# PDOC-094 

Sandia National Laboratories,

10 MWe Solar Thermal Central Receiver Pilot Plant

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SOLAR FACILITIES DESIGN INTEGRATION

PLANT MAINTENANCE/TRAINING MANUAL (RADL ITEM 2-37)
SECTION 3 - ELECTRICAL APPARATUS, BOOK 1 OF 2

Revised September 1982
July 1981

WORK PERFORMED UNDER
CONTRACT DE-AC03-79SF10499
MCDONNELL DOUGLAS ASTRONAUTICS COMPANY 5301 BOLSA AVENUE
HUNTINGTON BEACH, CA 92647

## U.S. Department of Energy

## 10 MWe Solar Thermal Central Receiver Pilot Plant Solar Facilities Design Integration

# PLANT MAINTENANCE/TRAINING MANUAL (RADL ITEM 2-37) SECTION 3 - ELECTRICAL APPARATUS, BOOK 1 OF 2 

July 1981
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## SECTION 3-ELECTRICAL APPARATUS

## INSTRUCTIONS:

1. This update is issued to incorporate corrections and additions to the preface, table of contents, and to incorporate additional information in paragraphs 3.1 Transformers, 3.2 Motor Control Centers, 3.3 Substations, 3.4 Junction Boxes, 3.5 Switchgear, and 3.6 Power Panels. This section has been printed in two parts for this update. Discard the original July 1981 issue as the content has been included in this printing.

This document is provided by the McDonnell Douglas Astronautics Company (MDAC) in accordance with Department of Energy Contract Number DE-AC03-79SF10499, Reports and Deliverables List Item 2-37. The material presented here is intended for training and maintenance usage by Southern California Edison Operations Personnel.

Specific notes on the organization and content of the document are as follows:

1. This document is organized in major sections that reflect the top level breakdown of the Master Equipment List as defined in RADL Item 2-19. This is in contrast to the subsystem approach used in designing the plant, however, is consistent with the Southern California Edison operating plant equipment lists.

Section 1 - Rotating Apparatus
Section 2 - Stationary Apparatus
Section 3 - Electrical Apparatus
Section 4 - Valves
Section 5 - Instrumentation
Section 6 - Control and Data Systems
Section 7 - Collector System
Section 8 - Special Heliostat Instrumentation and Meteorological
Measurements Equipment
Section 9 - Heating Ventilating and Air Conditioning
Section 10 - Facilities
2. Assignments to categories are made on the basis of the lowest level tag numbers. For example, maintenance information for the thermal storage extraction pump skid assembly (SA-309) is not listed in the stationary apparatus section, but broken down to the generic categories as defined by the tag number; i.e., pumps (Section 1.2), air operated stop valves (Section 4.2), pressure transmitter (Section 5.2), etc.
3. The Process Instrumentation Section (Section 5.0) is organized on the basis of sensor type as defined by the first letter of the designating tag number. It contains sensor-related information only. Signal conditioning equipment is treated in Section 6.0.
4. The information on the Collector System, which was provided by the Martin Marietta Corp. (MMC) and the major items of the Electrical Power Generation System equipment, provided by Southern California Edison is not provided herein. However, the various sections were structured for their inclusion where applicable.

Technical questions concerning this RADL Item should be directed to Mr. R. G. Riedesel at (714) 896-3357 or Mr. R. J. Perkins at (714) 896-3073.
1.0 Rotating Apparatus
1.1 Turbine-Generator
1.2 Pumps
1.3 Fans
1.4. Air Compressor
1.5 Blowers
1.6 Centrifuges
2.0 Stationary Apparatus
2.1 Heat Exchangers
2.2 Receiver Panels
2.3 Tanks, Vessels, and Receivers (Air or $\mathrm{GN}_{2}$ )
2.4 Deaerator
2.5 Condenser (turbine-generator)
2.6 Desuperheaters
2.7 Filters and Strainers
2.8 Demineralizers
2.9 Heaters
2.10 Dryers
2.11 Separators
2.12 Ullage Gas Supply and Conditioning
2.13 Auxiliary Boilers
2.14 Sewage Treatment Plant
2.15 Expansion Joints
2.16 Orifice Plates
3.0 Electrical Apparatus
3.1 Transformers
3.2 Motor Control Centers
3.3 Substations
3.4 Junction Boxes
3.5 Switchgear
3.6 Power Panels
3.7 Cables
3.8 Lighting
4.0 Valves
4.1 Modulating Control and Related Solenoid Valves
4.2 Air Operated Stop and Related Solenoid Valves
4.3 Motor Operated Vaives (MOV)
4.4 Other Solenoid Valves
4.5 Safety-Relief Valves
4.6 Check and Stop Check Valves
4.7 Manual Valves
4.8 Pressure Regulator
4.9 Rupture Discs
4.10 Traps
5.0 Process Instrumentation
5.1 ( $T$ ) Temperature
5.2 (P) Pressure and Differential Pressure
5.3 (F) Flowrate
5.4 (L) Level
5.5 (W) Weight/Force
5.6 (A) Analysis
5.7 (I) Current
5.8 (E) Voltage
5.9 (J) Power
5.10 (Y) Heat
5.11 (S) Speed/Frequency
5.12 (C) Conductivity
5.13 (Z) Position
5.14 (0) Deflection
5.15 (X) Vibration
6.0 Control and Data Systems
6.1 Subsystem Distributed Process Control (SDPC)
6.2 Control Console (CON)
6.3 Interlock Logic System (ILS)
6.4 Signal Conditioning Unit (SCU)
6.5 Red-Line Unit (RLU)
6.6 Data Acquisition System (DAS)
6.7 Data Acquisition Remote Multiplexer System (DARMS)
6.8 Operational Control System (OCS)
6.9 Beam Characterization System (BCS)
6.10 Special Heliostat Instrumentation and Meteorological MeasurementSystem (SHIMMS)
6.11 Solid State Relays
6.12 T.C. Reference Junctions
6.13 MCS Timing System
7.0 Collector System
7.1 Heliostat Assembly
7.2 Heliostat Drive System
7.3 Heliostat Pedestal Assembly
7.4 Heliostat Controller (HC)
7.5 Heliostat Field Controller (HFC)
7.6 Computer Control System
8.0 Special Heliostat Instrumentation and Meteorological Measurements Systems Equipment
8.1 Meteorological Equipment
8.2 Special Heliostat Instrumentation
9.0 Heating, Ventilating, and Air Conditioning
9.1 Material Data
9.2 Thermal Storage Control Buildings Cooling
9.3 Thermal Storage Electrical Equipment Building Cooling
9.4 Thermal Storage Control Building Heating

### 10.0 Facilities

10.1 Fire Protection
10.2 Elevator
10.3 Buildings
10.4 Electronics Enclosures
10.5 Receiver Tower
10.6 Pipe Rack

Equipment Number

PSS 0001
SCE 0003
SCE 0004
SCE 0005
SCE 0006
3.1 .1
3.1 .2
3.1 .3
3.1 .4
3.1 .5

P\&ID Dwg.
Number
3.1.1 TSS Load Center Transformer
3.1.1.1 Identification
Tag Number Description
PSS 0001
480 Volt load Center A
3.1.1.2 Description
Manufacturer: Abbott Power Corporation 7650 Stage Road Buena Park, CA 90620
Part No: See attached Abbott Power Corp manualTable of contents of contents forequipment list.
3.1.1.3 Vendor
Abbott Power Corporation
3.1.1.4 Procurement SpecificationStearns-Roger Spec F235.1 (DOE Spec 40E700-19S)
3.1.1.5 Operation/Maintenance
See attached Abbott Power Corporation manual
Note: Instruction for the 480 V motor control centers $B$ and $C$are also included.

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B/M NO.
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30A, 2POLE FUSE HOLDERS 53-3 CATALOG PAGE 34-1

DRAWINGS

## BILL OF MATERIAL

## CUSTOMER STEARNS-ROGER, INC. P.O. BOX 5888 DENVER, CO 80217

USER SOLAR PILOT PLANT

## CUSTOMER ORDER \# 4004621700

CUSTOMER SPECIFICATION $\neq$ C-21700SRF235-1 SECTION I, II \& III

UOB DESCRIPTION
480 VOLT LOAD CENTER INCLUDING:
(1) $5 \mathrm{KV}, 600 \mathrm{~A}$ LOAD BREAK SWITCH
(1) 1000 KVA POWER TRANSFORMER
(1) 480 V INDOOR SWITCHGEAR
(1) 480V 1600 AMP NON-SEGREGATED BUS DUCT
(2) 480 V MOTOR CONTROL CENTER


## NOTES

I

## BUS

PLATING ALUMINUM WITH TIN. PLATED JOINTS
RATING AS SHOWN IN SINGLE LINE DIAGRAM
SIZE AS SHOWN IN SECTION VIEW DRAWING
BRACING 22KA
BELLEVILLE TYPE SPRING WASHERS SHALL BE USED ON BUS JOINTS WITH STEEL BOLTS.

PAINT ANSI \#61 FOR SWITCHGEAR, ANSI \#70 FOR LOAD INTERRUPTER SWITCH DRAWINGS APPROVAL 4 REPRODUCIBLES, 8 PRINTS

FINAL 4 REPRODUCIBLES, 8 PRINTS
III. MECHANICAL NOTES

1. DESIGN SHALL COMPLY WITH UBC SEISMIC ZONE \#3. EQUIPMENT DESIGNED TO WITHSTAND LATERAL SEISMIC FORCES GENERATED BY A GROUND ACCELERATION OF 0.25G. SALIFORNIA CODE APPLIES.
2. EQUIPMENT TO HAVE A SERVICE LIfE OF (30) YEARS.
3. DOORS AND PANELS SHALL BE FLANGED AND ALL CORNERS SHALL BE WELDED AND GROUND OR FORMED ROUND. DOORS AND PANELS SHALL BE HELD IN PLACE BY SLOTTED HEAD SCREWS WITH RETAINERS WHICH SHALL FIT INTO ADJUSTABLE NUTS ON THE FRAME.
4. PROVIDE SUITABLE MEANS FOR LIFTING THE SWITCHGEAR,
5. SHIPPING SECTIONS TO BE IN WATER TIGHT. AND DUST PROOF CONTAINERS AS FAR AS COMMERCIAL PRACTICE ALLOWS.
IV WIRING
6. REFER TO SPECIFICATION JF16.01.01 PAGE 5 TO 7 FOR WIRING DIAGRAM INSTRUCTIONS.
7. EACH TERMINAL BLOCK SHALL HAVE AT LEAST $20 \%$ SPARE TERMINALS


## NOTES (CONTINUED)

IV WIRING (CONTINUED)
3. SHORTING TYPE TERMINAL BLOCKS REQUIRED FOR CURRENT TRANSFORMER
SECONDARIES.
4. USE RING TONGUE ON WIRING.
c) 5. ALL terminals to have covers. TEST

ALL BUSES AND POWER CIRCUIT BREAKERS SHALL UNDERGO A ONE-MINUTE 60HZ DIELECTRIC WITHSTAND TEST. THE TEST VOLTAGE SHALL BE 2200 VOLTS.


## REVISIONS

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline REV. \& 8/M \& page \& \multicolumn{2}{|l|}{description} \& Br \& OATE <br>
\hline B
B

$C$
$C$
$C$

D \& \[
$$
\begin{gathered}
5049-1 \\
5049-1 \\
5049-1 x \\
5049-1 \\
5049-1 \\
5049-1 \\
5049-1 x \\
5049-1 x \\
5049-1 x
\end{gathered}
$$

\] \& ( $\begin{gathered}3 \\ 6 \\ 2 \\ 1,2 \\ 5 \\ 5 \\ 5,6 \\ 3 \\ 2 \\ 2\end{gathered}$ \& \multicolumn{2}{|l|}{| revised vendor item 8-1 |
| :--- |
| ADDED ITEM 72-1 and 73-1 |
| REVISED NOTE FOR PAINT |
| REVISED DESCRIPTION ITEMS 1-1, 1-2, \& 1-3 PER CUSTOMER |
| ADD ITEM 56-2 |
| REVISED DESGRIPTION.ITEM 56-1.56-2 8 57-1 |
| ADD NOTE $\# 5$ |
| revised mechanical note \#1, adoed california code |
| APPLIES. NOTE I TO ADD STEEL BOLTS TO BELLEVILLE SPRING WASHERS. |} \& AC \& | $10 / 8 / 80$ |
| :--- |
| $11 / 5 / 80$ |
| $11 / 5 / 80$ |
| $11 / 2980$ |
| $12 / 3 / 80]$ |
| $12 / 8 / 80$ |
|  | <br>


\hline  \&  \& \multicolumn{2}{|l|}{| Afbbott Douver Corporation |
| :--- |
| 7650 stage road - buena park - california 90620 A MEMBER OF HEMA |} \& |l| ${ }^{\text {PROJ. NO. }}$ \&  \& \[

E. 5
\] <br>

\hline
\end{tabular}

| $1-5049-1-1$ | ELEVAT ION AND BASE PLAN SWGR. |
| :--- | :--- |
| $1-5049-1-2$ | SECTION VIEW SWGR. |
| $1-5049-2-1$ | ELEVATION AND BASE PLAN MCC |
| $2-5049-1-1$ | SINGLE LINE DIAGRAM SWGR. |
| $3-5049-1-1$ | THREE LINE DIAGRAM SWGR. |
| $3-5049-2-1$ | THREE LINE DIAGRAM MCC-B |
| $3-5049-2-2$ | THREE LINE DIAGRAM MCC-C |


| $\begin{array}{r} \text { DESIGN } \\ A C \end{array}$ | ELEC. ${ }^{\text {d }}$ | DESIGN | MECM. ${ }^{\text {d }}$ | $\begin{aligned} & \text { DRAWN ET ' } \\ & \text { AC/MA } \\ & \hline \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { DATE } \\ 9 / 12 / 80 \end{array}$ | EHK. | DATE | AP¢ 0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Afbbott Dowier ©opporation <br> 7GEC STAGE ROAD. BUENA DARK•CALIFORNIA 90620 A MEMBER OF YEMA |  |  |  |  |  |  | PROd. NO. ' 5049 |  |  |
|  |  |  |  |  |  |  | DWG. NO. ' 5049-1X |  |  |
|  |  |  |  |  |  |  | PAGE $\quad 5$ OF_ 5 |  |  |




DESIGNER EL. $\qquad$ ME.
$\qquad$ of $\qquad$

|  |  |  |  |  | ATERI | IAL | Ocated | ED IN | Nuni | IT No. |  |  |  |
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| 11 EMH | VEDOR | cabail sfock - 12 | DESCRIPTION OF MATERIAL |  | 23 | I | 1 m/ | T | T | T |  |  | Ttre |
| ${ }^{1-3}$ | * |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | DS-206 | AIR CIRCUIT PREAKER TYPE DS |  |  |  |  |  |  |  |  |  | 1 |
|  |  |  | 480 V 800AF/600AT M M |  |  |  |  |  |  |  |  |  |  |
|  |  |  | WITH TYPE LONG TIME AND SHORT TIME |  |  |  |  |  |  |  |  |  |  |
|  |  |  | TRIP CHARACTERISTICS, ALSO WITH MANUAL |  |  |  |  |  |  |  |  |  |  |
|  |  |  | RESET BELL ALAPM 1 N. 0.0 , 1 N.C. AND |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 2 N.O., 2 N.C. AUX. SWITCH AND SHMNT |  |  |  |  |  |  |  |  |  |  |
|  |  |  | TRIP AT 125 V DC (AMPTECTOR IIA) |  |  |  |  |  |  |  |  |  |  |
|  |  |  | (W FIG. 3B, 11C, 116) |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2-1 | w |  | CELL For item 1-1 CIRCuIt breaker | , |  |  |  |  |  |  |  |  |  |
| $\stackrel{\sim}{\sim}$ |  |  |  | 1 |  |  |  |  |  |  |  |  | 1 |
| $\stackrel{\text { a }}{ }$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2-2 | w | 8044217601 |  |  |  |  |  |  |  |  |  |  |  |
|  |  | - | CELL FOR ITEM 1-2 AND 1-3 PLUS | 1 | 33 |  |  |  |  |  |  |  | 7 |
|  |  |  | 2 FUTURE |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3-1 | w | 1400719604 | 5KV LOAD SWITCH 600A 30, 3 W |  |  |  |  |  |  |  |  |  |  |
|  |  |  | FAUTT Close |  |  |  | 1 |  |  |  |  |  | 1 |
|  |  |  | FAULT CLOSE NON-FUSIBLE (89) |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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ENG INEER
DESIGNER EL._ $\quad$ VC

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$\qquad$

PROJECI NO. $\qquad$
PAGE 4 OF $\qquad$

|  |  |  |  | MATERIAL LOCATED IN UNIT NO. |  |  |  |  |  |  |  |  |  |  |  | TOTAL QTY. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1TEM | VENDOR | CABBOII STOCK_U | DESCRIPTION OF MATERIAL | 1 | 2 | 3 |  |  | T | $\square$ | T |  |  |  |  |  |
| 24-1 | G.E. | 12IAV53K1A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | TYPE IAV UNDERVOLTAGE RELAY, 55 TO |  | 1 |  |  |  |  |  |  |  |  |  |  | 1 |
|  |  |  | 140 V (27UV) |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24-2 | G.E. | 12IAV51D1A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | IAV OVERVOLTAGE RELAY, 199V AC |  | 1 |  |  |  |  |  |  |  |  |  |  | 1 |
|  |  |  | ADJUSTABLE 16-64V (59G) |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 34-1 | OHMITE | AS DESCRIBED |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 200 OHM 250 WATT GROUNDING ADJUSTABLE |  | 1 |  |  |  |  |  |  |  |  |  |  | 1 |
|  |  |  | RESISTOR FOR USE WITH ITEM 24-2 (R) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\stackrel{\text { - }}{\stackrel{\sim}{\square}}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\stackrel{\rightharpoonup}{ \pm}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 41-1 | G.E. | 10AA009 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | ( AMMETER SWITCH 4 POSITION |  |  |  |  |  |  |  |  |  |  |  |  | 1 |
|  |  |  | (1-2-3-OFF), ROUND HANDLE (AS) |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50-1 | FPE | EON-6 | 6 AMP FUSES, 250 V |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50-2 | FPE | JCL-3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | JCL-3 | 3 AMP 600V FUSES |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
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ENGINEER
DESIGNER EL._ME.


ENGINEER_VC
DESIGNER EL. $\square$ ME
rRUJELI TW.
$\qquad$ UF $\qquad$

|  |  | Catalag |  | MTIERIAL LOCATED In UNIT NO. |  |  |  |  |  |  |  |  |  |  | TOTAL QTY. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITEM | VENDOR | CABBOIL STOCK_H2 | DESCRIPTION OF MATERIAL |  | 2 |  |  | IN | 第品 |  |  |  |  |  |  |
| 57-1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 57-1 | MARATHON | 1504SC | SHORTING T/B 4 POINT (STB) WITH COVERS |  |  |  |  |  |  |  |  |  |  |  | 1 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 60-1 | BURNDY |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | YA26 -2N | 2/0 lugs incoming cables |  |  |  |  | 3 |  |  |  |  |  |  | 3 |
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|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 63-1 | ANIXTER | 7315 | FLEXIBLE CONNECTOR 550A |  |  |  |  |  |  |  |  |  |  |  |  |
|  | ROYAL |  |  |  |  |  |  |  |  |  |  |  |  |  | 12 |
| 72-1 | FPE | PMT-1 | thermostat 22a |  |  |  |  |  |  |  |  |  |  |  |  |
| 73-1 | chromalox | OT-1225 |  |  |  |  |  | 1 | 1 |  |  |  |  |  | 2 |
| 90-1 | w |  | heater 120V 250W |  |  |  |  | 1 | 1 |  |  |  |  |  | 2 |
| $\stackrel{\omega}{\sim}$ |  |  | BREAKER LEVERING-IN CRANK |  |  |  |  |  |  |  |  |  |  |  | 2 |
| $\stackrel{\rightharpoonup}{\stackrel{\rightharpoonup}{+}}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| 90-2 | w |  | BREAKER LIFTING Yoke |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 |
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| 90-3 | ABBOTT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | travelling type Lifting device |  |  |  |  |  |  |  |  |  |  |  | 1 |
|  | POWER |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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## LETTER OF CLARIFICATION

1. CUSTOMER SPECIFICATION S-R F 235.1 CALLED FOR TIN PLATED AND SILVER PLATED BUS JOINTS. ABBOTT POWER WILL FURNISH TIN PLATED ALUMINUM BUS JOINTS FOR SWITCHGEAR, BUS DLCT AND MOTOR CONTROL CENTER. CUSTOMER APPROVAL REQUESTED.
2. CUSTOMER GENERAL SPECIFICATION JF16.0240 REQUIRES WELDED ALUMINUM BUS JOINTS, HOWEVER, ABBOTT POWER'S STANDARD USES BOLTED JOINTS. CUSTOMER APPROVAL FOR USING ABBOTT POWER'S STANDARD IS REQUESTED.
3. CUSTOMER SPECIFICATION S-RF 235-1 II-DS-10 CALLED FOR BREAKER LIFTING DEVICE. TRAVELLING TYPE LIFTING DEVICE AS SHOWN ON DRAWING 1-5049-1-1 WILL BE PROVIDED. CUSTOMER IS REQUESTED TO CHECK AND APPROVE.
4. SWITCHGEAR AND BUS DUCT WILL BE PAINTED ANSI \#61 LIGHT GREY AND MOTOR CONTROL CENTER WILL BE PAINTED WITH MANUFACTURER'S STANDARD TWO TONE GREY ANSI \#24/70. CUSTOMER APPROVAL IS REQUESTED.
5. SINGLE LINE DIAGRAM OF THE MOTOR CONTROL CENTER IS PART OF CUSTOMER'S SPECIFICATION. ABBOTT POWER WILL NOT FURNISH SINGLE LINE DIAGRAM FOR THE MOTOR CONTROL CENTER. CUSTOMER APPROVAL IS REQUESTED.
6. CUSTOMER SPECIFICATION S-R F235.1-III DS-4 SPECIFIED FOR STARTER OR CIRCUIT BREAKER DESIGNATION WHICH IS DIFFERENT FROM MANUFACTURERS STANDARD. A CROSS REFERENCE NUMBER IS PROVIDED ON the three line diagram for sustomer reference.
7. SIZE OF THE MOTOR CONTROL CENTER WILL BE AS SHOWN ON DRAWING \#1-5049-2-1.CUSTOMER IS REQUESTED TO CHECK AND APPROVE.
8. MOTOR CONTROL CENTER WILL BE WIRED ACCORDING TO CUSTOMER WIRING DIAGRAM JF30.40.05 ( $3 / 14 / 79$ ), JF30.40.10 ( $5 / 1 / 79$ ), SK-E75 ( $7 / 11 / 80$ ) AND SK-E76 (7/11/80) AND SPARE CONTACTS WILL BE FLURNISHED AS SHOWN ON THESE WIRING DIAGRAMS. CUSTOMER IS REQUESTED TO CHECK AND APPROVE.


$61 \mathrm{~N}[\mathrm{E}$


# INSTALLATION \& MAINTENANCE INSTRUCTIONS FOR NONSEGREGATED PHASE BUS SYSTEM 

## INSTALLATION \& MAINTENANCE INSTRUCTIONS FOR <br> NONSEGREGATED PHASE BUS SYSTEM

The following instructions apply to handing, installation and maintenance of the equipment supplied to you under contract \# $400+60,76 \pi$

Please refer to the drawings located in this manual for further reference.

## I. Receiving, Inspection \& Handiing

The following steps should be taken when handing and storing the equipment.

1. Configuration and size of bus duct will determine height to be stacked not to exceed 8 ft. in height. All standard size straight duct will be stacked 4 high.
All other irregular shaped ducts, I.E. bends, elbows, etc will be shipped singly or stacked depending on shape and size.
All duct support beams and hardware will be shipped and stacked for convenience of handing.
2. All bus duct should be wrapped with special seal corrugated cardboard and sealed with polyethylene sheeting. Bus duct when stacked will be separated by 2 X 4 wood dividers wrapped in cardboard to protect painted surfaces. One half inch steel banding will be utilized to strap duct together. Packaging will last indefinitely if items are not stored in direct sunlight or at temperatures below $32^{\circ} \mathrm{F}$.
Bus duct may be stored outside only in dry environment with 15\% humidty or less. Otherwise all duct should be stored indoors along with all assembly hardware, bus bar, insulating boots, etc.
3. All other bus system components such as bus duct supports may be stored outdoors as long as protection against moisture is provided.
4. Equipment should be stored so that all like items for one particular station are stored together bearing in mind that items to be installed first should be stored last thus allowing easy access to material. If prolonged storage is necessary, periodic inspection should be performed to assure packaging remains intact, taking special precautions against entrance of water which may cause future failure of equipment. Check stability of stacked items to prevent crushing or marring of the equipment.
A. Weathertight Splice Boots

The foliowing steps should be used when installing the weathertight splice boots.

1. Open the boot, and apply to the raised flat surfaces that will contact the bus bar sleeving and the raised flat area provided for the clamping screws, a $1 / 2$ " minimum wide $1 / 8$ thick layer of Dow Corning. Silicone Rubber Sealant Cat. No. 732-CLIl
2. With the boot still open, gently center and lower it over the splice area.
3. Press the boot closed and install clamping screws.
4. It will not be necessary to wipe off excess sealant that may push out. Be certain no holes, or unsealed areas remain.
5. The sealant will set dry to the touch in 30 minutes and completely cure in 24 hours. It will not become brittle.
6. Note: Install boot wherever possible with the nylon clamping screw holes down

## II. MAINTENANCE

A. Cleaning

In cleaning the housing we suggest you use plain detergent and water, however when cleaning the bus, use only mineral spirts, Do not use petroleum base products on the bus sleeving. It may cause a drying effect and cause the sleeving to crack and become brittle.
B. Maintenance Schedule

We recommend that the bus systems be spot checked every two years for excessive dirt, moisture and proper torque on splices.

We also recommend a complete cleaning of bus with mineral spirits and bus duct with detergent and water every six years.
I. Receiving

All packages, cases or crates leaving the factory are clearly marked at convenient places with case number, Abbott job number, customer order number and when for size and other reasons it is necessary to divide the equipment for shipment, with the unit number of the portion of equipment enclosed in each shipping section.

The contents of each package of the shipment are listed on the packing slip. This slip is forwarded with the shipment and put on the outside of the cases. To avoid the loss of small parts when unpacking, the contents of each case should be carefully checked against the packing slip before discarding the packing material. Notify the Abbott Power Corporation immediately if any shortage of material is discovered.

All elements before leaving the factory are carefully inspected and packed by workmen experienced in the proper handling and packaging of electrical equipment. Upon receipt of any apparatus an immediate inspection snould be made for any damage sustained while en route. If damage is evident or an indication of rough handling is visible, a claim for damage should be filed immediately with the transportation company and Abbott Power Corporation should be notified promptly. Information as to damaged parts, case number, and Abbott job number should accompany the claim. In cases where there is no external damage to the crate, and the damage is not discovered until after crating is removed, the claim should be made on the basis of concealed damage. Concealed damage must be reported within 15 days. In all cases where clains for damages must be made, action should be taken quickly, as lapse of time may void the claim.

## II. Handling

Before unpacking, indoor equipment may be moved by a forklift or a crane with slings under the skids. If crane facilities are not available, rollers under the skids may be used. Methods of handing outdoor equipment is the same as indoor, except the skid (the six inch channel base on the bottom of the assembly) will allow some sliding or skidding of the switchgear on the foundation surface.

## III. Storage

If it is necessary to store equipment for any length of time, the following precautions should be taken:

1) Uncrate the equipment.
2) Store in a clean dry place and cover with canvas or plastic to prevent deposit of dirt or other foreign substances on movable parts and electrical contact surfaces.
3) Batteries should be uncrated and put on trickle charge imnediately on receipt.
4) If dampness or condensation may be encountered in the storage location, heaters should be placed inside the units to prevent condensation.

Approximately 250 watts of heaters per unit will be required. Remove all cartons and other miscellaneous material packed inside units before energizing any heaters. If the equipment has been subject to moisture it should be tested with a 1000 V or 2500 V megger. A reading of at least 200 megohms should be obtained.
5) Breakers should be prepared for storage separately. Refer to appropriate breaker instruction book.

## IV. Description

Each switchgear unit is made up of a secondary and a primary enclosure.

## 1. Secondary Enclosure

The secondary enclosure is normally located on the front of the switchgear or breaker withdrawal side, although in certain units it may be on the side opposite to the breaker withdrawal area. It consists of a compartment with a hinged door or panel upon which are mounted the required instruments, control and protective devices. The teminal blocks, fuse blocks and some control devices are mounted inside the enclosure, nomally above the breaker and a wireway is provided to allow the passage of control wires between units.
2. Primary Enclosure

The primary enclosure contains the high voltage equipment and connections arranged in compartments to confine the effects of faults and to minimize the damage.
3. Circuit Breaker Removable Element

The renovable element consists of a circuit breaker with a tripfree operating mechanism mounted directly on the circuit breaker frame, interlock mechanism, the removable portion of the primary and secondary disconnecting devices, the operating mechanism control devices and necessary control wiring. Circuit breakers may be equipped with wheels or slides for easy removal and insertion.

The circuit breaker interlock mechanism is designed to obstruct the operator from removing the breaker from the connected position unless the circuit breaker is in the open position. This interlock is also designed to prevent the circuit breaker from being closed in an intermediate position when being removed or inserted into the cubicle. The secondary disconnecting device is used for connecting outside control circuits to the circuit breaker, operating mechanism trip and closing coils this device makes contact automatically when the removable element is properly positioned in its enclosure. All removable elements furnished on a particular requisition and of like design and ratings are completely interchangeable with each other. The removable elements as well as the stationary elements (cells) are built by the particular circuit breaker manufacturer with factory jigs and fixtures thus insuring interchangeability.
4. Primary Disconnecting Device

The primary disconnecting devices utilize materials of various alloys to insure against reduction of current carrying capacity due to oxidation of the contact surfaces. These contacts are of the high pressure line contact tube and socket design being backed up by heavy duty springs to insure contact pressure.
5. Bus Compartment

The main buses are enclosed in a metal compartment with removable covers to provide accessibility.

The bus is supported by an insulating material which is practically impervious to moisture and an excellent dielectric. The bus insulation can be either molded on the bars or sleeving which slides over the bar except at joints where the insulation is completed by either compound filled boxes, molded boots or tape.
6. Current Transformers and Cable Compartment

Current transformers, where possible are mounted in the breaker compartment over the porcelain insulators behind a barrier or in the cable compartment where provision is made for connecting the purchaser's primary cable by means of potheads or cable clamps.
7. Potential Transformer Compartment

Potential transformers are in a separate compartment and their location is dictated by the particular switchgear layout. In
walk-in weatherproof design, the transformers will be accessible from the walk-in aisle where possible.

The transformers are mounted on a movable support equipped with primary and secondary disconnecting devices. When the potential transformers are disconnected, they are at a safe striking distance from all live parts of the switchgear. In addition a grounding device is provided which contacts the fuses when the potential transformers are disconnected. In this position the transformer fuses may be safely removed and replaced. A barrier mounted at the rear of the carriage prevents access to all live parts.
8. Dummy Removable Element

If required, a dummy removable element can be provided and is used as a means of isolating circuits or bus sections, where operation is infrequent and a circuit breaker cannot be economically justified. The device consists of a framework to simulate the circuit breaker removable element with a set of six studs similar to those on the breaker and may be connected to provide a continous current path through the bus.

Under no circumstances should the dummy element be connected on disconnected when the bus is energized. Key interlocks are applied to insure that all sources of power are disconnected before the dunmy element can be inserted or removed.

## 9. Fuse Disconnecting Device

Cument limiting fuses with high intermupting rating are frequently used in metal-clad switchgear to protect transformers or cincuits where circuit breakers cannot be economically or functionally justified.

The fuses are mounted on a movable support equipped with disconnecting devices.

When fuses are disconnected, they are at a safe striking distance from all live parts of the switchgear. In addition a grounding device is provided which grounds the fuses after they are disconnected. In this position the fuses may safely be removed and replaced. The disconnecting devices are capable of interrupting transformer magnetizing current but should not be used to interrupt load current. Mechanical or key interlocks are used to prevent operation while the load is connected. This is generally accomplished by interlocking, in which the circuit breakers must be locked open before the disconnecting device can be opened or closed.
10. Grounding and Test Device

The grounding and test device provides a convenient means of grounding the cables or the bus in order to safeguard personnel who may be working on the cable or equipment. The device can also be used for applying power for high potential tests or for fault location, to measure insulation resistance and by using potential transformers, it can be used for phasing out cables. The three studs of the device are similar to those of the circuit breakers. The studs are mounted on a removable plate which can be placed in either of two positions, the bus or line side. To indicate the proper placement of the studs on the device, each position is marked "Line" or Bus".

To use, the device is rolled on slid into the metal-clad housing in place of the circuit breaker and racked into position the same as the circuit breaker.

Before any installation work is done, consult and study all drawings furnished by the Abbott Power Corporation for the particular requisition.

These drawings include arrangement drawings, wiring and schematic diagrams and a bill of material. Mats, screens, railings, etc., which are extermal to the switchgear, but which may be required to meet any local codes, unless required by the requisition, must be furnished by the purchaser.

## I. Location

The recommended aisle space required at the front and rear of the equipnent is shown on the arrangement drawing. The space in front must be sufficient to allow the insertion and removal of the ciruit breaker, and their transfer to other units.

The space at the rear must be sufficient for cable installation, for inspection and maintenance, and on some equipment to draw out potential trartsformers.

Preparation of Floor-Anchoring

## II. Indoor Equipment

The station floor must be strong enough to prevent sagging due to the weight of the equipment and to withstand the impact stress caused by opening of the circuit breakers under short circuit conditions. The impact loading is approximately $1 \frac{1}{2}$ times the static load.

Suitable means must be provided by the purchaser for anchoring the equipment to the floor. It is essential that the floor be level to avoid distortion of the structure, and the equipment be completely aligned prior to final anchoring.

It is reconmended that floor channel sills be embedded in the concrete. These sills must be level and straight with respect to each other and flush with the finished floor. Care should be taken to provide a smooth, hard and level floor under and in front of the equipment to facilitate installation and removal of the circuit breaker. If the floor is not level and flush with the floor channels it will be difficult to handle the breaker because it will not be level with respect to the stationary element and may not allow for the opening of hinged panels. Reconmended practice is to weld the switchgear structure to the floor channels using a tack weld at the center of each unit, front and rear as well as the ends. See figures 1 and 2.

Provision should be in the floon for conduits for primary and secondary cables, located in the area shown on the base plan. In the event primary and secondary cables are top entry, provision must be made to seal the area of entry to prevent foreign objects and dirt from entering the compartment.

## III. Outdoor Equipment

Outdoor equipment can be furnished with or without a walk-in aisle. Primary and secondary conduits should be installed in the area shown on the base plan prior to putting the equipment into place.

