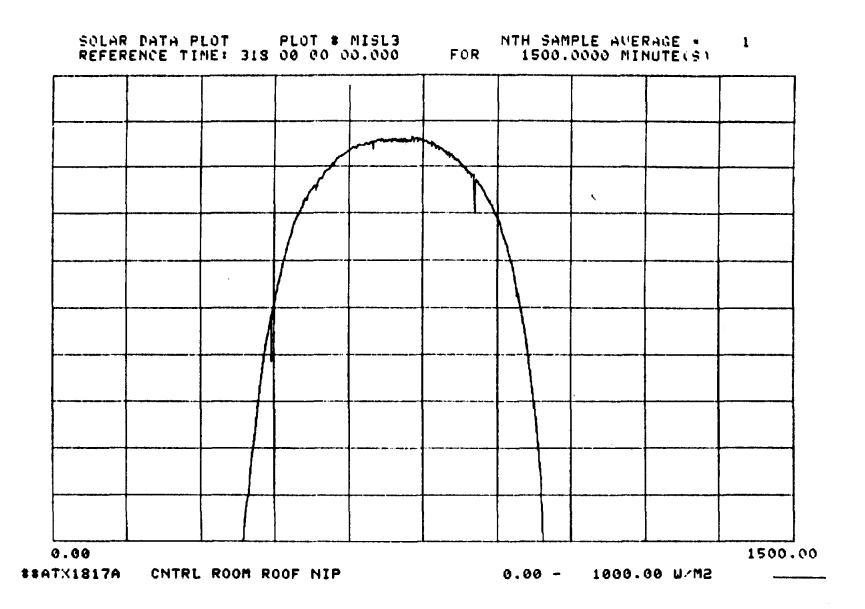


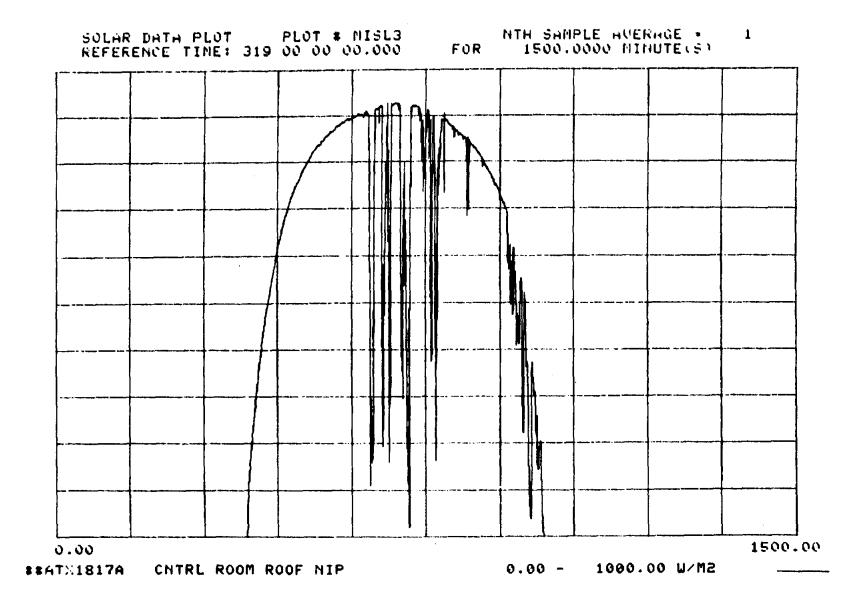


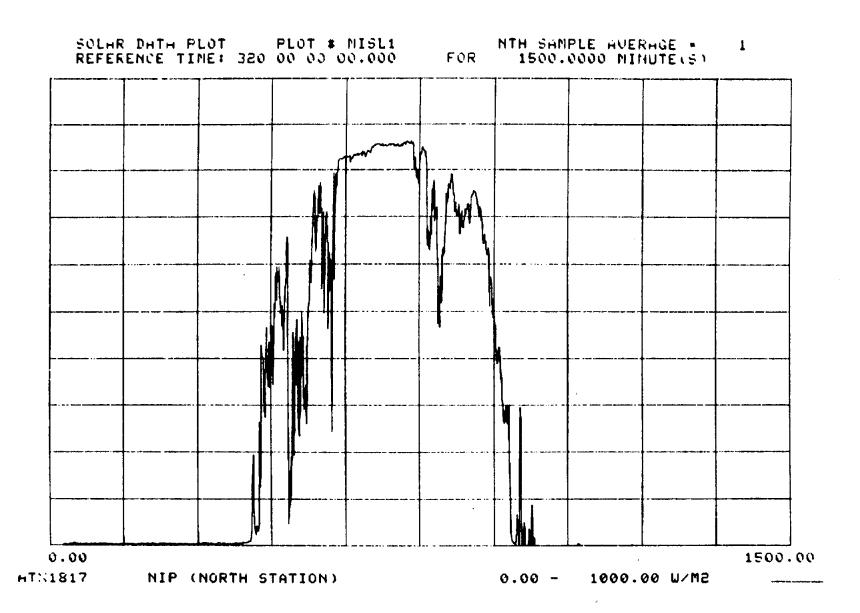


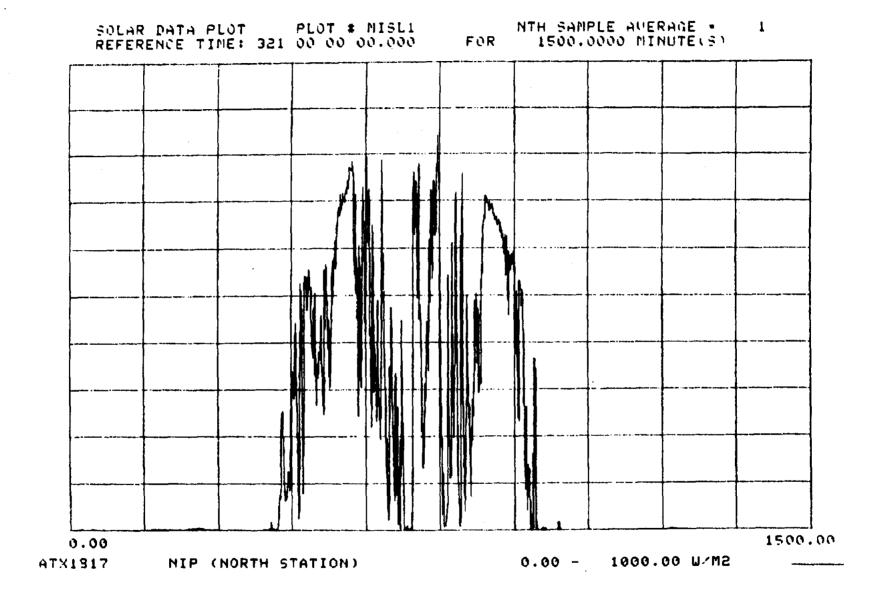


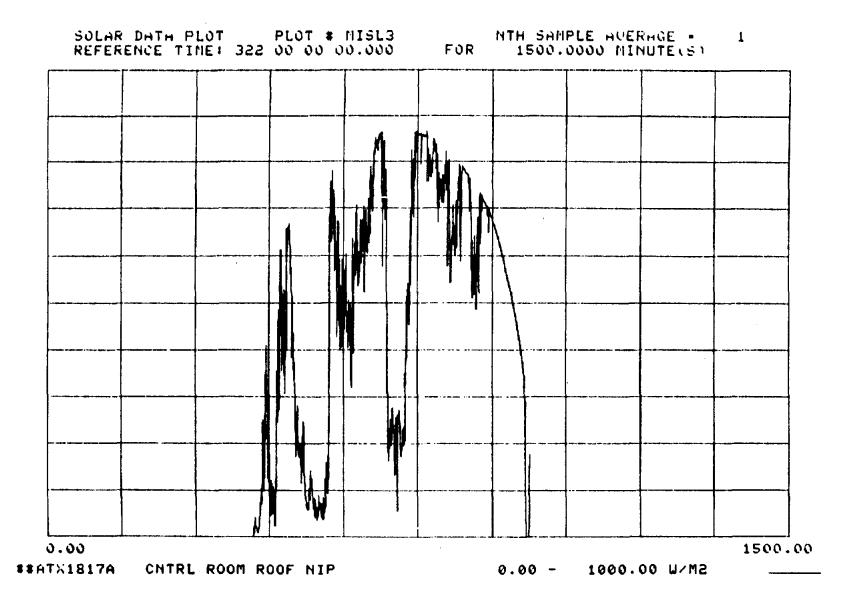


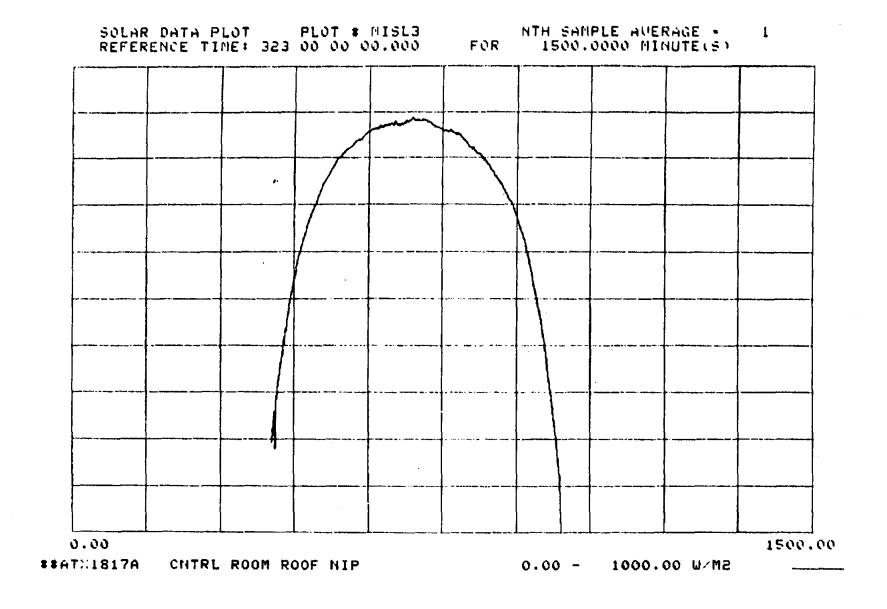


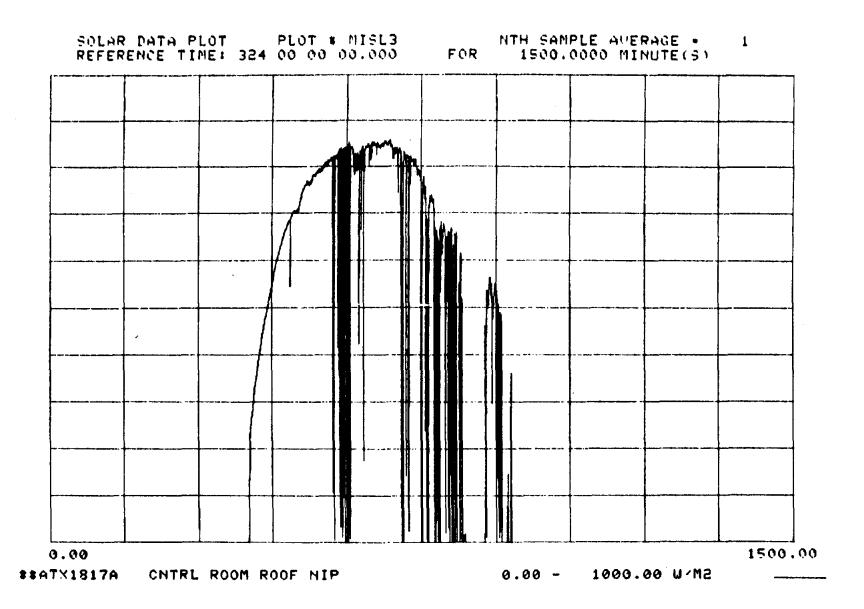


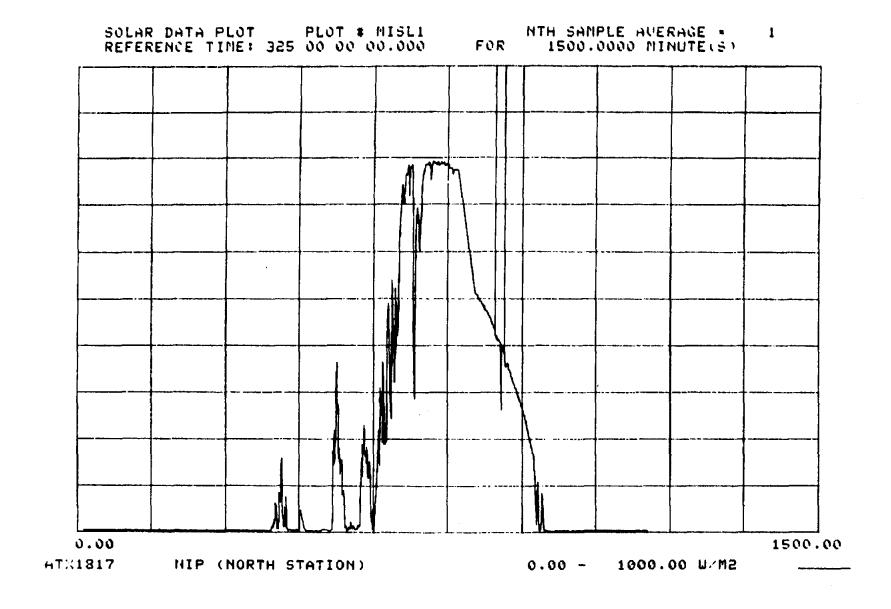


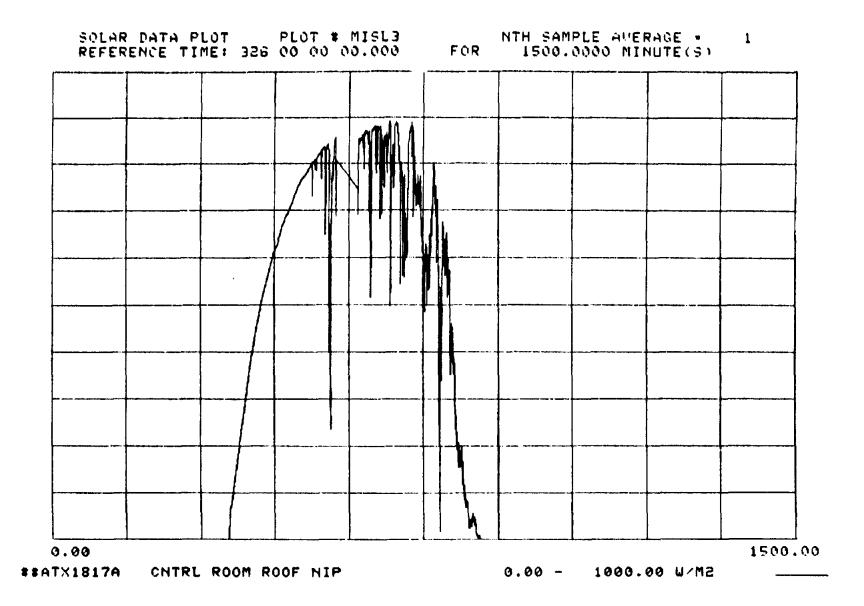


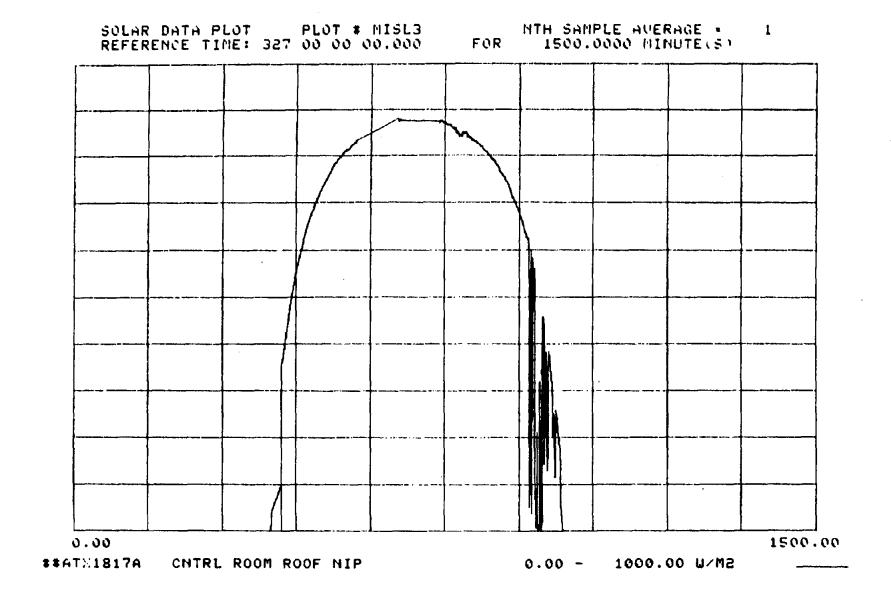


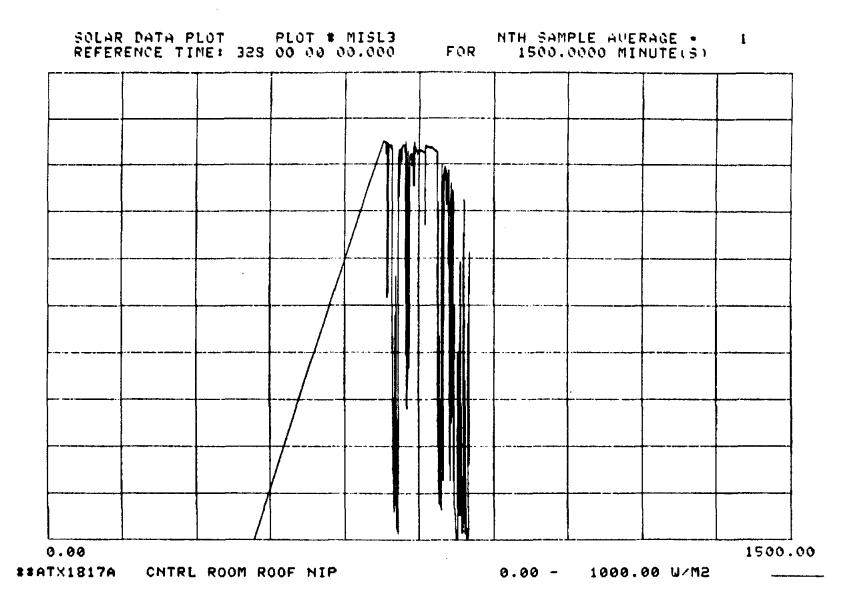




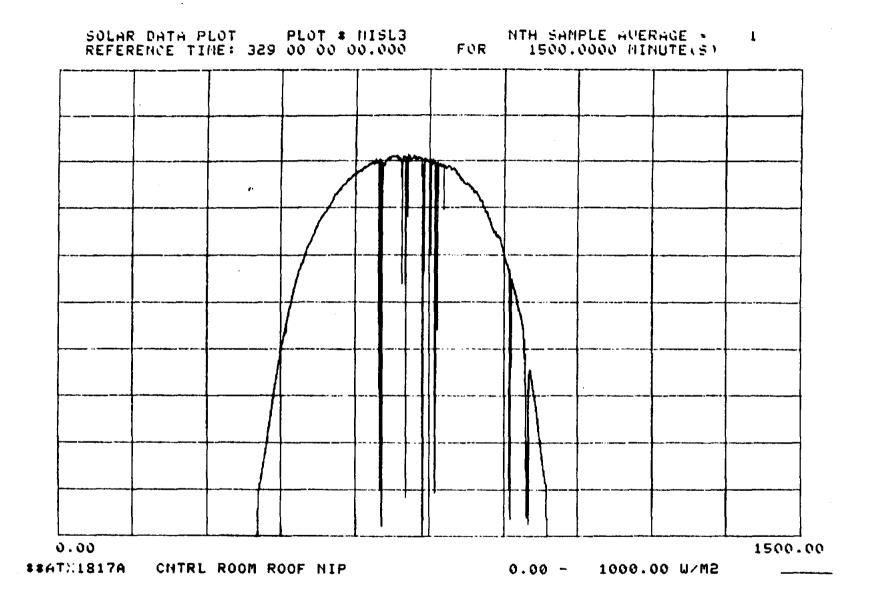


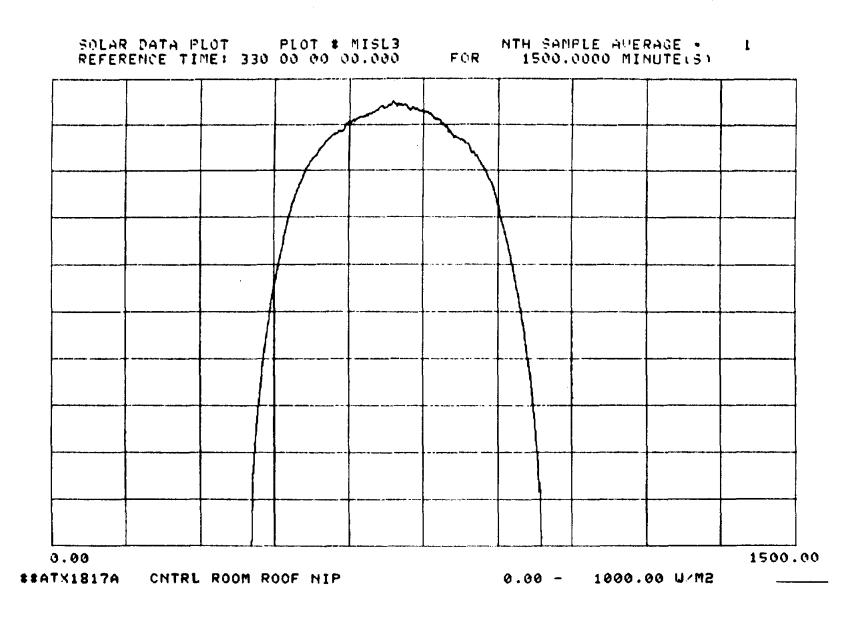


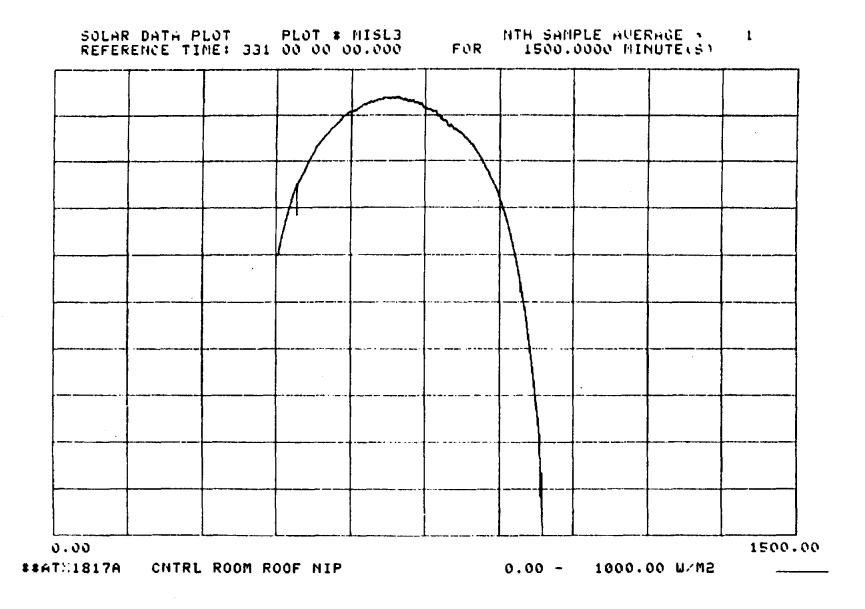


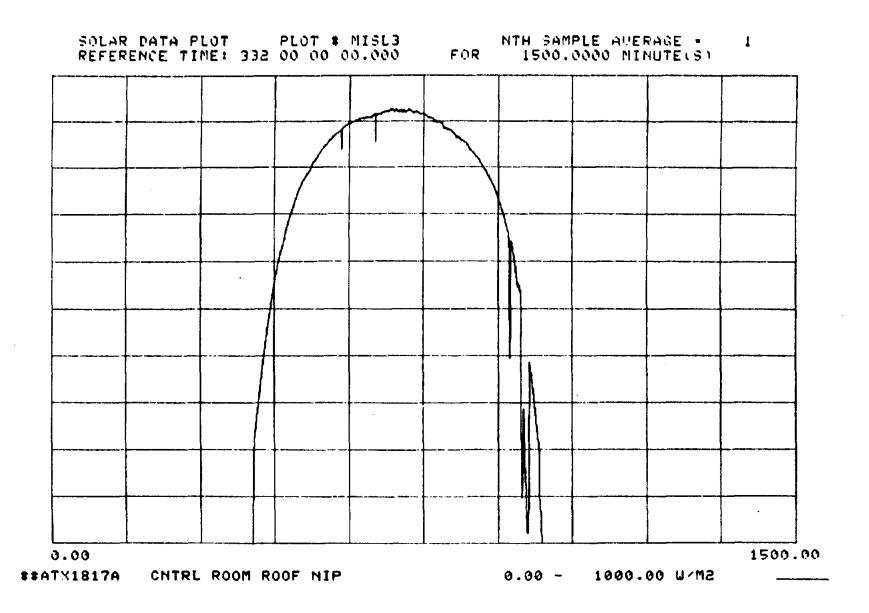


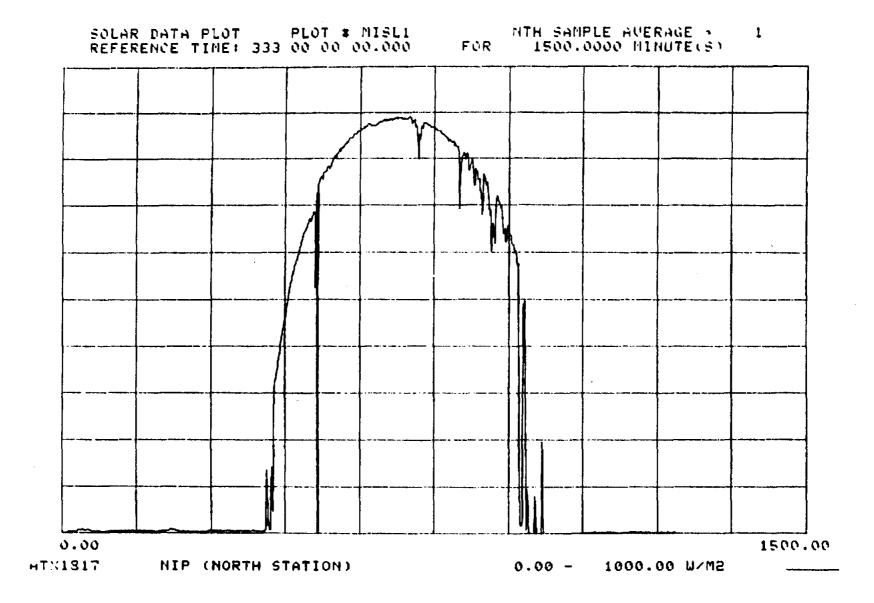


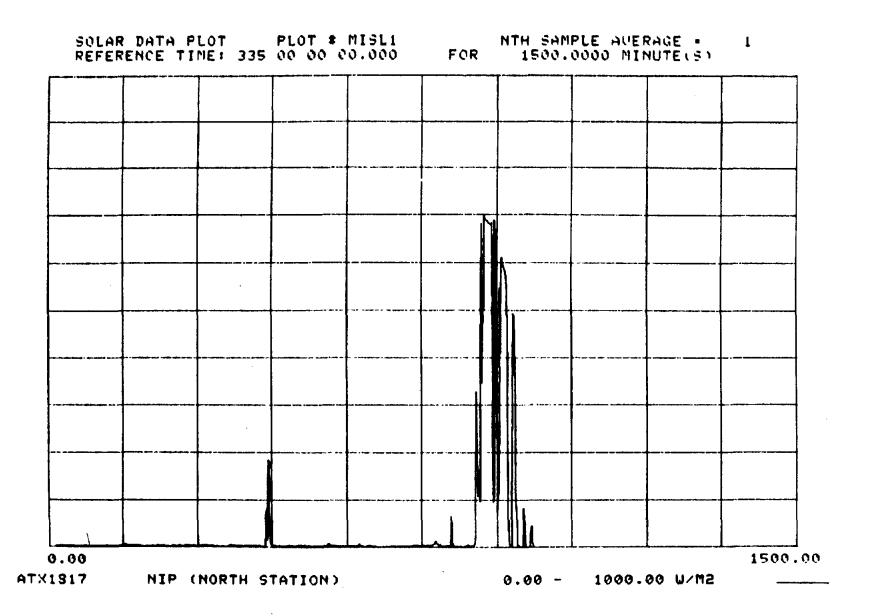


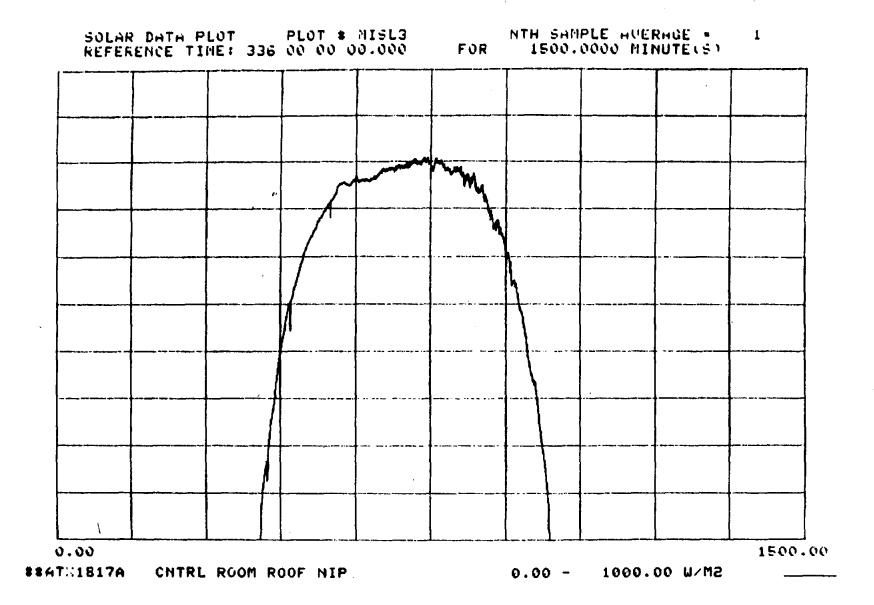


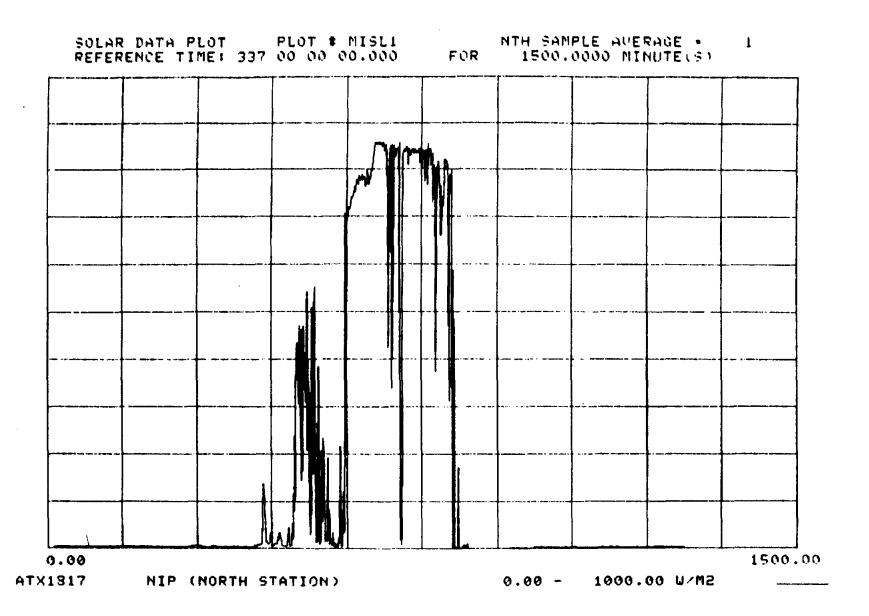


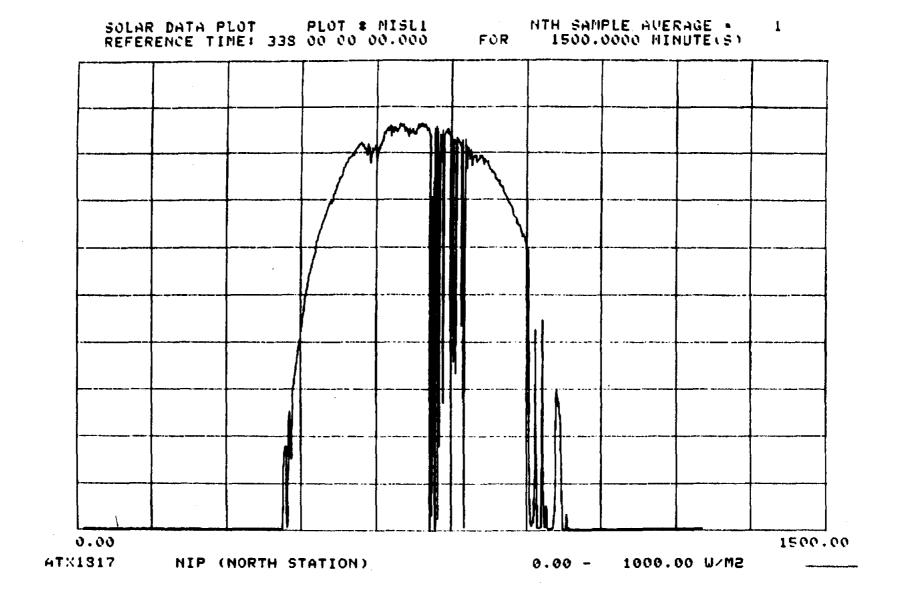


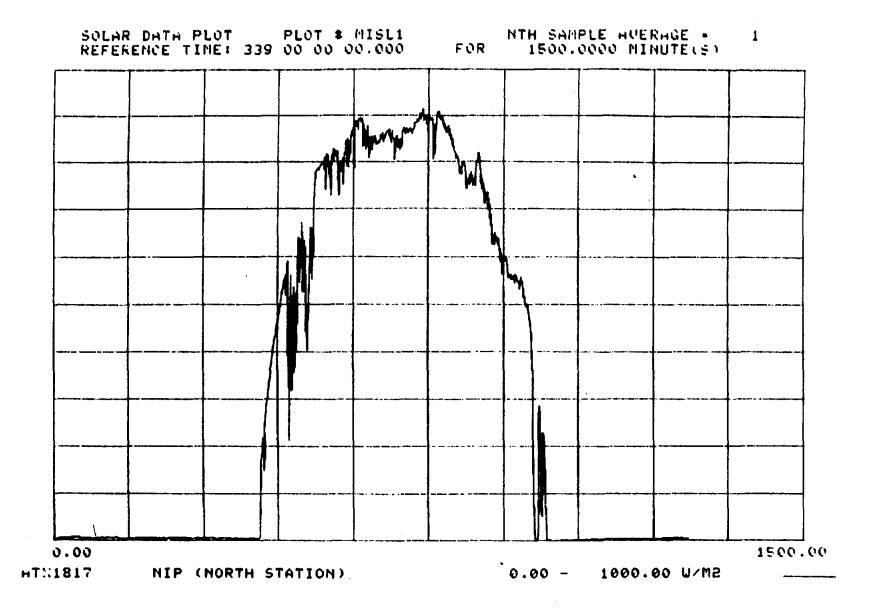