1. Outdoor Equipment Assembly (Non-Walk-In)

Mounting; sills should be embedded in concrete and level. If the-equipment is shipped in more than one section, all sections should be placed on the mounting sills and the sections bolted together|with hardware supplied. Refer to the "Assembly Hardware|' list of material shipped, for the proper size bolt to be used on the indicated assembly.

Prior to: placing the shipping splits together, cover all outside edges on the top and sides of the assembly that bolt together with the caulking compound supplied with the harcware.

Level and plumb the entire assembly. This may necessitate placing shims at intervals between each compartment of the assembly if the mounting sills are not level. Weld the assembly to the mounting sills. If shims are used for leveling and the $6^{\prime \prime}$ channel base does not sit flush on the leveling sills, grout around the outside of the base to prevent the entry of dirt, snow, rodents, etc..

Bolt on the roof caps over the shipping splits. See figure 4.
Prior to completing the assembly and preserving the integrity of the weatherproofing care should be taken to protect the instrments and insulation system from the elements.

After completing the assembly of the equipment in position, the space heaters should be energized, from a temporary source if necessary.
2. Outdoor Equipment (Walk-In Aisle)

When specified, outdoor equipment can be furnished with a weatherproof operating aisle. This equipment can be furnished in one of two ways. The equipment compartments, complete with
walk-in aisle can be shipped complete in multiples of 2-3 conpartments. These shipping sections are then assembled as described in "Outdoor Equipment Assembly (Non Walk-In) and the assembly when complete will include the walk-in section of the equipment.

When otherwise specified this type of equipment will be shipped in multiple sections of 5-6 compartments of switchgear sections and multiples of walk-in aisle sections separate. The switchgear sections should be installed and mounted as described in Outdoor Equipment Assembly (Non-Walk-In). After this has been complełed the walk-in section should be installed and attached to the switchgear section. After all sections are installed and joined together the roof cap should be installed as described in Outdoor Equipment Assembly (Non-Walk-In) with the addition of the roof caps between the switchgear and aisle sections. See figure 5.

The above procedure describes installation of a protected aisle enclosure with switchgear on one side only. If the aisle is common to two lineups of switchgear, the procedure will require slight modification. Refer to furnished drawings and instructions for specific requirements.
3. Bus Ducts

Bus ducts connecting between groups of metal-clad switchgear, or between metal-clad switchgear and other apparatus, should be installed as shown on the furnished arrangement drawings. Supports should be provided as indicated on the assembly drawings. Refer also to figure 3.

All joints in the bus including adjustable joints, should be assembled and insulated with tape or boots. Adjustable joints are provided in long runs of bus duct to allow for variations in building construction, etc.. These joints should be loosened before installation of the duct, then tightened after being set in the position required by the fixed points at the ends of the duct.

For outdoor bus ducts all renovable covers should have gasketing material installed at the factory. Joints at shipping splits should be gasketed, as per furnished drawings.

If outdoor bus ducts are equipped with strip heaters, connect these in accordance with furnished wiring diagrams, before energizing the bus.
4. Ground Bus

The ground bus is bolted to the switchgear frame near the bottom. It is arranged so that connections to the station ground can be made in any unit. Where the equipment is shipped in more than one group, the sections of the ground bus must be connected by using the splice plates furnished with the equipment. The switchgear ground bus must be connected to the station ground bus by a conductor having a current carrying capacity equal to that of the switchgear ground bus. It is very important that the equipment be adequately grounded to protect the operator from injury when short circuits or other abnormal occurrences take place, and to insure that all parts of the equipment, other than live parts, are at ground potential.
5. Lightning Protection

If not already installed in switchgear, it will be the responsibility of the purchaser to provide adequate lightning protection to protect the equipment and personnel from damage due to lightning.
6. Ground Fault Current Transformers

Through-type current transformers are furnished, where specified, for sensitive protection against ground faults.

Where shielded cables are used, the grounded sheath or jacket should not pass through the ground fault transformer. Armored cable should be terminated and grounded prior to entering the transformer.

Where potheads are used in units provided with ground fault current transformers, the pothead mountings must be insulated from ground.
7. Main Bus Assembly

The main bus bars and other connection bars may be either copper or aluminum. In either case the connection surfaces will be silver plated.

All field assembled joints in conductors, regardless of material or method of insulation, should be made as follows:

Wipe silver clean. Do not use abrasive on the silvered surface. A sufficient quantity of conductive grease should be applied to the joint at each contact area so that the complete contact area will be thoroughly sealed with excess grease squeezed out of the joint when tightened.

Bolt splice plates and bus bars together following enclosed installation instructions and the following torque value:

$$
\begin{aligned}
& \text { 1/2-13 } 480 \text { in. -lbs. } \quad 40 \mathrm{ft} .- \text { Ibs. } \\
& \text { 3/8-16 } 219 \text { in.-lbs. } 18.25 \mathrm{ft} .-1 \mathrm{bs} \text {. }
\end{aligned}
$$

Install the proper insulating boot over the joint.
8. Primary Connections:

The primary cable connections in most cases are reached through the bolted or hinged panels at the rear. Refer to installation drawings for specific locations.

Before any cable connections are made, the cables should be identified to indicate the phase relationship with the switchgear connections. There are two common methods of making primary cable connections; clamp type and potheads.
9. Control Cables:

When control conduits are used, entering from either, top, bottom or side, the concuit should be securely fastened by locknut and should not extend more than 4 inches when entering from the bottom.

Connect the cables to the termination blocks in accordance with the wiring diagrams furnished.

The cables from the control power source to the switchgear should be large enough to avoid excessive voltage drop during operations.
Where units have been split for shipment, any control or secondary leads which must connect across the split will be arranged with terminal blocks in the cross trough or convenient side sheet so that the wire can be reconnected. The wires will be cut to length, terminated, and formed before being folded back so that a minimm of time will be required for reconnecting them.






GENERAL GUIDELINES FOR SWITCHGEAR MAINIENANCE AND TESTINIG

This publication is only a general guideline for Installation/Maintenance and does not intend to cover all aspects of work or specifications. Not all items in this publication are intended to describe your equipment and only applicable sections should be adhered to. For desired specifications of assembly components, please consult applicable manufacture's literature and publications.

# GENERAL GUTDELTIES ECR SWITCHEEAR 

MAINTEIANCE AND TESTITG

## GENERAL GUIDELINES

FOR
SWITCHGEAR
MAINTENANCE AND TESTING

The following is a general guide for safe and economical testing and maintenance of switchgear and associated equipment. It is not intended to cover equipment of any particular mamufacturer or problems unique to specified conditions. Instead, it is a basic outline applicable to most switchgear and substation maintenance programs.

For specific maintenance problems or reconmendations refer to the required manufacturer's literature found elsewhere in this manual.

## I. Safety

All maintenance and testing must be done on apparatus de-energized from the commercial $a-c$ service. Where temporary feed for power is required to keep vital circuits in continuous operation, care should be taken to isolate these circuits from the equipment being serviced, with prior approval of a customer representative who is familiar with the system. Prior to any testing, all incoming power cables must be checked to determine that all electrical power has been removed and that temporary leads are not backfeeding into the equipment being serviced.
II. Schedules

A regular maintenance schedule should be established to obtain the best service and reliability from the switchgear. Plant operating and local conditions will dictate the frequency of inspection and maintenance requirements.

For specific information regarding the maintenance of devices, such as circuit breakers, relays, meters, etc., refer to the separate instruction books furnished for each device.

Under normal conditions the protective relays do not operate, therefore, it is important to check the operation of these devices regularly.

## III. Records

A permanent record of all maintenance work should be kept, the degree of detail depending on the operating conditions. In any event, it will be a valuable reference for subsequent maintenance work and for station operation. It is reconmended that the record include reports of test made, the condition of equipment and repairs and adjustments that were made.

BEFORE ANY COVERS ARE REMOVED OR ANY DOORS OPENED WHICH PERMIT ACCESS TO THE PRTMARY CIRCUITS, IT IS ESSENTIAL THAT THE CIRCUIT BE DE-ENERGIZED.

The primary circuits of metalclad switchgear are insulated in order to reduce the size of the equipment. However, this insulation, except in one or two instances, requires a certain amount of air gap between phases and to ground to complete the insulation. Inserting any object in this air space, when equipment is energized, whether it be a tool or a part of the body, may under certain conditions, in effect, short circuit this air gap and may cause a breakdown in the primary circuit to ground and cause serious damage or injury or both.

## IV. Switchgear

1. Enclosures

Switchgear enclosures should be inspected for evidence of leakage of water, dust, etc., and should be appropriately repaired, by caulking or other suitable means. Any portions of the switchgear that show signs of rust or oxidation should be resurfaced and painted to assure metal enclosure integrity.
2. Auxiliary Equipment

Assure that all auxiliary equipment such as interior lighting, exterior lighting, heaters, battery chargers, batteries, fans, etc., are fully operational within manufacturen's specifications. Repair or replace appropriate parts as needed.
3. Electrical Connections

Whether it be bus bar or cable connections within the switchgear enclosure assure that all connections are tight, and cormosion free. All conductors and connections should be insulated and protected against corona, tracking, and insulation breakdown.
(Page 3)

All main conductors should be tested for insulation breakdown between the conductor and ground, and between other conductors.

## 4. Air Circuit Breakers

4A) Disconnects
Check disconnects for freedom of movement, galling or friction in moving parts. Check for signs of heating on current carrying parts, loose or missing hardware and broken or missing cotter keys or retainer rings. Replace missing or broken parts and lubricate as per manufacturer's specifications.

4B) Main Contacts
Clean contacts and free from oxide or corrosion. Maintain 80\% or better contact mating on knife or butt type contact surface.

Check contact overtravel and positive stops. $1 / 16$ to $1 / 32$ inch overtravel is recommended to permit wiping action when contacts close. Set stops so as to limit overtravel to a safe amount, usually $1 / 16$ to $1 / 8$ inch. Check for proper operation high current disconnects and gangtype disconnects having main arcing contacts.

4C) Operating Mechanisms
The operating mechanism should be inspected for loose or broken parts; missing cotter pins or retaining keepers; missing nuts and bolts and for binding or excessive wear. All moving parts are subject to wear. Long-wearing and cormosion resistant materials are used by manufacturers and some wear can be tolerated before improper operation occurs.

Excessive wear usually results in loss of travel of the breaker contacts. It can affect operation of latches; they may stick or slip off and prematurely trip the breaker. Adjustments for wear are provided in certain parts. In others replacement is required.

The closing and tripping action should be quick and positive. Any binding, slow action, delay in operation, or failure to trip or latch must be corrected prion to returning to service.

## 4D) Circuit Breaker Auxiliaries

Inspect the closing motor or solenoid, shunt trip, auxiliary switches and bell alarm switch for correct operation, insulation condition and tightness of connections.

Check on-off indicators, spring-charge indicators, mechanical and electrical interlocks, key interlocks and padlocking fixtures for proper operation and lubricate where required. In particular, test the positive interlock feature which prevents the insertion and withdrawal of the circuit breaker while it is in the closed position.

The protective relay circuits should be checked by closing the breaker in the test position and manually closing the contacts of each protective relay to trip the circuit breaker.

Trip devices on low voltage breakers may be the electromechanical series overcurrent type with an air or fluid dash pot for time delay. These devices should be periodically tested for proper calibration and operation with low voltagehigh current test devices. Calibration tests should be made to verify that the performance of the breaker is within the manufacturer's published curves. It is very important that the manufacturer's calibration curves for each specific breaker rating be used and take into account that current-time curves are plotted as a band of values rather than a single line curve. It should be realized that short time calibration cannot be checked accurately because factory calibration equipment has synchronized timing devices to insure symmetrical currents whereas field test equipment features random closing and may product asymmetrical currents resulting in faulty readings. If the trip devices do not operate properly, the calibration and timing components should be repaired or replaced in line with the manufacturer's recommendations.

If the breakers are equipped with static tripping devices, they should be checked for proper operation and timing in line with the manufacturer's recommendations. Some manufacturer's recommend replacement of electro-magnetic devices with static devices in the interest of realizing more precision and a higher degree of reliability with the latter devices.
5. Molded Case Circuit Breakers

Molded case circuit breakers should be kept clean of external contamination so that internal heat can be dissipated normally. Further, a clean case will reduce potential arcing conditions between live conductors and between live conductors and ground. The structural strength of the case is important in withstanding the stresses imposed during fault current interruptions. Therefore, an inspection should be made for cracks in the case and replacements made where required.

Excessive heat in a circuit breaker can cause a malfunction in the form of nuisance tripping and possibly an eventual failure. The most common cause of excessive heat is loose connections. Periodic maintenance checks should involve a routine tightening of the circuit breaker terminals and bus bar connections. Molded case circuit breakers having noninterchangeable trip units are properly adjusted, tightened and sealed at the factory. Those having interchangeable trip units installed away from the factory could overheat if not tightened properly during installation. All connections should be maintained in accordance with manufacturers' reconmendations.

When testing circuit breaker tripping characteristics, it is reconmended that the overcurrent tests be performed on individual poles at 300 percent of rated current. The reaction of the circuit breaker to this overload is indicative of its reaction throughout its entire overcurrent tripping range. This load is chosen as the test point because it is relatively easy to generate the required current in the field and the wattage per pole from line to load is lange enough, so the dissipation of heat in the nonactive pole spaces is minor and does not affect the test results appreciably.
6. Relays

6A) Protective Relays
Inspect relay for loose terminals, lock screws and other parts; for filings or other foreign material in magnet gaps; for burned or dirty contacts; for sticky contact back-stops; for dirty, worn or broken bearings or other cause for sluggish operation; for danaged or maladjusted indicator tangets or holding devices. Performance tests of the relays will vary somewhat with the type of relay.

For a visual inspection, remove cover. Inspect the cover gasket, check glass for tightness in the frames, cracks, etc.. Clean glass inside and out.

First open trip circuit. Follow manufacturer's directions carefully since they will differ. Open the latches that hold the relay in the case and carefully remove relay from case. Remember electrical connections to the cases are still "hot".

Remove foreign material in the relay, such as dust, filings, etc.. Use dry compressed air 25 psi or lower.

Remove any rust or filings from disc or magnet poles with a magnet cleaner or brush.

Check clearance between magnet poles to assure that they do not rub.

Inspect relays for presence of moisture.
Clean or replace pitted or burned contacts if necessary.
Perform four types of tests for overcurrent relay testing; zero set, pick-up, time-current characteristics, and target and seal-in operation.

For overcurrent instantaneous relays, consult manufacturer's instruction leaflet to identify current terminals and contact teminals.

For over/under voltage relays, consult manufacturer's instruction leaflet to identify potential terminals and contact terminals. Then perform the zero set, pick-up, and timing tests.

For directional overcurrent relays, test the unit for pick-up and timing as for an overcurrent relay except the directional unit contacts must be blocked closed for this test or the overcurrent unit will not operate.

For percentage differential relays, again consult manufacturer's instruction book for proper connections and information on characteristics.

After completion of the electrical test, replace relays in their drawout compartments and mechanically operate the relay to check the wiring continuity to assure it will trip the proper equipment.

## 6B. Auxiliary Relays

Inspect auxiliary relays for dirt, dust, burned contacts, and proper operation. If applicable clean relay of dirt and dust. Burnish contacts for proper contact surface connection. Test
relay for proper operation. Repair or replace as needed.
7. Transformers

Visually inspect for chipped petticoats, fractured porcelain, etc., and replace any damaged parts. Clean all bushings as well as check gaskets for positioning, resilience and leaks. In general, clean insulators by polishing with a soft cloth dipped in solvent or utilizing a bushing cleaner. Never use water or caustic solutions to remove oxide and dirt deposits on porcelain glaze or resort to abrasives, steel wool or wire brushing. When the surface is clean, polish with a soft, dry cloth.

Remove rust on bushing caps and flanges by sanding, then primer and paint for application to metal surfaces.
"Ratio" test the transformer using a turns ratio counter to assure proper output voltage. Remove and analyze samples of the insulating liquid to establish the dielectric strength, acidity content, color, and specific gravity.

Inspect pressure relief diaphragns to assure that they are properly seated and seal the unit.

Check tap changer mechanism for proper operation.
For dry type transformers, in addition to the above, inspect and clean bushings; check and tighten connections as required. Clean the windings by vacuum or compressed air.

These tests should be performed on a two to three year schedule.
8. Meters

All meters due to their construction are delicate and must be handled and operated in the appropriate manner. Inspect each meter for abuse that could cause internal damage. Inspect the meter glass, the meter face, case and connection. Check for free movement of the needle. Apply the appropriate electrical component (ie.. $A C / D C$ volts, or $A C / D C$ current) to give half scale reading. Apply the component to obtain a full scale reading. Check meter reading for accuracy. Normal tolerance is $10 \%$, unless specific meters require more stringent requirements.
9. Switches

Safety, disconnect, transfer and pressure contact switches have a tendency to build up high resistance across the contacts if not
operated frequently. Several manufacturers have designed this apparatus in such a manner as to make it difficult to actually see the contacts and moving parts. Where possible, clean the main contact of the switch, adjust and place a thin film of Iubricant on them. Check fuse clips, connections to the bus or cable, and switchboards mounting and handles for tightness and proper alignment. When applicable, check the tension on the contacts when signs of discoloration caused by heating are noticed.

Due to the design of switch equipment, it is not necessary to perform electrical tests as in the case of a circuit breaker. However, there is one test that will indicate if the operating mechanism of the switch has deteriorated to the extent that the probability of failure in the near future is great. This test is called the ductor test and measures in millivolts the contact resistance drop. After exercising the switch several times, cleaning and making any adjustments necessary, with a ductor test set the resistance drop across each phase to be measured. If the drop exceeds 50 millivolts or has greater than $+20 \%$ variation between phases, part replacement is reconmended.
10. Auxiliary Equipment

10A) Motors
When applicable inspect motors for loose hardware, fittings, connections, and brushes. Inspect motor shaft for binding shaft rotation or excessive shaft end travel. Test motor windings with D.C. megohm meter for insulation breakdown.

10B) Lightning Arrestors
Lightning arrestors are generally sealed components, free of maintenance except for an occasional cleaning and mechanical inspection. Clean the arrestor thoroughly when inspecting the transformer. Check tightness of all bolted connections to ground and retighten as necessary. Megger (1000v.) test value should read infinity unless internal resistors are used in the manufacture of the lightning arrestor. Replace low reading or grounded arrestors.


- CASE:
- APPLICATION:
- INSULATION CLASS:
- FREQUENCY:
- IMPULSE LEVEL:
- CONTINUOUS THERMAL CURRENT RATING FACTOR:

Molded Reinforced Plastic.
Metering. Designed to fit over bus behind Westinghouse DS breaker.
600 Volts
$25-60 \mathrm{~Hz}$
10 KV
$1.33 @ 30^{\circ} \mathrm{C}$ Ambient;1.0 at $55^{\circ} \mathrm{C}$ Amb.


## CURRENT TRANSFORMER MODEL 350



SECONDARY EXCITING CURRENT.AMPERES. 60 Hz



The Abbott Magnetics Model 450 is designed for use with all types of electrical indicating, metering, recording instruments and protective relays in electrical power systems. The magnetic core and coils are mounted in a reinforced plastic case with a metal mounting base. The unit is epoxy filled to insure insulation qualities.
Secondary and primary windings are fully insulated and terminated at threaded studs. The units are supplied with terminal covers.

Winding ratios are indicated on the nameplate as well as on the side of each unit as shown in the outlined drawing above.

- FREQUENCY:
- STANDARD SECONDARY VOLTAGE:
- INSULATION CLASS:
- ACCURACY CLASS:
- CONTINUOUS THERMAL

CURRENT RATING FACTOR:

- WEIGHT:

60 Hz
120 V
$600 \mathrm{~V}, 10 \mathrm{Kv}$, Full Wave BIL
0.3 class at $W, X, M, Y: 1.2$ at $Z$

750 VA at $30^{\circ} \mathrm{C}$ Amb., 500 VA at $55^{\circ} \mathrm{C}$ Amb. 22 lb.


Jther ratios and burden capacities available upon request.
I. Med on reverse side.

## Abbott Mag̊netics @orporation

## POTENTIAL TRANSFORMER MODEL 450

TYPICAL PERFORMANCE



## GENERAL SPECIFICATIONS

Principle of Operation: See descriptions below.
Accuracy: See accuracy specifications below.
Position of use: Vertical (Scale)
Full Scale Deflection Angle: $250^{\circ}$ (except Synchroscopes: $360^{\circ}$ )
Full Scale Length: Approx. 71/4" (183 mm)
Pointer: Sword type, black
Scale Plate: Platform type, white
( s: ABS, black. Meets UL94/ASTM 635-68
Cover: Methacrylic acid resin with anit-static processing on both sides
Standard Color: Black (Munsell $N$ 1.5/0)
Terminal Plate: Phenol resin, black. Meets UL94/ ASTM 635-68
Mounting Screw: 5 mm in diameter
Measuring Terminal: 5 mm in diameter (nut type)
Dimensions: See page 12
Weight: Model 2101 Model 2102 Ammeter Approx. $0.91 \mathrm{lbs} .(0.4 \mathrm{~kg})$ Model 2102 Voltm . . . Approx. $1.3 \mathrm{lbs} .(0.6 \mathrm{~kg}$ ) Models 2105 \& 2106 Models 2107 \& 2108 Model 2109 Approx. $1.1 \mathrm{lbs} .(0.5 \mathrm{~kg})$ Approx. 2.2 lbs . ( 1 kg ) Approx. $1.3 \mathrm{lbs} .(0.6 \mathrm{~kg})$ Approx. $3.7 \mathrm{lbs} .(1.7 \mathrm{~kg})$
Dielectric Test Voltage: $2,600 \mathrm{~V}$ AC for one minute between the electrical circuit and the case.

## YEW

## medallion series



MODEL $210 T$ DC AMMETER (Moving Coil TyPe)


MODEL 2102 AC AMMETER (RMS Sensing Transducer Type)


$\triangle$ UNRLH TAY BE PLRCHASED FROTM: THERN NC. UUNONA, MINN. 55987 PART ND. 465 OR EQUAL

PHLLADELPHIA. PA. 19140
PART NE. 2203 IR EQUAL
A. HCOK mAY BE PLRCHASED FROM : LAUGHLN OR EQUAL PART NO. A- $32 S$
THAN SITE $3 / E$


FRONL VIEU

4 FERRULE DUPIEX MAY SE PURTMASED FROM
NEUCO, KANSMS CITY MO. DR EQUAL, SITE
3/G INII UIRE ROPE BREAKING STRENGTH $4200 \%-7=19$


## flexible Connectors

4




 © Cationatisac conact






## TERMINAL and SPLICE

## For Copper HYLUG and HYLINK <br> Types YA，YS


nest and indentor as listed results in this type of indent

Copper HYLUG and HYLINK compression connectors for copper wire．All sizes are tin－plated to resist corrosion．
dIE SET AS LISTED RESULTS IN A CIRCumperential crimp


Note：Die indexes and tooling listed between the heavy lines apply to the conductor and connectors listed within the same lines．Both HYDENT and over head die sets are listed．

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multirow[t]{2}{*}{cox：
ductor：} \& \multirow[t]{2}{*}{\[
\begin{aligned}
\& \text { stud } \\
\& \text { staz }
\end{aligned}
\]} \& \multirow[t]{2}{*}{NO．OF HOLES IN PAD} \& \multicolumn{2}{|l|}{cataloe number} \& \multirow{2}{*}{\(\underline{ }\)} \& \multirow{2}{*}{\(N\)} \& \multirow[t]{2}{*}{\[
\begin{aligned}
\& \text { OIE } \\
\& \text { INDEX }
\end{aligned}
\]} \& \multirow[t]{2}{*}{\[
\begin{aligned}
\& \text { DIE } \\
\& \text { TYPE }
\end{aligned}
\]} \& \multicolumn{7}{|l|}{－TOOLS，DIE SET CATALOC NO．，\＆\(\because \therefore\) ．} \\
\hline \& \& \& TERMINAL \& Sflice \& \& \& \& \& M06 \& Y34A \& Y35 \& Y45＊ \& Y488 \& \& Ycai \\
\hline \multirow[t]{2}{*}{6 Str．} \& 1／4 \& 1 \& mee \& \multirow[t]{2}{*}{Y286} \& K \& 1／2 \& 7 \& \[
\begin{gathered}
\text { MEST } \\
\text { MDENTOR }
\end{gathered}
\] \& － \& \begin{tabular}{l}
A6CD \\
Y34PR
\end{tabular} \& \(1-\) \& － \& － \& \& － \\
\hline \& \(1 / 2\) \& 2 NEMA \& Yuce－2N \& \& 56 \& \％ \& 7 \& DIE SET \& － \& A5CR 2 \& 2 USCRT 2 \& － \& － \& \& － \\
\hline \multirow[t]{2}{*}{4 Str．} \& 1／4 \& 1 \& YAAC \& \multirow[t]{2}{*}{YS4C} \& 3／6 \& 1／2 \& 8 \& \[
\begin{gathered}
\text { MEST } \\
\text { INDENTOR }
\end{gathered}
\] \& － \& \[
\begin{aligned}
\& \text { A4CU } \\
\& \text { Y34PR }
\end{aligned}
\] \& \& － \& － \& \& － \\
\hline \& 1／2 \& 2 NEMA \& Yatc－2N \& \& 口6 \& 3／8 \& 8,
161,
242 \& DIE SET \& \[
\begin{aligned}
\& W 1612 \\
\& W 2424
\end{aligned}
\] \&  \&  \& － \& \(\stackrel{\square}{\text { C242 }}\) \& \& \(\underline{742}\) \\
\hline \multirow[t]{2}{*}{3 Str．} \& \(x_{6}\) \& 1 \& Yl3C \& \multirow[t]{2}{*}{rs3c} \& 1／2 \& 1／6 \& 9 \& \[
\begin{aligned}
\& \text { MEST } \\
\& \text { IMDENTOR } \\
\& \hline
\end{aligned}
\] \& － \& \[
\begin{array}{ll}
\text { A3CD } \& \\
\text { Y34PR }
\end{array}
\] \& 1－ \& － \& － \& \& － \\
\hline \& 1／2 \& 2 NEMA \& YA3C－2N \& \& \％ \& 5／8 \& 162,
162,
203 \& DIE SET \& 二 \& \begin{tabular}{l} 
A3CR \\
A 203 \\
\hline
\end{tabular} \& ［ U3CRT 21 \& － \& － \& \& － \\
\hline \multirow[t]{2}{*}{2 Str．} \& \％ \& 1 \& Y／2C \& \multirow[t]{2}{*}{YS2E} \& \％ \& \(1 / 8\) \& 10 \& \[
\begin{aligned}
\& \text { NEST } \\
\& \text { NDENTOR }
\end{aligned}
\] \& － \& \begin{tabular}{l} 
A2CD \\
Y34PR \\
\\
\hline
\end{tabular} \& － \& － \& － \& \& － \\
\hline \& \(1 / 2\) \& 2 NEMA \& Yazc－2N \& \& 碞6 \& 5／8 \& \[
\begin{array}{r}
10, \\
162
\end{array}
\] \& DIE SEI \& W162 5 \& \(\left|\begin{array}{ll}\text { A2CR } \& 2 \\ \text { A162 } \& 1\end{array}\right|\) \& \(\left|\begin{array}{ll}\text { U2CRT } \& 2 \\ \text { U162 } \& 1\end{array}\right|\) \& － \& \({ }_{6} 1621\) \& \& － \\
\hline \multirow[t]{2}{*}{1 Str．} \& \(x_{6}\) \& 1 \& Yalc \& \multirow[t]{2}{*}{HSTC} \& \％／6 \& \％ \& 11 \& \[
\begin{gathered}
\text { NEST } \\
\text { INDENTOR }
\end{gathered}
\] \& － \& \[
\begin{array}{ll}
\text { A1CD } \& \\
\text { Y34PR } \& 1 \\
\hline
\end{array}
\] \& \(1-\) \& － \& － \& \& － \\
\hline \& 1／2 \& 2 NEMA \& YA1C－2N \& \& 1\％6 \& 5／8 \& \[
\begin{gathered}
11, \\
276
\end{gathered}
\] \& OIE SET \& － \& \begin{tabular}{|l|} 
AlCR \\
A276 \\
\hline
\end{tabular} \& \(\left|\begin{array}{ll}\text { UICRT } \& 2 \\ \text { U276 } \& 4\end{array}\right|\) \& － \& － \& \& － \\
\hline \multirow[t]{2}{*}{\(1 / 0 \mathrm{su}\).} \& \(K_{0}\) \& 1 \& Y225 \& \multirow[t]{2}{*}{Y525} \& 3／4 \& 1／8 \& 12 \& \[
\begin{gathered}
\text { NEST } \\
\text { INDENTOR }
\end{gathered}
\] \& － \& \[
\begin{array}{ll}
\text { A25D } \& \\
\text { Y34PR } \& 1
\end{array}
\] \& － \& － \& － \& \& － \\
\hline \& 1／2 \& 2 NEMA \& YA25－2M \& \& W6 \& 3／4 \& \[
\begin{gathered}
12, \\
163
\end{gathered}
\] \& DIE SET \& W163 4 \& \(\left|\begin{array}{ll}\text { A25R } \& 2 \\ \text { Al63 } \& 2\end{array}\right|\) \& \begin{tabular}{|l|l|} 
U25RT \& 2 \\
U163 \& 2
\end{tabular} \& － \& \begin{tabular}{ll} 
C163 \& \\
\hline
\end{tabular} \& \& － \\
\hline \multirow[t]{2}{*}{2／0 St．} \& 3／6 \& 1 \&  \&  \& \& K \& 13 \& \[
\begin{aligned}
\& \text { MEST } \\
\& \text { INDENTOR }
\end{aligned}
\] \& － \& \[
\begin{array}{|l|}
\hline \text { A26D } \\
\text { Y34PR }
\end{array}
\] \& － \& － \& \(-\) \& － \& － \\
\hline \& \(1 / 22\) \& 2 NEMA \& \[
Y A Z S-2 N
\] \& \& W6 \& 5／6 \& 13,

241 \& DIE SET \& \[
$$
\begin{array}{ll}
W & - \\
W 164 & 4 \\
W 241 & 3
\end{array}
$$

\] \& | A26R， | 2 |
| :--- | :--- |
| A164， |  |
| A241 | 2 |
|  | 2 | \& \[

$$
\begin{array}{|l|l|}
\hline 126 R T, & 2 \\
U 164, & 2 \\
U 241
\end{array}
$$
\] \& － \& $\begin{array}{ll}\text { c154，} \\ \text { C241 } & 1 \\ \end{array}$ \& － \& － <br>

\hline \multirow[t]{2}{*}{$3 / 0$ Str．} \& \multirow{4}{*}{1／2} \& 1 \& Y427 \& \multirow[t]{2}{*}{Y527} \& \multirow[t]{2}{*}{${ }_{3}$} \& 1／2 \& 14 \& \[
$$
\begin{aligned}
& \text { NEST } \\
& \text { INDENTOR }
\end{aligned}
$$

\] \& － \& \[

$$
\begin{array}{|ll|}
\hline \text { A27D } & 1 \\
\text { Y34PR } & 1
\end{array}
$$
\] \& － \& － \& $-$ \& － \& － <br>

\hline \& \& 2 NEMA \& 7227－2N \& \& \& 3／6 \& \[
$$
\begin{gathered}
14, \\
243
\end{gathered}
$$

\] \& OIE SET \& W243 3 \& | A27R | 2 |
| :--- | :--- |
| A243 | 2 | \& $\begin{array}{ll}\text { U27RT } & 2 \\ \text { U243 } & 2\end{array}$ \& － \& － 1 \& － \& <br>

\hline \multirow[t]{2}{*}{4／0 Str．} \& \& 1 \& Ya28 \& \multirow[b]{2}{*}{rs28} \& 1 \& 1／2 \& 15 \& \[
$$
\begin{aligned}
& \text { NEST } \\
& \hline \text { NDENTOR }
\end{aligned}
$$

\] \& \& | A280 |
| :--- | :--- |
| Y34PR |
| 1 | \& － \& － \& | C280 |
| :--- | :--- |
| Y48PR | \& － \& <br>

\hline \& \& 2 NEMA \& YA28－2N \& \& 11／6 \& \％ \& 15
BG

243 \& DIE SET \& \begin{tabular}{ll}
W－8G \& 2 <br>
W243 \& 3 <br>
\hline

 \& A28R $2: 1$ \& 

U28RT <br>
$U .8 G$ <br>
U243 <br>
<br>
<br>
\end{tabular} \& － \& $\begin{array}{ll}\text { C28R } & 2 \\ \text { C243 } & 1\end{array}$ \& － \& 1 <br>

\hline
\end{tabular}

> Type YA (cont.)



## HYLUG

 Type YA-LB


JHC HI-CAP Time Delay fuses, Class J Dimension, with 200,000 amperes RMS interrupting capacity and great current limitation - to which has now been added substantial time delay. CSA Listed at 100,000 amperes.


| Symbol | Ampere <br> Rating | Dimensions in Inches |  |  |
| :---: | :---: | :---: | :---: | :---: |
| JHC | 15 to 30 | 21/4 | $1 / 2$ | ${ }^{13} / 16$ |
|  | 35 to 60 | 23,8 | 5/8 | 11/66 |



| Symbol | Ampere Rating | Dimensions in Inches |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| JHC |  |  | B | c | D |  |  | G | H | J | K |
|  | 65 to 100 | 45/8 | 35/8 | 11/8 | 3/4 | 1/8 | 1 | 1/2 | $9 / 52$ | $3 / 8$ | 25/8 |
|  | 110 to 200 | 53/4 | $43 / 8$ | 15/8 | 11/8 | 316 | 13/8 | ${ }^{11} / 16$ | $9 / 32$ | $3 / 8$ | 3 |
|  | 225 to 400 | 71/8 | 51/4 | 21/8 | 15/8 | $1 / 4$ | 1\%8 | ${ }^{15} / 16$ | $13 / 32$ | 17/32 | 33. |
|  | 450 to 600 | 8 | 6 | 21/2 | 2 | 3/8 | 21/8 | 1 | 17/32 | ${ }^{11} 16$ | 33/4 |

## STRIP ELEMENTS



Utility clamps secure strip elements to fiat surfaces or surfaces with large radii such as large tanks. Threaded studs are weided to surface. heaters are positioned, then clamps are bolted down. Where more than one ciamp is used. tighten nuts and then back off $y_{2}$ turn to allow for expansion.


Milited plate. Heaters may be held in position in platens and similar objects with a steel plate recessed to hesters' width, thickness and positions, then screwed to the working plate or surface.

Oven mounting. Easy application of strip olements to ovens may be made simply with the use of welded-on studs and secondary insulation bushings (see Additional Features).
Mounting holes in tabs are slotted to allow for expansion.


## MAXIMUM WORK TEMPERATURES

Strip elements can generally be used in the following applications at maximum temperatures shown. without exceeding capability if properly installed:

| Froe Air Chrome steel sheath. | Air Temp. .... $950^{\circ} \mathrm{F}$ |
| :---: | :---: |
| Moving Air-air volume at 16 fps | Air Temp. |
| Rust-resisting iron sheath. Chrome steel sheath....... | $\begin{array}{r} 425^{\circ} \mathrm{F} \\ .950^{\circ} \mathrm{F} \end{array}$ |
| Clamp-on | Work Temp. |
| Rust-resisting iron sheath. Chrome steel sheath........ | $\begin{aligned} & \ldots 300^{\circ} \mathrm{F} \\ & \ldots 700^{\circ} \mathrm{F} \end{aligned}$ |
| The above maximum work temperatures are based on $\mathbf{1 0}$ watte per square inch. If elements have a lower watt density, work temperature may be increased. |  |
| MAXIMUM SHEATH TEMPERATURES |  |
| Rust-resisting iron Chrome steel...... Incoloy. | $\begin{aligned} & \therefore . \\ & 750^{\circ} \mathrm{F} \\ & \cdots .1200^{\circ} \mathrm{F} \\ & \cdots .1600^{\circ} \mathrm{F} \end{aligned}$ |

EXCLUSIVE CONSTRUCTION


High-quality, coiled nickel-chrome re sistor wire is uniformly spaced over the width and length of the strip ele ment. then embedded in high-grade refractory material which both insulates the wire and transfers heat rapidly. Refractory is then compressed to rock hardness and maximum density under tremendous hydraulic pressure to improve heat transfer from coil to sheath. Elements are oven baked at high temperatures to semi-vitrify and mature the refractory

## Installation

Chromalox strip elements in most cases can be applied with standard hardware. However, for firm contact and best heat transfer, stocked Chromalox strip heater clamps are recommended. See page 13. Instruction Bulletin P00400 is packed with each shipment.

## Thermostatic Control

Automatic temperature controls may be selected and in stalled as described in Controls Section.

## Connecting Lead Wires

should be nickel-plated copper, nickel or alloy. Copper will oxidize and loosen connections. Refer to page 79 for wire, bus bar, etc.

High-voltage Use
Where line voltage is above 300 V ( 600 V maximum), Chromalox strip elements can be connected in series for air heating, providing they are mounted on secondary insulation bushings (see below). Maximum voltage for clamp-on installations is 480 V to ground.

## additional features-see following tables for ordering information



Secondary Insulation Bushings
Needed at each end of strip heaters when connected in series on line voltages a bove 300Y.
Note: To accommodate bushings, a $11 / 33^{\prime \prime} \times{ }^{11 / 1 s^{\prime \prime}}$ dia. hole is substituted for the standard siot in each mounting tab when bushings are on same purchase order as strip heaters; otherwise, $17 / 33^{17} \times{ }^{11 / 16^{\prime \prime}}$ dia. mounting hole in tabs should be specified for heaters. Additional price includes two bushings, hardware and eniarging mounting holes. All types except NS.


## Coramic Post Terminal Insulators

Use with insulated wire to protect against electrical shock ... to wire several heaters where Bx or conduit is not required. Wires can leave heater terminals at any angle. For strip heaters only. All types except NS and SN.


Without Mounting Tabs
Permits installing more heat in a given confined space.
Specify "'without mounting tabs' if this feature is needed. All types except NS.


Protective Terminal Cover
Guards terminals from spillovers, dripping, grounding or short circuits.
Removable cover, with BX fitting, is shipped separately.
Types PT and SE only.

## $11 / 2^{\prime \prime}$ wide



| DIMENSIONS-T ${ }^{\text {a ches }}$ |  |  | RUST-RESISTING IRON SHEATH See pg. 6 for max. sheath and work temp. |  |  |  |  | CHROME STEEL SHEATH <br> See pg. 6 for max. sheath and work temp. |  |  |  |  | Approx Net Wt. Lbs |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| oviral | $\stackrel{\text { B }}{\text { Mes. Hole }} \text { Conter }$ | $\underset{\substack{\text { mithout } \\ \text { Mitg. Tobs }}}{0}$ | Vome | mma | Watts <br> Sq. In. | enabo Number | $\begin{aligned} & \text { Prownat } \\ & \text { (PCN) } \end{aligned}$ | Vamo | Wmbumber | $\begin{aligned} & \text { Watts } \\ & \text { Por } \\ & \text { Sq. In. } \end{aligned}$ | Catatey Nember | Pexativa Mo. (PCN) |  |
| 71/2 | 61/2 | 6 | 120 | 150 | 11 | OT-715 | 129314 | 120 | 200 | 15 | OT-702 | 129613 |  |
|  |  |  | 240 | 150 | 11 | OT-715 | 129322 | 240 | 200 | 15 | OT-702 | $229621$ | $.50$ |
| 8 | 7 | 61/2 | 120 | 150 | 10 | OT-815 | 129330 | 120 | 250 | 17 | OT. 802 | 129630 |  |
|  |  |  | 240 | 150 | 10 | OT-815 | 129349 | 240 | 250 | 17 | OT. 802 | $129648$ | $.50$ |
|  |  |  | 120 | 175 | 12 | OT-817 | 129357 | 120 | 400 | 27 | OT-804 | 129656 | . 56 |
|  |  |  | 240 | 175 | 12 | OT. 817 | 129365 | 240 | 400 | 27 | OT-804 | 129664 | . 56 |
| 101/2 | $91 / 2$ | 9 | 120 | 250 | 10 | OT-1025 | 129373 | 120 | 350 | 15 | OT.1003 | 129672 | . 75 |
|  |  |  | 240 | 250 | 10 | OT. 1025 | 129381 | 290. | 350 | 15 | OT-1003 | 129680 | . 75 |
| 12 | 11 | 101/2 | $\cdots$ | $\cdots$ | $\cdots$ | ........ | ....... | 120 | 400 | 17 | OT. 1004 | 129699 | . 88 |
|  |  |  | . | . | . | ....... |  | 240 | 400 | 17 | OT-1004 | 129701 | . 88 |
|  |  |  | 120 | 250 | 8 | OT-1225 | 229390 | 120 | 250 | 8 | OT-1202 | 129710 | . 88 |
|  |  |  | 240 | 250 | 8 | OT.1225 | 129402 | 240 | 250 | 8 | OT-1202 | $129728$ | $.88$ |
|  |  |  | $\cdots$ | -•• | -• | ....... | . $\cdot$. $\cdot$. | 120 | 350 | 14 | OT. 1203 | 129736 | . 88 |
|  |  |  | $\ldots$ | ... | . | ....... | $\ldots$ | 240 | 350 | 14 | OT-1203 | 129744 | . 88 |
|  |  |  | $\cdots$ | ... | $\cdots$ | ....... | ...... | 120 | 500 | 17 | OT-1205 | 129752 | . 88 |
|  |  |  | $\cdots$ | $\cdots$ | $\cdots$ | ........ | ...... | 240 | 500 | 17 | OT-1205 | 123760 | . 88 |
| 14 | 13 | 121/2 | $120$ | 300 | $8$ | $\text { OT. } 1430$ | 129410 | 120 | 500 | 14 | OT-1405 | 129779 | 1.0 |
|  |  |  | $240$ | 300 | 8 | OT-1430 | 129429 | 240 | 500 | 14 | OT-1405 | 129787 | 1.0 |
| 151/4 | 141/4 | 133/4 | 120 | 325 | 8 | OT-1532 | 129437 | 120 | 500 | 12 | OT-1505 | 129795 |  |
|  |  |  | 240 | 325 | 8 | OT-1532 | 129445 | 240 | 500 | 12 | OT. 1505 | 129808 | $1.13$ |
| 17\% | 167\% | 163/8 | 120 | 350 | 6.5 | OT-1835 | 129453 | 120 | 500 | 10 | OT-1805 | 129816 | 1.38 |
|  |  |  | 240 | 350 | 6.5 | OT.1835 | 129461 | 240 | 500 | 10 | OT. 1805 | 129824 | 1.38 |
|  |  |  | 120 | 375 | 7 | OT-1837 | 129470 | 120 | 750 | 15 | OT-1807 | 129832 | 1.38 |
|  |  |  | 240 | 375 | 7 | OT-1837 | 129488 | 240 | 750 | 15 | OT-1807 | 129840 | 1.38 |
|  |  |  | 120 | 500 | 10 | OT-1850 | 129496 | 120 | 1000 | 19 | OT-1801 | 129859 | 1.38 |
|  |  |  | 240 | 500 | 10 | OT-1850 | 129509 | 240 | 1000 | 19 | OT-1801 | 129867 | $\begin{aligned} & 1.30 \\ & 1.38 \end{aligned}$ |
| 191/2 | 181/2 | 18 | 120 | 350 | 6 | OT-1935 | 129517 | 120 | 500 | 9 | OT-1905 | 129875 | 1.5 |
|  |  |  | 240 | 350 | 6 | OT-1935 | 129525 | 240 | 500 | 9 | OT-1905 | 129883 | $\begin{aligned} & 1.5 \\ & 1.5 \end{aligned}$ |
|  |  |  | 120 | 500 | 8 | OT-1950 | 129533 | 120 | 750 | 13.5 | OT.1907 | 129891 | 1.5 |
|  |  |  | 240 | 500 | 8 | OT-1950 | 129581 | 240 | 750 | 13.5 | OT. 1907 | 129904 | 1.5 |
|  |  |  | $\cdots$ | . | -• | . $\cdot$..... | . $\cdot$. | 120 | 1000 | 18 | OT-1901 | 129912 | 1.5 |
|  |  |  | $\cdots$ | $\cdots$ | . |  | $\cdots$ | 240 | 1000 | 18 | OT-1901 | 129920 | 1.5 |
| 21 | 20 | 191/2 | 120 | 500 | 8 | OT-2150 | 129550 | 120 | 750 | 12 | OT-2107 | 129939 |  |
|  |  |  | 240 | 500 | 8 | OT-2150 | 129568 | 240 | 750 | 12 | OT-2107 | 129947 | 1.63 |
| 231/4 | 223/4 | 221/4 | 120 | 500 | 7 | OT-2450 | 129576 | 120 | 500 | 7 | OT-2405 | 129955 |  |
|  |  |  | 240 | 500 | 7 | OT-2450 | 129584 | 240 | 500 | $?$ | OT-2405 | 229963 | $\begin{aligned} & 1.01 \\ & 1.81 \end{aligned}$ |
|  |  |  | 120 | 750 | 10 | OT-2475 | 129592 | 120 | 750 | 10 | OT-2407 | 129971 | 1.81 |
|  |  |  | 240 | 750 | 10 | OT-2475 | 129605 | 240 | 750 | 10 | OT-2407 | 129980 | 1.81 |
|  |  |  | $\cdots$ | $\cdots$ | - | ....... | ..... | 120 | 1000 | 14 | OT-2401 | 129998 | 1.81 |
|  |  |  | $\cdots$ | ... | . | . $\cdot$..... | ...... | 240 | 1000 | 14 | OT-2401 | 130008 | 1.81 |

Speaity: Quantity, Catalog No., PCN, Volts, Watts, Strip Heaters. For additional features (page 6) available for Type OT, add: Without Mounting Tabs; Secondary Insulation Bushings-PCN 255716; Protective Terminal Cover-Catalog No. OT-AC-1, PCN 129242; Set of Two Ceramic Post Terminal InsulatorsPart No. 1-41059, PCN 259805.

Classification of Cartridge Fuses By Underwitters' Laboratories, Inc.
 over 10,000 amperes. Teated and listed per U.L Standards for fuses No. 1988. Neither Class lecter nor No. 1988. Nerther Class labter
interrupting rating on labels.

Class K: Teated and labelled for interrupting rating of 50,000 . 100.000 or 200.000 rms amps ac per NEC par. $240-80 \mathrm{C}$. Tested and ladelled per UL. Standards No. 198.3. Required by Stds. to have a specific degree of current
limitation but may NOT be so labelled per NEC par. 240-60b. Time Delay (min of 10 sec . at $500 \%$ of ratingl optional. Class and int. rating printed on label. Ali Economy Fuse Class K fuses have 200.000 amp. interrupting rating $\square$


Clase K-9: Fajr degree of current limitation. Usually supplied as Time Delav. No longer made by Economy.

Class J: $0-600$ amps., 600 V or less. Labelled as "Current Limiting" and for 200,000 symm. amps., ac interrupting rating. No time delay. Dimansions not interchangeable with other fuse ctasses. ECONOMY. JCL

Class L: 601-6000 amps.. 600V or less. Labelled as "Current Limiting" and for 200.000 symm. amps., ac interrupting rating. No time delay. Fuses bolt to bus bars.
ECONOMY: LCL
Cless R. Meet all Class $\times 100000$ amp requirements plus measured current limitation at 50.000 and 200,000 ampa. Labelled Currant Limiting and all have 200.000 amp. interrupting rating. Resemble Class K plus rejection feature to meet 1975 NEC par $240-60 \mathrm{~b}$. Economy Fuse offers Class $K$ combined with Class R as in table below.

| SELECTION CHART |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TRADE NAME $\longrightarrow$ |  | Eco |  | Economy Renewable |  | ECON ${ }^{+}$ |  | ECON. <br> LIMITER |  | ECONOLIM* |  |  |  |  | ECO* ECON |  |
| DESCRIPTION |  | Catalog Symbol Identification |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | EON | EOS | ERN | ERS | ECN | ECS | LEN | LES | NCL | SCL | JCL | LCL | MCL | MOL | MEN |
|  | $U$ L. CLASS | H | H | H | H | AK5 | RK5 | RK5 | RK5 | RK1 | RK 1 | J | 1 |  | sceilane | ous: |
| interaupting RATING | $\begin{aligned} & \text { Nor Over } \\ & 10.000 \text { Ampa } \\ & \hline \end{aligned}$ | $\times$ | X | $\times$ | $\times$ |  |  |  |  |  |  |  |  |  | X | X |
|  | 100,000 Ampa a.c. |  |  |  |  |  |  |  |  |  |  |  |  | $\times$ |  |  |
|  | 200,000 Amps. a.c. |  |  |  |  | X | $\times$ | x | $\times$ | $x$ | x | $x$ | $x$ |  |  |  |
| degree OF CURAENT LIMITATION | Excellent |  |  |  |  |  |  |  |  | x | $\times$ | x | $\times$ | $\times$ |  |  |
|  | Very Good |  |  |  |  |  |  | x | $\times$ |  |  |  |  |  |  |  |
|  | G000 |  |  |  |  | $\times$ | $\times$ |  |  |  |  |  |  |  |  |  |
| DIMENSIONS | $13 / 32^{\prime \prime} \times 1.1 / 2^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  | $\times$ | $\times$ | $\times$ |
|  | "N.E.C." | $\times$ | $\times$ | x | $\times$ | $x$ | $x$ | X | X | x | X |  |  |  |  |  |
|  | Non-interch. Dim. per U.L. |  |  |  |  |  |  |  |  |  |  | X | X |  |  |  |
| VOLTS (a.c.) | 250 or less | - x |  | $\times$ |  | $\times$ |  | $\times$ |  | $\times$ |  |  |  |  | $\times$ | x |
|  | 600 or less |  | $x$ |  | $\times$ |  | x |  | $x$ |  | X | $\times$ | $\times$ | X |  |  |
| $\begin{aligned} & \text { TIME-DELAY MIN OF } \\ & 10 \mathrm{SEC} \text {. AT } 500 \% \end{aligned}$ |  |  |  |  |  | X | X | X | x |  |  |  |  |  |  |  |

## Econolim ${ }^{\circledR}$ Current-Limiting, Energy Limiting, and High Interrupting Capacity Fuses

Fuses under the trademark "Econolim" are manufactured with silver links, quartz-sand filler, and melamine tubes. This line includes Underwriters' Laboratories, Inc. Clasees $\mathrm{K}-1$, J , and L , as well as midget dimension MCL fuses (aee
CLASS
1317 Econolim High Interrupting Capacity Fuses, U.L. Class K-1
Use on applications for fault currents up to 200,000 amperes, where very fast clearing is required to limit current and where fuse holders are of NEC dimensions. Ideal for


## Class

1318 Econolim Current-Limiting Fuses, U.L. Class J
Applications of this type fuse are for fault currents up to 200,000 amperes, for high degree of current limitation, and to comply with NEC paragraph 240-23(b). For use only in Class J fuse holders which will not accept Clans H or K fuses. Note: No U.L. listed Class $J$ fuces have time delay.


## CLASS

## 1319

Econolim® Current-Limiting Fuses, U.L. Class L
Uned on installations for fault curreats up to 200,000 amperes, for mounting in bolted pressure switches, zervice interrupters, switchgear, and fused air circuit breakers. Ideal for protection of large circuit breakers which may not have adequate interrupting ratings.

| Amperas: | Cotalor Mumbers | Ner Esch | Comion Oumentiv |
| :---: | :---: | :---: | :---: |
| 01 | LCLEO1 |  | 1 |
| 800 | SCls00 |  | 1 |
| 1000 | LCL. 1000 |  | 1 |
| 1200 | CCL1200 |  | 1 |
| 180 | LCLIES0 |  | 1 |
| 2000 | LCL2000 |  | 3 |
| 2500 | LCL2500 |  | 3 |
| 3000 | LCL 3400 |  | 3 |
| 4000 | Lel4000 |  | 3 |
| 8000 | LELS000 |  | 3 |
| 0000 | LCLe000 |  | 3 |

- For 4001-6000 amperes, specify whether 4 or 6 hole drilling is desired.
个 Other ratings available on request
page 35). All of these fuses have a high degree of current limitation with low $I_{t}$ energy let-through and low peak let-through current as well as the highest interrupting rating recognized by U.L. for low voltage fuses. Ask for detailed tochnical data by the FPE Class Number shown. with inadequate interrupting ratings. These fuses meet the current limiting requirements of U.L. Class K-1 standards.


CLASS
1312A Econolim* Type RF Fuses
Econolim Type RF fuses for protection of special descriptive catalog sheets Class rectifier equipment are made and available in $130,250,600$ and 600 volt ratings. Ask for

1312A.

Military-Specification Fuses: FPE-Economy Fuse can provide fuses to meet Department of Defense Specification MIL-F 15160 D or E, and WF-1726 as "qualified products." We also qualify under proposed specification WF-1814.
General Services Administration Fuses: FPE-E conomy Fuse can provide fuses under the various parts of GSA Specification W-F-791d and e.

ECO" "ONE-TIME" CARTRIDGE FUSES are UL listed and labelled as Class $H$ for use on circuits where available fault currents do not exceed 10,000 amperes. They feature caps rolled into the tubes, staking to prevent cap
rotation, links visibly soldered to caps and stamped-in-brass identification. This fuse provides lowest cost short-circuit protection. For detailed data, ask for Class 1340 Descriptive Sheets.



EXCLLSIVE DESIGN: Federal Pacific's exclusive construction (patented) has three insulating air spaces and two heat shields for eviellent performance with constant comfort temperature and low droop. Other patents pending.
SMARTLY STYLED: The smartly styled. mist beige color acrylic cover blends whth the decor of any room. Easv-to-read gold dial has actual teriperature numbers with a wide range of settings from $4)^{3}$ to $85^{\circ}$

SNAP ACTION SWITCH: Bi-metal actuated. quick-make. quickik switch eliminates interierence noises.
. IIT KIT: High limit kit (field selected) is especially desmable for se applications where maximum limited heat range is desired.
THERMOMETER KIT: Easily installed in the field. Glass thermometer is mounted in decorative plastic housing. Attaches to thermostat with pressure sensitive adhesive backing.


## Line voltage electric heat thermostat

## DESCRIPTION AND ORDERING INFORMATION

| Catalog Number PMT1 |  | Catalog Numberl PMT2' |  |
| :---: | :---: | :---: | :---: |
| Single line break (single pole) single throw switch. Makes and breaks electrical load - switch closes on temperature fall. |  | Double line break. Two single pole single throw switches. Opens all ungrounded conductors of electrical load when in "OFF" position only. Makes and breaks single load-switch closes on temperature fall. |  |
| SPECIFICATIONS |  |  |  |
| Control Range | e Volts AC | Ampacity | Watts Non-induc |
| $40^{\circ} \mathrm{F}$. to $85^{\circ} \mathrm{F}$. | 120 Vac. | 22 Amps. | 2640 |
|  | . 208 Vac. | 22 Amps. | 4566 |
|  | 240 Vac. | 22 Amps. | 5280 |
|  | 277 Vac. | 19 Amps. | 5280 |
| ACCESSORIES |  |  |  |
| Catalog Number | Description |  |  |
| PATTK | Thermometer kit. Glass thermometer mounted in decorative plastic housing. Pressure sensitive adhesive backing for field mounting to stats. |  |  |
| ULK | Temperature limit kit. Provides tamper proof, adjustable upper temperature limit. ${ }^{\circ}$ Field installed in all models. |  |  |

## SUGGESTIONS FOR CORRECT INSTALLATION OF WALL THERMOSTATS

The best location for a thermostat is on an inside wall or partition, 50 to 54 inches above the floor.

Precautions to be observed:

1. Install thermostat at least 3 feet from doonways.
2. Do not install in stairwells or draft areas.
3. Install thermostat so that air can circulate freely around the unit. Do not block with shelving, etc.
4. Avoid heat from hot pipes, ducts, lamps, TV's and similar appliances. Heat from woll switches may also affect a thermostat.
5. Rooms not seperated by walls, such as living-dining areas, should be controlled by a single thermostat.


## INSTALLATION PROCEDURE

1. Rernove knob by pulling out.
2. Remove snap-on cover. Pull out bottom and lift up and off.
3. Wire as shown in schematic diagram below.
4. Fasten to box with captive screws.
5. Replace snap-on cover.
6. Line up flat of cam shaft, with flat in knob recess and press knob beck in place.

## WIRING PROCEDURE

1. Wire lengths should be cut to minimum code requirements.
2. Strip wires $3 / 8$ to $1 / 2$ inch long.
3. Note LINE and LOAD markings near switch terminals. Do Not reverse these connections or thermostat will not operate properly.
4. Insert wire leads under the terminal screws as shown. Tighten securely. Loose connections run hot and will affect the performance of the thermostat.
5. Rotate the cam to "LO" or "OFF" position. This dlowe the "flat" at the top of the cam to clear the screw driver blede.
6. Mount thermostat to outlet box using a small shank screw driver. This will avoid damage to the bi-metal. The base plate mounting slots are designed to bend sward the outlet box during tightening. This simplies the installation by eliminating any thermostat distortion.

## WIRING DIAGRAMS

## CAUTION

DO NOT REVERSE LINE AND LOAD CONNECTIONS TO THE THERMOSTAT


Terminals are approved for copper or aluminum wire.

## DESCRIPTION

The Type LAV relays are single phase induction disk relays designed to respond, with time delay, to either an increasing or a decreaing voltage, or both. Some modeis are frequency compensated, and some include an instantaneous unit (hinged ammature type). Most models listed in the Selection Guide include a target seal-in urit on all contacts.

The basic mechanism of all models is an induction-disk unit with either a tapped coil or a tapped resistor for setting pickup.

In the overvoitage models, the relay is calibrated on increasing voltage to close the aormally open contact at tap setting. The time dial adjusts the angle through which the disk rotates and, hence the time delay.

In the undervoltage models, the relay is calibrated on decreasing voltage to close the normally closed contact at tap setting. The time dial adjusts the angle through which the disk rotates at voltages above tap setting.

In the combined overvoltage and undervoltage models, the relay is calibrated on increasing voltages to close the normally open contacts at tap setting and on decteasing voltages to close the normally closed contacts at various percentages of tap setting.

For the undervoltage and combined undervoltage and overvoltage relays, the two connecting plug S2 case is used to prevens faise tripping when the relay is removed or replaced. Either plug completes the coil circuit and thus opens the normally closed contact used with undervoltage operation. Both plugs are needed to complete the contact circuits.

## APPLICATION

## overvoltage relays

Type IAC overvoltage relays are used for protection against smple overvoltage, but osher applications are also common. They are applied to ground detection, both on feeders and on ac generators, and they are also used in timed switching arrangements. where their dependability and accuracy make them preferabie to purely mechanical timing relays.

For protection against overvoltage in a three-phase system, use the IAV51A relay (Fig. 2). For instantaneous protection as well as time delay, use the IAV71B.

For the detection of grounds on ungrounded three-phase systems, two methods are in general use. One measures the zero sequence potential (Fig. 4), and the other measures the actual voltage between the system neutral and ground (Fig. 6).

For the circuit of Figure 4, use Type LAV51D, a low pickup relay which has its operating circuit tuned to the rated frequency. The potential transformers used in this circuit are connected grounded-Y primary, broken- delta secondary. The primaries should have ratings equal to the line-to-line voltage of the system, and the secondaries can have ratings of either 67 or 115 volts.

Select a relay model with a continuous rating of three times the potential transformer secondary voltage. This is necessary because, when a ground occurs, the zero sequence voltage may be up to three times the normal transformer secondary voltage. Thus. with a potential transformer secondary rated 67 volts, use a 199 -volt relay coil. For ground fault protection of ac rotating machines, use a circuit similar to that shown in Figure 6 applying Type LAV51D or LAV5iK relays. These are low-pickup relays whose coil circuits are cuned by capacitors to their rated frequencies. The circuiss are thus rendered only one-eighth as sensitive to the third harmonic as they are to the rated frequency.

In Figure 6. a distribution transformer is connected between the machine neutral of the generator and:ground. Normally there is no voltage on the transformer but during a fault, there is a voltage with a worst-case magnitude equal to the phase-to-ground value.

Greater sensitivity can be obtained by choosing a distribution transformer with higher secondary voltage. in such a case, the relay will not carry the fault voltage continuously, and provision must be made to de-energize the operating coil using an aux-


Fig. 1. Type IAV71A overvaltage relay (out of case)
iliary relay. The short-time rating for bot: LAV51D and LAVSIK is 360 volts for If seconds.

The LAV51M relay may be used for definite time delay and the time is adjustabl: from 3 to 30 seconds by means of a ture diai Operating time is defined as the time tc close the contacts with voltage suddenly raised from zero to the sated value.

## UNDERVOLTAGE RELAYS

For simple undervoitage protection, select the IAV relay according to the time voltage characteristic required.

In a typical automatic-preferted emergency throwover scheme, the undervolage contacts of the IAV54E relay are used to trip the circuit breaker in the normal source circuit, and the auxiliary switch ( $52 b$ ) of this normal source breaker permirs the voltage closing contacts of an IAV51A relay in the emergency source to close its circuit breaker.

## COMBIMED UNDERVOLTAGE and overvolitage relays

Types IAV53, LAV69, lav70, and IAV 73 relays are time-delay, over-and undervoltage relays having two contacts, one of which closes on overvoltage and the orher on undervoltage.

## REFERENCES:



## Type IAV

## Time Delay Voltage Relays

FRi IENCY COMPENSATION
The followng Type IAV relays are fre:uncy compensated:
Thervotage relays-LAV71, IAV72
Cincervoltage relays-IAV74A
Lindervoltage and Overvoltage relays:AvT3A. IAV73B
These relays have uniform characteristics. ver a frequency range of $30-90$ Hertz A remel application is on systems supplied by indro-generators where the frequency ends to increase wien faults occur. Fresuency compensation is provided by an-R-C arcut across the wound shading coils of the suctioo disk operating coil and core unit.

## CHARACTERISTICS

Type LAV relays will continuously withund rued voltage on all taps, and tap voitage on all laps above rated voitage. For the
minimum and maximum taps shown in the list below, the following intermediate taps are available:

| Tap Range | Taps Available |
| :---: | :--- |
| $5.4-20$ | $5.4,7.5,12.5,20$ |
| $10-40$ | $10,15,25,40$ |
| $16-64$ | $16,24,40,64$ |
| $28-112$ | $28,42,70,112$ |
| $55-140$ | $55,64,70,82,93,105$, |
| $110-280$ | $-120,10,128,140,164 ; 186$, |
|  | $220-560$ |
|  | $220,240,280$ |
|  | $220,280,328,372$. |
|  | $420,480,560$ |

The overvoltage relays and the undervoltage relays are provided with time dials for adjustment of time delay.

The combined under- and overvoltage relays are made both with and without timedelay adjustment. Modeis IAV53, -69, and -73 have time delays which are functions of the setting of the undervoltage contacts. Model IAV70.has a time dial which permits adjustment of time delay independently of the voltage settings.

## TRIPPING CIRCUITS AND CONTACT RATINGS

The current carrying rating of the contact circuit is determined by whether the relay has a seal-in unit and by the tap used on the seal-in coil. Without a seal-in unit the relay contacts will close and carry 30 amperes for tripping duty and 2 amperes continuously at control voitages of 250 volts de or less. Refer Section 7381 for data on target seal-in units.

## SELECTION GUIDE-Type IAV

| General Dencipinon | $\begin{aligned} & \text { hownd } \\ & \text { Volth } \\ & \text { AC } \end{aligned}$ |  |  | $\begin{aligned} & \text { Targen } \\ & \text { Soct } \\ & \hline \end{aligned}$ | Combect | Maded Numbers |  | $\mathrm{Cume}_{\text {Size }}$ | Approx Wi, ib (ig) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | max |  |  | 60 Hertz | 50 Hem |  | Nom | Ship |

## JVTIVOLTAGE (DEVICE Ne S9)

| 2mend owr. ovemarrepp and compol racky ins deloy I io 10 <br> xame is nmow <br> $=\cos$ | $\begin{aligned} & 115 \\ & 200 \\ & 200 \\ & 460 \end{aligned}$ | $\begin{array}{r} 55 \\ 70 \\ 110 \\ 220 \end{array}$ | $\begin{aligned} & 140 \\ & 140 \\ & 280 \\ & 560 \end{aligned}$ | 0.212 | 1-N.O. | $\begin{array}{r} \text { I2IAVSIA1A } \\ \text { AフA } \\ \text { A2A } \\ \text { ABA } \end{array}$ | $\begin{array}{r} \text { IZIAVS IAAA } \\ \text { A9A } \\ \text { ASA } \end{array}$ | \$1 |  | ${ }^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\cdots{ }_{-\infty} \quad$ SiA | $\begin{aligned} & 115 \\ & 199 \\ & 280 \end{aligned}$ | $\begin{array}{r} 55 \\ 70 \\ 110 \\ \hline \end{array}$ | 140 140 280 | $\begin{aligned} & 0.2 / 2 \\ & (1) \end{aligned}$ | 2-N.O. | $\begin{array}{r} \text { 12IAVS2A1A } \\ A 7 A \\ A 2 A \end{array}$ | $\begin{array}{r} \text { 12lAYS2AAA } \\ \text { ASA } \\ \hline \end{array}$ |  | $(5,4)$ | $\begin{gathered} 15 \\ (48) \end{gathered}$ |
| Leve Mctup |  |  |  |  |  |  |  |  |  |  |
|  -ange - om ofery 0.35 to 7.1 | $\begin{aligned} & 115^{\circ} \\ & 199^{\circ} \\ & 345^{\circ} \end{aligned}$ | 10 | 40 64 112 | $0.2 / 2$ | $\begin{gathered} 3=0 \\ 1-N . O \end{gathered}$ | $\begin{array}{r} \text { 121AV5102A } \\ 01 A \\ 09 A \\ \hline \end{array}$ | 12IAVSIDSA DAA D10A | \$1 | $\begin{gathered} 12 \\ (5.4) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (6.8) \\ \hline \end{gathered}$ |
| - Nose 3 :50\% of cop semberg <br> - 4.comi on no. 10 ros. | $6{ }^{\circ}$ | 5.4 | 20 |  |  | 121AV51K1A | 121av5ik2A | S1 $\dagger$ | $\begin{gathered} 13 \\ (5.9) \end{gathered}$ |  |
| $\begin{aligned} & \Rightarrow \text { an invilo or lavsik acopt } \\ & \text {-0 Conear } \end{aligned}$ | 199\% | 16 | 64 |  | 2-M.O. | 121AV5201A |  | 51 | 12(5.4) |  |
|  | - $\mathbf{7}^{\mathbf{4}}$ | 3.4 | 20 |  |  | 12tav52K1A | 121AV52K2A | S17 | $\begin{gathered} 13 \\ (5.9) \end{gathered}$ | $\begin{gathered} 16 \\ (7.3) \end{gathered}$ |
|  |  |  |  |  |  |  |  |  |  |  |
| -porve dowe min men diley. <br>  <br> -20 macern of romed ravil | $\begin{array}{r} 115 \\ 208 \\ 200 \\ \hline \end{array}$ |  | 35 100 110 | $0.2 / 2$ | I-N.O. | $\begin{array}{r} 121 \mathrm{AVS} 1 \mathrm{MIA} \\ \mathrm{MAA} \\ \hline \end{array}$ | 121AVS1M2A | 51 | $\begin{gathered} 12 \\ .(5.4) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (6.8) \end{gathered}$ |
| Remenery Compensetor |  |  |  |  |  |  |  |  |  |  |
|  | 115 | 55 | 140 | :0.282 | 1-N.O. | l2tav71ala | 121AV7143A | 51 | $\begin{gathered} 13 \\ (5.9) \end{gathered}$ | $(7.3)$ |
| - Me memary comomenteat; for urdrof <br> - Prow socesomonk: general dutr tor ac <br> -row swemage arorecimon and wolroge <br> $\rightarrow$ Hece seance 1010 wecond trove delay. | $\begin{array}{r} 115 \\ 230 \\ 230 \end{array}$ | $\begin{array}{r} 55 \\ 110 \\ 110 \end{array}$ | 140 280 280 |  |  | 121AV7182A 85A $86 A \Delta$ | 121av71ajat ...... |  |  |  |
| $\cdots \cdots \geqslant 0$ comorn | 115 | 55 | 140 |  | 2-N.O. | 121AVT2A1A |  |  |  |  |
| $=\rightarrow 0 \text { Connot }$ | $\begin{array}{r} 115 \\ 200 \end{array}$ | 155 | $\begin{aligned} & 140 \\ & 280 \end{aligned}$ |  |  | 121AV72414t | 12HV7284At |  |  |  |
| - 2nO Connoch | 115 | 55 | 140 |  |  |  | I21AY72CA4 |  |  |  |

IVSID. 51 K .52 D . and 52 K - 10 Second Rating at 360 volvs udes external capecitor
It unat adjustable $120-200$ volts
$\therefore 2$. wnit adustable $180-300$ volis

## SELECTION GUIDE-Type IAV



## Time Delay Voltage Relays

## dIAGOAMS AND CHARACTERISTICS



Fig. 2 Trpiead external for Iype lav51a used for overvaltage protection.


Generator
P.8. 4. Typical externai for ground fault pratection 3ph. Ungrouaded system Type IAV51D


Fig. 6. Trpical external for ground fault pr. ection of an as rotating machise Type IAV51D or 51K


Fig. 3. Typical time Volfage aurve for Types LAV51A, 71 and 72


Pip. 5. Typical Time Voltage eurve fer Types LAV5ID and 51K.