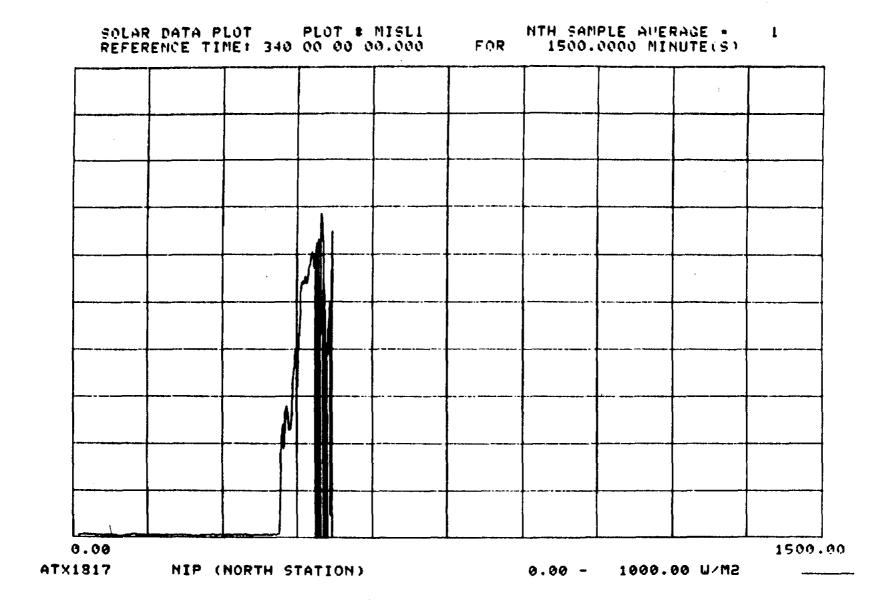


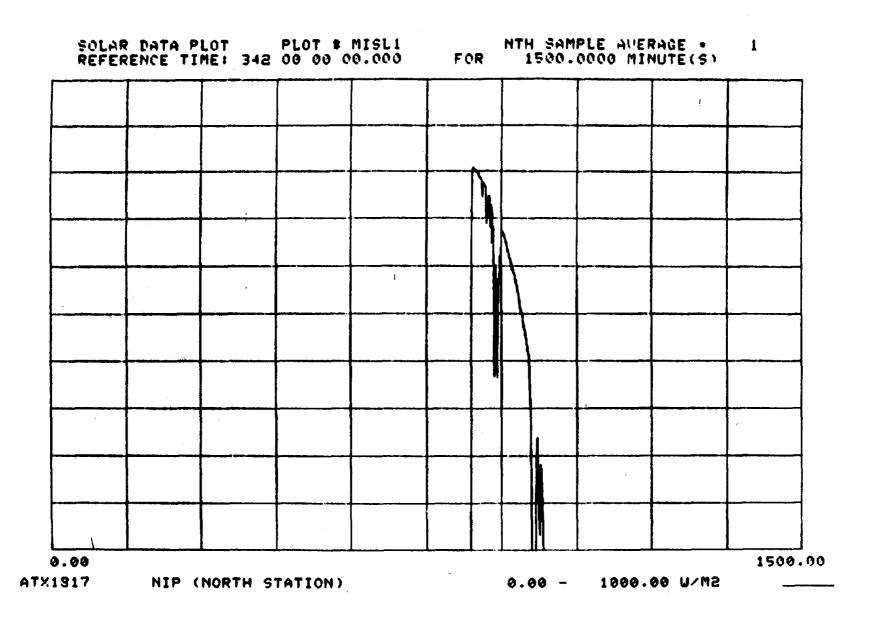


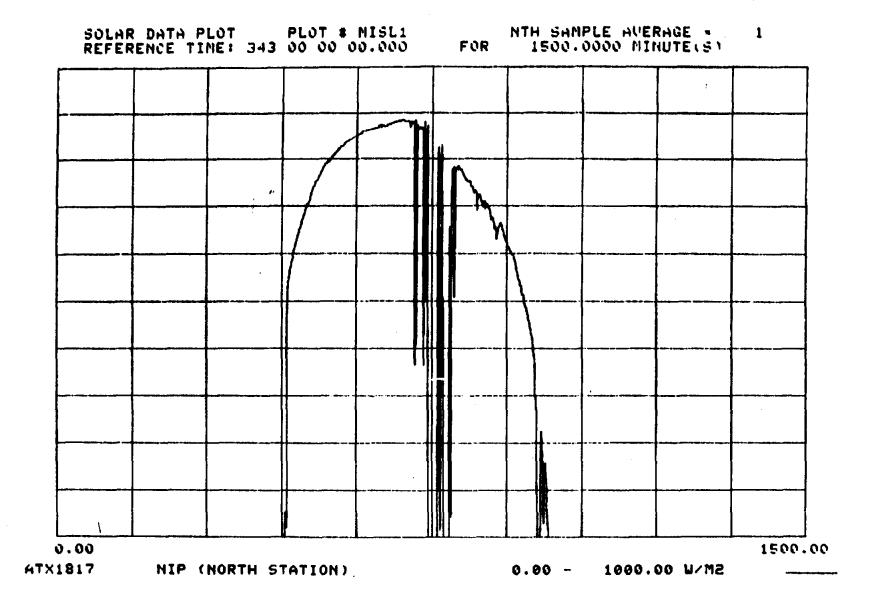


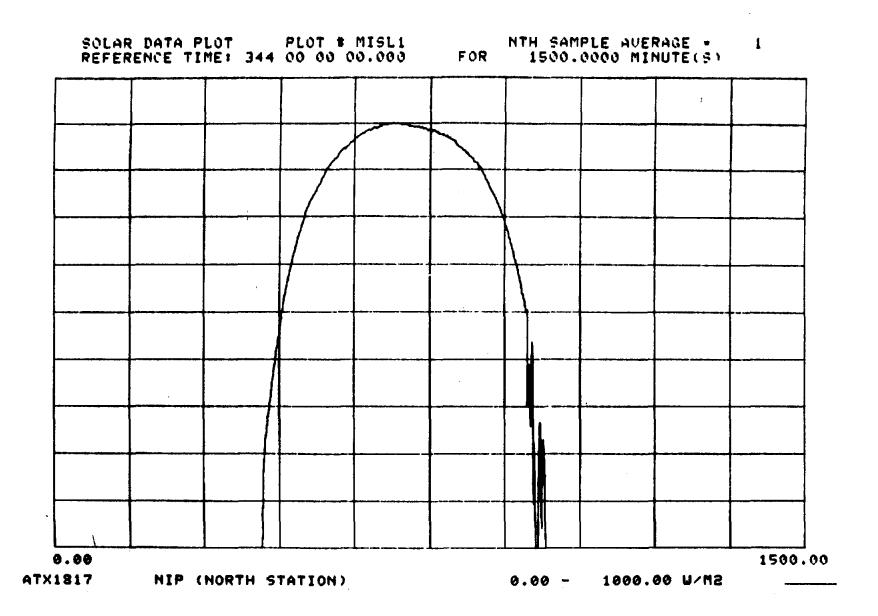


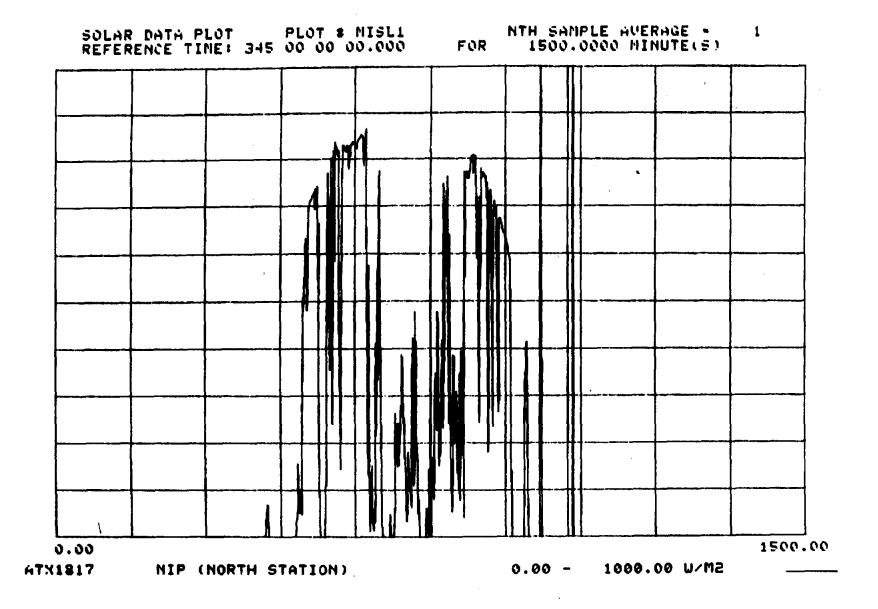


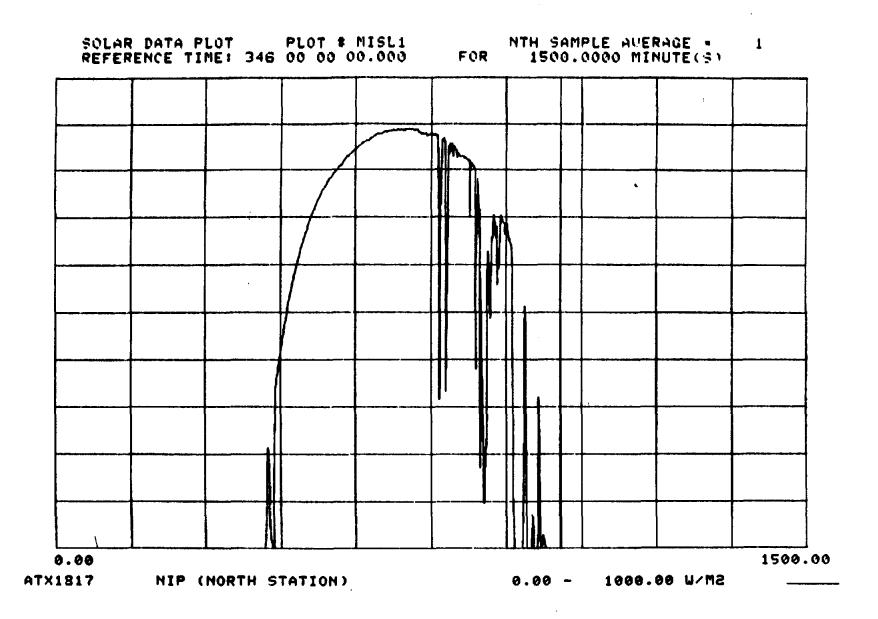


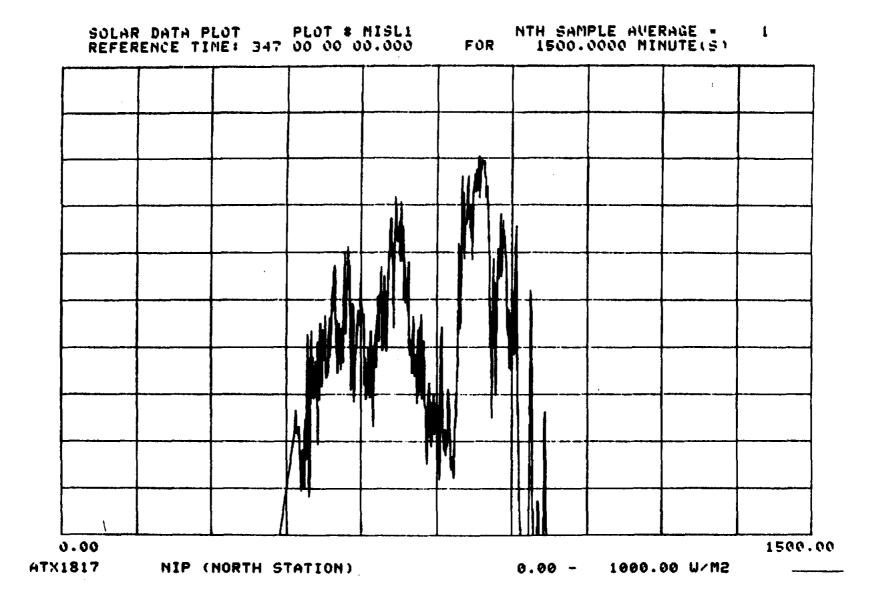




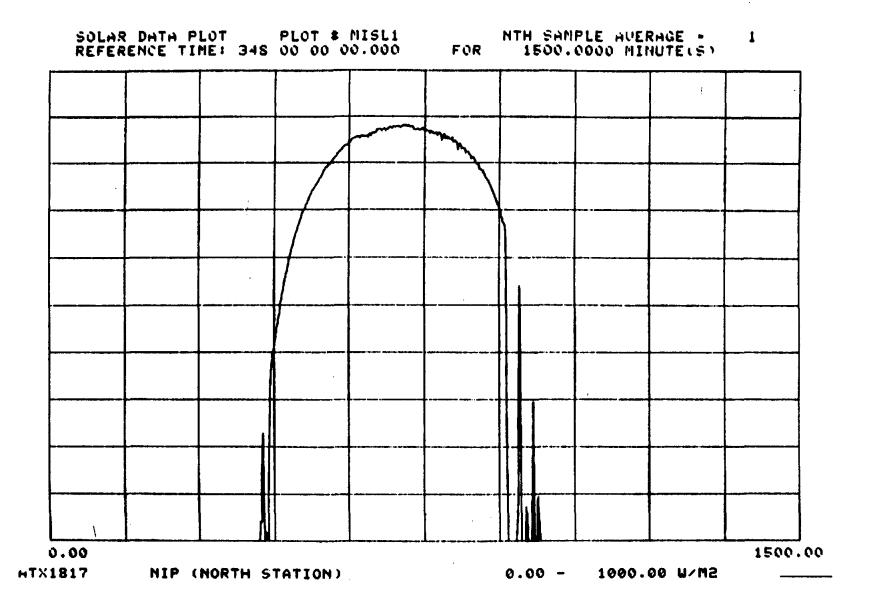


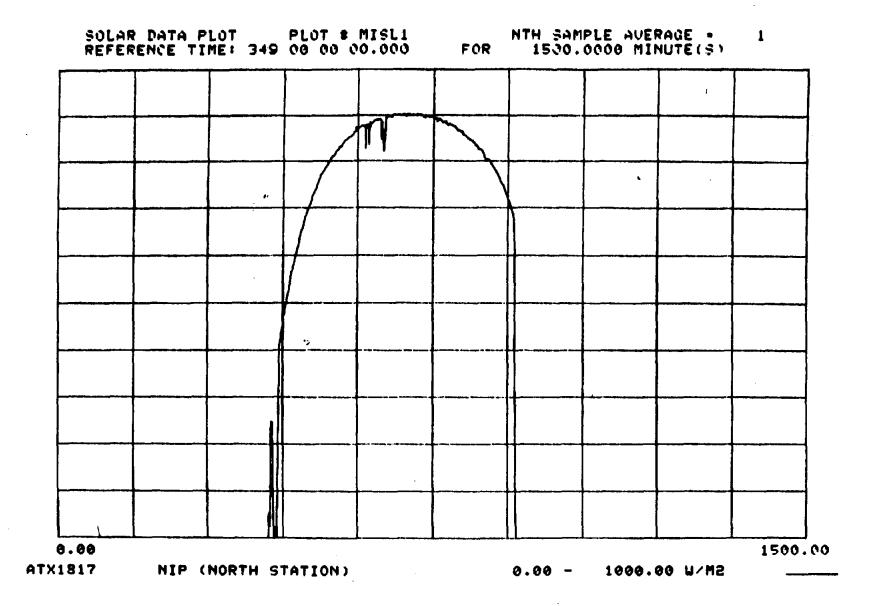


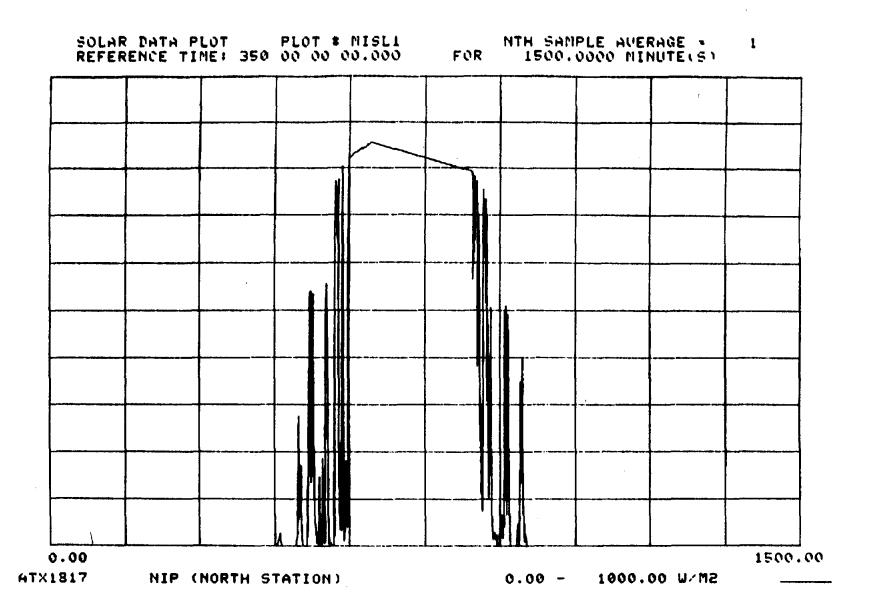