Fig. 7. Typical Time Voltoge eurve for Types IAV53K, 53L 73A and 73B

## VOLTAGE RELAYS

Types
IAV51A IAV53D
IAV52A IAV53K
IAV53A IAV53L
IAV53B IAV53M
IAV53C IAV53N


## General (6) Electric

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## VOLTAGE RELAYS

## TYPES

IAV5TA
IAV52A
IAV 53A, 53B, 53C, 53D, 53K, 53L, 53M and 53N

## DESCRIPTION

Type IAV elays are single-phase, voltage operated, induction-disk relays with adjustable time delay. * The IAV5IA and IAV52A are overvoltage relays. The IAV53A, B, C, D, K, L, M, N are over- and undervoltage relays.

## APPLICATION

These IAV relays are used for protection against alternating current overvoltage, for permissive control and tripping of automatic equipment, and for ground detection on equipment and feeders.

Fig. 10 shows the typical connections for the application of an IAV51A relay for protection against * overvoltage in a three-phase system. The IAV52A can be used for applications requiring two trip output * circuits. The operating time characteristics for these relays are shown in fig. 12.

* Fig. 11 shows the connection diagram for IAV53 over- and undervoltage relays. The IAV53A has separate normally open and normally closed contacts with seal-in units on each contact. A typical application for permissive control and tripping of automatic equipment would utilize the normally open contact to enable the machine breaker closing circuit when nomal machine voltage is present, and the normally closed contact to operate the machine breaker trip circuit for undervoltage conditions. The operating time characteristics for the IAV53A and IAV53B relays are shown in Fig. 13. The IAV53D time characteristics are shown in Fig. 14 .

The IAC53C is designed for ground fault protection, and would normally be applied with a phase-toneutral connection, giving 58 percent of rated voltage. The relay is adjusted to have a 10 -second operating time for either a ground on the connected phase ( 0 volt operates the UV contact), or a ground on another phase (rated volts operates the $O V$ coil).

## RATINGS AND BURDENS

The operating circuit ratings available are shown in Table I. The operating coil will stand rated voltage continuously on any tap and will stand tap voltage continuously on the taps above rated voltage.

TABLE I

| RELAY | VOLTAGE RATINGS |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 300 Hz | 140 Hz | 100 Hz | 60 Hz | 50 Hz | 40 Hz | 35 Hz | 25 Hz |
| IAV51A | 115 |  | 115 | $115$ | $115$ | $\begin{aligned} & 115 \\ & 199 \end{aligned}$ |  | 115 199 |
|  |  | ; |  | $\begin{aligned} & 208 \\ & 230 \\ & 460 \end{aligned}$ | 208 230 460 |  |  | $230$ |
| IAV52A | - |  |  | $\begin{aligned} & 115 \\ & 199 \\ & 230 \\ & 460 \end{aligned}$ | $\begin{aligned} & 115 \\ & 199 \\ & 230 \end{aligned}$ |  |  | $\begin{aligned} & 115 \\ & 199 \\ & 230 \end{aligned}$ |

These instructions do not purbort io cover all details or variations in equipment non to provide for every posscble contingency to be met un connectcon witi unstullation, operation or maintenance. Should firther information be desered or should particular problems arise which are not covered sutficientlu for


To the extent required the products lescrioed herein meet applicable ANSI, IEEE and NEMA standards; but no such assurance is given whin respect to local codes and ordinances because they vary greatly.

TABLE I (Con't.)

| RELAY | VOLTAGE RATINGS |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 300 Hz | 140 Hz | 100 Hz | 60 Hz | 50 Hz | 40 Hz | 35 Hz | 25 Hz |
| IAV53A |  | 115 | 115 | $\begin{aligned} & 115 \\ & 230 \\ & 460 \end{aligned}$ | $\begin{aligned} & 115 \\ & 230 \end{aligned}$ |  | 230 | $\begin{aligned} & 115 \\ & 230 \end{aligned}$ |
| IAV538 |  |  |  | 115 230 460 | $\begin{aligned} & 115 \\ & 230 \end{aligned}$ |  |  | 115 |
| IAV53C |  |  |  | $\begin{array}{r} 115 \\ 199 \\ \hline \end{array}$ | $\begin{aligned} & 115 \\ & 199 \end{aligned}$ |  |  | 115 199 |
| LAV530 |  |  | 115 | $\begin{aligned} & 115 \\ & 240 \end{aligned}$ |  |  |  | 115 |

The current-closing rating of the contacts is 30 amperes for voltages not exceeding 250 volts. The current-carrying ratings are affected by the selection of the tap on the seal-in coil as indicated in
table II

| FUNCTION | AMPERES |  |
| :--- | :---: | :---: |
|  | 2-Amp TAP | 0.2 -Amp TAP |
| Tripping Duty | 30 | 3 |
| Carry Continuously | 3 | 0.3 |

he two-ampere tap has a d-c resistance of 0.13 ohms and a 60 cycle impedance of 0.53 ohms while the 0.2. ..ipere tap has a seven-ohm d-c resistance and a 52 ohm 60 cycle impedance. The tap setting used on the seal-in element is determined by the current drawn by the trip coil.

The 0.2 -ampere tap is for use with trip coils that operate on currents ranging from 0.2 up to 2.0 amperes at the ninimum control voltage. If this tap is used with trip coils requiring more up to 2.0 there is a possibility that the seven-ohm resistance will red with trip coils requiring more than two amperes, breaker will not be tripped.

The two-ampere tap should be used with trip coils that take two amperes or more at minimum control voltage, provided the tripping current does not exceed 30 amperes at the maximum control voltage. If the tripping current exceeds 30 amperes an auxiliary relay should be used, the connections being such that the
tripping current does nat pass through the

The above data in regard to
the Types IAV53B and IAV530 which contact rating applies to all relays covered by these instructions except limi ied in their current-carrying capacity by seal-in units. In these cases, the contact ratings are

| FUNCTION | VOLTS | AMPERES |  |
| :---: | :---: | :--- | :--- |
|  |  | $a-c$ | $d-c$ |
| Make and | 125 | 1.5 | $0.3 * *$ |
| interrupt | 250 | 0.75 | $0.15 * *$ |
| at | 600 | 0.00 | 0.00 |

[^0]
## REPRESENTATIVE

Burdens for the various relay types are given in Table III.
tABLE III

| $\begin{aligned} & \text { RELAY } \\ & \text { TYPES } \end{aligned}$ | VOLTAGE RATING | $\begin{gathered} \text { TAP *** } \\ \text { SETTING } \end{gathered}$ | $\begin{aligned} & \text { VOLT- } \\ & \text { AMPS } \end{aligned}$ | POWER FACTOR | WATTS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 60 - CYCLE BURDENS |  |  |  |  |  |
| $\begin{gathered} \text { IAV51A } \\ \& \\ \text { IAV52A } \end{gathered}$ | 115 | $\begin{array}{r} 140 \\ 120 \\ 105 \\ 93 \\ 82 \\ 70 \\ 70 \\ 64 \\ 55 \end{array}$ | $\begin{aligned} & 1.3 \\ & 1.8 \\ & 2.4 \\ & 3.1 \\ & 3.9 \\ & 5.4 \\ & 6.6 \\ & 9.2 \end{aligned}$ | $\begin{aligned} & 0.34 \\ & 0.35 \\ & 0.34 \\ & 0.33 \\ & 0.32 \\ & 0.31 \\ & 0.31 \\ & 0.35 \end{aligned}$ | $\begin{aligned} & 0.4 \\ & 0.5 \\ & 0.7 \\ & 0.9 \\ & 1.2 \\ & 1.7 \\ & 2.1 \\ & 3.2 \end{aligned}$ |
| $\begin{aligned} & \text { IAV53A, } \\ & \text { IAV53B, } \\ & \underset{\&}{\text { IAV53D }} \end{aligned}$ | 115 | $\begin{aligned} & 140 \\ & 120 \\ & 105 \\ & 93 \\ & 82 \\ & 70 \\ & 64 \\ & 54 \end{aligned}$ | $\begin{array}{r} 2.2 \\ 3.0 \\ 4.0 \\ 5.4 \\ 7.0 \\ 9.9 \\ 12.0 \\ 17.0 \end{array}$ | $\begin{aligned} & 0.32 \\ & 0.30 \\ & 0.31 \\ & 0.31 \\ & 0.32 \\ & 0.34 \\ & 0.36 \\ & 0.39 \end{aligned}$ | $\begin{aligned} & 0.7 \\ & 0.9 \\ & 1.2 \\ & 1.7 \\ & 2.2 \\ & 3.4 \\ & 4.3 \\ & 6.6 \end{aligned}$ |
| IAV53C | 115 | NO TAPS | 5.7 | 0.29 | 1.7 |
| $50-\mathrm{CYCLE}$ burdens |  |  |  |  |  |
| $\begin{gathered} \text { IAV51A } \\ 8 \\ \text { IAV52A } \end{gathered}$ | 115 | $\begin{aligned} & 140 \\ & 120 \\ & 105 \\ & 93 \\ & 82 \\ & 70 \\ & 64 \\ & 55 \end{aligned}$ | $\begin{aligned} & 1.2 \\ & 1.6 \\ & 2.1 \\ & 2.8 \\ & 3.6 \\ & 5.1 \\ & 6.2 \\ & 8.2 \end{aligned}$ | $\begin{aligned} & 0.34 \\ & 0.34 \\ & 0.34 \\ & 0.38 \\ & 0.36 \\ & 0.34 \\ & 0.34 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.4 \\ & 0.5 \\ & 0.7 \\ & 1.9 \\ & .3 \\ & 1.7 \\ & 2.7 \\ & 2.9 \end{aligned}$ |
| $\begin{gathered} \text { IAV53A } \\ \& \\ \text { IAV53B } \end{gathered}$ | 115 | $\begin{array}{r} 140 \\ 120 \\ 105 \\ 93 \\ 82 \\ 70 \\ 64 \\ 55 \end{array}$ | $\begin{array}{r} 1.9 \\ 2.5 \\ 3.4 \\ 4.6 \\ 6.0 \\ 8.4 \\ 12.9 \\ 13.2 \end{array}$ | 0.32 0.30 0.29 0.31 0.32 0.35 0.29 0.35 | $\begin{aligned} & 0.6 \\ & 0.8 \\ & 1.0 \\ & 1.4 \\ & 1.9 \\ & 2.9 \\ & 3.7 \\ & 4.6 \end{aligned}$ |
| IAV53C | 115 | NO TAPS | 4.8 | 0.32 | 1.6 |
| 25 - CYCLE BURDEHS |  |  |  |  |  |
| $\begin{gathered} \text { IAV51A } \\ 8 \\ \text { IAV52 } \end{gathered}$ | 115 | $\begin{array}{r} 140 \\ 120 \\ 105 \\ 93 \\ 82 \\ 70 \\ 64 \\ 55 \end{array}$ | $\begin{aligned} & 1.1 \\ & 1.5 \\ & 2.1 \\ & 2.7 \\ & 3.4 \\ & 4.9 \\ & 5.8 \\ & 8.2 \end{aligned}$ | 0.50 0.49 0.49 0.47 0.49 0.49 0.49 0.49 | $\begin{aligned} & 0.5 \\ & 0.8 \\ & 1.0 \\ & 1.2 \\ & 1.7 \\ & 2.4 \\ & 2.9 \\ & 4.0 \end{aligned}$ |

**Minimum pickup volts.

TABLE III (Con't.)

| RELAY <br> TYPES | VOLTAGE <br> RATING | TAP ** <br> SETTING | VOLT- <br> AMPS | POWER <br> FACTOR | WATTS |  |
| :---: | :---: | :---: | :---: | :--- | :--- | :---: |
| 25 - CYCLE BURDENS (COn't.) |  |  |  |  |  |  |
| IAV53A | 115 | 140 | 1.7 | 0.32 | 0.5 |  |
| \& |  | 120 | 2.3 | 0.30 | 0.7 |  |
| IAV538 |  | 105 | 2.9 | 0.30 | 0.9 |  |
|  |  | 93 | 4.2 | 0.30 | 1.3 |  |
|  |  | 82 | 5.3 | 0.32 | 1.7 |  |
|  |  | 70 | 7.5 | 0.34 | 2.6 |  |
|  |  | 64 | 9.5 | 0.34 | 3.3 |  |
|  |  | 55 | 12.9 | 0.39 | 5.0 |  |
| IAV53C | 115 | NO TAPS | 4.2 | 0.38 | 1.6 |  |

*Minimum pickup volts.

## CHARACTERISTICS

The Type IAV51A is an overvoltage relay with single-circuit closing contacts which close when the voltage increases to pickup value as set on the tap block. The time delay in closing the contacts is determined by the setting of the time dial at the top of the shaft. The time-voltage characteristics of this * relay are shown in Fig. 12.

The IAV52A relay is similar in every respect to the IAV51A relay except that it has additional contacts - for closing a second circuit. The time-voltage characteristics are shown in fig. 12

The IAV53A relay is an under-and overvoltage relay with double-throw contacts. The left-hand contacts close as the voltage increases to some predetermined value. The right-hand contacts close when the voltage decreases to same lower value. Between these two voltage values both contacts are open. Time-voltage

* Characteristics are shown in Fig. 13.

The Type IAV53B relay differs from the Type IAV53A relay in that it does not have seal-in elements. * Time-voltage characteristics are shown in Fig. 13.

The Type IAV53C relay is similar to the Type IAV53A relay except that there are no taps on the coil. The relay is adjusted to close its right contacts in 10 seconds when the voltage is reduced from 58 percent rated voltage to zero voltage; with this calibration the relay closes its left contacts in approximately 10 seconds when the voltage is increased from 58 percent of rated voltage to rated voltage. These relays are used connected line-to-ground so that under normal conditions the relay receives 58 percent of rated phase-to-phase voltage and both relay contacts are open. If the phase to which the relay is connected is grounded, the relay voltage goes to zero and the right-hand contacts close in 10 seconds. If either of the other two phases are grounded, the relay voltage increases to rated voltage and the left-hand contacts close in approximately 10 seconds.

The IAV53D relay is similar to the Type IAV53B relay except that it has a shorter time curve. Time* voltage characteristics are show in Fig. 14.

- The Type IAV53K is similar to the Type IAV53A, IAV53L to IAV53B, IAV53M to IAV53C and IAV53N toIAV530. All four relays are in the double-end case with contacts connected between the upper and lower blocks and operating coils connected to both blocks. The purpose of this is to avoid false tripping of the breaker if the connecting plugs are removed and subsequently reinserted with the relay in the reset position, i.e., circuit opening contacts closed. Insertion of either plug causes the relay to pick up; both plugs must be in place before the contact circuits are completed. See internal connections fig. 6-8 for coil and contact circuits.


## CONSTRUCTION

These relays are of the induction disk construction. The disk is actuated by a potential operating cail on a laminated U-magnet. The disk shaft carries the moving contact, which completes the trio or alarm circuit when it touches the stationary contact or contacts. The disk shaft is restrained by a soiral soring - ve the proper contact closing valtage, and its motion is retarded by permanent magnets acting on the It, $n$ to give the correct time delay.

* There is a seal-in unit mounted to the left of the shaft as shown in Fig. 15. This unit has its coil in series and its contacts in parallel with the main contacts such that when the main contacts close, the
seal-in unit picks up and seals in. When the seal-in unit picks up, it raises a target into view which latches up and remains exposed until released by pressing a button beneath the lower-left corner of the cover.

The case is suitable for either surface or semi-flush panel mounting and an assortment of hardware is p. -vided for either mounting. The cover attaches to the case and also carries the reset mechanism when one is required. Two of the cover screws have provision for a sealing wire.

The case has studs or screw connections at both ends or at the bottom only for the external connections. The electrical connections between the relay units and the case studs are made through springbacked contact fingers mounted in stationary molded inner and outer blocks between which nests a removabie connecting plug which completes the circuits. The outer blocks, attached to the case, have the studs for the external connections, and the inner blocks have the terminals for the internal connections.

The relay mechanism is mounted in a steel framework called the cradle and is a complete unit with all leads being terminated at the inner block. This cradle is held firmly in the case with a latch at the top and the bottom and by a guide pin at the back of the case. The cases and cradles are so constructed that the relay cannot be inserted in the case upside down. The connecting plug, besides making the electrical connections between the respective blocks of the cradle and case, also locks the latch in place. The cover, which is fastened to the case by thumbscrews holds the connecting plug in place.

To draw out the cradle from a single ended case, the cover must first be removed. Then the connecting plug can be drawn out. In so doing, the trip circuit is first opened, then the voltage circuits are opened. After the connecting plug has been removed, the lower latch can be released and the cradle easily drawn out. To replace the cradie, the reverse order should be followed.

RECEIVING, HANDLING AND STORAGE

## RECEIVING

These relays, when not shipped as a part of a control panel, will be shipped in cartons designed to protect them against damage. Immediately upon receipt of the relay, an examination should be made for any damage sustained during shipment. If injury or rough handling is evident, a damage claim should be filed ince with the transportation company and the nearest General Electric Sales Office should be notified .nptly.

## HANDLING

Reasonable care should be exercised in unpacking the relay in order that none of the parts are damaged or the adjustments disturbed.

## STORAGE

If the relays are not to be installed immediately, they should be stored in their original cartons in a place that is free from moisture, dust, and metallic chips.

## ACCEPTANCE TESTS

Immediately upon receipt of the relay an INSPECTION AND ACCEPTANCE TEST should be made to insure that no damage has been sustained in shipment and that the relay calibrations have not been disturbed.

If no pickup value for the left contact is soecified on the requisition for the relays with tap blocks, the relay is shipped with the tap plug in the fifth tap. If pickup is specified, the tap plug is set in the tap corresponding to this value. If a specified value does not coincide with one of the taps the tap plua is put in the tap nearest the required value (the lower tap is used if the value is half way between two taps) and the spring is adjusted to obtain the required pickup.

## VISUAL INSPECTION

Check the nameplate stamping to insure that the model number and rating of the relay agree with the
sition. requisition.

Remove the relay from its case and check that there are no broken or cracked molded parts or other as of piysical damage and that all screws are tight. Check that the shorting bars are in the proper docation(s) and that they are properly formed (see Fig. 9).

QUTION
EVERY CIRCUIT IN THE DRAWOUT CASE HAS AN AUXILIARY BRUSH. IT IS ESPECIALLY IMPORTANT ON CURRENT GIPCUITS ANU OTHER CIRCUITS WITH SHORTING BARS THAT THE AUXILIARY BRUSH BE BENT HIGH ENOUGH TO ENGAGE THE EWWEGTING PLUG OR TEST PLUG BEFORE THE MAIN BRUSHES DO. THIS WILL PREVENT CT SECONDARY CIRCUITS FROM Er"r OPENED.

## : ELTANICAL INSPECTION

1. On relays which have time dials, the dials will be set at zero before the relay leaves the factory. It is necessary to change this setting in order to open the relay contacts.
2. On all relays with locked time dials, make sure the two time-dial locking screws are tight. These locking screws are to prevent the dial from moving when the relay is subjected to high operating torque.
3. The moving contact should be fastened securely in its support and should engage the stationary contact about in the midde or at least $1 / 16$ inch inside the periphery of the stationary contact.
-4. The stop arm leaf spring should deflect about $1 / 64$ inch and the $s t o p$ arm should clear the molded block by at least . 020 inch.
4. Any foreign material must be cleaned out of stator air gaps. Clearance between the disk and either the drag magnet or $U$-magnet should be at least 0.010 inch for any position of the disk.
5. End play of the disk should be from 0.005 inch to 0.010 inch. End play should not be so great as to allow the disk to strike the $U$-magnet or the drag magnet. Check that top and bottom pivot and bearing
screws are tight.
6. There should be no noticeable friction in the rotating structure.
7. Rotate the time dial to the zero position. Check by means of a neon lamp that the contacts just close. There should be approximately $1 / 32$ inch wipe on the stationary contact. If the contact does not close, adjust the disk position by backing off the two clamping screws on the stop arm and rotating the stop arm relative to the cutout in the disk. This provides a coarse adjustment. Retighten the
clamping screws.
or fine adjustment of contact closing, run the stationary contact brush in or out by means of its adjusting screw; after this adjustment, check that the screw is held firmily in its support.
8. On double-throw relays, the support post of the upper spring should clear the insulating plate by at
least $1 / 64$ inch.

## ELECTRICAL TESTS

A. ORAWOUT RELAYS GENERAL

Since all drawout relays in service operate in their cases, it is recommended that they be tested in their cases or an equivalent steel case. In this way any magnetic effects of the enclosure will be accurately duplicated during testing. A relay may be tested without removing it from the panel by using a $12 \times$ LAli3A test plug. This plug makes connections only with the relay and does not disturb any shorting bars in the case. Of course, the $12 \times 2 A 12 A$ test plug may also be used. Although this test plug allows connections are made to 3. 3. POWER REQUIREMENTS GENERAL

All alternating-current operated devices are affected by frequency. Since non-sinusoidal waveforms can be analyzed as a fundamental frequency plus harmonics of the fundamental frequency, it follows that aliernating-current devices (relays) will be affected by the applied waveform.

Therefore, in order to properly test alternating-current relays it is essential to use a sine wave of current and/or voltage. The purity of the sinting-current relays it is essential to use a sine wave exeressed as a finite number for any particular relay, (i.e. its freedom from harmonics) cannot be $=$ : fetworks, or saturating electromagnets (such relay, however, any relay using tuned circuits, R-L or sy man-sinusoidal wave forms.

Similarly, relays requiring d-c control power should be tested using d-c power and not full wave retified power. Unless the rectified supply is well filtered, many relays will not operate properly --e dips in the rectified power. Zener diodes, for example, can turn off during these dips properly due to Hi: the d-c source should not contain more than 5 percent ripple. (han source should not contain more than 5 percent riple.

## C. PICKUP VOLTAGE TEST

The pickup voltage should be checked on one or more taps on relays which close contacts on increasing
voltage. The drop-out voltage should be checked on one or more taps on relays which close contacts on creasing voltage. See relay nameplates for values of pickup or drop-out voltages (closing voltages, right eft contact).

## D. TIME-VOLTAGE TEST

The time-voltage curves should be checked for one or more settings.

* Recommended test connections for the above test are shown in Fig. 17 for the overvoltage relays such as the Types IAV51A and IAV52A. The under- and overvoltage relays such as the Types IAV53A, IAV53B, IAV53C and IAV53D can be checked for time of closing left contacts by using connections shown in Fig. 17 , and for closing right contacts by the connections shown in Fig. 18. Of course the seal-in unit shown in the figure is not used in the case of the IAV53B and [AV53D, but all stud numbers are correct. Stud numbers 1 and 2 should be substituted for stud numbers 9 and 10 on Fig. 18 for testina the undervoltage contacts of the Type IAV53C relay. (See internal diagram, Fig. 5.) See internal connections, Figs. 6-8, for contact and coil connections for IAV53K, IAV53L, IAV53M and IAV53N.


## INSTALLATION

## INSPECTION

At the time of installation, the relay should be inspected for tarnished contacts, loose screws, or other imperfections. If any trouble is found, it should be corrected in the manner described under MAINTENANCE. Check the nameplate for model number and rating.

## LOCATION

The location should be clean and dry, free from dust and excessive vibration, and well lighted to faciliate inspection and testing.

## MOUNTING

The relay should be mounted on a vertical surface. The outline and panel drilling dimensions are shown in Fig. 19 for relay Types IAV51A, IAV52A and IAV53C. Fig. 20 shows outline and panel drilling for relay Types IAV53A, IAV53B and IAV530. Fig. 21 shows the outline and panel drilling for relay Types IAV53K, IAV53L, IAV53M and IAV53N.

## CONNECTIONS

* Internal connections are shown in Figs. 1 to 8 for the various relays.


## GROUND CONNECTIONS

One of the mounting studs or screws should be permanently grounded by a conductor not less than No. 12 B\&S gage copper wire or its equivalent.

## FIELD INSTALLATION TESTS

Before the relay is put in service, the pickup voltage and time-voltage tests described in ACCEPTANCE EESTS (ELECTRICAL TESTS) should be mace to determine that the adjustments have not been disturbed.

The relay may be tested while mounted on the panel, either from its own or another source of power, by inserting a separate testing plug in place of the connecting plug. Or, the cradle can be drawn out and replaced by another wich has been laboratory tested.

## PERIOOIC CHECKS AND ROUTINE MAINTENANCE

In view of the vital role of protective relays in the operation of a power system it is important that a periodic test program be followed. It is recognized that the interval between periodic checks will vary depending upon environment, type of relay and the user's experience with periodic testing. Until the user accumulated enougn experience to select the test interval best suited to his individual requirements is suggested that the points ilsted under INSTALLATION PROCEDURE be checked every six months.

## MAINTEMANCE

## 3:SK $2 \times \mathrm{MD}$ BEARINGS

The lower jewel may be tested for cracks by exploring its surface with the point of a fine needle. If is necessary to replace the jewel, the jewel should be turned up until the disk is centered in the sir gap, after which it should be locked in position by the set screw provided for the purpose.

## GONTACT CLEANING

For cleaning fine silver contacts, a flexible burnishing tool should be used. This consists of a flexible strip of metal with an etched roughened surface, resembling in effect a superfine file. The zolishing action is so delicate that no scratches are left, yet corroded material will be removed rapidly and thoroughly. The flexibility of the toal insures the cleaning of the actual points of contact. Sometimes an ordinary file cannot reach the actual points of contact because of some obstruction from some other part of the relay.

Fine silver contacts should not be cleaned with knives, files or abrasive paper or cloth. Knives or files may leave scratches which increase arcing and deterioration of the contacts. Abrasive paper or cloth may leave minute particles of insulating abrasive material in the contacts and thus prevent closing.

The burnishing tool described above can be obtained from the factory.

## SERVICING AND ADJUSTMENTS

TARGET AND SEAL-IN UNIT
For trip coils operating on currents ranging from: 0.2 up to 2.0 amperes at the minimum control voltage, et the target and seal-in tap plug in the 0.2-ampere tap.

For trip coils operating on currents ranging from 0.2 up to 2.0 amperes at the minimum control voltage, set the target and seal-in tap plug in the 0.2 -ampere tap.

For trip coils operating on currents ranging from 2 to 30 amperes at the minimum control voltage, olace the tap plug in the 2.0 -ampere tap.

The tap plug is the screw holding the right-hand stationary contact of the seal-in element. To che the tap setting, first remove the connecting plug. Then, take a screw from the left-hand stationary con...t and place it in the desired tap. Next, remove the screw from the other tap, and place it in the out of adjustment. Sion be the higher tap value and $a-c$ pickup will be increased the same time as pickup for direct current will VOLTAGE SETTING

The voltage at which the contacts operate may be changed by changing the position of the tap plug in the tap block at the top of relay for relays such as the IAV51A, IAV52A, IAV53A, IAV53B, and IAV53D which have tapped coils. The range of this adjustment is from 55 to 140 volts on the 115 volt ratings, 70 volts on the 460 volt ratings. ratings, 110 to 280 volts on the 208,230 and 240 volt ratings, and 220 to 560

The pickup of the relay for any voltage tap is adjusted by means of a spring-adjusting ring. The ring may be turned by inserting a tcol in the notches around the edge (see Fig. 15.) By turning the ring, the operating voltage of the relay may be brought into agreement with the tap setting employed if, for some reason, this adjustment has been disturbed. The adjustment also permits any desired setting between the various taps. The relay is adjusted at the factory to operate from any time-dial position at a finimum voltage within five percent of the tap setting for the relays with the tapped coils mentioned oltage for the overvoltage relays is the mine operating value on all the overvoltage relays. Operating just make.

On the under- and overvoltage relays such as the IAV53A, IAV53B, IAV53C, and IAV53D, the operating oltage for a given tap setting is the minimum voltage at which the left-hand contacts close. The right:nd contacts will then close at a certain percentage of operating voltage. If it is desired to change $\because$ is jercentage, the right-hand moving contact may be rotated on the shaft after first loosening the $\therefore$ Imsing screws that hold it in place. Changing the position of this contact gives an adjustment of the to close the right-nand contacts between 50 and 95 percent of the voltage whinadustment of the tic:s. Changing the position of the right-hand and 95 percent of the voltage which closes the left-hand :intacts close. Hence, simultaneous adjustments for contacts changes the voltage at which the left-hand sesired characteristic.

- indicates revision

The time of operation of the overvoltage relays is determined primarily by the setting of the time dial, while that for the under-and overvoltage relays is determined by the spread of the contacts as exlained under VOLTAGE SETIING. Further adjus tment is obtained by moving the permanent magnet along its suoporting shelf; moving the magnet in toward the back of the relay decreases the time while moving it out eases the time.

* Fig. 12 shows the time-voltage characteristics of the Type IAV51A and IAV52A relays with the dial setting for obtaining each characteristic. To make time settings, set the time dial to the number required (to give the desired characteristic) by turning it until the number lines up with the notch in the adjacent frame. The time indicated by the curves is the time required to close the relay contacts when the voltage is suddenly increased from a value below pickup to the value on the curve.
* Fig. 13 shows the characteristics of the Type IAV53A and IAV53B relay. The time characteristic of the relay is automatically determined by the setting of the ratio of the voltage to close the right contacts * to the voltage to close the left contacts. Fig. 14 shows the time-voltage characteristics of the Type IAV53D relay. No curve is given for the Type IAV53C since its time-voltage characteristics are explained under the section heading CHARACTERISTICS.

The time-voltage characteristics are plotted in percent thus making them applicable for all tap settings.

## BEARING AND CONTACTS

See MAINTENANCE.

## RENEWAL PARTS

It is recommended that sufficient quantities of renewal parts be carried in stock to enable the prompt replacement of any of those worn, broken or damaged. Parts bulletin number GEF-2149 gives a list of those most subject to wear in ordinary operation and to damage due to possible abnomal conditions.

When ordering renewal parts, address the nearest Sales Office of the General Electric Company, specify Uuantity required, name of part wanted as shown by Figs. 15 and 16 , and give complete nameplate data, luding serial number. If possible give the General Electric Company's requisition on which the relay was ...nished.


* SHORT F!NGER
*Fig. 1 (K-6209664-6) INTERNAL CONNECTIONS OF THE TYPE IAV5TA RELAY, FRONT VIEW


Fig. 2 ( $\mathrm{K}-6209665-3$ ) INTERNAL CONNECTIONS OF THE TYPE IAV52A RELAY, FRONT VIEW


Fig. 3 (K-6209666-3) INTERNAL CONNECTIONS OF THE TYPE IAV53A RELAY, FRONT VIEW


Fig. 4 (K-6400143-2) internal connections of the types iav53b and iav530 relays, front vied


Fig. 5 (K-6400385-2) internal CONNECTIONS OF THE TYPE IAV53C RELAY, FRONT VIEW

*Fig. 6 ( $\mathrm{K}-6556579-0$ ) INTERNAL CONNECTION DIAGRAM FOR TYPE IAV53M RELAY

*Fig. 7 (K-6556475-1) INTERNAL CONNECTION OIAGRAM FOR TYPE IAV53K RELAY


NOTE:AFTER ENGAGING AUXILIARY BRUSH, CONNECTING PLUG travels $1 / 4$ INCH before engaging the main brush on the terminal block


$$
\begin{aligned}
& \text { OEVICE FUNCTION NUMBERS } \\
& 52 \text { - POWER CIRCUIT BREAKER } \\
& 59 \text { - A-C OVERVOLTAGE RELAY, TYPE IAVSIA } \\
& \text { a - AUXILIARY CONTACT CLOSED WHEN BREAKER CLOSES } \\
& \text { S! - SEAL-IN UN IT WITH TARGET } \\
& \text { TC - TRIP COIL }
\end{aligned}
$$

* Fig. 10 (K-6375692-1) CONnection diagram for the type iav5ia relay used for overvoltage protection


$$
58 \text { - UNDER AND OVERVOLTAGE RELAY. }
$$


*Fig. 12 (8918488A) Time-VOLTAGE CuRve types iav5ia and IAV52A relays ( $\pm 15 \%$ TOLERANCE)





*Fig. 15 (8007378) fRONT VIEW OF TYPE IAV5TA RELAY WITHDRAWN FROM CASE

*Fig. 16 (8007379) BACK VIEW OF TYpe iavsia relay withorawn from case


$$
\begin{aligned}
& \text { DEVICE FUNCTION NUMBERS } \\
& 59 \text { - OVERVOLTAGE RELAY TYPE IAV } \\
& \text { SI - SEAL-IN UN:T WITH TARCET }
\end{aligned}
$$

*Fig. 17 (K-6154391-2) TEST CONNECTIONS FOR OVERVOLTAGE RELAYS


```
DEVICE FUNCTION NUMBERS
58 - unOER and overvoltage relay, type lav53
SI - SEAL-IN UNIT WITH TARGET.
```

*Fig. 18 ( $\mathrm{K}-6375693-1$ ) test connections for unoervoltage contacts of over-and undervoltage relays

-fig. 19 (K-6209270-2) OUTLINE AND PANEL dRILLING FOR RELAY types iAv51A, Iav52A, IAv53C

PANEL LOCATION

*Fig. 20 (K-6209271-5) outline and panel drilling for relay types lav53A, iav53b and iav53d


PANEL DRILLING FOR SURFACE MOUNTING (FRONT VIEW)
*Fig. 21 (K-6209272-4) CUTLINE AND PANEL DRILLING DIMENSIONS FOR RELAY TYPES LAV53K, IAV53L AND IAV53M RELAYS

## GENERAL (3) ELECTRIC



## TYPE IAV VOLTAGE RELAYS



Fig. I. Typical IAV relay

## ORDERING INSTRUCTIONS

1. Always specify the complete nameplate data of the relay.
2. Specify the quantity, catalog number (if listed), reference number (if listed), description, and this bulletin number.
3. Standard hardware, such as screws, bolts, nuts, washers, etc., is not listed in this bulletin. Such items should be purchased locally.
4. For prices, refer to the nearest office of the General Electric Company.

Relay models covered by this bulletin are listed in the left hand column of the tabulation beginning on page 3.

To find the catalog number of a renewal part:
(1) From illustrations on pages 1 and 2, find reference letter for required part.
(2) Locate reference letter and/or description of part in column headings at top of tabulation.
(3) Note numeral at intersection of reference letter column and model number line. This numeral, when added to reference letter, provides key to catalog number of part, which is listed in table on page indicated.

## Example:

To find catalog number of stationary main contact for Model 12LAV51A7A relay:
(1) Figure 2 on page 2 indicates that reference letter for stationary main contact is " G ".
(2) Locate reference letter " G " in column headings on page 3.
(3) At intersection of " $G$ " column and Model 12IAV51A7A line find numeral " 1 ". Complete reference symbol is therefore "G-1". Referring to page 9, catalog number is found to be 6209430G1 (one require per relay).


Fig. 2. Typical IAV relay, front view


Fig. 3. Typical IAV relay unit, back view NOTE: Resistor locations vary.


[^1]| Relay <br> Model Number |  |  |  | אlquessv matos lomə卬 |  |  |  | Drag Magnet |  |  |  |  |  |  |  | sədd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Page | 8 | 8 | 8 | 8 | 8 | 8 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9，10 | 10 | 10 | 10 | 10 |
| Ref． | $\mathrm{A}^{*} \delta$ | B | C | D | E＊F | F＊ | $\mathrm{G}^{*}$ | H | I＊ | J＊ | O＊＇ | S＊ | T＊${ }^{\text {F }}$ | U† | V | W† | X $\dagger$ | Y |
| 12LAV52B1A | 17 | 1 | 1 | 1 | － | 5 | 6 | 7 | 4 | － | 2 | － | 3 | － | 1 | － | 2 | 1 |
| 12IAV52C1A | 52 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 4 | 1 | － | 9 | 1 |
| 652 C 2 A | 53 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 2 | 1 | － | 9 | 1 |
| ¢52C3A | 54 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 4 | 1 | － | 9 | 1 |
| ¢52C4A | 63 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 8 | 1 | － | 9 | 1 |
| ¢52C5A | 66 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 7 | 1 | － | 9 | 1 |
| ¢52C6A | 67 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 8 | 1 | － | 9 | 1 |
| ¢52C7A | 70 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | － | － | 2 | 1 | － | 9 | 1 |
| 12IAV52DIA | 52 | 1 | 1 | 1 | － | 4 | 4 | 4 | 2 | － | － | 5 | － | 4 | 1 | － | 9 | 1 |
| 12IAV53A1A | 1 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A2A | 2 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A3A | 26 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A4A | 14 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A5A | 15 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | ． | 1 | 1 |
| 53A6A | 13 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A7A | 23 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | ＿ | 1 | 1 |
| 53A8A | 28 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A9A | 34 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| 53A10A | 39 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | 1 | － | 1 | 1 |
| $12 \mathrm{LAV53B1A}$ | 1 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53B2A | 2 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | － | － | － | ＿ | － | － | 1 | － | 1 | 1 |
| $53 \mathrm{B4A}$ | 14 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53B5A | 15 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53B6A | 13 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| ¢12IAV53B1R | 1 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | $\ddagger 3$ | － | $\ddagger 12$ | $\pm 3$ |
| $\phi 53 \mathrm{~B} 2 \mathrm{R}$ | 2 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | $\ddagger$ | － | $\ddagger 12$ | $\pm 3$ |
| ¢53B4R | 14 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | $\ddagger 3$ | － | $\ddagger 12$ | $\ddagger 3$ |
| ¢53B5R | 15 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | $\ddagger 3$ | － | $\ddagger 12$ | $\ddagger 3$ |
| $\phi 53 \mathrm{B6R}$ | 13 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | $\ddagger 3$ | － | $\ddagger 12$ | $\ddagger$ |
| 12IAV53C1A | 57 | 3 | 1 | 1 | 1 | 1 | 5 | 5 | 1 | － | － | － | － | － | 1 | － | 8 | 1 |
| 53 C 2 A | 58 | 3 | 1 | 1 | 1 | 1 | 5 | 5 | 1 | － | － | － | － | － | 1 | － | 8 | 1 |
| 53C3A | 59 | 3 | 1 | 1 | 1 | 1 | 5 | 5 | 1 | － | $\sim$ | － | － | － | 1 | － | 8 | 1 |
| 53 C 4 A | 60 | 3 | 1 | 1 | 1 | 1 | 5 | 5 | 1 | － | － | － | － | － | 1 | － | 8 | 1 |
| 53 C 5 A | 58 | 3 | 1 | 1 | 1 | 1 | 5 | 5 | 1 | － | ＿ | － | － | － | 1 | － | 8 | 1 |
| 53C6A | 61 | 3 | 1 | 1 | 1 | 1 | 5 | 5 | 1 | － | － | － | － | － | 1 | － | 8 | 1 |
| 12LAV53D1A | 1 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53D2A | 42 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53D3A | 13 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53D4A | 2 | 3 | 1 | 1 | 1 | 1 | 5 | 4 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 12LAV53E1A | 69 | 3 | 1 | 1 | 2 | 2 | 5 | 4 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 53 E 2 A | 59 | 3 | 1 | 1 | 2 | 2 | 5 | 4 | － | － | － | － | － | － | 1 | － | 1 | 1 |
| 12IAV53K1A | 1 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | － | 4 | 7 | 2 |
| 53K2A | 2 | 3 | 1 | 1 | 1 | 1 | 5 | 7 | 5 | 1 | － | － | － | － | － | 4 | 7 | 2 |

＊Recommended for stock for normal maintenance
$\dagger$ Not shown
万 Assembly of laminations，pole pieces，coil and tap block
$\ddagger$ Basic model number covers drawout case．semi－flush mounting．For drawout case surface mounting， affix＇S＇in place of＇$R$＇
obsolete models－if parts are needed，give quantity，catalog number，description and complete nameplate reading when ordering


[^2]

* Recommended for stock for normal mainterance
$\dagger$ Not shown
$\delta$ Assembly of laminations, pole preces. coil and tap block
$\ddagger$ Basic model number covers drawout case, semi-flush mounting. For drawout case surface mounting affix 'S' in place of ' R '
© Obsolete models - if parts are needed, give quantity, catalog number, description and complete nameplate reading when ordering

| Relay Model Number | K1quassv поつ gutiexacio |  |  | кtquassy maxos jamar | Moving Contact and Spring Assembly, Upper |  |  |  |  |  |  | Resistor（Adjustable） | Resistor（Fixed） |  |  |  | Terminal Block Assembly，Lower |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Page | 8 | 8 | 8 | 8 | 8 | 8 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9，10 | 10 | 10 | 10 | 10 |
| Ref． | A＊${ }^{\text {\％}}$ | B | C | D | E＊${ }^{\text {F }}$ | $\mathrm{F}^{*}$ | $\mathrm{G}^{*}$ | H | $\mathrm{I}^{\text {＊}}$ | J＊ | $\mathrm{O}^{+1}$ | $\mathbf{S}^{*}$ | T＊ 1 | UT | V | W ${ }^{+}$ | X1 | Y |
| $\begin{array}{r} \text { 12IAV69A1A } \\ 69 A 2 A \end{array}$ | $\begin{aligned} & 90 \\ & 91 \end{aligned}$ | 4 4 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 1 | － | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 7 \\ & 7 \end{aligned}$ | 5 | 6 6 | 2 2 | － | － | －－ | － |  | $\begin{aligned} & \hline 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & \mathbf{n 1} \\ & \hline 5 \end{aligned}$ | 2 |
| $\begin{array}{r} \text { 12LAV69B1A } \\ \text { 69B2A } \\ 69 \mathrm{B3A} \end{array}$ | $\begin{aligned} & 90 \\ & 91 \\ & 95 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \end{aligned}$ | 1 1 1 | － | $\begin{aligned} & 4 \\ & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 7 \\ & 7 \\ & 7 \end{aligned}$ | 5 5 5 | － | － | － | － | － | － | － | $\begin{array}{r} 4 \\ 4 \\ 4 \end{array}$ | $\begin{aligned} & 5 \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \\ & 2 \end{aligned}$ |
| $\begin{array}{r} \text { 12IAV70A1A } \\ \text { 70A2A } \end{array}$ | $\begin{aligned} & 92 \\ & 93 \end{aligned}$ | $1$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 1 | － | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 7 \\ & 7 \end{aligned}$ | 6 | 6 | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | － | － | － | － | － | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ |
| $\begin{array}{r} \text { 12IAV70B1A } \\ 70 \mathrm{~B} 2 \mathrm{~A} \end{array}$ | $\begin{aligned} & 92 \\ & 93 \end{aligned}$ | 1 | 1 | 1 | － | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 7 \\ & 7 \end{aligned}$ | 6 | － | － | － | － | － | － | － | 4 4 | $\begin{aligned} & 5 \\ & 5 \end{aligned}$ | 2 2 |
| $\begin{array}{r} \text { 12IAV71A1A } \\ \text { 71A3A } \end{array}$ | $\begin{aligned} & 45 \\ & 45 \end{aligned}$ | 1 | 1 | 1 | － | $\begin{aligned} & \mathbf{3} \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 4 4 | 1 | － | － | 2 | － | 3 22 | 1 | － | $\begin{aligned} & 8 \\ & 8 \end{aligned}$ | 1 |
| $\begin{array}{r} \text { 12IAV71B2A } \\ 71 \mathrm{~B} 3 \mathrm{~A} \\ 71 \mathrm{~B} 4 \mathrm{~A} \\ 71 \mathrm{~B} 5 \mathrm{~A} \\ 71 \mathrm{~B} 6 \mathrm{~A} \end{array}$ | $\begin{aligned} & 45 \\ & 45 \\ & 88 \\ & 85 \\ & 85 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | － | 3 3 3 3 -3 | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \\ & 4 \\ & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & \mathbf{3} \\ & \mathbf{3} \\ & \mathbf{3} \\ & \mathbf{3} \\ & \mathbf{3} \end{aligned}$ | － | $\begin{aligned} & 7 \\ & 7 \\ & 7 \\ & 7 \\ & 7 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | $\begin{array}{r} 9 \\ 9 \\ 9 \\ 9 \\ 10 \end{array}$ | $\begin{array}{r} 3 \\ 22 \\ \hline 3 \\ 3 \end{array}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | － | $\begin{aligned} & 14 \\ & 14 \\ & 14 \\ & 14 \\ & 14 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ |
| 12IAVT2A1A： | 45 | 1 | 1 | 1 | － | 5 | 6 | 4 | 2 | － | － | 2 | － | 3 | 1 | － | 9 | 1 |
| $\begin{array}{r} \text { 12IAV72B1A } \\ 72 \mathrm{~B} 3 \mathrm{~A} \end{array}$ | $\begin{aligned} & 45 \\ & 85 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | － | $\begin{aligned} & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & 6 \\ & 6 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | － | $\begin{aligned} & 7 \\ & 7 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | $\begin{aligned} & 9 \\ & 9 \end{aligned}$ | $\begin{array}{r} 3 \\ 22 \end{array}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | － | 4 | 1 |
| 12IAV73A1A 73A2A | $\begin{aligned} & 44 \\ & 48 \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & \mathbf{5} \\ & \mathbf{5} \end{aligned}$ | 7 | $\begin{aligned} & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | － | 2 | － | 3 | － | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | 7 | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ |
| 12IAV73B1A | 44 | 3 | 1 | 1 | 1 | 5 | 5 | 7 | － | － | － | 2 | － | 3 | － | 4 | 7 | 2 |
| 12IAV74A1A | 46 | 2 | 1 | 1 | － | 6 | 3 | 4 | 1 | － | － | 2 | － | 5 | － | 3 | 5 | 2 |

＊Recommended for stock for normal maintenance
$\dagger$ Not shown
$\delta$ Assembly of laminations，pole pieces，coil and tap block

GEF-3897, TYPE LAV RELAYS

| Ref. Symbol | Fig. <br> No. | Catalog Number | No. Per Relay | Ref. Symbol | Fig. <br> No. | Catalog Number | No. Per Relay |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OPERATING COIL ASSEMBLY |  |  |  | OPERATING COIL ASSEMBLY (Cont'd) |  |  |  |
| A-1 | 3 | 721-6293205G7 | 1 | A-56 | 3 | 721-6293206G40 | 1 |
| A-2 | 3 | G8 | 1 | A-57 | 3 | G57 | 1 |
| A-3 | 3 | G14 | 1 | A-58 | 3 | G58 | 1 |
| A-4 | 3 | G27 | 1 | A-59 | 3 | G59 | 1 |
| A-5 | 3 | G28 | 1 | A-60 | 3 | G60 | 1 |
| A-6 | 3 | G29 | 1 | A-61 | 3 | G61 | 1 |
| A-7 | 3 | G30 | 1 | A-62 | 3 | G68 | 1 |
| A-8 | 3 | G31 | 1 | A-63 | 3 | G69 | 1 |
| A-9 | 3 | G35 | 1 | A-64 | 3 | G70 | 1 |
| A-10 | 3 | G37 | 1 | A -65 | 3 | G73 | 1 |
| A-11 | 3 | G41 | 1 | A-66 | 3 | G79 | 1 |
| A-12 | 3 | G42 | 1 | A-67 | 3 | G80 | 1 |
| A-13 | 3 | G43 | 1 | A-68 | 3 | G89 | 1 |
| A-14 | 3 | G49 | 1 | A-69 | 3 | G90 | 1 |
| A-15 | 3 | G50 | 1 | A-70 | 3 | G91 | 1 |
| A-16 | 3 | G54 | 1 | A-71 | 3 | G97 | 1 |
| A-17 | 3 | G57 | 1 | A-72 | 3 | G101 | 1 |
| A-18 | 3 | G58 | 1 | A-73 | 3 | G108 | 1 |
| A-19 | 3 | G62 | 1 | A-74 | 3 | G109 | 1 |
| A-20 | 3 | G63 | 1 | A-75 | 3 | G122 | 1 |
| A-21 | 3 | G64 | 1 | A-76 | 3 | G123 | 1 |
| A-22 | 3 | G79 | 1 | A-77 | 3 | G133 | 1 |
| A-23 | 3 | G86 | 1 | A-78 | 3 | G140 | 1 |
| A-24 | 3 | G90 | 1 | A-79 | 3 | G148 | 1 |
| A-25 | 3 | G111 | 1 |  |  |  |  |
| A-26 | 3 | G112 | 1 | DISK AND SHAFT ASSEMBLY |  |  |  |
| A-27 | 3 | G113 | 1 |  |  |  |  |
| A-28 | 3 | G117 | 1 |  |  |  |  |
| A -29 | 3 | G119 | 1 | B-1 | 3 | 721-6293210G1 | 1 |
| A-30 | 3 | G120 | 1 | B-2 | 3 | G3 | 1 |
| A-31 | 3 | G121 | 1 | B-3 | 3 | G4 | 1 |
| A-32 | 3 | G123 | 1 | B-4 | 3 | G2 | 1 |
| A-33 | 3 | G125 | 1 | B-5 | 3 | G6 | 1 |
| A-34 | 3 | G127 | 1 |  |  |  |  |
| A-35 | 3 | G132 | 1 |  |  |  |  |
| A-36 | 3 | G135 | 1 | TOP BEARING |  |  |  |
| A-37 | 3 | G144 | 1 |  |  |  |  |
| A-38 | 3 | G147 | 1 |  |  |  |  |
| A-39 | 3 | G148 | 1 | C-1 | 2 | 721-6209409G1 | 1 |
| A -40 | 3 | G149 | 1 |  |  |  |  |
| A-41 | 3 | G151 | 1 |  |  |  |  |
| A - 42 | 3 | G155 | 1 | JEWEL SCREW ASSEMBLY |  |  |  |
| A-43 | 3 | G158 | 1 |  |  |  |  |
| A -44 | 3 | G164 | 1 |  |  |  |  |
| A-45 | 3 | G169 | 1 | D-i | 3 | 721-6209457G1 | 1 |
| A-46 | 3 | G 171 | 1 |  |  |  |  |
| A-47 | 3 | G176 | 1 |  |  |  |  |
| A-48 | 3 | G180 | 1 | MOVING CONTACT AND SPRING ASSEMBLY (UPPER) |  |  |  |
| A-49 | 3 | G183 | 1 |  |  |  |  |
| A-50 | 3 | G191 | 1 |  |  |  |  |
| A-85 | 3 | G203 | 1 |  |  |  |  |
| A-86 | 3 | G204 | 1 | E-1 | $\dagger$ |  | 1 |
| A-88 | 3 | G211 | 1 | E-2 | $\dagger$ | G10 | 1 |
| A-89 | 3 | G216 | 1 |  |  |  |  |
| A-90 | 3 | G217 | 1 | MOVING CONTACT AND SPRING ASSEMBLY (LOWER) |  |  |  |
| A-91 | 3 | G218 | 1 |  |  |  |  |
| A -92 | 3 | G219 | 1 |  |  |  |  |
| A-93 | 3 | G220 | 1 |  |  |  |  |
| A-94 | 3 | G225 | 1 | F-1 | 2 | 721-6158531G1 | 1 |
| A -95 | 3 | G226 | 1 | F-2 | 2 | G2 | 1 |
| A -99 | 3 | G227 | 1 | F-3 | 2 | G3 | 1 |
| A-96 | 3 | G228 | 1 | F-4 | 2 | G5 | 1 |
| A-97 | 3 | G231 | 1 | F-5 | 2 | G6 | 1 |
| A.98 | 3 | G232 | 1 | F-6 | 2 | G12 | 1 |
| A-51 | 3 | 721-6293200G5 | 1 | F-7 | 2 | G13 | 1 |
| A-52 | 3 | C28 | 1 | F-B | 2 | G14 | 1 |
| A-53 | 3 | G29 | 1 | F-9 | 2 | G15 | 1 |
| A-54 | 3 | G32 | 1 | F-10 | 2 | G16 | 1 |
| A-55 | 3 | G39 | 1 | F-11 | 2 | G17 | 1 |

[^3]TYPE LAV RELAYS, GEF-3897

| Ref. Symbol | Fig. <br> No. | Catalog Number | No. Per Relay | Ref. Symbol | Fig. No. | Catalog Number | No. Per Relay |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MADN STATIONARY CONTACT |  |  |  | CAPACITOR |  |  |  |
| G-1 | 2 | 721-6209430G1 | 1 | U-1 | $\dagger$ | 721-21F802 | 1 |
| G-2 | 2 | G2 | 1 | U-2 | $\dagger$ | 21 F803 | 1 |
| G-3 | 2 | G3 | 1 | U-3 | $\dagger$ | 21 F804 | 1 |
| G-4 | 2 | G2 | 2 | U-22 | $\dagger$ | $21 F 805$ | 1 |
| G-5 | 2 | G3 | 2 | U-4 | $\dagger$ | 21 F807 | 1 |
| G-6 | 2 | G4 | 2 | U-5 | $\dagger$ | 21 F808 | 1 |
| G-7 | 2 | G4 | 1 | U-6 | $\dagger$ | 21 F809 | 1 |
|  |  |  |  | U-7 | $\dagger$ | 21 F811 | 1 |
| 8 DRAG MAGNET |  |  |  | U-8 | $\dagger$ | 21 F813 | 1 |
|  |  |  |  | U-9 | $\dagger$ | 21 F815 | 1 |
| E-4 | 2 | 721-237C749G1 | 1 | U-11 | $\dagger$ | $21 F 902$ | 1 |
| H-5 | 2 | G2 | 1 | U-12 | $\dagger$ | 21 F903 | 1 |
| H-6 | 2 | G3 | 1 | $\mathrm{U}-13$ | $\dagger$ | 21 F906 | 1 |
| H-7 | 2 | G4 | 1 | U-14 | $\dagger$ | 21 F914 | 1 |
| SEAL-IN UNIT (LEFT) |  |  |  |  |  |  |  |
| I-1 | 2 | 721-6293203G1 | 1 | END PLATE |  |  |  |
| I-2 | 2 | G2 | 1 |  |  |  |  |
| [-3 | 2 | G3 | 1 | $\begin{aligned} & V-1 \\ & V-2 \\ & V-3 \end{aligned}$ | 1 | 721-237C740G1 <br> 721-6128447P1 <br> P1 | 121 |
| I-4 | 2 | G4 | 1 |  |  |  |  |
| [-5 | 2 | G11 | 1 |  |  |  |  |
| I-6 | 2 | G203 | 1 |  |  |  |  |
| SEAL-EN UNIT (RIGHT) |  |  |  |  |  |  |  |
| $J-1$ | 2 | $721-6293203 G 5$ | $1$ | TERMINAL BLOCK ASSEMBLY (UPPER) |  |  |  |
| $\mathrm{J}-2$ | 2 | G202 | $1$ |  |  |  |  |  |  |  |
| INSTANTANEOUS UNIT |  |  |  | $\begin{aligned} & W-1 \\ & W-2 \\ & W-3 \\ & W-4 \end{aligned}$ | $\begin{aligned} & \dagger \\ & \dagger \\ & \dagger \\ & \dagger \end{aligned}$ | 721-6418058G42G127G236G292 | 1111 |
| O-1 |  | 721-6293204G24 |  |  |  |  |  |
| O-2 | $\dagger$ | G29 | 1 |  |  |  |  |
| O-3 | $\dagger$ | G37 | 1 |  |  |  |  |
| O-4 | $\dagger$ | G43 | 1 |  |  |  |  |
| O-5 | $\dagger$ | G62 | 1 | TERMINAL BLOCK ASSEMBLY (LOWER) |  |  |  |
| $0-6$ | $\dagger$ | G81 | 1 |  |  |  |  |  |  |  |
| O-7 | $\dagger$ | 721-6293203G120 | 1 |  |  |  |  |  |  |  |
| RESISTOR (ADJUSTABLE) |  |  |  | $\begin{aligned} & X-1 \\ & X-2 \end{aligned}$ | $\dagger$ | 721-6418058G23 <br> G24 | 1 |
| S-1 | $\dagger$ | 721-403A321P2 | 1 |  |  |  | 1 |
| S-2 | $t$ | P3 | 1 | $X-3$ | $t$ | G67 | 1 |
| S-3 | $\dagger$ | P4 | 1 | X-4 | $\dagger$ | G89 | 1 |
| S4 | $\dagger$ | P13 | 1 | $\begin{aligned} & X-5 \\ & X-6 \end{aligned}$ |  | G126 | 1 |
| S-5 | $\dagger$ | P15 | 1 |  | $t$ | G178 | 1 |
| S-6 | $\dagger$ | P20 | 1 | $\begin{aligned} & X-6 \\ & X-7 \end{aligned}$ | $\dagger$ | G292 | 1 |
| S-7 | $\dagger$ | P21 | 1 | $\begin{aligned} & X-7 \\ & X-14 \end{aligned}$ | $\dagger$ | G65 | 1 |
| S-8 | $\dagger$ | P23 | 1 | X-8 | $t$ | 721-6418060G3 | 1 |
| S-9 | $\dagger$ | P30 | 1 | $X-9$$X-10$ | $\dagger$ | G4 | 1 |
| S-10 | $\dagger$ | P42 | 1 |  | $\dagger$ | G5 | 1 |
|  |  |  |  | $\begin{aligned} & X-10 \\ & X-11 \end{aligned}$ |  | G23 | 1 |
| RESISTOR (FDXED) |  |  |  | $\begin{aligned} & X-12 \\ & X-13 \end{aligned}$ | $\dagger$ | 721-6193049G23 | 1 |
| T-1 | $\dagger$ | 721-59012 18G1-3750 | 1 | X-13 |  | G67 | 1 |
| T-2 | $\dagger$ | 721-403A322P19 | 1 | CONNECTING PLUG |  |  |  |
| T-3 | $\dagger$ | P23 | 1 |  |  |  |  |  |  |  |
| T-4 | $\dagger$ | P26 | 2 |  |  |  |  |  |  |  |
| T-5 | $\dagger$ | P79 | 1 |  |  |  |  |
| T-9 | $\dagger$ | P116 | 1 | Y-1 | 1 | 721-6118736G5 | 1 |
| T-6 | $\dagger$ | P140 | 1 | Y-2 |  | G5 | 2 |
| T-10 | $t$ | P183 | 1 | Y -3 | 1 | G1 | 1 |
| T-7 | $\dagger$ | 721-403A32313 | 1 | Y -4 |  | G1 | 2 |

t Not shown
3 Specify complete relay model number when ordering drag magnet

CONTAC＇I BLOCK ASSEMBLY

| Relay Model Type | Lower Contact Block Catalog No． | Upper Contact llinck Catalog No． | Relay Model Type | Lower Contact Block Catalog No． | Upper Contact Block Catalog No． |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12IAV51A | 721－6193048G9 | － | 12LAV54E | 721－6193048G118 | 721－6193048G228 |
| 51 C | 6193048G9 | － | ｜ 54 F | 6193048G118 | ｜6193048G228 |
| 51D | 6193048G9 | － | 54H | 6193048G118 | 6193048G228 |
| 51H | 6193048G9 | － | 54．J | 6193048G118 | 6193048G228 |
| 51 J | 6193048G9 | － | 55C | 6193048G118 | 6193048G119 |
| 51 K | 6193048G95 | － | 56B | － |  |
| 51 M | 6193048G9 | － | 57A | 6193048G9 | － |
| 52A | 6193048 G 22 | － | 58B | 6193048G3 | － |
| 52 B | 5193048G258 | － | 60B | 6193048G92 |  |
| 52 C | 6193048G22 | － | 69A | 6193048G118 | 6193048G2 79 |
| 52D | 6193048 G 22 | － | 69B | 6193048G118 | 6193048G279 |
| 53A | 6193048 G 12 | － | 70A | 6193048G118 | 6193048G2 79 |
| 53 B | 6193048 G 12 | － | 70B | 6193048G118 | 6193048G2 79 |
| 53C | 6193048G9 | － | 71A | 6193048G9 |  |
| 53D | 6193048G12 | － | 71B | 6193048 G 103 |  |
| 53E | 6193048G12 | －${ }^{-}$ | 72A | 6193048 G 22 | － |
| 53 K | 6193048G279 | 721－6193048C： | 72B | 6193048G92 | － |
| 53 L | 6193048 G 279 | ｜6193048Ci：${ }^{\text {a }}$ | 73A | 6193048G279 | 6193048G2 79 |
| 53 M | 6193048 G 118 | 6193048Gこ：的 | 73B | 6193048G279 | 6193048G279 |
| － 53 N | $\downarrow \begin{aligned} & \text { 6193048G279 } \\ & \\ & 6193048 \mathrm{G9}\end{aligned}$ | －6193048C以 ${ }_{\text {－}}$ | －74A | $\downarrow$ 6193048G118 | －6193048G228 |

EXTEIINAL NUXILIARIES

| Relay | Catalog Rosistı． |  | Capacitor |  |
| :---: | :---: | :---: | :---: | :---: |
| Model No． | Catalog No． | Nu ．Req． | Catalog No． | No．Req． |
| 12IAV51K1A | －－－ | － | 721－28F914 | 1 |
| 12IAV51K2A | －－－ | － | 128F914 | 1 |
| $12 \mathrm{IAV} 56 \mathrm{B4HN}$ | 721 －365A436P805 | 1 | $21 F 918$ | 1 |
| 12LAV56B5HN | 365A436P804 | 1 | 21 F918 | 1 |
| 12LAV56B6HN | 365A436P804 | 1 | 21 F918 | 1 |
| 12IAV56B7HN | 365A436P803 | 1 | 21 F 918 | 1 |
| 12IAV56B8HN | 365A436P805 | 1 | $21 F 918$ | 1 |
| $12 \mathrm{IAV} 56 \mathrm{B9} \mathrm{HN}$ | 365A436P805 | 1 | $21 \mathrm{F9} 18$ | 1 |
| 12IAV56B10HN | －－－ | － | 21 F 905 | 1 |
| 12 LAV 56 B 11 HN | 365A436P864 | 1 | 21 F900 | 1 |
| 12IAV56B12HN | 365A436P803 | 1 | $21 F 918$ | 1 |
| 12IAV56B13HN | 365A436P870 | 1 | $21 F 918$ | 1 |
| 12 IAV 56 B 14 HN | 365A436P805 | 1 | 21 F918 | 1 |
| 12IAV58B1R | －－－－ | － | 26F330 | 1 |
| 12IAV58B2R | － | － | 23 F10 | 1 |
| 12LAV58B3R | －－－－ | － | 23 F 2 | 1 |
| 12IAV58B4R | －－－ | － | 26 F330 | 1 |
| 12IAV58B5R | 3887726 | 1 | 26 F330 | 1 |
| 12IAV60B1A | －－ | － | 28 F902 | 1 |
| 12IAV60B2A | －－－ | － | 28 F 903 | 1 |
| 12LAV60R3A | －－－－ | － | $28 \mathrm{F9} 96$ | 1 |
| 12LAV60B4A | －IC9006C102B | 1 | － 28 F902 | 1 |

## GENERAL (6) ELECTRIC



The SBM is a compect, positive acting switch for control and transfer service on paneis and switchboards, 600 voits and under. Up to 10 stages. 2 contacts per stage can be provided, with independent action, both electrically and mechanically, through eight positions.

## Ideal For Switchboards-

-The SBM switch is especially adaptable for switchboard applications where space is at a premium. When a control swich is required for use in an explo-sion-proof or watertight enclosure, space is normally not a controlling factor, and the SB-1 switch, which is somewhat larger, is used.
The SBM switch is normally supplied for mounting on panels up to $1 / 4$ inch thick. If requested, it can also be supriigd for mounting on panels of one and and a half inches.
compact design of the SBM switch permits close center-to-center line
mounting distances and, at the same time, easy access to the terminals for wiring. Also, since the switch is enclosed, there is no need for clearance at the back of the panel to remove a separate cover. This further reduces space requirements.

## Ratings

The SBM switch is rated for a mechanical life of 500,000 operations. The
electrical ratings are 600 volts ac or dc, 20 amps continuous or 250 amps for three seconds. The interrupting rating depends upon the voltage and character of the circuit. The table below illustrates the interrupting duty of a single contact and contacts in series when various conditions exist on a circuit.

SBM is recognized under the component program of Underwriters' Laboratories, Inc.

Interrupting Rating (amperes)

| Clrcuit Volts | Non-inductive |  | Inductive |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Number of Contacts |  |  |  |
|  | 1 | 2 in series | 1 | 2 in series |
| 24 dc | 10 | 30 | 8 | 25 |
| 48 dc | 8 | 25 | 6 | 18 |
| 125 dc | 5 | 15 | 4 | 10 |
| 250 dc | 1 | 3 | 1 | 2.5 |
| 600 dc | 0.4 | 0.8 | 0.3 | 0.7 |
| 115 ac | 40 | 75 | 24 | 50 |
| 230 ac | 25 | 50 | 12 | 25 |
| 460 ac | 20 | 30 | 10 | 20 |
| 600 ac | 15 | 25 | 8 | 12 |

## Construction Features



STANDARD


TARGET conotes


KEYED

## Escutcheons

Two basic types of escutcheons are available: the standard and the target. The standard type shown on the left is a molded black phenolic material with white lettering for clear reading of the positions. A target type escutcheon, shown in the middle, is normally furnished on breaker control switches. An aluminum front plate houses the target mechanism with a window in the center to show green for the trip position, red for the closed position, and black for the pull-to-lock position. The target has a slip action so that it will remain green when the handle retums
to NORMAL from the TRIP position, and red when it returns from the CLOSE position. This shows the operator the last operation of the switch.
On the right a modified standard is shown with keyways for use with a removable type handle.

Aluminum circuit designation plates are available for all three types.
The standard and keyed escutcheons can be fumished in painted colors of red, green, yellow, blue, gray, orange, brown, and white, but must be specified on each order.




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## Handles

Four types of molded black phenolic handles shaped for easy gripping are available with the SBM switch: pistol grip, oval, knurled, and lever. Any of the standard handles except the lever, may be adapted for removable handle keying. A fixed handle may be easily removed for replacement by a screw in the front of the handle. A white pointer, fumished with the handles
(except the lever) and mounted near the escutcheon, give a clear identification of the position that the handle is in. For mateh and line up with SB-1 switches, type SB-1 pistol grip, oval, knurled, and round handies can be furnished for use with SBM switches. The same colors are available for the handles as were listed for the escutcheons.

## Cams and Contacts

The silver to silver contacts of the SBM switch are of double-break design, as seen at left, which reduces arcing and subsequent pitting of contacts. Each contact is operated by a double surface cam, one surface for closing, the other surface for opening. This construction provides opening and closing action not dependent on springs.



## Terminal Connections

Terminal connections are brought to the corners of each stage, allowing screw connections to be made over a large angle. This angular displacement of connection points allows the switches to be mounied on three-inch centers or less.

## Jumpers

Jumpers are furnished assembled, where required, on all standard listed switches. For special switches or unlisted switches, separate jumpers can be ordered


| Contacts Handle End. | Positions |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 3 | 2 | 1 |
|  | 1 |  |  | $X$ |
| $0-11-00$ | 2 |  | X |  |
| 0 | 3 | X | X |  |

## Break-Before-Make Contacts

Contacts on SBM switches are normally non-overlapping (break-before-make). This sequence is illustrated above. which shows that contact No. 1 opens before contact No. 2 closes.

Another normal function is illustrated by contact No. 3, which is shown closed in two adjacent positions. When switching between these positions, this contact will always remain closed.


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## Spring Action

Torsion springs return the switch handle to or lowards the 12 o'clock or No. 3 position. The travel of the handle is limited to $90^{\circ}$ to either side of this position. The switches may be furnished with spring return both ways, or only one way, with maintaining action in the opposite direction. You can also have spring return from position No. 1 ( 9 o'clock) to position No. 2 (10 o'clock) and/or spring return from position No. 5 ( 3 o'clock) to position No. 4 (2 o'clock) with maintained action in the other positions. Torsion springs are housed in the rear half of the positioning chamber. There is no need to modify the chamber to accommodate the springs.



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## Pull-To-Lock

A pull-to-lock mechanism is designed for spring-return switches. When the handie is turned to the 9 o'clock position, it can be pulled out and locked in that position. When the handle is pushed in, the handle spring returns to the normal position. This pull-to-lock feature does not actuate contacts, but merely prevents the spring return of the handle.