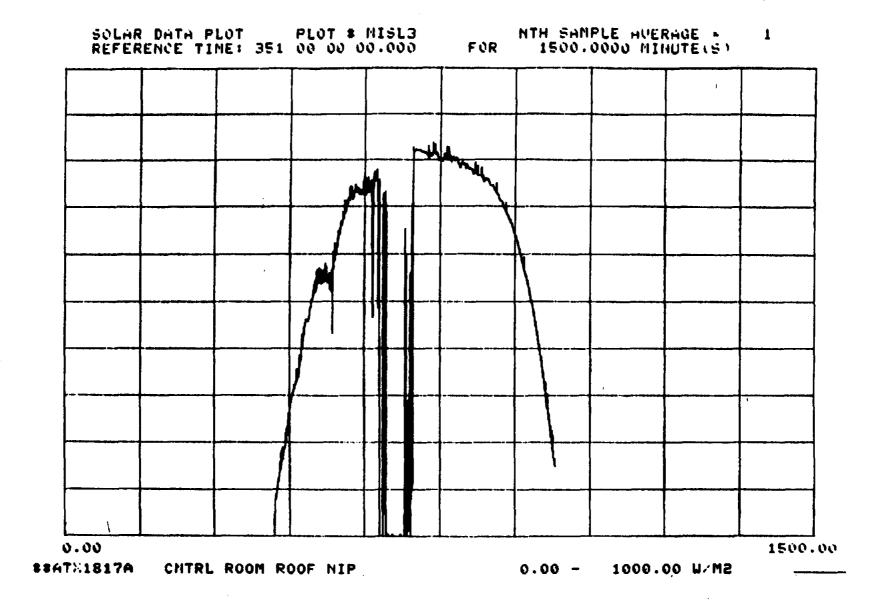


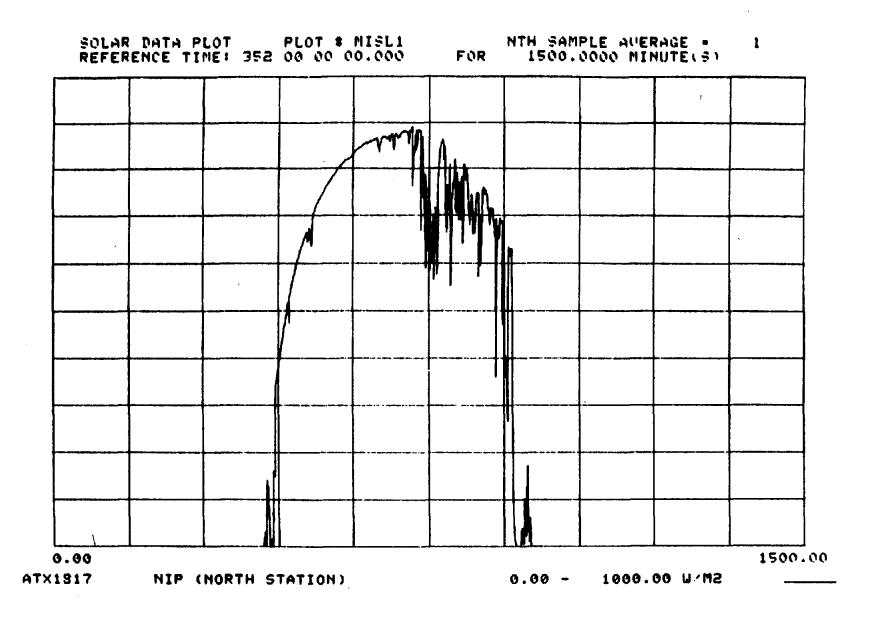




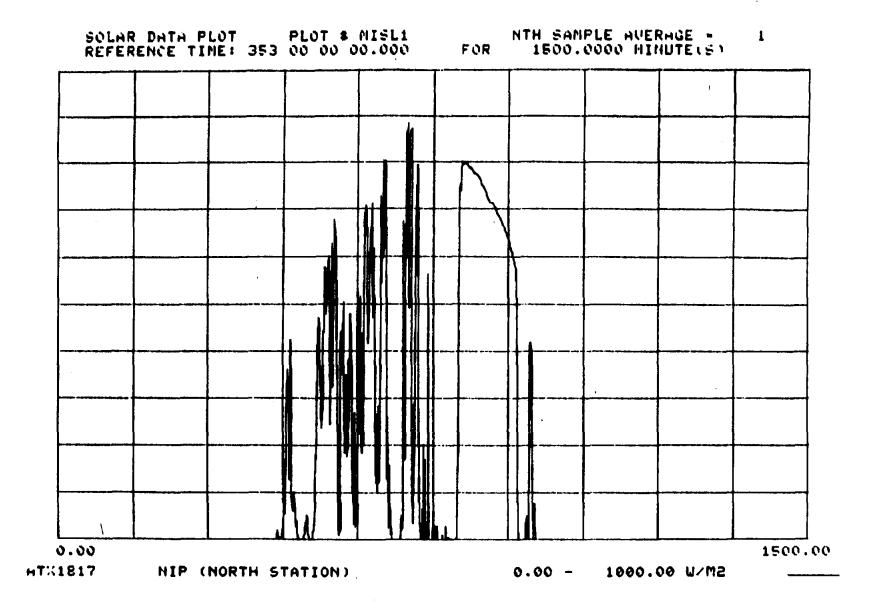


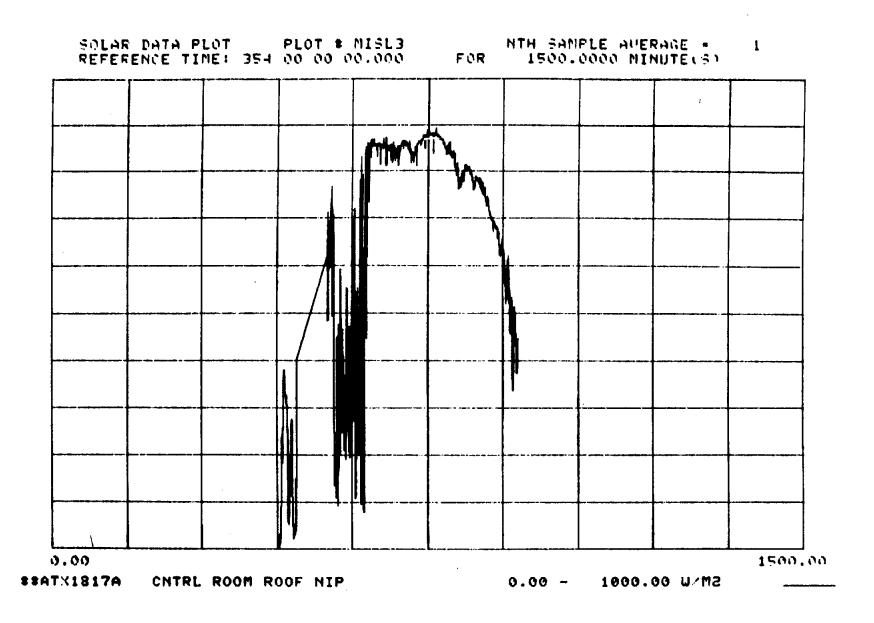


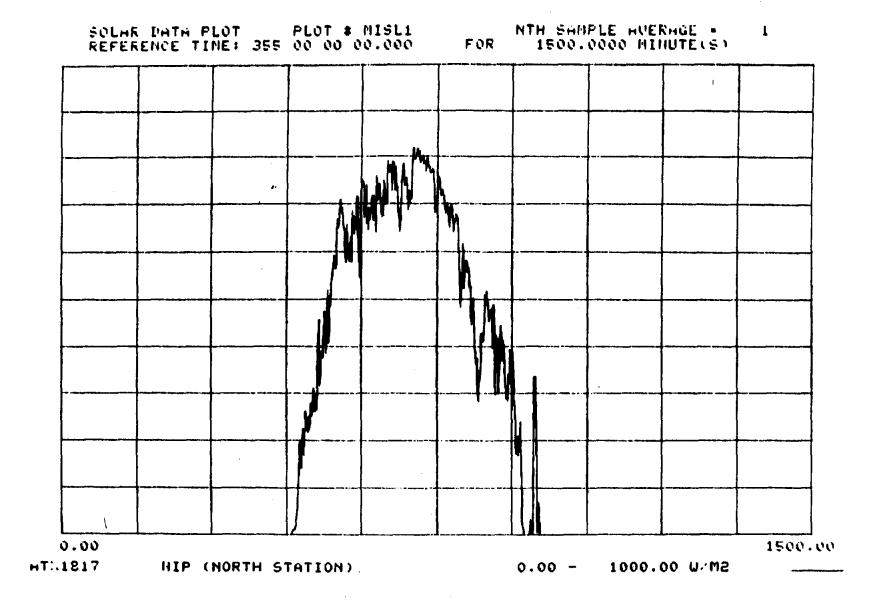


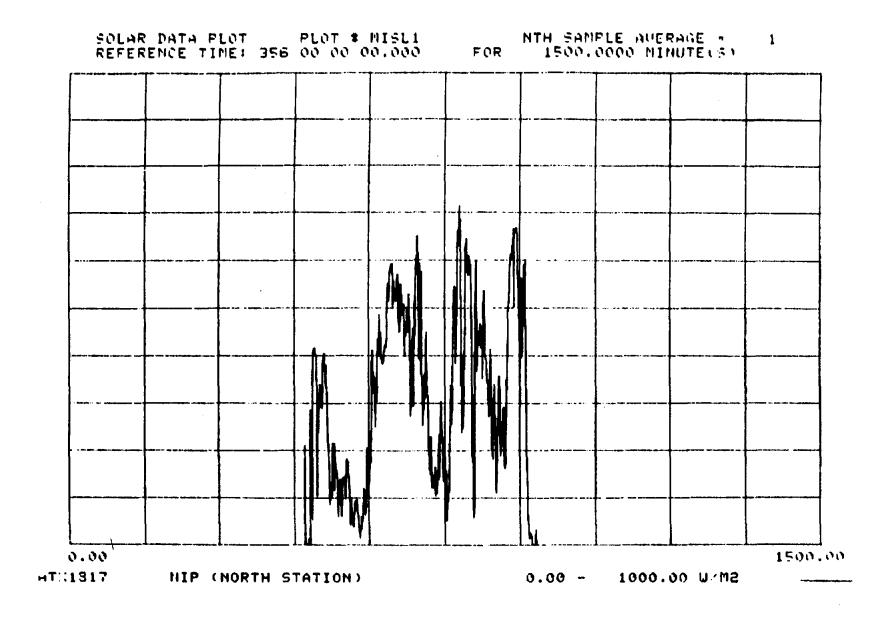


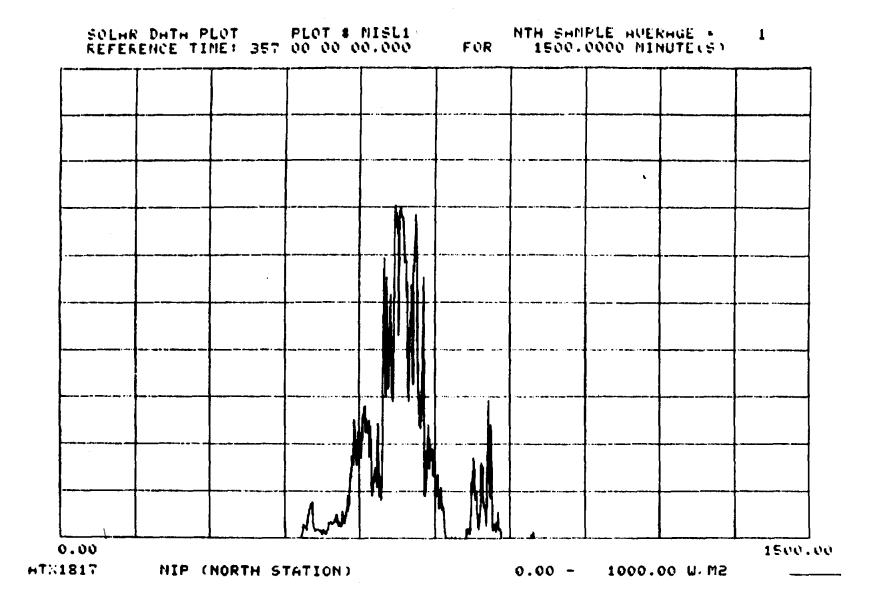


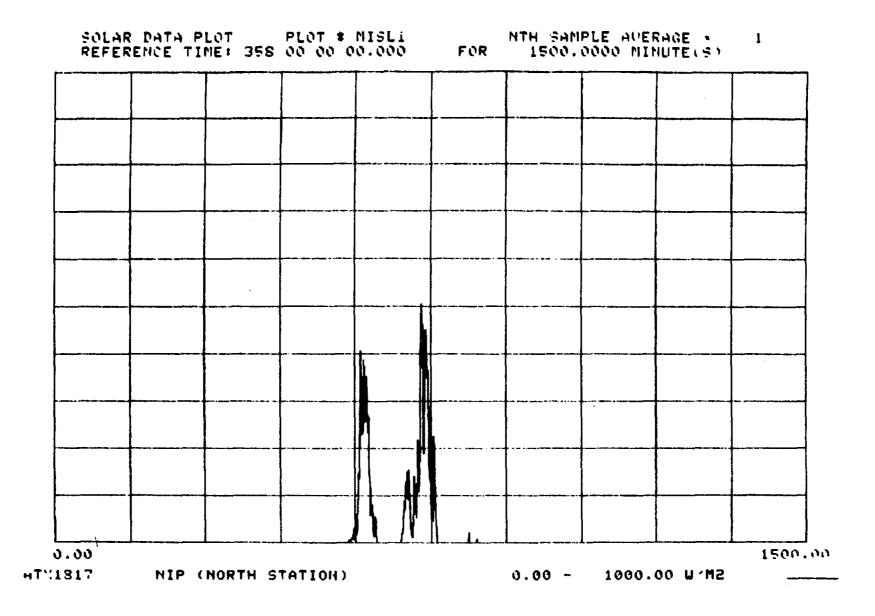


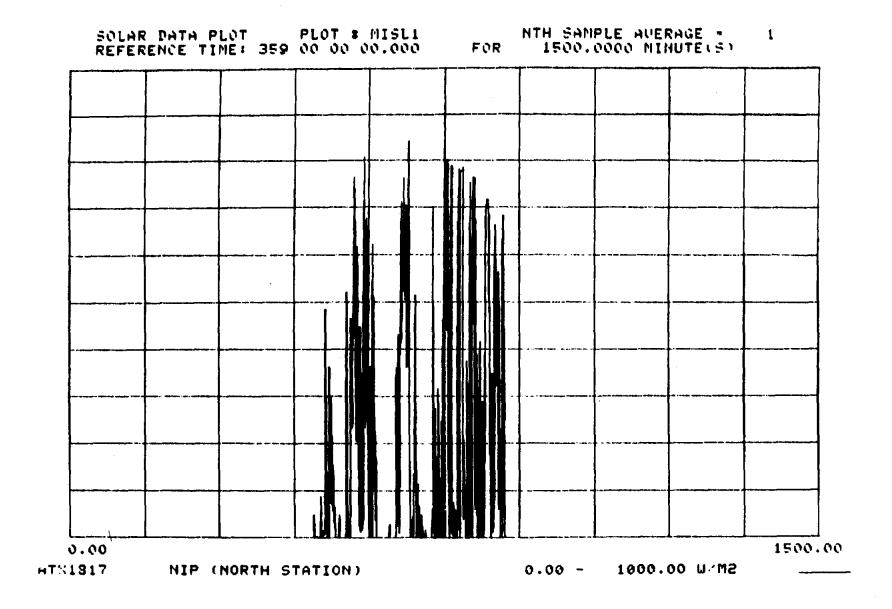


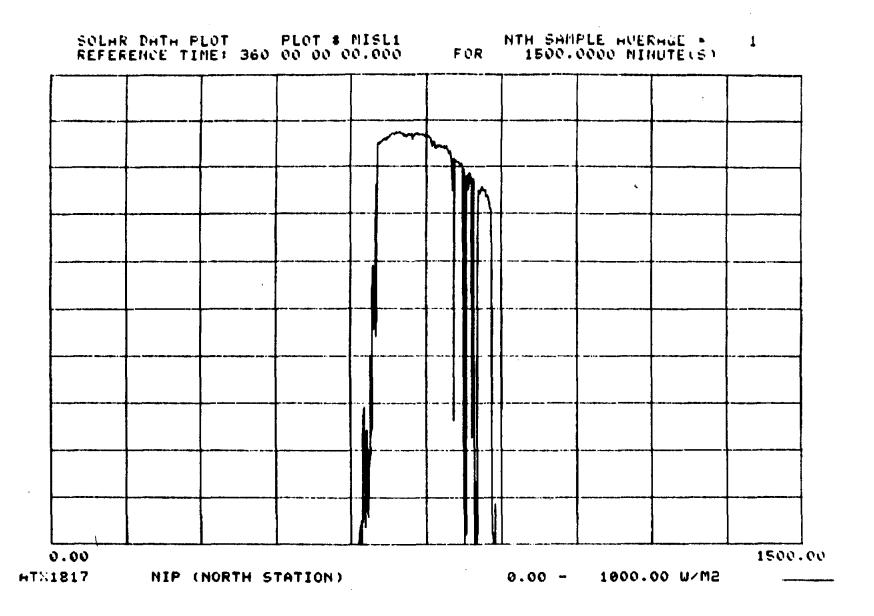


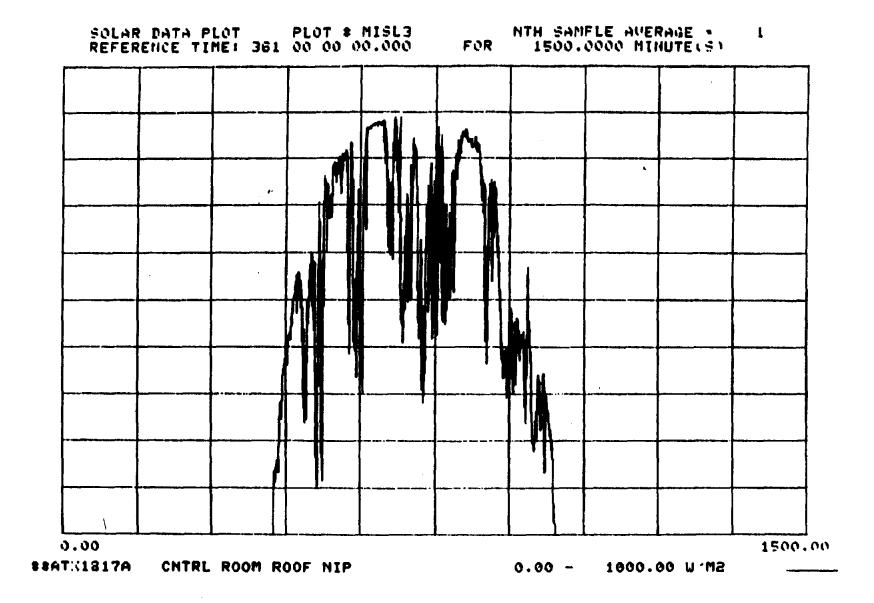