INCORRECT

| CONTACTS HANDLE END |  | POSITIONS (BACK VIEW) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| OH1O OH10 | 1 |  |  |  |  |  |  |  | X |
|  | 2 |  |  |  |  |  |  | X |  |
| $3^{3}+10004$ | 3 |  |  |  |  |  | $X$ |  |  |
|  | 4 |  |  |  |  | X |  |  |  |
| $5$ | 5 |  |  |  | X |  |  |  |  |
|  | 6 |  |  | X |  |  |  |  |  |
| $\begin{aligned} & 7 \\ & 0 \end{aligned}$ | 7 |  | X |  |  |  |  |  |  |
|  | 8 | X |  |  |  |  |  |  |  |

CORRECT

| CONTACTS HANDLE END |  | POSITIONS (BACK VIEW) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| 1.HTO OHto | 1 |  |  |  |  |  |  |  | X |
|  | 2 |  |  |  | X |  |  |  |  |
| $\begin{aligned} & 3 \\ & \text { OHO OHO } \\ & \text { OHO } \end{aligned}$ | 3 |  |  |  |  |  |  | $\times$ |  |
|  | 4 |  |  | X |  |  |  |  |  |
| $\stackrel{5}{5}_{0}+\mathrm{H}^{\circ} \mathrm{OH}$ | 5 |  |  |  |  |  | X |  |  |
|  | 6 |  | X |  |  |  |  |  |  |
| ${ }^{7} \text { OHO OHt }{ }^{8}$ | 7 |  |  |  |  | X |  |  |  |
|  | 8 | X |  |  |  |  |  |  |  |



ESCUTCHEON (FRONT VIEW)

Fig. 5. Diagram of unworkable and correct arrangement


ESCUTCHEON (FRONT VIEW)

| CONTACTS HANDLE END |  | POSITIONS PBACK VIEW |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| O-H-O-1 | 1 |  |  |  |  | X | X |  | X |
|  |  |  |  |  |  |  |  |  |  |
| HO-H1O |  |  |  |  |  |  |  |  |  |
|  | 4 | X | X |  |  |  |  |  |  |
| OHHOH | 5 | X |  |  | X |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Hodro |  |  |  |  |  |  |  |  |  |
|  | 8 |  |  |  |  | X | X |  | X |

Fig. 6. Contact arrangement to meet cam limitations


Fig. 7. Diagram showing 45-degree slip action of cam

| CONTACTS <br> HANDLE END |  | POSITIONS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Close | Norm of fer close | Norm ofter trip | Trip |
| $\text { OHO } \mathrm{HH}^{2}$ | 1 | $\times$ |  |  |  |
|  | 2 |  |  |  | $x$ |
|  | 3 | X |  |  | X |
|  | 4 | $\times$ |  |  |  |
| $0$ | 5 |  | $\times$ | $\times$ |  |
|  |  |  |  |  |  |
| $0{ }^{7}{ }^{7} 0 \mathrm{O}^{8}$ | 7 | $\times$ | $\times$ |  |  |
|  | $\theta$ | X | X |  |  |

Fig. 8. Breaker control switch model 16SB1B2
(INCORRECT)

(CORRECT)

|  |  | 3 | $3 N$ | $2 N$ | 2 | 1 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 |  | 2 | 1 |  |  | $X$ | $X$ | $X$ |
| $0-1 H$ | $0-1 H$ | 2 |  |  | $X$ | $X$ | $X$ |  |
| 3 |  | 4 | 3 |  | $X$ | $X$ | $X$ |  |
| $-H O$ | $0-1 H$ | 4 |  | $X$ | $X$ | $X$ |  |  |

LIMITATION NO. 2
(SBM, SB-1, 9 \& 10 )
Limitation No. 2 (SBM, SB1, -9 \&-10)
On a 4-position pulf-to-lock switch the slip contact cannot be closed in the 2 N and 2 positions (As shown in the top diagrem) without closing in position 1. To accomplish this a stage is added, and the contacts are connect in series as shown in the bottom diagram.
(INCORRECT)

|  |  | 2 | 2N | IN | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 |  |  | $\times$ | X |
| OHOO OHFO | 2 |  | X | X |  |

(CORRECT)


LIMITATION NO. I

$$
(5 \mathrm{SB}-1,9 \text { a } 10)
$$

Limitation No. 1 (S3-1, -9 8.10)
A slip contact and standard contact cannot be on the same stage, as shown in the top diagram.

A stage must be added and contacts split up, as shown in the bottom diagram, one contact per stage. (Does not apply to SBM)
(INCORRECT)

(CORRECT)

|  |  |  | 2N | IN | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 1 |  |  |  | 1 1 |
| OHFO O-H1-9 | 2 |  |  |  | X |
| 34 | 3 |  | $x$ | X |  |
| OHOO O-HO | 4 |  | X |  |  |

LIMITATION NO. 3
(SBM, SB-1, 9 日 10)
Limitation No. 3 (SBM, SE-1, -98,-10)
A contact cannot be closed in the normal after position without also closing in the position itself, as shown in the top diagram. To accomplish this, a stage must be added and the contacts set up as shown in the bottom diagram, with the contacts placed in series by jumpers. dumpers required are shipped loose with the switch.

Fig. 9. Slip-cam limitations

## GENERAL

Contacts on Type SB switches are normally non-overlapping (break-before-make). This sequence is illustrated in Fig. 10 which shows that Zontact No. 1 opens before Contact No. 2 closes, when turning from Position 1 to Position 2. Another normal function is illustrated by Contact No. 3, which is shown closed in two adjacent positions (Positions 2 and 3). When switching between these positions, the contact will always remain closed. There are some circuits where this action is not desired, such as switching current transformers to an ammeter. Here, the contacts must overlap (make-before-break) to prevent damaging the meter.

## SBM SWITCH

To get this overlapping action on the contacts, 90 degrees between positions is required. Figure 11 illustrates an ammeter switch (similar to Model 10AA009) with overlapping contacts. The overlapping action takes place in the intermediate positions (Positions 2, 4, 6, and 8). The inter-
mediate position is identified by an " $X$ " in the block above this position in the operating requirement table. Contacts 1 and 2 are shown overlapping in the intermediate Positions 4 and 6. Contact 2 is shown making in intermediate Position 4 before Contact 1 breaks, when going from Position 3 (OFF) to Position 5 (PHASE 1), and Contact 1 will make before Contact 2 breaks, when going from Position 5 to Position 7.

Figure 12 illustrates an ammeter switch for three independent current transformers (similar to Model 10AA013). This switch also has overlapping contacts and intermediates at Positions 2, 4, 6, and 8; however, the overlapping action takes place between the intermediate position and the actual position. The " $X$ " on the line between the positions of the contacts identifies this action. When turning from Position 5 (PHASE 1) to Position 7 (PHASE III), Contact 1 makes before Contacts 2 and 3 break. Also, Contact 2 and 3 break before Contacts 4 and 5 make, and Contacts 4 and 5 make before Contact 6 breaks. All this action takes place within the 90
degrees between positions, by use of a special cam.

## S8-1,-9, AND-10 SWITCHES

Basically, the overlapping action is the same as with the SBM switch, but it is not limited to positions which are 90 -degrees apart.

To get a make-before-break action, as shown in Fig. 13, a minimum of $371 / 2$ degrees between positions is required. To get a make-before-break as shown in Fig. 14, a minimum of 60 degrees is required. The flexibility of the SB-1, -9 , and $\cdot 10$ switch allows the combination of $371 / 2$ degrees and 60 de grees in the same switch to give you an ammeter switch which reads as many as six, independent, current transformers with either 1 or 2 OFF's (see Fig. 15).

A special contact sequence which requires a contact to close in adjacent positions, but to open momentarily between them, is shown by Contact 1 in Figure 16. A minimum of 60 degrees between positions is required. When less than 60 degrees is required, use two contacts in parallel, as shown in Fig. 17.

| AMMETER |  |
| :---: | :---: |
| OFF |  |
| 3 |  |
| 2 |  |


| CONTACTS HANDLE END |  | POSITIONS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 3 | 2 | 1 |  |
| a-1to a-1to | 1 |  |  | x |  |
|  | 2 |  | x |  |  |
| $3{ }^{3} \mathrm{H}$ | 3 | X | X |  |  |
|  |  |  |  |  |  |


| AMMETER |  |  | INTER. POSITION |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\left.x^{8}\right\|^{7}\left[\begin{array}{l}6 \\ \hline\end{array}\right.$ |  |  |  |  |  |
|  | CONTACTS ODD EVEN |  | POSITIONS |  |  |  |  |  |
| OFF |  |  | 8 | 7 | $6{ }^{6} 5$ | 4 | 2 | 1 |
| 31 | O-1to allo | 1 |  | $\times \times$ | x | x* | 0 | x* |
| $\bigcirc$ | -nto orto | 2 |  |  | *x* |  |  |  |
| 2 | -1-0 | 3 |  |  | *xa |  |  |  |
|  | coro orno | 4 |  | x* |  |  |  |  |
|  | 0-1to 0-10 | 5 |  | x* |  |  |  |  |
|  | Onto onto | 6 |  | *x | x*x | cos | $x$ | $x$ |
|  | O-1to o-lto | 7 | $\times \times$ | $\times \times$ | $\times \times \times$ | $\cdots \times$ |  | * |
|  | OHo Ono | 8 |  |  |  |  |  | $\infty$ |
|  | O-lto ofto | 9 |  |  |  |  |  | $\infty$ |
|  | -nmo onmo |  |  |  |  |  |  |  |

Fig. 10. Typical non-overlapping (break-beforemake) sequence

Fig. 11. Overlapping contacts for SBM ammeter-type switch connected at end of seconcary

Fig. 12. Overlapping contacts for -BM ammeter-type switch, with three ndependent circuits


| $\begin{aligned} & \text { CONTACTS } \\ & \text { HANDLE END } \end{aligned}$ |  | POSITIONS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 3 | Inter | 2 | Inter | 1 |
| $1 \quad 2$ |  | X | $\times$ |  |  |  |
| $\left\{\begin{array}{l} 1 \\ 0-11-0-10^{2} \\ 3 \end{array}\right.$ | 2 |  | X | X | $x$ | $\times$ |
|  | 3 |  |  |  | $x$ | $\times$ |
|  | 4 | $\times$ | $\times$ | $\times$ | $\times$ |  |

Fig 13. Overlapping contacts for SB. 1 ammerer-vpe switch connected at end of secondary (two current transformers) 3.1.1-117

To prevent operation of equipment by unauthorized persons, switches with removable handles are available. The handle is keyed to a specific scutcheon, to be inserted and removed in a designated position. Handies can also be mutually keyed to other escutcheons, so that they are either interchangeable or non-interchangeable with other switches.

This feature is available for SBM, SB-1, and SB-9 switches, but ordering procedures differ.

## SBM SWITCHES



Fig. 18. SBM switch keyed escutcheon with eight available keyway locatons. Keywavs 1-3-5 are shown

The keyed escutcheon on the SBM switch (Fig. 18) has eight possible keyway locations. Three are normally used and are assigned by the factory. The choice is influenced by several factors:
a. If the handle is to be interchangeable with that "of another switch, the position in which each handle is to be removeable must be considered.
b. If the handle is to be non-interchangeable, the keyways assigned to other removeable handles in the same panel must be considered.
c. If no special instruction is given by the customer when he orders, the factory will assign keyways at random; if more than one SBM switch has a removable handle, they will be keyed to be non-interchangeable.

A removable handle is furnished as a separate item, not with the switch it operates, because in some cases the ingle handle operates many switches. he handle is keyed so that it will fit through the keyways on the escutcheon in a specific position.

When ordering a removable handle, specify the type, the position in which it is to be removable, and the switch or switches it will be used with. The factory will assign the handle. To

TABLE 1 Nomenclature guide for SBM removable handles

| 1st Nu mber | 2nd Number | 1st Letter | 2nd Letter | 3rd No. | 4th <br> No. | 5th <br> No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Handle Type | Removable in Position | Common Code | Action of Rotation | Escutcheon Keyways |  |  |
| 1 = Knurled | 1 | W | W = CW \& CCW | 1 | 1 | 1 |
| $2=$ Oval | thru |  | $L=C C W$ (special) | thru | thru | thru |
| $\begin{gathered} 3=\underset{\text { grip }}{\text { Pistol }} \end{gathered}$ | 8 |  | $\mathrm{R}=\mathrm{CW}$ (special) | 8 | 8 | 8 |

## Example 1: 21WW135

This oval handle has keys at positions which, when it is in position 1 , or nine o'clock, will line up with escutcheon keyways 1, 3, and 5. It is therefore removable in position 1.
identify SBM removable handles, see Table 1.

## SB-1 \& SB-9 SWITCH

The keyed escutcheon for the SB-1 \& SB-9 switch is normally furnished with three keyways (see Fig. 19). The circumferential location of the keyways will vary, depending on the location, etc., in which the handle is to be removable. The location of the keyways is assigned by the factory.

Table 2 gives a list of standard keyed escutcheons and the proper removable handie for removing the handle in both the vertical $(12$ $0^{\prime}$ clock) position and $90^{\circ}$ cew (9 o'clock) position. Escutcheons $6016164 \mathrm{P}-2$ thru P-14 are used on switches if the throw does not exceed $90^{\circ}$ on either side of the vertical ( 12 $0^{\prime}$ clock) position, and P-23, 24 and 25 are used when the throw does exceed this limit.


Fig. 19. SB-1 escutcheon for use with removable handle 3.1.1-118

Oval handles 16SB1CC1 thru 32 are listed with direction and degree of throw from the positions in which they are removable. The code letters $A$ thru $Z$ in the left hand column identify the escutcheons used on the basic unlisted switches.

Example: 16SB1AB300SAM3Y, the 2nd form letter $A$ identifies a keyed escutcheon 6016164P-3.

When a special keyed escutcheon is required, different from any of those listed, the code letter " X " is used followed by the part number.

## Example: 16SB1AB300SX34M2Y.

All keyed escutcheons will now have the part number stamped at the bottom left hand corner instead of the code letters previously stamped at the bottom righthand corner. If the code letter or other indentification is desired, it will be stamped at the bottom righthand corner by requisition only (three characters maximum). The 16SB1CC oval type removable handle will now have the form number only stamped on the lower face of the handle. Those removable handles which have metal shanks (6119745G) will have the group number stamped on the shank. When a switch with a keyed escutcheon for a removable handle is ordered, be sure to specify the position in which the handle is to be removable. If an existing handle will be used, give the number of the existing handle.

VOLTMETER TRANSFER
SWITCH, three-phase, trans-
fers four wires phose-lo-phase
and phase-to-neutral,
Model No. 10AA006. Knuried handle.

Fig. 31. VOLTMETER switch, two three-phose, three-wire circuits,
Model No. 10AA007.
Knuried handle.



WIRTNG DIAGRAM דmon - WIRING DIAGRAM


Fig. 32
AMMETER TRANSFER SWITCH,
three CT's (connect at end of secondary), Model No. IOAA008. Knurled handle.

Fig. 33.
AMMETER TRANSFER SWITCH,
three CT's with off
Iconnect at end of secondaryl,
Model No. 10AA009.
For wiring, sel Fig. 32.
Knurled handle.


AMMETER TRANSFER SWITCH three independent circuits, Model No. JOAAOIO. Knurled handle.

INSTRUCTIONS
GEH-2038C
SUPERSEDES GEH-2038B

## CONTROL AND TRANSFER SWITCH

Type SBM


## General (git) Electric



| 1A | Handle |
| :--- | :--- |
| 5 | Mounting Screw |
| 8 | Target Escutcheon |
| 12 | Front Plate |
| 13 | Stops |
| 15 | Rocker Arm |
| 16 | Sleeve |
| 17 A | Positioning Wheel |
| 18 | Positioning Spring |
| 19 | Sleeve |
| 20 A | Torsion Spring |
| 21 | Spring Actuator |

[^4]Fig. 1 (0184B5484-0) Exploded View of Type SBM Switch

# CONTROL AND TRANSFER SWITCH <br> TYPE SBM 

## DESCRIPTION

## INTRODUCTION

The Type SBM switches are cam operated devices having two mechanically and electrically separate contacts per stage. The switch is totally enclosed, having no cover. The contact terminals are brought out to the corners, allowing screw connections to be made over a large angle. The switch is 80 constructed so as to allow the addition of 1 or 2 extra stages to the switch with a minimum of effort.

## APPLICATION

The Type SBM switches are intended primarily for the control of electrically operated devices such as circuit breakers, small motors and magnetic switches, and for the transfer of meters, instruments and relays.

## OPERATION

The Type SBM switches are rotary cam operated switches. Rotation of the shaft causes contacts to open or close, depending upon the shape and setting of the cams. Each stage consists of two mechanically nd electrically separate contacts. This is acomplished by means of two cams and two cam followers, assembled with moving contacts.

Each cam is constructed so as to have two operating surfaces. These surfaces operate on the cam follower. The cam follower has two tips which are located in offset horizontal planes lining up with the two cam operating surfaces. Thus, as the cam is rotated, one surface operates against the closing cam follower tip, while the opening cam follower tip is relieved. Both cam follower tips are always in contact with the cam surfaces. This allows for a positive closing and opening action not dependent upon springs.

Each cam follower has a spring loaded moving contact assembled to it. The compression spring acts to give adequate contact pressure when a contact is closed. The moving contact is held to the cam follower by a pin passing through a hole in the cam follower and angled slot in the moving contact. As the contacts close, the moving contact slides along this slot while compressing the spring thus causing relative motion or "wipe" between moving and stationary contacts.

Some applications, particularly of momentary contact switches, which have a torsion spring to return the switch to a central-neutral position, require a contact action which lags behind the switch motion (lost motion or slip contacts). Such contacts use cams with a special loose fit on the shaft. When the shaft has turned far enough tc close or open these contacts, it can be rotated 45 degrees in the reverse direction without moving the cams, but beyond this point, the cam moves with the shaft and the contacts either open or close as the case may be.

Momentary contact switches have a torsion spring that returns the switch to a central or neutral position when the handle is released after operation to a side position or positions. This torsion spring is designed for maximum of 90 degrees operation to each side of the central position. The torsion spring may have one end cut off or tied back in such a manner as to be effective on one side of the central position only. That is, the switch may have momentary contact to one side of the central position and maintaining contacts to the other side.

In some momentary contact (spring returr:) switches, a locking device is provided by which the shaft may be held against the action of the torsion spring by pulling out the handle when the switch is turned to one of the side positions.

## POSITIONING

A detent wheel, mounted on the square shaft and acted upon by a spring loaded roller arm, gives positive positioning action to the switch.

## REMOVABLE HANDLES

The removable handle option may be obtained with up to 3 keyways in the escutcheon. The keyway locations are at the discretion of the customer. The handle is removable in one position. Any style handle can be used for this operation.

## ADD-A-STAGE

A shaft extension is provided to enable an additional stage to be coupled to the existing switch in the event that more contacts are required when the switch is in the hands of the customer.

These instructions do not purport to cover all details or variations in equipment nor to provide for every possible contingency to be met in connection with installation, operation or maintenance. Should further information be desired or should particular problems arise which are not covered sufficiently for the purchaser's purposes, the matter should be referred to the General Electric Company.

To the extent required the products described herein meet applicable ANSI, IEEE and NEMA standards; but no such assurance is given with respect to local codes and ordinances because they vary greatly.

## RATINGS

The switch is rated for a mechanical life of 500,000 operations. The electrical rating is 600 volts, 20 amperes continuous. The interrupting rating depends on several factors; namely, voltage, current and inductance of the circuit. It may be necessary to use two or more contacts in series to insure adequate interrupting ability on highly inductive circuits. The interrupting ratings are shown in Table I.

TABLE I

| Circuit | Non-Inductive Cir. |  |  | Inductive Circuit |  |
| :---: | ---: | :---: | :---: | :---: | :---: |
|  | Number of Contacts |  |  |  |  |
|  | 1 | 2(in ser) | 1 | 2(in ser) |  |
| 24 DC | 10.0 | 30.0 | 8.0 | 25.0 |  |
| 48 DC | 8.0 | 25.0 | 6.0 | 18.0 |  |
| 125 DC | 5.0 | 15.0 | 4.0 | 10.0 |  |
| 250 DC | 1.0 | 3.0 | 1.0 | 2.5 |  |
| 600 DC | 0.4 | 0.8 | 0.3 | 0.7 |  |
| 115 AC | 40.0 | 75.0 | 24.0 | 50.0 |  |
| 230 AC | 25.0 | 50.0 | 12.0 | 25.0 |  |
| 460 AC | 12.0 | 25.0 | 5.0 | 15.0 |  |
| 600 AC | 10.0 | 20.0 | 8.0 | 12.0 |  |

## CONSTRUCTION

The Type SBM switch is built up with a series of stages which are nested into each other, an operating shaft, a front support and a rear support.

The complete stack is tied together with two tie bolts threaded into the front support. These tio bolts also act as a bearing for the cam follow in each stage. Each stage consists of four statior. contacts and two moving contacts, (double break construction) two cams and two cam followers. The cams are mounted on the operating shaft. In case only one contact is required in a stage, a cam follower assembly is omitted.

## CONTACT IDENTIFICATION

The contacts are marked for identification using a standard system. On each side of the switch midway on the barriers, is a confined marking strip. These strips are located between the two screws which define a contact. The marking strip on the right side, front view, looking toward the rear is numbered 1, 3, 5, etc. starting at the panel end. Those on the left side are marked $2,4,6$, etc. If a contact is omitted the terminal screws are also omitted for that contact.

## ENCLOSURES AND MOUNTING

The basic switch is totally enclosed except for an opening in the bottom to allow for a visual inspection of the contacts.

All switches are furnished for mounting in panels $3 / 32$ to $1 / 4$ inch thick. Variation in panel thickness is taken up by the use of two saddle washers mounted between the handle and escutcheo-

## INSTALLATION

## RECEIVING

Immediately upon receipt of a switch, examine it for any damage sustained in transit. If injury or rough handling is evident, file a damage claim at once with the transportation company and promptly notify the nearest General Electric Apparatus Sales Office. The switches are completely assembled and packed in individual cartons before shipment.

If the switches are for stock purposes or not for immediate installation, they should be left in the shipping carton and stored in a clean dry location.

## MOUNTING

For panel mounted switches, holes should be
provided in the panel as shown in Fig. 2.
To mount a switch on a panel, first remove the handle and escutcheion, including where provided, the position-indicating pointer and the curved spring washers (saddle spring). Next, hold the switch in place on the back of the panel and insert the mounting screws through the escutcheon, panel, and spacers (if used) into the switch front support, but do not tighten the mounting screws. Attach the pointer, saddle springs and handle. Align the escutcheon on the panel.

When mounting removable-handle switches be certain that the shaft of the switch is properly positioned, so the handle is easily removed before the mounting screws are tightened.

## MAINTENANCE

## SERVICING

## CONTACT CLEANING

At regular intervals, the switch contacts should be inspected for wear and burning. An opening at the bottom of the switch has been provided for this. (see Fig.3) If the contacts are slightly pitted or coated with sulphide, they should be cleaned with a flexible
burnishing tool similar to that included in the XRT relay tool kit.

WARNING: Since many of the parts of this switch are molded of a polycarbonate material, DO NOT use any lubricants and/or cleaning agents in any form (incly ing aerosol sprays commonly available). Hyd. carbons (oils and related products may chemically attack such parts resulting in possible switch failure.

## RENEWAL PARTS

## TYPE SBM CONTROL SWITCHES



Fig. 1. Typical SBM control switch (fixed knurled handle, standard escutcheon, and ten stages of maintained contacts).

## ORDERING INSTRUCTIONS

1. Always specify the complete nameplate data of the switch.
2. Specify the quantity, catalog number (if listed), reference number (if listed), description, and this bulletin number.
3. Standard hardware, such as screws, bolts, nuts, washers, etc., is not listed in this bulletin. Such items should be purchased locally.
4. For prices, refer to the nearest office of the General Electric Company.


Fig. 2. Exploded view of typical iwo-stage type SBM swifch.
Maintained contact construction shown. For spring return action, references 19,20 , and 21 replace references $15,16,17$, and 18 .

## CONTROL SWITCHES

## PRINCIPAL RENEWAL PARTS

| Ref. No. | Catalog Number | Description |
| :---: | :---: | :---: |
| 1A | 888B 208AAP 1 | Handle, fixed, pistol grip |
| +1B | 888B 208ABP 1 | Handle, fixed, oval |
| 1 C | 888B 208ACP 1 | Handle, fixed, knurled |
| $\dagger 10$ | 6248034P2 | Handle, fixed, lever |
| +2A | 127A6780G1 | $\ddagger$ Handle assembly, removable, standard |
| $\dagger 2 \mathrm{~B}$ | 127A6780G 3 | $\ddagger$ Handle assembly, removable, engraved ' $R$ '" |
| $\dagger 2 \mathrm{C}$ | 127A6780G4 | $\ddagger$ Handle assembly, removable, engraved ' I ', |
| 3 | 307V511P1 | White pointer for handle |
| $\dagger 4^{\prime}$ | 307 V 516 | Spring washer for pointer |
| 5A | 6049905P1 | Mounting screw, 3/32-1/4 inch panel |
| 5B | 6049905P8 | Mounting screw, 1-11/2 inch panel |
| 6 | NP-202491 | Circuit designation plate (specify engraving) |
| 7 | 127A6768P1 | Escutcheon, fixed handle, no target (specify engraving) |
| 8A | 127A6757G1 | Escutcheon, fixed handle, with target (specify engraving) |
| 8B | 127A6757G 2 | Escutcheon, fixed handle, with target ("TRIP' - "CLOSE") |
| 8 C | 127A6757G3 | Escutcheon, fixed handle, with target ('STOP" - "START") |
| 8 D | 127A6757G4 | Escutcheon, fixed handle, with target (specify engraving) |
| 8 E | 127A6757G 5 | 8 Escutcheon, fixed handle, with target ('TRIP" - "CLOSE") |
| 8 F | 127A6757G6 | 8Escutcheon, fixed handle, with target ("STOP" - "START") |
| $\dagger 9$ | 888B 207P1 | $\ddagger$ Escutcheon, removable handle (specify engraving) |
| $\dagger 10$ | 127A6763P1 | sLocking plate |
| $\dagger 11$ | 307V508P1 | Shaft coupling (removable handle switches only) |
| 12 | 127A6753P1 | Front plate |
| 13 | 127A6754P1 | Stop wheel (standard) |
| +14A | 127A6764G1 | §Stop wheel and shaft assembly, 3/32-1/4 inch panel |
| $\dagger 14 \mathrm{~B}$ | 127A6764G 2 | \$Stop wheel and shaft assembly, 1-1 1/2 inch panel |
| 15 | 127A6772G 1 | Roller arm assembly |
| 16 | 6074939P91 | Roller arm bearing sleeve |
| 17A | 127A6774P1 | Index wheel, 8 points, 45 degree spacing |
| +178 | 127A6774P 2 | Index wheel, 7 points, 45 degree spacing |
| +17C | 127A6774P3 | Index wheel, 4 points, 90 degree spacing |
| 17D | 127A6774P4 | Index. wheel, 3 points, 90 degree spacing |
| *18 | 127A6781 | Positioning spring |
| 19 | 307V510P1 | Torsion spring sleeve |
| * 20A | 127A6775P1 | Torsion spring, standard (spring return CW and CCW) |
| * $\dagger 20 \mathrm{~B}$ | 307V513P1 | Torsion spring, special (spring return CCW to normal only) |
| * $\dagger 20 \mathrm{C}$ | 307V513P2 | Torsion spring, special (spring return CW to normal only) |
| 21 | 127A6760G1 | Torsion spring actuator |
| 22 | 127A6755P2 | Front bearing |
| 23 | 237C755P1 | Front support |
| 24 | 237C756P1 | Barrier cover plate |
| * 25 | 127A6770G1 | Cam follower and moving contact assembly |
| 26 | 237C759P(T) | Cam |
| *27 | 127A6749G1 | Stationary contact, upper |
| *28 | 127A6751G1 | Stationary contact, lower |
| 29 | 6047297P1 | Connection screw |
| 30 | 237C757P1 | Intermediate barrier only (no contacts) |
| 31 | 237C758P1 | $\pi$ Rear support only (no contacts) |
| 32 | $\Delta$ | Rear bearing and shaft assembly |
| 33 | NP-202490 | Rear bearing retainer and nameplate |
| 34 | 127A6756G( 0 ) | Tie bolt |

[^5]I Specify numeral molded in cam.
$\pi$ Uses same contacts as intermediate barrier (References 27, 28, and 29).
$\Delta$ Specify model number of $s$ witch.
$\Delta$ Specify number of stages in switch.

# GENERAL ELECTRIC COMPANY SWITCHGEAR BUSINESS DEPARTMENT PHILADELPHIA, PA 19142 

## GENERAL ELECTRIC




Fig． 3 Bottom View of Type SBM Switch


Fig． 4 View of Type SBM Switch with Additional Stage in Position

## KEPAIR ANL REFLACEMENT

In some cases，it is desirable to either replace a contact stage or to add an additional amount of contacts．

In such cases，it might be advantageous not to disturb the existing switch but to add directly to the present switch．In order to do this，the proper contact sequence should be ordered（no more than two stages）noting that this is for adding to an existing switch．These parts will be received assembled with a U－shaped bracked and a coupling with a square hole will also be received．Fig． 4 shows a Type sBM switch with an additional stage already in position．

To install these additional contacts，loosen the two tie bolts at the rear of the switch about $3 / 32$ inch．slide the loose bracket over the shaft and tie bolts so that the inner part of the bracket slot rests on the tie bolts between the tie bolts and nameplate．Tighten the tie bolts．Slide the coupling over the shaft extension on the present switch，then slide the shaft extension on the new
barrier assembly into the coupling，keeping the shaft of the new contact barriers in the proper position to give the correct contact sequence cor－ responding to the handle position．This should cause the side holes in the two U－shaped brackets to line up．Fasten the brackets together with the hardware supplied．

If it is desired to disassemble the switch for any reason，the following procedure should be followed：Place an identifying mark on the handle end of shaft corresponding to a position on the escutcheon such as 12 O＇clock．Remove the escut－$^{\prime}$ cheon．Remove the three screws fastening the front plate to the front support．If there are stops in the front support，the position relative to the shaft identification mark should be noted．Remove the stops，spacer and star wheel if they are present．

Unscrew the tie bolts and remove the front support．If any torsion springs are present，pull one tie bolt back far enough so that one arm of the torsion spring can be sprung away from the sprirm actuator．Remove the spring actuator，spring $\varepsilon$ any spacers present．Femove the molded covt． plate exposing the contacts of the first stage．

Each cam has one number and seven letters around the shaft opening on one side of the cam and eight letters on the other side of the cam. When removing cams, mark the letter of the cam which corresponds to the shaft identification mark; thus cam and cam followers are removed in succession. This is done to each succeeding barrier.

When reassembling, it is only necessary to stack the cams back into the shaft in the same order as taken off, keeping the proper cam letter lined up with the shaft identification mark.

Before tightening the tie bolts into the front support, make sure that all the barriers are properly nested.

The parts which fit into the front support may now be assembled, placing the stops, if present, in their proper position with respect to the shaft identification mark.

## RENEWAL PARTS

It is recommended that sufficient quantities of renewal parts be carried in stock to enable the prompt replacement of any that are worn, broken or damaged.

When ordering renewal parts, address the nearest Sales Office of the General Electric Company, specify quantity required, name of part wanted, and give complete nameplate data.

GENERAL ELECTRIC COMPANY POWER SYSTEMS MANAGEMENT BUSINESS DEPT. PHILADELPHIA, PA. 19142

## GENERAL ( ELECTRIC

# CLF uses, Current-limiting <br> High-interrupting Capacity 

Current Rating: 3-4000 Amperes
Inferrupting Rating: 200,000 Amperes, rms Symmetrical

## WELDING FUSE (800-2000 amps, 600 volts ac)

Similar in short-circuit protection characteristics to the Class I fuse, the welding fuse is specifically designed for welding circuit applications.


## CLASS J FUSE ADAPTER KITS

A new adapter kit permits 225-600-ampere Class J fuses to mount in 600 -volt Class K 5 fuse spacings. This kit comprises adapter bars which bolt directly to the fuse tangs.

|  | Switehgear Equipmant Products-P(R2100 |  |  |
| :---: | :---: | :---: | :---: |
| Amperes | Class J fuse | Cataico number for odaptor kit for Class kS mounting | * |
| 225 | GF81225 | 01180871361 |  |
| 250 | 6FEE250 | 01160711361 |  |
| 300 | GFA1300 | 011897113G1 |  |
| 350 | GF86350 | 0116ET13G1 |  |
| 400 | Gram00 | 01140711361 |  |
| 450 | Gram50 | $011687113 G 2$ |  |
| 500 | GFi3500 | 0116871362 |  |
| 600 | 6F96600 | 011607113G2 |  |

## CLASS J PULLOUT BLOCK


(Phero 1226009)
Pis. 7. Clese d pulicur bleck


Mo. 78
Clase $\begin{gathered}\text { D Pullout Blocks } \\ \text { Dimonsions }\end{gathered}$
Fig. 7

- Changed since Mar 10, 1976 issue


# FUSE HOLDERS <br> $53-3$ 

## CLASS H \& CLASS R

| Class $\boldsymbol{H}$ CAT. NO. |  | POLES | VOLTS | AMP3 | CLASS HER <br> FUSE SIZE | (1) | N0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| f30A1s | R 30415 | 1 | 250 | 30 |  |  |  |
| F30ans | R30A2S | 2 | 250 | 30 |  | Yes | Yes |
| f30a3s f30A1sp | R30A35 R30A15P | 3 | 250 | 30 | Allholders | Yes | Yes |
| f30arsp | R30415P |  | 250 | 30 | ${ }^{\text {occepl }} 9$. | Yes | Yes |
| F30A3SP | R3OA3SP | 3 | 250 250 | 30 | 2 'long | Yes | Yes |
| F30A18 | R30als | 1 | 250 | 30 |  | Yes | Yes |
| ${ }^{\text {F30A2 }}$ | R30A2B | 2 | 250 | 30 |  | Yes | Yes |
| F30036 | R30A3B | 3 | 250 | 30 |  | Yes | Yes |
| 6F30A 15 | 6R30AIS | 1 | 600 | 30 |  |  |  |
| 6F30A25 | 6R30A2S | 2 | 600 | 30 | All holders | Yes | Yes |
| 6F590435 | 6R30A3S | 3 | 600 | 30 | acceptifuses | Yes | Yes |
| 6f30A15P | 6R30AISP | 1 | 600 | 30 | 1316 Diameter $x$ | Yes | Yes |
| 6F30A2SP | 6R30A2SP | 2 | 600 | 30 | 5 long | Yes | Yes |
| 6F30A3SP | 6R30A3SP | 3 | 600 | 30 |  | Yes | Yes |
| 6F30A18 | 6R30A18 | 1 | 600 | 30 |  | Yes | Yes |
| 6F30428 6F30438 | 6R30A28 | 2 | 600 | 30 |  | Yes | Yes |
| SCREW | 6R30A38 | 3 | 600 | 30 |  | Yes | Yes |
| SCREW | NECTIONS | AVAIL (CO | $\begin{aligned} & \text { BLE FOR } \\ & \text { SULT FAC } \end{aligned}$ | 60 AMP CTORYI | 600 VOLT APPLICA | tions |  |
| 6FGOA 18 | 6RGOAIB | 1 | 600 | 60 | Accepts tuses |  |  |
| ${ }_{6}^{6560 A} 28$ | 6R60A 28 | 2 | 600 | $\infty$ | 1.1 16. Diameter $x$ | Yes | Yes |
| 6F60A38 | 6R60A38 | 3 | 600 | $\infty$ | $5.1{ }^{-1}$ long | Yes | Yes |
| f60als | R60AIS | 1 | 250 | 60 |  | Recognized | No |
| Fboazs | R60a2S | 2 | 250 | $\infty$ | All holders | Recognized | No |
| Fboajs | R60A3S | 3 | 250 | $\infty$ | acceot tuses | Recognized | No |
| Ftoals | R60A18 | 1 | 250 | \$0 | 1316 Diameter $x$ 3 tong | Recognied | Yos |
| F60anz | R60428 | 2 | 250 | + | 3 'tong | Listed | Yes |
| F6an38 | R60A3B | 3 | 250 | + |  | Listed | Yes |
| figoals | R100A18 | 1 | 250 | 100 | Accept fuses |  |  |
| F100428 | R100A28 | 2 | 250 | 100 | 1 Diameter $x$ | Yos |  |
| F100A38 | R100A38 | 3 | 250 | 100 | 5.7/8" long. | Yes |  |
| 6F100418 | 6R100ali | 1 | 600 | 100 | Acrept tuses |  |  |
| 6F100A28 | ORIOAA2B | 2 | 600 | 100 | 1.1/4" Diameter $x$ | Yos | yes |
| 6F100A38 | 6R100A38 | 3 | 600 | 100 | 7.7/8" long | yos | Yes |
| F200Als | R200als | 1 | 250 | 200 | Accepts fuse |  |  |
| F200A38 | R200A3日 | 3 | 250 | 200 | 1.1.2000m. 7 | Yes | Yes |
| 6 6200als | 6R200A18 | 1 | 600 | 200 | Accepts fusa |  |  |
| 6F200A3B | OR200A3E | 3 | 600 | 200 | 2.1/2' $\times 9.5 / 8^{\prime \prime}$ | Yos | Yes |
| fa00alb | R400A18 | 1 | 250 | ${ }^{400}$ | Accupts fuses |  |  |
| F400A38 | R400438 | 3 | 250 | 400 | 2 Diom. $\times 8.5 / 8^{\prime \prime}$ | Yes | Yes |
| 6F400A18 | SR400418 | 1 |  |  | Accepts tuses |  |  |
| bf 400 A 38 | SR400A3B | 3 | +00 | 400 | 2.1/3. Diam. $x$ | Yos | Yes |
|  | bricomja | 3 | 500 | 400 | 11.5/8" | Yes | Yes |
| f600al 18 | R6000 18 | 1 | 250 | +00 | Accepts fuse | Yes | Yes |
| f600438 | R600438 | 3 | 250 | 600 |  | Yes | Yee |
| of600als | R600A1日 | 1 |  |  | Accoprs tuse |  |  |
| Of 6000438 | 6R600A38 | 3 | 600 | 600 | 13.3/8. | $\begin{aligned} & Y \neq z \end{aligned}$ | Yen |

Reinforcing Members are available for 30 and 60 Amp fuse holders on request - odd "R" before the above catalog number. Reinforcing Mombers are standard on 100, 200 and 400 Amp tuse hoiders.
Reinforcing Members are standard on 30 through 400 Amp Class R fuse holders.
bowing green, ohio 43402 telephome: (419) 352-9441

## DIMENSIONS: 30 Amp-250 Volt. Class H



Fig. 1


Pig. If

| DIAGRAM DIMENSIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| CAT. NO. | PIC. NO. | A | 8 |
| F30AIS | 1 | 1.7/32 | 3/4 |
| F30A2S | 1 | 2-5/32 | 1.1/4 |
| F30435 | III | 3-1/8 | 2-1/2 |
| F30A1SP | I | 1.7/32 | 3/4 |
| F30A2SP | 11 | 2-5/32 | 1.1/4 |
| F30A3SP | III | 3-1/8 | 2-1/2 |
| F30A18 | 1 | 1.7/32 | 3/4 |
| F30A28 | 11 | 2-5/32 | 1-1/4 |
| F30A38 | 111 | 3-1/8 | 2-1/2 |

(Catalog dimensions are for reference only, not to be construed as inspection standards)

MARATHON'S


Resistance - a most fundamental property of electricity in relation to its conductor. The higher the resistivity of the conductor the higher hear leval generated with the pessoge of current. In fusing applications, this heat must be dissipated. The heat generated in a fuse clip can actually reduce the life of the fuse, clip and conductor os well as the protection power of the fusing device.

No longer is it necessary for heat buildup to rob equipment of protection and extended life. Utilize our "Cool-Clip", a revolutionary new fuse clip that is the result of on extensive anylitical optimization process.
"Minimum A but maximum 8 " is the secret behind the "Cool-Clip". Extremely good contoct between the fuse and "Cool-Clip" causes the fuse and elip to operate considerably cooler than other clips.

Minimum outword movement of the spring at points " $C$ " meons a minimum expenditure of energy; the fuse is held in place with more force. The greater " $B$ " distance reduces to near nothing the possibility of exerting excess pressure at stress point "D". No more broken or sprung tuse clips.

# HEAVY DUTY 

TERMINAL BLOCK - BARRIER TYPE asctmeal rating

 mpinaering colviog.

- 600 Volf
-up te 75 Ampe depending on termination uned* - Wre Renge
will eceormmodote up to a 110 AWC wirs in cecordence with the Metional Electricol Code
Serewn-ilreag, nicked platod, 10-32x7/16 serroted moahmer heed. stonderel.
1500 series
5/0" Line to line speeing U Slot Mount

1600 Series
21/32" Line to line specting Inboard Mount


TERMINAL BLOCK - ENCLOSED TYPE

nattrocal ramme
-300 Volts*
-55 Ampe"
-Wire size - 114-16 AWG Copper

## 1103 F 1200 Series

ExCTHCAL RATME

- 11009 Seriee. 600 Volt - 70 Ampe ${ }^{\circ}$
-1200 Series, $600 \mathrm{Volt} \mathrm{-} 70 \mathrm{Amps}$ "


(M) MARATHON sPECIAL PRODUCTS
(M) special products


## DIMENSIONS: 1500 Series


(Cetriog dimemsions ore for reference only, not so be construed as inspection stondards)


## POWER BLOCKS

*Refer to Bulletin 2.0 for Power Block Ratings and Standards.


600 VOLTS:* TWO AND THREE CIRCUITS
(ONE CIRCUIT AVAILABLE ON SPECIAL REQUEST)

| GENERAL INFORMATION |  |
| :---: | :---: |
| APPLICATION | electrical rating |
| Designed for use with heoting, air conditioning | - 600 volts* |
| and refrigeration, elevator systems, material | - Wire range "14 AWG - 600 MCM , aluminum |
| handing equipment, control panels, motor control. switchgear and any area where a reliable connect | or copper wire depending on block selected Double and triple circuits are standard |
| is needed to horness power. | - Single circuits ovailable on request |
| HARDWARE |  |
| Connector - one piece aluminum or copper | STANDAROS |
| Base $\quad$ - ${ }^{\text {tin peneralal }}$ purpose phenolic | U.L. Recognized File No. E62806 C.S.A. Certified File No. 19766 |

CATALOG NUMBER AND SPECIFICATIONS


ORDERING CODE


Non-Descript
Ne. of Circuits
 Numerical Sequence

$\qquad$ ,



STYLE 210-25 (25 WATT-SIZE 2"×9 $1 \mathbf{1 6}^{\prime \prime}$ )

|  | rpm | Romm | mam |  |  |  |  | Soce | Tree | ${ }^{\text {anmus. }}$ | man. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $13 \pm 550$ | C300 | 1 | $5 \times$ |  |  |  |  | 135505 | 23716 |  |  |  |  |  | $\cdots$ |
| ${ }_{13}$ \|rss |  | 2 | 3 3 |  |  |  | -: | ${ }_{1215562}$ | 0372 | 500 | 2 |  |  |  |  |
| \|riss | , 33031. | 5 | 268 <br> 28 <br> 24 |  |  |  |  | ${ }^{1} 1 \mathbf{1 7 5 5 0 4}$ | ${ }_{0}^{0375}$ | , 750 | 18 |  |  |  | - |
| \|r350 | 23628 | 7.5 | 1.82 |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 Fsse | 0303 | 10 | 158 |  |  |  |  | 1314577 |  | 1.350 | 13 |  |  |  |  |
| \|17850 | ${ }_{03048}^{030}$ | ${ }^{15}$ | ${ }_{1}$ |  |  |  |  | 1357 |  | 2.000 | 12 |  |  |  |  |
| 13950 |  |  | 10 |  |  |  |  | 12575 | - 1978 | 3 | 110 |  |  |  |  |
| ,17599 | 03006 | 50 | 7 |  |  |  |  |  | ${ }^{20}$ | S.000 | 070 |  |  |  |  |
| ${ }_{1}^{13850}$ | 0267 0306 | 78 | S0 |  |  |  |  | i3Ps51 | 0331 | -0,000 | - ${ }_{0}^{\text {cos }}$ |  |  |  |  |
| ${ }_{13} 17850$ | ${ }_{030}$ | 150 | 4 |  |  |  |  | 13547 | 0315 | 20.000 | 050. |  |  |  |  |
| , 13850 | 0370 0371 | 200 | 23 |  |  |  |  | , 13F5900 |  | 20.000- | $0.011$ | - |  |  |  |

## STYLE 210-50 (50 WATT—SIZE 4"x9/16").

| ${ }_{40}$ | 1,mem | 0 | anin |  |  |  |  | not | Tre | amin | max | F-- |  |  | . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ${ }_{0}^{050}$ |  |  |  |  |  |  | ${ }^{13 P 611}$ | 0369 | , 50 | -30 | - |  |  |  |
| ${ }_{1} 376001$ | 2561 | $\because 0$ | 230 | $\because$ | $\checkmark$ |  |  | - ${ }_{1781813}^{13812}$ | ${ }^{058}$ | 57.000 | 2til | $\cdots$ |  |  |  |
| ${ }_{138602}$ | 0x2 | 23. |  |  | $\downarrow$ | $\cdots$ |  |  |  |  |  |  | - |  | - |
| ${ }_{13170000}$ | - | is | 82 |  | - |  |  | (137615 | ${ }^{0} 5$ | $\cdots$ | -16 |  |  |  |  |
| $13+605$ | Osas | 100 | 7 |  |  |  |  | ${ }_{13}^{138617}$ | O573 | 2.500 5.000 | 14 |  |  |  |  |
| 137000 | Osob | 130 | 50 |  |  |  |  |  |  |  |  |  |  |  |  |
| ${ }^{137500000}$ | csol | - | ${ }_{4}^{5}$ |  | - |  |  | ${ }^{1375028}$ | ${ }^{0588}$ | 11.50 | 01 |  |  |  |  |
| 1378000 | -ssee | 300 | \% | - |  |  |  | ${ }^{13} 35 \mathrm{~A}, 5$ | ${ }_{\text {Oss }}$ | 50000 | ${ }^{20} 6$ |  |  |  |  |
| 13560 | 0568: | $\cdots$ | 35 |  |  |  |  | [JFA38 | 2591 | $0 \times 0$ | cis |  |  |  |  |


(W) SARMTTED FOR

Descriptive Bulletin 32-850

Page 1

Power Centers
Including
Type DS Switchgear.


## Page 2

## Table of Contents

## Definition - Advantages -

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Incoming Line Section
High Voltage Switches and
Fuses-Descriptive
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Liquid Transformers-Descriptive
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## Definition

A Power Center is defined as a coordinated assembly consisting of 3 phase transformers with high voltage incoming tine sections and an assembly of Type DS Low Voltage Switchgear, with the following parameters:

Transformer Kva-112.5 thru 2500 High Voltage- 2400 V thru 13.800 V Low Voltage-208, 240, 480 or 600 V

Power centers may be indoor or outdoor, with a selection of high voltage incoming sections and a choice of transformer types as shown under "components," and an arrangement of Type DS Switchgear to suit the application.

Power centers as defined herein come within the category of "Secondary Unit Substations" as defined in NEMA Standards.

## Why Power Centers?

Power centers follow the modern system concept of locating transformers as close as practicable to areas of load concentration at utilization voltages, thus minimizing the lengths of secondary distribution cables and buses. This concept provides several basic advantages over older methods. such as:

- Reduced power losses.
- improved voltage regulation.
- Improved service continuity.
- Reduced likelihood of faults.
- Increased flexibility.
- Minimized installation expense.
- Availability of non-flammable types of transformers eliminates necessity of vaults.
- Efficient space utilization.


## Advantages of Westinghouse Power Centers

- Single responsibility.
- Complete coordination, both mechanical and electrical.
Page 2
Page 3
Page 4
- Extreme flexibility, with wide choice of components and ratings to meet exact
application requirements.
- Optimum safety to operators.
- Modern design.
- Meets all ANSI, IEEE and NEMA Standards.


## Types of Systems

```
A. Simple Radial
    - Simplest and least costly.
    - Easy to coordinate.
    - No idle parts.
```



## B. Primary Selective Radial

 Similar to simple radial, with added advanrage of spare primary incoming cable circuit. By switching to spare circuit, duration of outage from cable failure is limited.

## C. Secondary Selective

Normally operates as two electrically idependent unit substations, with bus tie breaker( $T$ ) open, and with approximately half of total load on each bus. In case of failure of either primary incoming circuit, only one bus is affected, and service can be promptly restored by opening main breaker ( $M$ ) on dead bus and closing tie breaker ( $T$ ). This operation can be made automatic, with duration of outage on either bus limited to a few seconds.

Since the transformers are not continuously paralleled, secondary fault currents and
breaker application are similar to those on radial unit substations.

Either transformer can be removed from service and isolated with no interruption of service on either bus, by first closing the tie breaker and then opening the associated main breaker.

Service continuity and substation capacity can be further improved by substituting selector type primary switches, as in $B$.


## D. Spot Network

The transformers are paralleled through network protectors. In case of primary voltage failure, the associated protector automatically opens. The other protector remains closed, and there is no "dead time" on the bus, even momentarily. When promary voltage is restored, the protector automatically checks for synchronism and recloses.

- Secondary voltage regulation is improved by paralleled transformers.
- Secondary fault capability is increased by paralleled transformers, and the
feeder breakers must be selected accordingly.
- Primary switches are usually selector or duplex type, so that transformers can be transferred to alternate live sources, thus shortening duration of overloads.


Components of Power Centers

1. High Voltage
Incoming Line Section

2. Transformer Section

3. Low Voltage Switchgear Section



## A. Air Interrupter Switch

Primary Power Switch, Type PPS (for liquid transformers only)

## Features

- Quick-make, quick-break stored energy spring mechanism.
- De-ion arc interruption.
- Switch parts molded in tough cast resin. with transparent blade housings.
- Safety interlock between access door and switch mechanism.
- Adequate insulated cable connections to transformer bushings.
- Furnished fused or unfused; fuses either CLE current limiting or RBA non-current limiting type.
- Proven reliability.


## Configurations Available



Load Interrupter Swith. Type WLI
(standard for Ventilated Dry and Gas Filled transformers: optional for liquid transformers)


## Features

- Quick-make, quick break stored energy spring mechanism.
- De-ion arc interruption.
- Positive switch position indication by operating mechanism.
- Safety interlock between access door and mechanism.


## Configurations Available


B. Cable terminal compartment only, air filled.

Available with all transformer types. Extends to floor and completely encloses cables and terminals. Arranged for either bottom or top cable entrance.


## C. Miscellaneous Types of High Voltage

Incoming Equipment

1. Type FSP load-interrupter switchgear units, metal-clad switchgear construction, with "rollout" air switch elements, fused or unfused, 15 Kv . indoor or outdoor. Fuses are Type CLE current limiting only, voltage to suit application.
2. Type DH-P "Porcel-Line" metal-clad switchgear, 5 Kv to $15 \mathrm{Kv}, 75$ to 1000 Mva interrupting rating, indoor or outdoor.
3. Liquid Filled Switch.
4. Oil Fused Cutouts.

Type CLE and CLT current limiting nonexpulsion, non-refillable fuses.


Culaway view of type CLE- 2 fuse showing pure silver elements.

Type CLE and CLT power fuses are basically of inorganic construction, the only organic material used being the glass-resin outer casing and the plastic indicator. The fuse elements are pure silver designed to combine maximum load carrying ability with the most favorable short circuit interruption characteristics, plus being "fatigue proof." This added feature is made possible by bending or spiralling the element prior to assembly, making the element structurally stronger and distributing expansion uniformly to withstand the most severe type of duty cycling without failure. These fuses are filled with a high purity silica sand of controlled grain size, and sandwiched between the sand filling is an additional layer of pulverant arc quenching material. The addition of this band of filler to the fuse changes its melting characteristics and facilitates low current interruption making it more suitable for transformer protection.

Type RBA non-current limiting, refillable. expulsion type fuses.


Fuse Refill
The boric acid refill is probably the most important component of the RBA fuse. It is designed to interrupt currents of short circuit magnitude within $1 / 2$ cycle, and through its two de-ionizing chambers in parallel. have selective operation and interruption for both low-current and high current faults. This is achieved by movement of the arc through the boric acid cylinder by a helical spring and rod. Intense heat from the arc, as it strikes, decomposes the dry boric acid. On decomposition the boric acid forms water vapor and inert boric oxide. The electrical interruption is caused by the steam de-ionizing the arc as it is drawn through the cylinder by the action of the spring and rod. The high particle turbulence of boric acid causes the rate of de-ionization in the cylinder to exceed the ionization rate of the electrical arc. This action prevents the arc from restriking.

Upon operation of the fuse under fault condition, the fuse holder is disconnected, the fuse refill removed, and replaced with a new refill.


Cross-section drawing showing component parts a type CLE- 1 fuse unit.

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## Transformer Section

## Liquid Filled Transformers

## Advantages

Standardized bushing height of 55 inches for all ratings allows subsequent uprating at minimum cost.

A proven rectangular core and coil design. pioneered by Westinghouse in 1954, is used in conjunction with a computer program to provide rugged, dependable service and an optimized design.
Insuldur system of thermally stabilized insulating material-allows user $12 \%$ additional Kva capacity of $55 / 65^{\circ} \mathrm{C}$ rated units or maximum $55^{\circ} \mathrm{C}$ Kua capacity at $40^{\circ} \mathrm{C}$ average ambient.
An automated plant, designed specifically for the production of rectangular core form transformers, assures uniform quality and shipping expediency.

## General Design Features

These transformers are designed for indoor or outdoor use-oil or Silicone immersedwith a standard temperature rise of $65^{\circ} \mathrm{C}$. Either a flange or throat can be furnished on the high and low voltage side for connections to primary and secondary equipment.

High and low voltage terminals are located on opposite sides of the unit for a "straightthru" line-up. Bushing height is standardized at 55 inches to permit ease of coordination with other equipment and later uprațing at minimum costs.

Cooling is accomplished through flat, tubular coolers welded to the tank wall. A welded-on tank cover / handhole provides sealed tank oil preservation. Standard tank pressure is 5 psi.

Lifting hooks are provided for lifting the entire unit and lifting loops for lifting the tank cover. The base is designed for skidding in any direction.

## Standard Finish

The Westinghouse standard finish is a three-coat system applied as follows:
A. All surfaces are shot blasted or pickled to a semi-white metal to form a completely clean surface.
B. A caustic wash and phosphatized coating to inhibit corrosion and furnish a base for high mechanical strength of paint bonding.
C. An epoxy-melamine primer cost cured in oven at $150^{\circ} \mathrm{C}$.
D. A Westinghouse top coat, composed of an alkyd-melamine enamel paint system containing special pigments selected to give long outdoor service in varying climatic exposures and maintain attractive appearance, is applied and given a baked finish at $150^{\circ} \mathrm{C}$.
E. An air-dry version of Item $D$ is applied to touch up units prior to shipment.

Standard outdoor tank color is ANSI No. 24. ANSI No. 70 can be supplied but must be specified. Other colors or other paints may be available on special request. Standard indoor color is ANSI No. 61 light grey.

Standard Features and Accessories


## Rectangular Core and Coils

WSS Tap Changer
The Westinghouse externally operated WSS tap changer provides positive sequence line voltage changes under de-energized conditions. An in-line assembly, the WSS features through-type stationary contact studs rigidly supported by a molded plastic channel. Moving contacts are spring loaded, silver plated copper which move along the stationary line by means of a rack and pinion.

This design has no rivets, bolts or nuts, thus assuring the proper contact of current carrying parts when taps are changed. The WSS benefits the user through a reduction of repair or replacement costs by eliminating faulty tap changer operation-the cause of failure in $20 \%$ of all power transformers.

Rectangular Aluminum Wound Coils


The Wesringhouse rectangular wound coil features aluminum conductor in both high and low voltage windings. The low voltage winding is accomplished on a constant tension machine and consists of full width sheet aluminum extending the full height of the coil. High voltage strap aluminum is wound directly over the low voltage winding on a constant tension traversing machine. Layer to layer and high to low insulation is diamond epoxy paper which when heat treated bonds the complete coil into a solid configuration.

The advantage of low voltage sheet aluminum is a continuous cross section of conductor that allows the electrical centers of high and low voltage windings to easily align themselves, virtually eliminating the vertical component of short circuit force.




The benefit is a coil so uniform and compact, the chance of windings overlapping during short circuit is minimized, reducing failure rate, repair and/or replacement cost.


The Westinghouse exclusive stacked core provides a superior flux path by utilizing the patented step-lap joining of core legs to top and bottom yokes. Hand stacked Hypersil steel punchings with interlocking laminations can be more uniformly and rigidly braced to prevent shifting during service.

The user can benefit through reduced sound levels, lowered iron and total losses, and decreased exciting current to lower total operating cost.

On wye-wye units a fourth leg is added to provide a path for circulating third harmonic flux during unbalance condition.

## Wolded Frame

The Westinghouse exclusive welded frame provides a superior six piece supporting structure for the core and coils. End plates are thick steel slabs that are assembled in a mechanical and pressure jig around the core and coils, then welded to top and bottom plates to form a rigid structure that will not loosen during assembly, shipment, or in service. To determine the thickness of members used (even the thickness of weids), a short circuit calculation is made for each unit to determine the forces of short circuit.

The resuit is an assembly that restrains more effectively vertical and horizontal components of force, decreasing the probability of failure during severe short circuits.

This benefits the user by a reduction in repair or replacement costs and a reduction in

downtime that means loss of service or lost production.

## Super Insuldur Insulation

The Westinghouse Super Insuldur Insulation effectively upgrades cellulose insulating materials thermally for increased load and overload capability. The chemical stabilizers in the Insuldur process retard insulation breakdown under severe temperature
conditions. Dimensional changes in the insulating materials are minimized, insuring a tighter structure. The resuit is greater strength and coil integrity throughout the life of the transformer

The user benefit is a coil that better withstands short circuit and allows an operation at $10^{\circ} \mathrm{C}$ higher temperature on a $55^{\circ} \mathrm{C}$ rated unit with a $\mathbf{1 2 \%}$ increase in Kva capacity.


Welded Frame

## Optional Accessories


Forced Air Cooling-Provisions for fan cooling are included on transformers 750 Kva and larger. Complete fan cooling equipment is available and when in operation will give the following OA/FA ratings:
750 Kva OA ........ 862 Kva FA
1000 Kva OA ....... 1150 Kva FA
1500 Kva OA ....... 1725 Kva FA
2000 Kva OA ....... 2300 Kva FA
2500 Kva OA. . . . . 3125 Kva FA


Dial Hot Spot-Dial hot spot winding temperature equipment including a current transformer may be specified.

Alarm Contacts--SPDT Alarm contacts may be added to the thermometer, liquid level gauge and pressure relief device.

Further Information
Prices: Price List 47-150
Dimensions: Technical Certification Section 47-159.

Fault Protection and Indication-Reprint 200

Rectangular Coil Core Form Transformers: SA-10099

Bulletin IC/FF-38R Monsanto Askarel Guide

Westinghouse Insuldur: SA-9025B
Why Westinghouse Rectangular Coil Core Form Transformers Withstand Short Circuits: M-7205

The South Boston Value Siory: MA-375.

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## Dry Type Transformers

## Application

Ventilated and gas filled sealed dry type transformers are ideally suited for indoor and outdoor applications. Ventilated units may be installed in practically any indoor location not subject to submersion or to a high concentration of destructive fumes, or outdoor with a weather-proof case. Gas filled sealed dry type units offer the ultimate in safety and low maintenance with high impulse levels. They can be installed indoor or outdoor or completely submersed

## Benefits

Reliability and Long Life

- Windings are protected by Nomex" insulation having very high temperature and dielectric characteristics.
- A $220^{\circ} \mathrm{C}$ fully coordinated insulation system is used.
- Each prototype unit is subjected to a complete set of short circuit calculations which have been verified by full size testing.
- Coil types are coordinated with voltage application, i.e., Barrel type/cylindrical coils on 1.2 and 5 Kv class; Disc coils on 8.6 and 15 Kv class.
- The ventilation system is engineered to assure proper operating temperature in the coils.
- On FA units air is positively directed under pressure through the coil ducts at high speed to assure thermal operation under the $220^{\circ} \mathrm{C}$ allowable limit.


## Low Environmental Cost-

Safety and Versatility

- Ventilated dry type transformers are supplied with lightning arresters when speci fied allowing confident application to any exposed line regardless of line BIL.
- Air insulated and cooled by natural convection, these transformers retease no toxic gases and are fire and explosion resistant. Elimination of these principal liquid-filled transformer potential hazards makes them especially desirable for installation in schools, hospitals, hotels, theatres, factories, etc., where large groups of people are present.
- Where space limitations are a consideration ventilated dry type, transformers offer lower weight and absence of liquid allowing their mounting in such places as balconies to save floor space and yet provide safe operation.
- Gas filled sealed dry type transformers
are the safest transformers available with a completely hermetically sealed heavy gauge steel tank-they can be installed anywhere.


## Value

Proven Methods and Materials

- Westinghouse testing standards are the highest in the industry. New designs are given complete load, short circuit, and insulation tests to prove methods and materials used in manufacture. Verified production line models receive standard quality control inspections and tests by
our most experienced personnel. Certified reports on routine tests can be obtained on all units, and special tests or reports can be obtained by special orders


## Further Information

Prices:
PL 47-330
Description:
DB47-351
Ordering Information and Dimensions: DS 47-370


## Insulation Class

Dry type transformers are insulated with $220^{\circ} \mathrm{C}$ system materials with temperature ratings as follows:

| Maximum Ambient | Average Rise | Hottest Spot Windinq Temperature Risp |
| :--- | :--- | :--- |
| $40^{\circ} \mathrm{C}$ | $150^{\circ} \mathrm{C}$ | $180^{\circ} \mathrm{C}$ |
| $40^{\circ} \mathrm{C}$ | $115^{\mathrm{C}} \mathrm{C}$ | 145 C |
| $40^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $110^{\mathrm{C}}$ |

### 3.1.1-150

## Maintenance

Dry type transformers are practically maintenance free, except for periodic inspection of the connections. On ventilated dry type transformers any accumulation of dust or dirt should be removed by brushing or blowing dry air on the unit. See IL 47-067-1 Gas filled sealed dry type transformers only require periodic checks of pressure and temperature. They require less maintenance than liquid filled or open ventilated dry type transformers.

## Design Features

## 1. Case-Ventilated Dry Type

The case has removable panels for access to the taps and core and coil inspection and the complete case structure can be removed and knocked down to reduce size and weight for rigging into tight locations. The case is constructed of 13 gauge steel and painted ANSI $=61$ light gray.

Standard case accessories are: jack pads, ground pad, diagrammatic nameplate, provisions for rolling, and protected ventilation grille.

## Gas Filled Sealed Dry Type

Sealed Tank
The transformer will be of sealed tank construction to prevent breathing. Tank will be hermetically sealed and will be tested at 15 psi pressure. It will be provided with welded-on $1 / 4$ " thick Yukon coolers.

Shot Blast
The case and coolers will be cleaned by shot blast and phosphatized before the paint is applied.

Finish
Paint finish will be manufacturer's standard, applied over a properly prepared surface. The color will be light gray ANSI No. 61 (indoor) or dark gray ANSI No. 24 (outdoor)

The transformer will be insulated and cooled with $\mathrm{C}_{2} \mathrm{~F}_{6}$ fluorocarbon gas.

Bushings
The transformer tank will be fitted with rolled flange, inert are welded bushings for the high voltage and low voltage connections to insure that the tank is hermetically sealed

## 2. Core and Coil Assembly

Core and coil assemblies are rigidly braced to withstand mechanical forces under line fault conditions and to resist vibration and shock forces during shipment.

Coils are concentrically assembled on the core legs and rigidly positioned laterally by spacers between the inner-most insulating cylinder and the core. Horizontal and vertical stresses set up during faults do not exceed the inherent strength of the conductors and support system.

## 3. Core

## Ventilated Dry Type and Gas Filled Sealed Dry Type

Material used to form the core is non-aging, cold rolled, high permeability silicon steel. Bulk material is cut to width and sheared to length by especially hardened and ground cutters to prevent edge damage and burrs that would short between laminations and reduce core efficiency.

Core faminations are firmly clamped by structural steel members for greater strength and lower noise levels. The insulation on the core clamps prevent a metallic short across the stacked laminations. Core clamps and all structural parts are grounded to prevent an induced voltage buildup

The resulting compact, rigidly clamped structure formed by the core and coil assembly provide a low loss, low sound level design with the strength to withstand repeated short circuit forces.

## 4. Coils

## Ventilated Dry Type and Gas Filled Sealed Dry Type

## Conductor Material

Aluminum is the standard conductor material. Where design considerations require, copper may be substituted.

## Insulation

The insulating structure of the coil is designed for operation at 220 degrees Centigrade hot spot temperature $\left(150^{\circ} \mathrm{C}\right.$ average rise). High voltage conductor insulation and layer insulation is DuPont Nomex ${ }^{\text {® }}$. This tough, long life high temperature (Class H) Nomex material is especially resistant to humidity and repeated thermal cycling.

The low voltage coils are usually of cylindrical or strip construction and high vottage coils are usually of the continuous pancake or random wound disc type construction. Large air ducts provide insulation between windings and form vertical cylinders for natural ventilation. The free area in the pancake coils between porcelain spacers further facilitates the flow of cooling air.


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## 5. Taps

## Ventilated Dry Type

The taps can be reached from the front or back by removing a panel which also protects tampering with the taps.
The taps are rigidly supported by brazing them on the central section of the HV coils. Taps are changed by moving the flexible bolted links from one connecting point to the other. To simplify these changes, the connections are clearly identified.

## Gas Filled Sealed Dry Type

De-energized Tap Changer
A tap changer will be supplied to permit changing connections in the high voltage windings from outside the transformer case. The tap changer is designed for operation only when the transformer is de-energized. Provision will be made for padlocking in any position. A packing gland seals the operating shaft at the tank wall. The external housing prevents gas loss due to perme-
ability through the gland packing material. The housing cover may be either gasketed or soidered.

## 6. Arresters

Ventilated dry type power centers are sup plied with RM arresters when specified to provide maximum surge protection for the transformer and associated secondary equipment.

Located in the transformer section, the RM arresters protect against a possible double surge voltage at the transformer terminals even though arresters may be used on the incoming line. The possibility of exceeding BIL level due to reflected voltages is dependent on length and character of cable and steepness of surge.

This protection has added importance when LV apparatus or equipment in use has a tower BIL level than the LV transformer

winding. Due to electrostatic coupling, a surge transmitted through a transformer could be as much as $11 / 2$ to 2 times as great as would be anticipated on the basis of turns ratio alone and could damage this LV equipment. Therefore, RM arrester at HV terminals are desirable.

In applying arresters, it shouid be remembered to use an arrester with a sparkover to operate below the BIL of the apparatus and to install the arresters at the apparatus to be protected.
7. Isomode Pad (Vibration Dampeners) On Ventilated Dry Type Units
After removal of the shipping braces, the core and coil assembly rests on rubber Isomode pads to isolate normal core vibrations from the case, foundation or any conduit or bus duct connected to the case.

## Coil Impregnation

High temperature moisture and chemical resistant varnish maintains superior bond strength, high dielectric strength and good power factor at elevated temperatures associated with $220^{\circ} \mathrm{C}$ insulation systems. The thermal aging characteristics, thermal stability and physical resistance to common solvents exceeds that of commonly used varnishes. The resistance to alkalis, acids. and moisture is excellent. High and low voltage coils are impregnated with this varnish and baked before assembly.

## Bushings on Gas Filled Sealed Dry Type

 TransformersGas filled transformers are equipped with rolled flange, inert arc welded bushings, type RFW, for the HV and LV outlets. These bushings insure a hermetically sealed tank while allowing flexibility for conductor expansion and contraction.


Accossories -Ventilated Dry Type

## Outdoor Cases



Standard Outdoor Case


Tamper-Resistant Outdoor Case

## Outdoor Cases

Ventilated dry type units are available with outdoor and outdoor tamper-resistant construction.

Special ventilating grills allow required cooling air to flow in and out of the case but block the passage of rain, fine spray or wind-driven snow

An extra dip and bake of varnish and appropriately located space heater protect against damage to the core and coils from condensation during thermal cycling.

## Cooling on Ventilated Dry Type Units



Small Units


Large Units
Forced air cooling is available on all units 300 Kva and above. With air blast equipment in operation the units have forced cooled ratings of 133 percent of the selfcooled rating. Single phase 230 volt fan motors are turned on or off by a Type TRC winding temperature relay.

## Hot Spot Relay


included on all AA/FA units and available as an optional accessory on AA units, the Hot Spot Relay indicates winding hot spot temperature.

The Hot Spot Temperature is an indication of the load being carried by the iransformer. Alarm contacts are furnished to signal overload conditions. On fan cooled units, a separate set of contacts turn the fans on when the AA rating is exceeded.
type AA/FA units and available as an optional accessory on ventilated dry type $A A$ self-cooled units.

## Description

The type TRC Opt-i-Therm is a thermocouple actuated, optically isolated temperature indicator and control. The instrument indicates hottest spot temperature in degrees centigrade and provides contacts for starting and stopping cooling fans, operating alarm signals and lights and actuating breaker trip coils or initiating other shut down or load reduction procedures.

The actuating thermocouple is wound into the transformer low voltage coil at the point of highest temperature. The instrument, therefore, indicates the actual hottest spot temperature of the transformer rather than a simulated hot spot temperature from conventional instruments.

The ability of this type TRC relay to more accurately measure hot spot temperatures offers three benefits: 1. The ability to safely and reliably carry heavier overloads. 2. The ability to size a transformer more nearly to the actual load which means lower first cost. 3. More accurate fan control has the benefit of longer transformer life and fewer failures.

## Gas Filled Sealed Dry Type Transformers

Temperature Indicator Hot Gas, Two Switch, Dial Type, Submersible, Direct Mounted


A dial-type thermometer with alarm contacts with maximum resettable indicating hand will be provided. It will indicate the temperature of the gas above the core and coils.

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Type DS Low Voltage
Switchgear Section

Modern design Type DS Low Voltage Metal Enclosed Switchgear and Circuit Breakers provide

- Integral solid-state type breaker tripping systems
- "Metal-clad" safety features
- Two-step stored-energy breaker closing
- Glass polyester insulation
and many other features for coordinated, safe, convenient, trouble-free and economical control and protection of low-voltage distribution systems.



## Ratings

600 volts ac
50 to 4000 Amperes continuous
22,000 to 200,000 amperes interrupting capacity

## Features

Two-Tone Standard Indoor Finish-Pearl gray (ANSI No. 61) with contrasting charcoal gray on breaker compartment doors.

Four Position Drawout-Breakers can be in connected, test, disconnected or remove position with compartment doors closed.

Standard Welded Aluminum Main BusesReduce maintenance. Purchaser's connections are silver plated copper. (All-copper buses optionall.

Wiring Protection-Provided by slotted plastic wiring channels with removable covers, and enclosed steel troughs for interunit cross wiring.

Isolated Incoming Connections-Reduce possibility of fault transmission between incoming source and main bus.

Protection During Levering OperationWhen levering the breaker between the connected, test and disconnected positions, the operator is fully protected by a steel barrier (faceplate) from contact with live parts and from arcs and hot gases.

Two-Step Stored Energy Closing Mecha-nism-Spring charging (1) and spring release to close breaker (2) are independent operations, and always give positive control of the instant of closing.