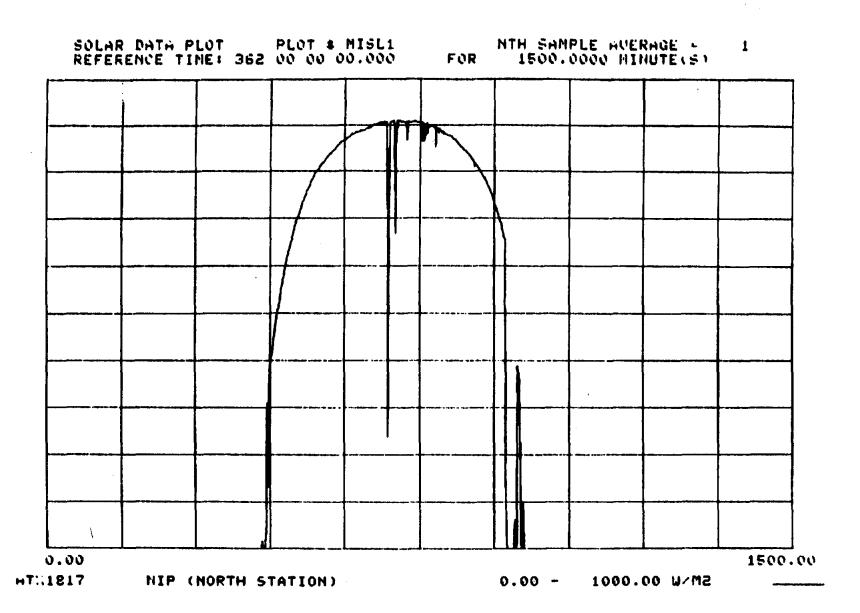


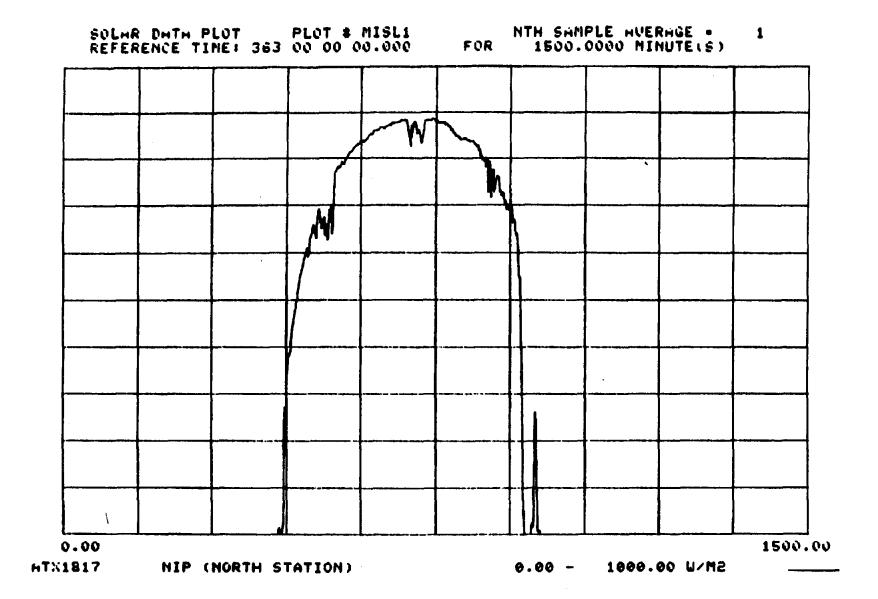


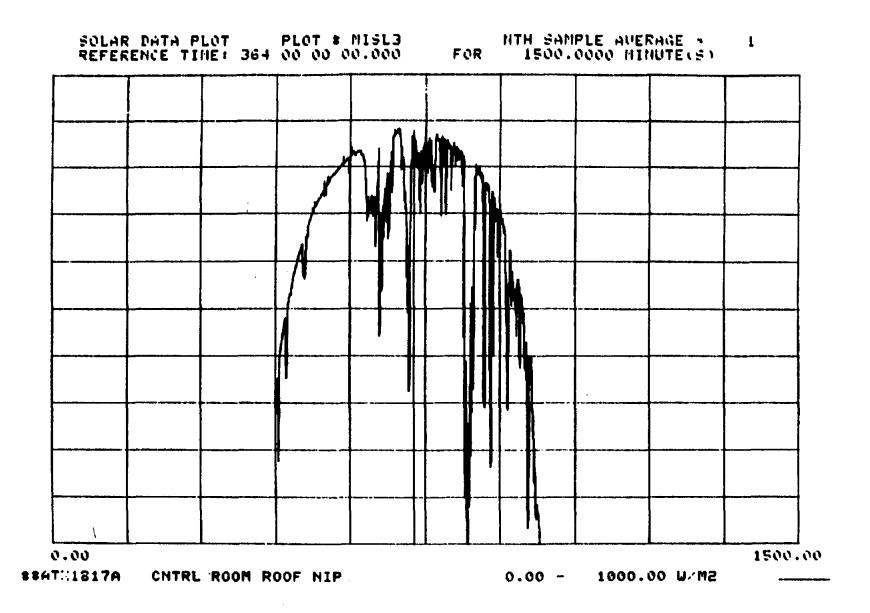


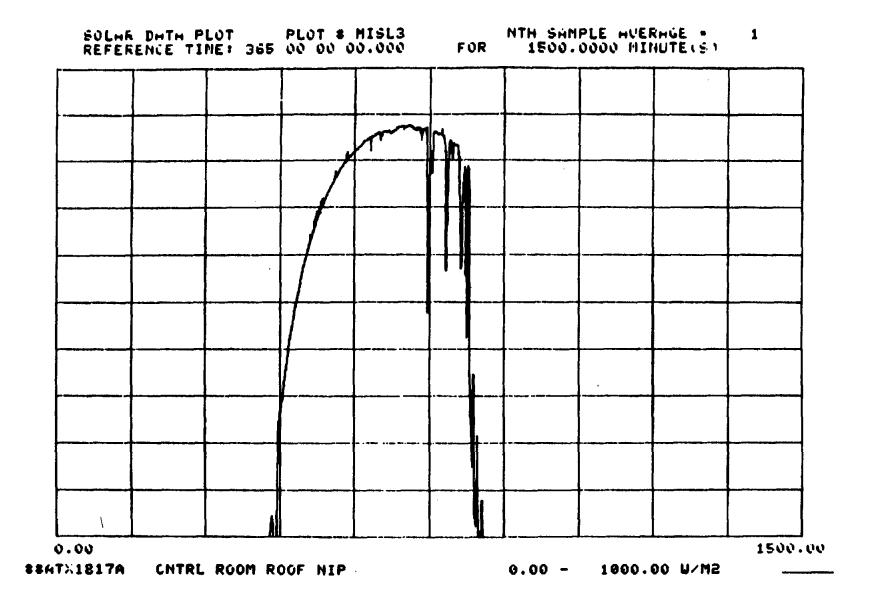






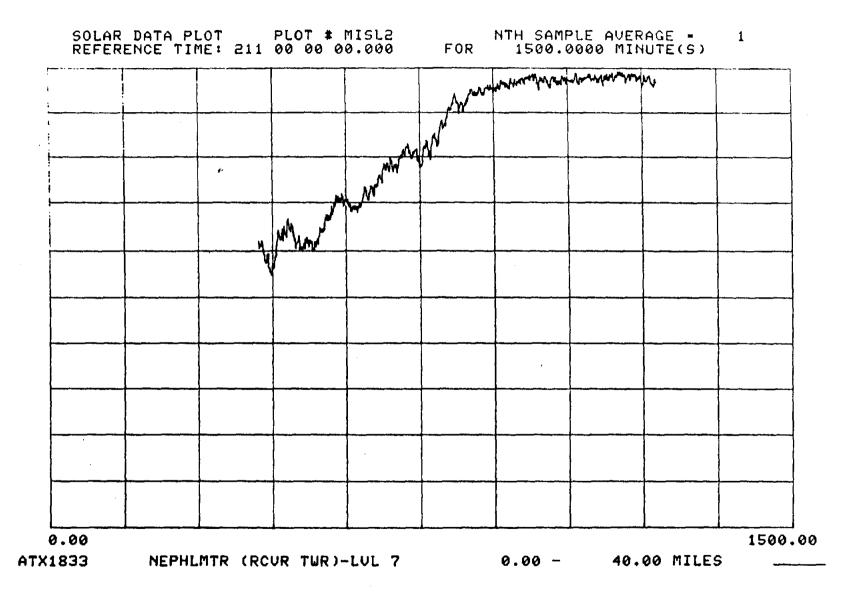


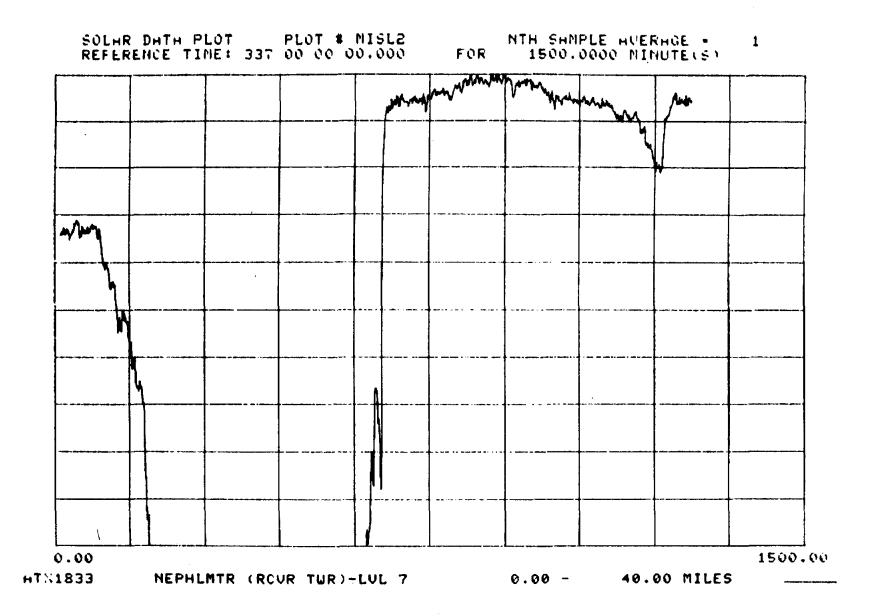


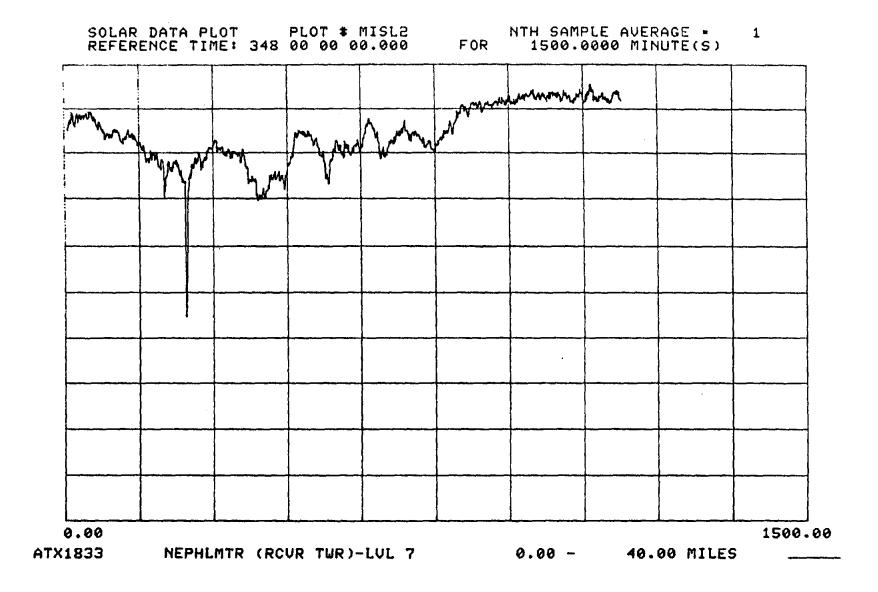


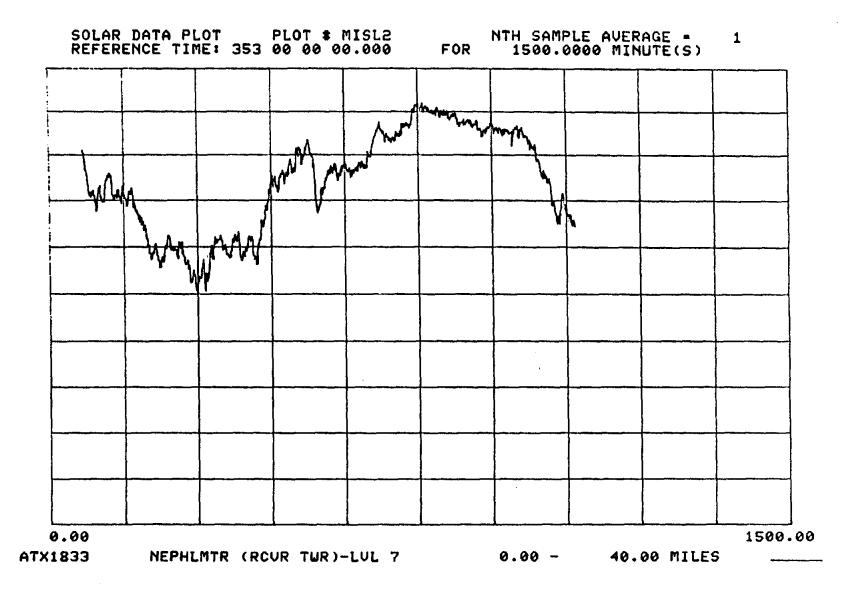
## 5.8 NEPHALOMETER DATA

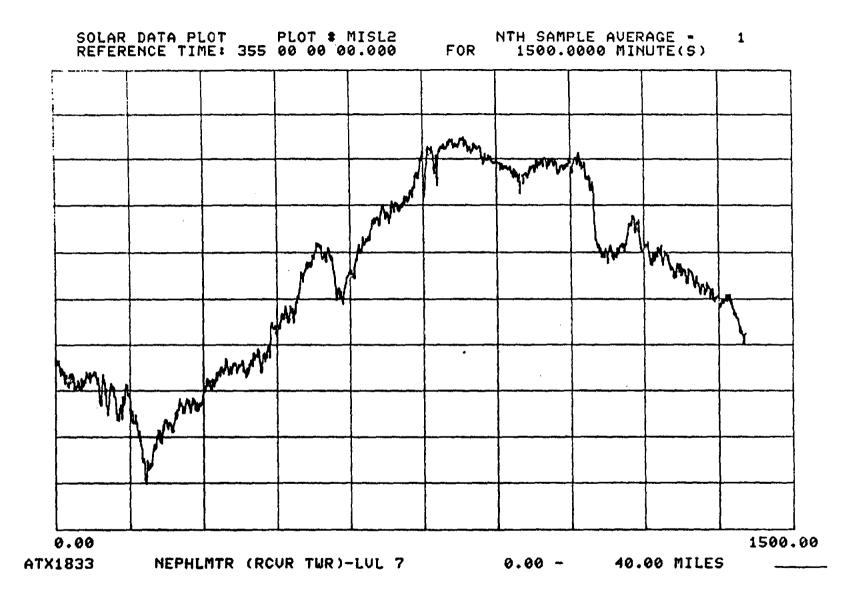
An integrating nephalometer (tag ID ATX 1833) is installed and operating at the Solar One site on the 7th level of the receiver tower. Data from this instrument can be used to detect air pollution and provide a measure of atmospheric particle contamination, as indicated by variations in visibility values. Plots of visibility for 9 days during 1983 are included in this report. the specific days are: 211, 337, 348, 353, 355, 359, 361, 362, and 364. The instrument was recalibrated early in the fourth quarter of 1983, so the data from days 337 through 364 are for the same calibration. An analysis of these data relative to other meteorological parameters is underway to identify any correlations. At present, there is no apparent correlation between nephalometer data and cloud activity. Examination of dewpoint, barometric pressure, and wind data in parallel with nephalometer data may yield more fruitful results.

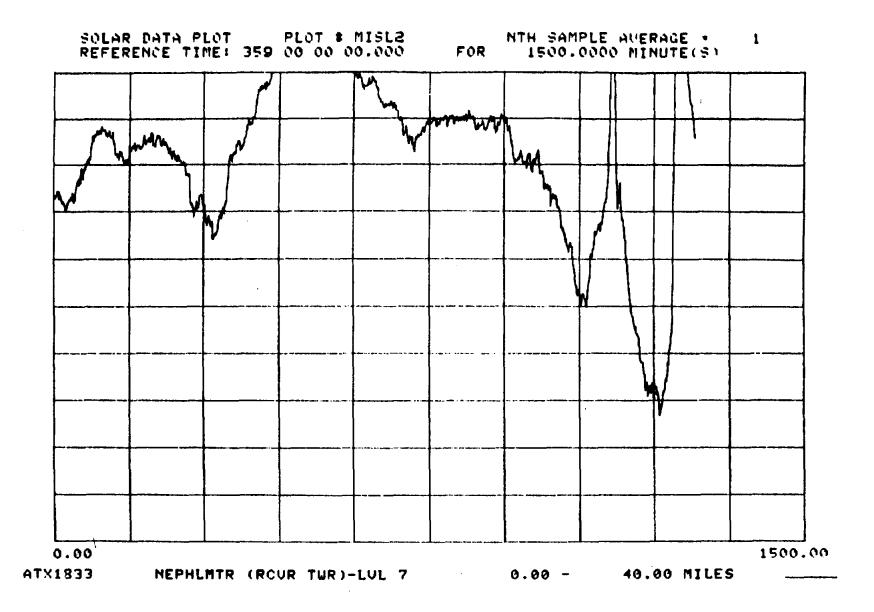


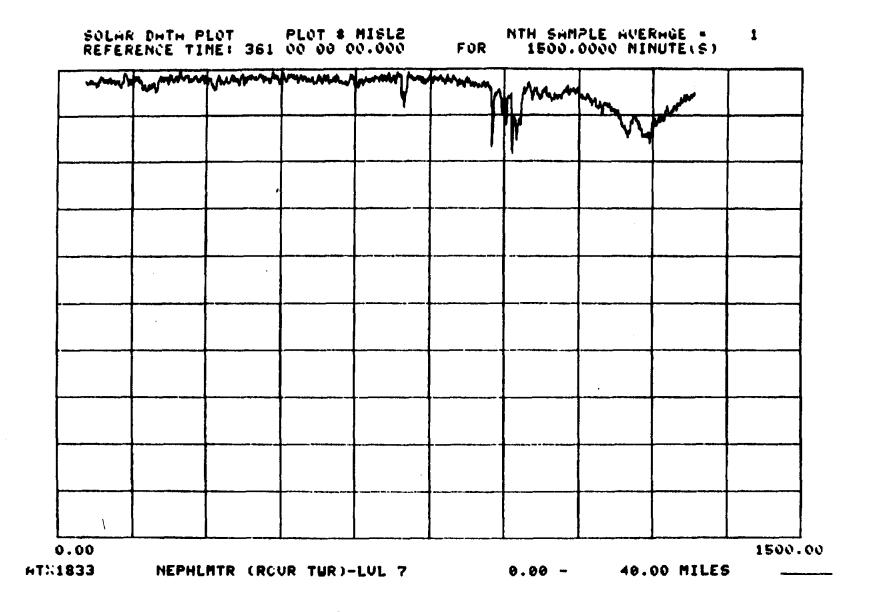


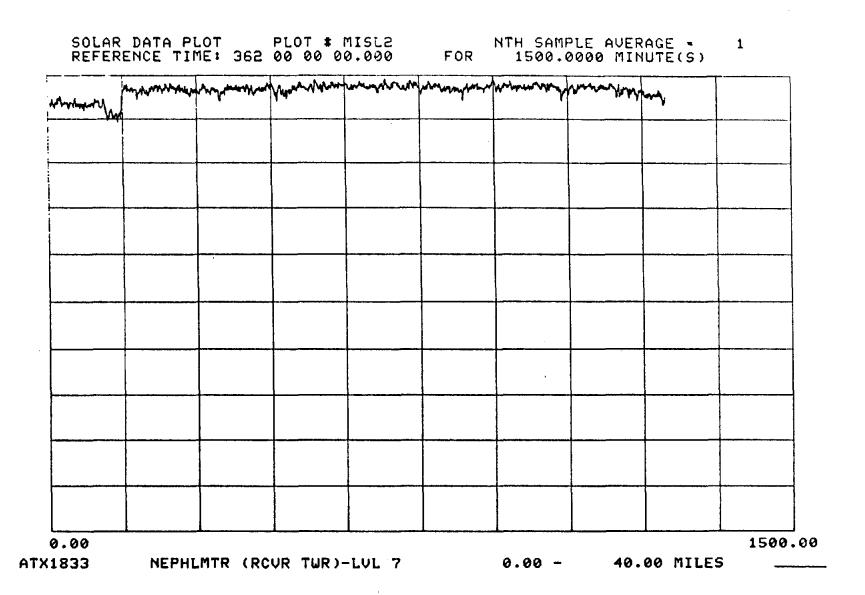


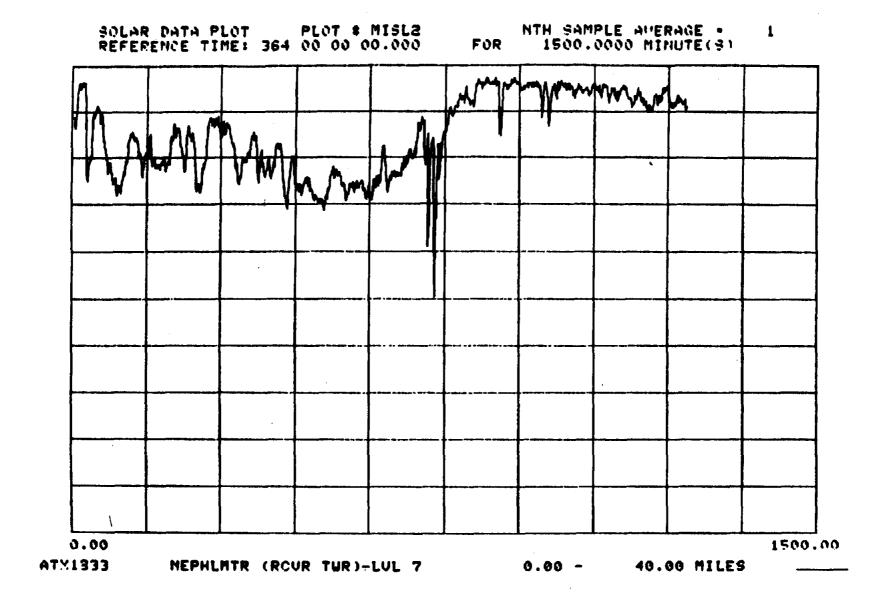












## 5.9 HAIL DATA

The Solar One Site experienced at least one incident of hail in 1983. It occurred sometime in August, with the specific date unknown, since the cubes were not monitored on a daily basis. This also means that it is possible that there was more than one incident, though it is not likely, based upon the hail cube analyses performed. The hail cube configuration and sand shield installation are shown in Figures 38, 39, and 40 on pages 52, 53, and 54 of this report. Six hail cubes are installed at the four meteorological stations and the two collector field locations as shown in Figure 8 on page 16 of this report.

The six hail cubes were removed and shipped to the State Water Survey Division of the Illinois Department of Energy and Natural Resources in Champaign, Illinois for analysis. Dr. Wayne M. Wendland, Head of the Climatology and Meteorology Section, was the principal point of contact for this contracted effort. The data contained in this section are the results of the hail cube analyses performed.

Table 11 shows the size distribution of hail stones which impacted the tops of the hail cubes analyzed. It should be noted that the hail cube at the east station had no indentations; therefore, the results presented here are for the five hail cubes as indicated. The class intervals are presented in centimeters, although they were measured in tenths of an inch; therefore, there appear to be ranges without measurements between each of the class intervals. The size distributions for the west station, northwest quadrant, and the north station, are rather similar, whereas those for the northeast quadrant and the south station appear to be from a different population. This is probably the result of a small sample size on some pads because of the small scale size of the hail storm that yielded no hail stone impressions on the east station cube and a different size distribution at the northeast quadrant and south station locations relative to the remaining three hail cube locations. This suggests that the hail storm center was located to the northwest of the collector field. Also note from Table 11 that three of the hail cubes suggested that the hail arrived from the west-northwest, whereas two suggested the northwest. (270° indicates west and 360° indicates north at Solar One.)

Table 12 shows the kinetic energy applied to the top surface of each of the five hail cubes, by class interval, and as a total number. It can be seen from the table that the total kinetic energy deposited ranged from 6.56 x  $10^6$  gm-cm<sup>2</sup>/sec to 1.96 x  $10^8$  gm-cm<sup>2</sup>/sec. If the south station and northeast quadrant are neglected, the range is much smaller, from 8.24 x  $10^7$  gm-cm<sup>2</sup>/sec to 1.96 x  $10^8$  gm-cm<sup>2</sup>/sec.

Table 13 shows the momentum transferred to the top surface of each of the five hail cubes. The total momentum ranges from 2.60 x  $10^3$  gm-cm/sec to 1.13 x  $10^5$  gm-cm/sec. However, if the south station and northeast quadrant are neglected, the values range from 4.70 x  $10^4$  gm-cm/sec to 1.13 x  $10^5$  gm-cm/sec.

Table 11. SOLAR ONE 1983 HAIL DATA - SIZE DISTRIBUTION OF HAILSTONES FROM TOPS OF FIVE HAIL CUBES\*

CLASS INTERVAL (CM)	WEST STATION	NORTHWEST QUADRANT	NORTH STATION	NORTHEAST QUANDRANT	SOUTH STATION
< 0.25	43	80	55	5	34
0.25-0.36	8	20	12	2	5
0.38-0.48	49	46	21	2	5
0.51-0.61	44	29	22	1	5
0.64-0.74	21	22	9	1	2
0.76-0.86	11	11	3	-	1
0.89-0.99	0	2	1	-	-
1.01-1.12	2	<u>-</u>		-	_
Total Indentations	178	210	123	11	52
Direction fro		320°	295°	320°	290°
which hail hit the hail cube** NW		NW	WNW	NW	WNW

<sup>\*</sup>No indentations were found on the east station hail cube.

<sup>\*\*</sup>Determined by relative impact frequency on sides.

Table 12. SOLAR ONE 1983 HAIL DATA - KINETIC ENERGY APPLIED TO TOPS OF HAIL CUBES

MIDPOINT OF CLASS	(UNITS ARE GM-CM <sup>2</sup> /SEC)				
INTERVAL (CM)	WEST STATION	NORTHWEST QUADRANT	NORTH STATION	NORTHEAST QUADRANT	SOUTH STATIC
0.12	6.68 x 10 <sup>5</sup>	1.67 x 10 <sup>6</sup>	1.0 x 10 <sup>6</sup>	1.67 x 10 <sup>5</sup>	<b>4.</b> 17 →
0.17	1.16 x 10 <sup>8</sup>	1.09 x 10 <sup>8</sup>	$5.0 \times 10^{7}$	4.76 x 10 <sup>6</sup>	1.19 x
0.22	$2.45 \times 10^{7}$	1.62 x 10 <sup>7</sup>	1.23 x 10 <sup>7</sup>	5.57 x 10 <sup>5</sup>	<b>2.</b> 79 →
0.27	$2.30 \times 10^{7}$	2.41 x $10^7$	9.86 x 10 <sup>6</sup>	1.10 x 10 <sup>6</sup>	2.19 >
0.32	2.17 x 10 <sup>7</sup>	$2.17 \times 10^{7}$	5.92 x 10 <sup>6</sup>		<b>1.</b> 97 ≯
0.37		6.58 x 10 <sup>6</sup>	3.29 x 10 <sup>6</sup>		
0.42	$1.06 \times 10^{7}$			<b>** =</b> *	~ ~
Total Kinetic Energy	1.96 x 10 <sup>8</sup>	1.79 x 10 <sup>8</sup>	8.14 x 10 <sup>7</sup>	6.58 x 10 <sup>6</sup>	1.93 >

Table 13. SOLAR ONE 1983 HAIL DATA - MOMENTUM TRANSFERRED TO TOPS OF HAIL CUBES

MIDPOINT		(UNITS ARE GM-			
OF CLASS INTERVAL (CM)	WEST STATION	NORTHWEST QUADRANT	NORTH STATION	NORTHEAST QUADRANT	SOUTH STATION
0.12	1,320	3,300	1,980	330	825
0.17	20,237	18,998	8,673	826	2,065
0.22	38,280	25,230	19,140	870	4,350
0.27	12,096	12,672	5;184	576	1,152
0.32	28,952	28,952	7,896		2,632
0.37		8,220	4,110		
0.42	12,436	w **			
				<del></del>	
Total Momentum	1.13 x 10 <sup>5</sup>	9.74 × 10 <sup>4</sup>	$4.70 \times 10^4$	$2.60 \times 10^3$	1.10 x 10 <sup>4</sup>

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