## Motor Operated Siored-Energy Closing

 Mechanisms are supplied on electrically operated breakers. Standard control voltages are 48, 125 and 250 dc , and 120 and 240 acRemote Closing and Tripping can be accomplished with manually operated breakers, by charging the closing mechanism manually, and ciosing and tripping it remotely through electric spring release and shunt trip coils; available as optional attachments.

## Closing Spring Automatic Discharge-

Mechanical interlocking automatically discharges the closing springs when the breaker is removed from its compartment.

Breaker Inspection-When withdrawn on the rails, breaker is completely accessible for visual inspection: tilting is not necessary. The rails are permanent parts of every breaker compartment.

Current Transformers for metering and instrumentation are mounted in the breaker compartments, and are front accessible. Accuracies meet ANSI Standard C37.20, Section 20-4.6.3 for Low Voltage Metal Enclosed Switchgear.

Integral Solid-State Type Breaker Overcurrent Trip Systems-provide maximum reliability and excellent repeatability, and require minimum maintenance. No external control source is required. Continuous stepless current pickup and time delay adjustments are made with sealed potentiometers, with no fixed taps or bands and no contact corrosion. Two types available: Standard Amptector II-A and Optional Amptector I-A

Ground Fault Tripping is available optionalIr as an integral part of Amptector I-A.

Change in Trip Rating-The overcurrent trip pickup range is established by the rating of the current sensors on the breaker. A continuous long delay pickup adjustment $50 \%$ to $125 \%$ of sensor rating is provided. The sensors can be readily changed to provide a different pickup range.

Glass Polyester Insiulation-Westinghouseproduced glass polyester, with excellent mechanical, dielectric and thermal properties, is used for the insulation system.

Double Steel Safety Barrier in front of each breaker during normal operation provides maximum safety.

Interphase Barriers-on breakers provide maximum insulation security. The barriers are easily removable for breaker inspection.

Provision for Padlocking-All breakers include provision for padlocking open to prevent electrical or manual closing. This padlocking also secures the breaker in the connected, test or disconnected position by preventing levering.

Ease of Inspection and Maintenance-Type DS switchgear and breakers are designed for maximum accessibility and the utmost facility of inspection and maintenance.

Conformity to Standards-Type DS switchgear and breakers conform to the following standards: NEMA SG3 \& SG5; ANSI C37.13, C37.46. C37.17 \& C37.20 (IEEE NO. 27).


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## Metal-Clad Safety Features



Outer door with quick-opening latches closes compartment completely with breaker in or cut. All controls are protected from unauthorized or accidental operation. Full-sized metal shield on breaker face protects operator from live parts, arcs and hot gases while operating, racking or checking Amptector set-
tings. Double interlocked device prevents racking until contacts are open; contacts can't be closed until racking is complete. Separate cable entrance and bus compartments can be provided; removable barriers give access to bus compartment for inspection or cleaning.

Glass Polyester Insulation
Offers far better mechanical, thermal and electrical properties than phenolics. It has the mechanical strength to resist shortcircuit forces; is highly resistant to heat, flame and moisture; and has been designed with generous creepage distances. Often used on 5 Kv and 15 Kv metal-clad switch-gear-Westinghouse gives these materials to you on all insulating parts in Type DS 600 volt switchgear.


Two-step Stored-energy Closing


Gives operator positive control of closing after spring mechanism is charged. Breaker can't close while you're still charging. Operation is op-tional-full manual, full electric, or manual charge and remote electric release.

On manual breakers, the spring mechanism is manually charged by one downward stroke of the lever without pumping, and released by the mechanical 'push-to-close" release button. On electrically operated breakers. the mechanism is normally charged and released electrically, but can be charged manually by pumping an accessory lever 10 to 12 times and released mechanically.

An interlock discharges the closing springs as the breaker is removed from the compartment. The system is patterned after 5 Kv and 15 Kv metalclad switchgear.


DS Breaker Levering Operation


DS Breaker Faceplate


DSL Breakers and Combinations


Type DSL Breakers are coordinated combinations of Type DS breakers and series connected current limiting fuses. They are intended for applications requiring the overload protection and switching functions of air circuit breakers on systems whose available fault currents exceed the in terrupting rating of the breakers alone, and/or the withsiand and interrupting ratings of "downsiream" circuit components.

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## Arc Chute

There are three basic means of extinguishing an arc: lengthening the arc path; cooling by gas blast or contraction; deionizing or physically removing the conduction particles from the arc path. It was the discovery by Westinghouse of this last method which made the first large power air circuit breaker possible.
The De-ion principle is incorporated in all of these circuit breakers. This makes possible faster arc extinction for given contact travel; assures positive interruption and minimum contact burning.

## Levering Mechanism

The worm gear levering mechanism is selfcontained on the breaker drawout element
and engages slots in the breaker compartment. A removable crank is used to lever the breaker between the Connected-TestDisconnected positions.
Mechanical interlocking is arranged so that levering cannot be accomplished unless the breaker is in the tripped position.

## Stored Energy Mechanism

A cam-type closing mechanism closes the breaker. It receives its energy from a spring which can be charged by a manual handle on the front of the breaker or by a universal electric motor.
Release of the stored energy is accomplished by manually depressing a bar on the front of the breaker or electrically energizing a releasing solenoid.

## Contacts

All air circuit breakers have solid block. silver tungsten, inlaid main contacts. This construction insures lasting current-carrying ability, which is not seriously impaired even after repeated fault interruptions or repeated momentary overload.
It is not necessary to provide a substantial margin of safety above the actual circuit load current to prevent contact deterioration.
The main cointacts are of the butt type and are composed of a multiplicity of fingers to give many points of contact without alignment being critical.

All Type DS breakers are available as either manually or electrically operated.


Standard Amptector II-A Solid-State Trip


The Westinghouse Amptector II-A is a solid-state device that provides adjustable overcurrent tripping for Westinghouse Type DS low-voltage a-c power circuit breakers. Only one Amptector II-A is required per breaker, and it receives all its energy from a set of sensors--one mountud on each pole of the breaker. It develops an output for an associated trip actuator when preselected conditions of current magnitude and duration are exceeded.

The device can be supplied in three models or combinations of three independent continuously adjustable overcurrent tripping functions: long delay, short delay and instantaneous.
These models are:
DU (Dual)-Long delay and instantaneous
SE (Selective)-Long delay and short delay
TR (Triple)-Long delay, short delay and instantaneous
Model DU is the basic standard, and will be supplied when not otherwise indicated or required

Amptector II-A Characteristics


## Amprecior I-A and II-A

Each Ampiector includes terminal receptacles to permit easy fiald checking of operation and calibration with an exiernal power supply. A specially designed portable test device with a plug to match the Amprector receptacle is available to provide the utmost in simplicity for checking Amptector operation.

## Available Sensor Ratings

| Breaker | Frame Size. Amperes | Senser Ralinqs. Amperes |
| :---: | :---: | :---: |
| DS.206. DSL-206 or DS 2065 | 800 | $\begin{aligned} & 50,100,150, \\ & 200,300,400 . \\ & 600,800 \end{aligned}$ |
| $\begin{aligned} & \text { DS } 416 \text {. DSL-416 or } \\ & \text { DS } 416 \text { S } \end{aligned}$ | 1600 | 100. 150. 200. <br> 300. 400, 600 <br> 800, 1200. 1600 |
| DS 420 | 2000 | 2000 |
| D5 632 | 3200 | 2400, 3200 |
| 0*840 | 4000 | 4000 |

The narrow-band characteristic curves graphically illustrate the close coordination obtainable in breaker sysiems with Amplector tripping devices. Repeatability within $2 \%$.

The particular breaker current rating for any breaker frame size is determined by the rating of the sensor used.

The breaker current rating for any frame size can be changed by simply changing the sensors, which are easily removed from the breaker drawout element. The wide range of long-delay pickup makes one set of sensors suitable for a number of current ratings The Amptector irself need not be changed when the associated sensors are changed.

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Optional Amptector I-A Solid-State Trip


Offers all of the features of Standard Amptector II-A, plus:

- Integral ground fault protection (optional), with adjustable pickup and delay.
- Resettable operation indicators for Ground, Overload and Short circuit.

Amptector I-A can be supplied in various combinations of four independent continuously adjustable overcurrent tripping functions:

Long delay (L)
Short delay (S)
Instantaneous (I)
Ground (G)
The following combinations are available:

| LI | LIG |
| :--- | :--- |
| LS | LSG |
| LSI | LSIG |

Amptector I-A Characteristics


Model Ll is the basic standard and will be supplied when not otherwise indicated.

Amptector I-A

| Ground Pick-Up Value-Amperes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dial Setting | 50 | 100 | 150 | 200 | 300 | 400 | 600 | $\begin{aligned} & \text { sor R } \\ & 800 \end{aligned}$ | 1200 | 1600 | 2000 | 2400 | 3200 | 4000 | Secondary Current I |
| A | 13 | 57 | 60 | 65 | 80 | 110 | 145 | 180 | 260 | 330 | 400 | 530 | 640 | 800 | 1.0 |
| B | 18 | 67 | 75 | 85 | 110 | 150 | 205 | 260 | 385 | 505 | 600 | 770 | 1000 | 1200 | 1.5 |
| C | 22 | 75 | 85 | 100 | 130 | 185 | 250 | 325 | 480 | 625 | 760 | 960 | 1200 | N.A. | 1.9 |
| D | 33 | 100 | 120 | 145 | 200 | 270 | 385 | 500 | 730 | 970 | 1200 | N.A. | N.A. | N.A. | 3.0 |

All pick up values may vary $\pm 10 \%$
(1) Current of this value from the secondary of an external ground transtormer will cause the ground element to function. Ground element pick-up can aiso be lested using this value. All sensors must be disconnected during test.

## Optional Breaker Attechments and

 Accessories(a) Shunt trip on manually operated breakers, for any standard control voltage. An auxiliary switch is also required.
(b) Auxiliary contacts on manually operated breakers, usually consisting of one 4 contact auxiliary switch. Maximum of three 4 contact auxiliary switches available on any breaker, manually or electrically operated. The contact rating is 10 amperes. (Two 4 contact switches are standard on each electrically operated breaker.)
(c) Compartment position switch ("TOC'), 6 or 12 contact, actuated by movement of drawout breaker between the connected and test positions. Most common uses are for disconnecting remote control circuits of electrically operated breaker, and for bypassing " $b$ " interlocking auxiliary contacts, when breaker is withdrawn to test position.
(d) Undervoltage trip (ac and dc available). Acts to trip the breaker when the Voltage on its solenoid coil is insufficient to restrain a spring-loaded core. The dropout point is within 30 to 60 percent of the nominal coil voltage and is not adjustable. Available as either instantaneous or time delay type. The time delay is within 2 to 7 seconds afte: zero voltage occurs, and is not adjustable. The device automatically resets when the breaker opens; approximately one minute is required for resetting of the sime delay type.
(e) Overcurrent trip switch (OTS). A latching type switch with two independent contacis either normaliy open or normally closed. Operates only when the breaker is tripped automatically on an overload or fauit condition (including Amptector l-A integral ground fault trip ping). It may be used for alarm and/or interlocking circuits. Resetting is done by a pushbutton on the breaker face plate, or by a remote switch through an optional reset coil.
(t) High load switch (HLS-available with Amptector I-A only). A self resetting relay which picks up on an overload condition at a lower value than the long delay
pickup setting of the tripping device, thus, giving advance warning of an overload condition. The device is completely independent of the overcurrent tripping system, does not trip the breaker, and does not replace any protection in any phase. Adjustment is from 60 to 100 percent of the long delay pickup setting. The time delay is fixed and is approximately one minute. One normally open contact is provided.
(g) Electric Lockout (Manual Breakers). in order to close the breaker after manually charging the closing mechanism, it is necessary to operate an electrical pushbutton on the breaker faceplate. This pushbutton is in series with any required external interlocking. The mechanical "push-to-close" bar is made inoperative when the breaker is in the connected position. An electric spring release attachment (operated by the electrical pushbutton), a chargedspring limit switch, and an auxiliary switch are required.
(h) Electric close release on manually operated breakers, for any standard controi voltage. Breaker can be closed by remote control switch or pushbutton after spring is manually charged. A charged-spring limit switch and an auxiliary switch are also required.
(i) Key interlock. Operative only after breaker has been withdrawn beyond

disconnected position. Blocks any breaker from being levered into compartment. Breaker can be stored in compartment, and can be completely removed for maintenance or for use as a spare without disturbing interlock. No modification of breaker required.
(j) Operation counter.
(k) Ac capacitor trip.
(I) Latch check switch.
(m) Mechanical interlock.

## Standard Control Diagram

Standard control diagram for Type DS electrically operated breaker, for ac or dc control source



Terminal Blocks


Current Transformert

## insulation

All insulation is Westinghouse glass polyester, which has been compounded to include the dielectric and mechanical strength necessary for the application. It is highly resistant to heat, flame and moisture, and has been designed with generous creepage distances.

## Bus Isolation

The incoming line is isolated from the main bus to reduce the possibility of fault transmission between them. Bus sections are also isolated at a bus tie breaker.

## Wiring

Enclosed plastic wiring troughs are used throughout the switchgear. Control circuit terminal blocks are mounted on the rear frame where they are readily accessible for purchaser's connections and inspection. Main circuit terminals may be oriented to suit cable entrance

Buses and Connections


1600 and 2000 Ampere Bus and Aisers

Available main bus ratings in Type DS switchgear are 1600, 2000, 3200, 4000 and 5000 amperes. All ratings are based on a standard temperature rise of $65^{\circ} \mathrm{C}$ above
a maximum ambient air temperature of $40^{\circ} \mathrm{C}$ outside of the switchgear enclosure.

Details of standard bare welded aluminum main buses, in conjunction with silver

3200. 4000 and 5000 Ampere Bus and Risers


Bus and Cable Compgrtment with Barriers Removed

The rear portion of the switchgear assembly houses the main bus, connections, and terminals.

A ground bus is furnished the full length of the switchgear assembly and is fitted with terminals for purchaser's connections.
plated copper for shipping breaks and for field connections, are shown above.

Optional bare copper main buses with silv, plated bolted joints are available.


Cable Connection Compartment with Barriers in Place

Type RCT Meter Type Current Transformers for Mounting in Circuit Breaker Compartments

| For Breaker Type* |  |  |  |  | ANSI Meter Accuracy Classification |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DS-206 | DS. 416 | DS-420 | DS-632 | DS. 840 | Ratio | B-0.1 | 8-0.2 |
|  |  |  |  |  | 100/5 | 1.2 | - |
|  |  |  |  |  | $150 / 5$ $200 / 5$ |  | 1.2 |
|  |  |  |  |  | 300/5 | 0.6 | 0.6 |
|  |  |  |  |  | 400/5 | 0.6 | 0.6 |
|  |  |  |  |  | 600/5 | 0.6 | 0.6 |
| + |  |  |  |  | 800/5 | 0.3 | 0.3 |
|  |  | 4 |  |  | 1200/5 | 0.3 | 0.3 |
|  |  |  |  |  | 1500/5 | 0.3 | 0.3 |
|  |  |  |  |  | $1600 / 5$ $2000 / 5$ | 0.3 0.3 | 0.3 0.3 |
|  | 1 |  |  |  |  |  |  |
|  |  |  |  |  | $\begin{aligned} & 2500 / 5 \\ & 3000 / 5 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | 0.3 0.3 |
|  |  |  |  | 1 | 4000/5 | 0.3 | 0.3 |
|  |  |  |  |  | $5000 / 5$ $6000 / 5$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ |
| - Also for Types DSL-206, DSL-416. DSL-632 and DSL-840 limiter type equipments. |  |  |  | 1 |  | , |  |
| Current transformers with meter accuracy classifications at higher burdens and/or suitable for relaying are also available. They will be mounted in. the rear cable connection compartment. |  |  |  |  |  |  |  |

## Control Voltages and Currents

Standard control voltages, rated control currents and standard ranges are as follows:

| Controt Voltage | 48 Dc | 125 Dc | 250 Dc | 120 Ac | 240 Ac |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Close current (SR). amp. | 5.0 | 2.0 | 1.0 | 3.0 | 2.0 |
| Shumt trip current, amp. | 5.0 | 2.0 | 1.0 | 2.0 | 1.0 |
| Spring charge motor amo. | 7.5 | 3.0 | 1.5 | 3.0 | 1.5 |
| Control voltage range. Close- | 38.56 | $100 \cdot 140$ | 200.280 | 104-127 | 208-254 |
| Trip - | 28-56 | 70-140 | 140.280 | 60.127 | 208-254 |

Motor currents are running currents; inrush is approximately $400 \%$. Motor running time to charge spring approximately 5 seconds.

## Potential Transformers

Potential transformers are rated 10 Kv BIL. and are protected by both primary and secondary fuses. The primary fuses are dead front safety pullout type, NEMA Class J.

## Control Power Transformers

Control transformers are provided when required for Ac control of circuit breakers, space heaters, and/or transformer fans. Like potential transformers, they are protected by pullout type primary fuses and also secondary fuses.

## Switchgear Accessories

Standard accessories furnished with each Type DS switchgear assembly include:

- One breaker levering crank.
- One manual spring charging lever, if electrically operated breakers are included.
- Insulating covers or 'boots" are furnished on live main stationary disconnecting contacts in compartments equipped for future breakers. One additional set is provided for each size breaker furnished.

Test plugs are furnished when "Flexitest" relays, Flexitest watthour meters or Flexitest Type FT-1 test switches are mounted on the switchgear.

## Miscellaneous

For feeder circuit instrumentation, small 2 inch $2 \%$ accuracy class ammeters and Type W-2 ammeter switches can be mounted on the horizontal stationary panels adjacent to the breaker compartment doors. The ammeters and switches are immediately associated with definite breaker circuits. Other devices, such as control pushbuttons, indicating lights and test switches can be mounted on these panels, within space

limits. Removable covers provide access to wiring.

Interference interlocks are supplied on breakers and in compartments where the compartments are of the same physical size, to insure that a Type DS-206 breaker cannot be inserted into a compartment intended for a Type DS-416 or DS-420 breaker, and a TVpe DS-416 or DS-420 breaker cannot be inserted into a compartment for a Type DS-206 breaker.

Standard wire is Type SIS, stranded copper, polyethylene insulated, No. 14 AWG minimum, with crimped insulation grip ring tongue terminals.

Optional Accessories


- Portable test kit for testing and calibration of Amptector trip devices. Utilizes standard 120 volt, 20 ampere single phase 60 Hz supply, available from any outlet.

Outdoor Type DSO Switchgear


Type DSO outdoor switchgear consists of - Traveling type geared breaker lifter.
standard Type DS indoor structures assembled in a heavy gauge completely weatherproof enclosure, with a generous internal "walk-in" front operating aisle extending through all units of the assembly. A reinforced access door with holder, provision for padlocking and "panic" hardware is provided at each end of the aisle.

Standard features also include:

- Bolted hinged rear doors for access to cable and bus compartments.
- Labyrinth door openings.
- Filtered ventilation openings.
- Space heaters.
- Lighting outets and convenience receptacles.
- Rigid base structure: no channels required.
- Walk-in aisle within shipping group shipped complezely asembled.

The interior finish is similar to indoor switchgear. The standard exterior finish is ANSI No. 24 dark blue-gray. An asphalt coating is provided on the underside and base.

## Metal Enclosed Bus Runs

For connecting outdoor transformers through building walls to indoor switchgear, low voltage metal enclosed buses in ratings from 600 amperes to 5000 amperes are available. These buses can also be used for bus tie circuits between separate low voltage switchgear assemblies.

Design and construction follow Low Voltage Switchgear Standards, with bare alurninum or copper conductors with silver plated bolted joints and glass polyester supports. Momentary ratings (minimum 50,000 amperes) are as required. Standard finish colors are ANSI No. 61 pearl gray indoor and No. 24 dark blue-gray outdoor.

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## Air Interrupter Switch Ratings

Application Data.<br>Dimensions and Weights

## Transformer Primary Fuse Application

Primary Power Switch, Type PPS
(for liquid transformers only)

- $15 \mathrm{Kv}, 95 \mathrm{Kv}$ BIL (fuse voltage to suit application).
- 600 A continuous and load interrupting.
- 61,000 A asymmetrical momentary. 40,000 A asymmetrical fault close rating.

Load Interrupter Switch, Type WLI
(standard for Ventilated Dry and Gas Filled transformers: optional for liquid transformers)

- $5 \mathrm{Kv}, 60 \mathrm{Kv}$ BIL, and $15 \mathrm{Kv}, 95 \mathrm{Kv}$ BIL.
- 600 A and 1200 A continuous and load interrupting.
- Momentary ratings 40,000 A and 80.000 A asymmetrical.
- Fault close in ratings 20,000 A, 40,000 A and 61,000 A asymmetrical

| System Circuit Volts | Fuse Data Identification |  |  | Interrupting Rating |  | Max. Transf. Kva Rating (1) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Type | Kv | Maximum Amperes | Amperes Symm. | Equiv. <br> 3 Ph. Mva | Self Cooled | Forced Air |
| 2400 | CLE- 1 <br> CLE-2 <br> RBA-200 <br> RBA 400 <br> RBA-800 | $\begin{aligned} & 2.4 \\ & 2.4 \\ & 8.3 \\ & 8.3 \\ & 8.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 225 X \\ & 450 X \\ & 200 \mathrm{E} \\ & 400 \mathrm{E} \\ & 720 \mathrm{E} \end{aligned}$ | $\begin{aligned} & 50.000 \\ & 40.000 \\ & 19,000 \\ & 37,500 \\ & 37,500 \end{aligned}$ | $\begin{aligned} & 205 \\ & 165 \\ & 80 \\ & 150 \\ & 150 \\ & \hline \end{aligned}$ | $\begin{array}{r} 670 \\ 1335 \\ 600 \\ 1190 \\ 2140 \end{array}$ | $\begin{array}{r} 780 \\ 1560 \\ 695 \\ 1385 \\ 2500 \end{array}$ |
| 4160 | CLE-1 <br> CLE-2 <br> RBA-200 <br> RBA-400 <br> ABA. 800 | $\begin{aligned} & 5.5 \\ & 5.5 \\ & 8.3 \\ & 8.3 \\ & 8.3 \end{aligned}$ | $\begin{aligned} & 225 X \\ & \text { 450X } \\ & 200 E \\ & 400 E \\ & 720 E \end{aligned}$ | $\begin{aligned} & 50,000 \\ & 50,000 \\ & 19.000 \\ & 37.500 \\ & 37.500 \end{aligned}$ | $\begin{aligned} & 360 \\ & \mathbf{3 6 0} \\ & 137 \\ & 270 \\ & 270 \end{aligned}$ | $\begin{aligned} & 1155 \\ & 2315 \\ & 1030 \\ & 2055 \\ & 3700 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1350 \\ & 2700 \\ & 1200 \\ & 2400 \\ & 4320 \end{aligned}$ |
| 4800 | CLE-1 <br> CLE-2 <br> ABA-200 <br> RBA-400 <br> RBA. 800 | $\begin{aligned} & 5.5 \\ & 5.5 \\ & 8.3 \\ & 8.3 \\ & 8.3 \end{aligned}$ | $\begin{aligned} & 225 X \\ & 450 X \\ & 200 E \\ & 400 E \\ & 720 E \end{aligned}$ | $\begin{aligned} & 50.000 \\ & 50,000 \\ & 19,000 \\ & 37.500 \\ & 37.500 \end{aligned}$ | $\begin{aligned} & 415 \\ & 415 \\ & 158 \\ & 310 \\ & 310 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1335 \\ & 2675 \\ & 1190 \\ & 2375 \\ & 4280 \end{aligned}$ | $\begin{aligned} & 1560 \\ & 3120 \\ & 1385 \\ & 2775 \\ & 5000 \end{aligned}$ |
| 6900 | CLE-1 <br> CLE-2 <br> RBA- 200 <br> RBA 400 <br> RBA. 800 <br> CLT | $\begin{aligned} & 8.3 \\ & 8.3 \\ & 8.3 \\ & 8.3 \\ & 8.3 \\ & 8.3 \end{aligned}$ | $\begin{aligned} & 125 \mathrm{E} \\ & 200 \mathrm{E} \\ & 200 \mathrm{E} \\ & 400 \mathrm{E} \\ & 720 \mathrm{E} \\ & 300 \mathrm{C} \end{aligned}$ | $\begin{aligned} & 50.000 \\ & 40.000 \\ & 16.600 \\ & 29.400 \\ & 29.400 \\ & 50.000 \end{aligned}$ | $\begin{aligned} & 600 \\ & 480 \\ & 200 \\ & 350 \\ & 350 \\ & 600 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1065 \\ & 1705 \\ & 1705 \\ & 3415 \\ & 6150 \\ & 2560 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1245 \\ & 2000 \\ & 2000 \\ & 3985 \\ & 7170 \\ & 2985 \end{aligned}$ |
| 7200 | CLE-1 <br> CLE-2 <br> RBA-200 <br> RBA. 400 <br> RBA-800 <br> CLT | $\begin{aligned} & 8.3 \\ & 8.3 \\ & 8.3 \\ & 8.3 \\ & 8.3 \\ & 8.3 \end{aligned}$ | $\begin{aligned} & 125 E \\ & 200 \mathrm{E} \\ & 200 \mathrm{E} \\ & 400 \mathrm{E} \\ & 720 \mathrm{E} \\ & 300 \mathrm{C} \end{aligned}$ | $\begin{aligned} & 50.000 \\ & 40.000 \\ & 16.600 \\ & 29.400 \\ & 29.400 \\ & 50.000 \end{aligned}$ | $\begin{aligned} & 625 \\ & 500 \\ & 205 \\ & 365 \\ & 365 \\ & 625 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1115 \\ & 1785 \\ & 1785 \\ & 3565 \\ & 6420 \\ & 2670 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1300 \\ & 2080 \\ & 2080 \\ & 4160 \\ & 7500 \\ & 3110 \\ & \hline \end{aligned}$ |
| 12.000 | CLE-1 <br> CLE-2 <br> CLE-3 <br> RBA-200 <br> RBA-400 <br> CLT | $\begin{aligned} & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \end{aligned}$ | $\begin{aligned} & 65 E \\ & 125 X \\ & 200 x \\ & 200 E \\ & 400 E \\ & 175 \mathrm{C} \end{aligned}$ | 85.000 85.000 <br> 50.000 <br> 14.400 <br> 29.400 <br> 50.000 | $\begin{aligned} & 1770 \\ & 1770 \\ & 1040 \\ & 300 \\ & 610 \\ & 1040 \\ & \hline \end{aligned}$ | 905 1745 2790 2970 5945 2595 | $\begin{aligned} & 1030 \\ & 1985 \\ & 3175 \\ & 3465 \\ & 6930 \\ & 3025 \\ & \hline \end{aligned}$ |
| 12.470 | CLE-1 <br> CLE- 2 <br> CLE-3 <br> RBA-200 <br> RBA-400 <br> CLT | $\begin{aligned} & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \end{aligned}$ | $\begin{array}{r} 65 E \\ 125 \mathrm{X} \\ 200 \mathrm{x} \\ 200 \mathrm{E} \\ 400 \mathrm{E} \\ 175 \mathrm{C} \end{array}$ | $\begin{aligned} & 85.000 \\ & 85.000 \\ & 50.000 \\ & 14.400 \\ & 29.400 \\ & 50.000 \end{aligned}$ | $\begin{aligned} & 1835 \\ & 1835 \\ & 1080 \\ & 310 \\ & 635 \\ & 1080 \\ & \hline \end{aligned}$ | $\begin{array}{r} 940 \\ 1810 \\ 2900 \\ 3085 \\ 6170 \\ 2695 \\ \hline \end{array}$ | $\begin{aligned} & 1070 \\ & 2060 \\ & 3300 \\ & 3600 \\ & 7200 \\ & 3140 \\ & \hline \end{aligned}$ |
| 13.200 | CLE-1 <br> CLE-2 <br> CLE- 3 <br> RBA. 200 <br> RBA-400 <br> CLT | $\begin{aligned} & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \end{aligned}$ | $\begin{gathered} 65 E \\ 125 X \\ 200 X \\ 200 E \\ 400 E \\ 175 C \end{gathered}$ | 85.000 <br> 85.000 <br> 50,000 <br> 14,400 <br> 29.400 <br> 50.000 | $\begin{aligned} & 1945 \\ & 1945 \\ & 1145 \\ & 330 \\ & 670 \\ & 1145 \end{aligned}$ | $\begin{aligned} & 1000 \\ & 1920 \\ & 3070 \\ & 3265 \\ & 6530 \\ & 2855 \end{aligned}$ | $\begin{aligned} & 1935 \\ & 2180 \\ & 3490 \\ & 3810 \\ & 7620 \\ & 3330 \end{aligned}$ |
| 13,800 | CLE-1 <br> CLE 2 <br> CLE-3 <br> RBA-200 <br> RBA-400 <br> CLT | $\begin{aligned} & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \\ & 15.5 \end{aligned}$ | $\begin{gathered} 65 E \\ 125 X \\ 200 x \\ 200 \mathrm{E} \\ 400 \mathrm{E} \\ 175 \mathrm{C} \end{gathered}$ | 85,000 85.000 <br> 50.000 <br> 14.400 <br> 29.400 <br> 50,000 | $\begin{aligned} & 2030 \\ & 2030 \\ & 1195 \\ & 330 \\ & 670 \\ & 1195 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1045 \\ & 2000 \\ & 3200 \\ & 3415 \\ & 6830 \\ & 2985 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1185 \\ & 2280 \\ & 3650 \\ & 3985 \\ & 7970 \\ & 3480 \end{aligned}$ |

Type CLE Current Limiting Fuses: Through 7.2 Kv Fuse Rating-
For Self Cooled
Transformers
1.4
1.49
1.4
1.4

| For Forced Air | (1) Maximum Transformer Kva Ratings are based |
| :--- | :---: |
| Transformers | on Ratios of Maximum Fuse Current Rating to |
| 1.2 | Transformer Full Load Curren (lf /r) as listed |
| 1.31 | at Ift. For a $55^{\circ} \mathrm{C}$ Rise Liquid Filled Trans- |
| 1.2 | former use the Kva Rating for $65^{\circ} \mathrm{C}$ rise |
| 1.2 | $\left(55^{\circ} \mathrm{C}\right.$ rating $\left.\times 1.12\right)$. |

Type RBA Expulsion Type Non-Current Limiting Fuses, all RatingsType CLT Curren: Limiling Fuses. all Ratings

These apolications are subject to modification when specific factors such as Transformer Characteristics. These applications are suber Protective Devices. Coordination Requirements and Load Variations may indicate a different if/I: Ratio.

## Dimensions of High Voltage Incoming Line Sections-Inches (Approximate)

Type PPS Air Interrupter Switch (For Liquid Filled Transformer Only)


Type WLI Air Interrupter Switch (Single Units as Shown; See Note for Duplex)

Note: Two (2) units each 33 (or 36) wide, with iwo (2) cable areas, required for duplex arrangements.

| Unit <br> Depth C | Cable Sp. <br> F(I.D.) | Cable So. <br> G(O.D.i |
| :--- | :--- | :--- |
| (1) 49.28 | 16.97 | 15.84 |
| (3) 55.28 | 22.97 | 21.84 |
| 30 | 27.69 | 26.56 |
| 62 | 29.69 | 28.56 |
| 70 | 37.69 | 36.56 |
| 80 | 47.69 | 46.56 |

(1) Provides $18^{\prime \prime}$ max. stress cone space for top entrance.
(2) Required for add'l stress cone space for top entrance, or for $54^{\prime \prime}$ deep dry ivpe trans-
Min for case.
(3) Min for single unit selector type, 5 KV . with bottom entrance; top entrance $70^{\prime \prime}$
Min. for single unit selector type, 15 Kv , with botiom entrance; top entrance 80"
s) Except 15 Kv with 61,000 A (tault close) rating
$36^{\prime \prime}$ wide.

Min. depth with pothead: 5 Kv 49.28; 15 Kv 55.28
For gas filled sealed dry type transformer, refer to Westinghouse

Approximate Weights-Lb
Single unit. 2 pos., unfused; indoor 1500: outdoor
1800. (Use two for Duplex.)

Single unit selector, unfused: indoor 1800 .
outdoor 2100.
Indoor transition-300
Outdoor throat-200
Fuses, set of 3-200.

Cable Entrence Compartment


Front Eievation


Plan

For Liquid Filled Transformer, Indoor or Outdoor


Front Elevation
For Ventilated Dry Transformer

Height and Depth of Compartment same as Trans

Approx. Weight 300 Lb .

3 Phase Transformer Secondary Ampare Ratings

|  |  | Liquid Filled $55 / 65^{\circ} \mathrm{C}$ Rise |  |  | Liquid Filled $65^{\circ} \mathrm{C}$ Rise |  | Ventilated Dry $150^{\circ} \mathrm{C}$ Rise |  | Sealed Dry $150{ }^{\circ} \mathrm{C}$ Rise |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Kva | Sec. Volts | OA $55^{\circ}$ | OA $65^{\circ}$ | FA 65 ${ }^{\circ}$ | OA | FA | AA | FA | AA |
| 300 | $\begin{aligned} & 208 \\ & 240 \\ & 480 \\ & 600 \end{aligned}$ | $\begin{aligned} & 833 \\ & 722 \\ & 361 \\ & 289 \end{aligned}$ | $\begin{aligned} & 933 \\ & 808 \\ & 404 \\ & 323 \end{aligned}$ | 二 | $\begin{aligned} & 833 \\ & 722 \\ & 361 \\ & 289 \end{aligned}$ | - | $\begin{aligned} & 833 \\ & 722 \\ & 361 \\ & 289 \end{aligned}$ | $\begin{aligned} & 1191 \\ & 962 \\ & 481 \\ & 385 \end{aligned}$ | $\begin{aligned} & 833 \\ & 722 \\ & 361 \\ & 289 \end{aligned}$ |
| 500 | $\begin{aligned} & 208 \\ & 240 \\ & 480 \\ & 600 \end{aligned}$ | 1389 1203 601 481 | 1556 1347 674 539 | - | 1389 1203 601 481 | 二 | 1389 1203 601 481 | 1852 1604 802 641 | $\begin{aligned} & 1389 \\ & 1203 \\ & 601 \\ & 481 \end{aligned}$ |
| 750 | $\begin{aligned} & 208 \\ & 240 \\ & 480 \\ & 600 \end{aligned}$ | 2083 1804 902 722 | 2333 2021 1011 808 | 2683 2324 1162 929 | $\begin{aligned} & 2083 \\ & 1804 \\ & 902 \\ & 722 \end{aligned}$ | 2396 2075 1038 830 | 2083 1804 902 722 | $\begin{aligned} & 2778 \\ & 2406 \\ & 1203 \\ & 962 \end{aligned}$ | $\begin{aligned} & 2083 \\ & 1804 \\ & 902 \\ & 722 \end{aligned}$ |
| 1000 | 208 240 480 600 | 2778 2406 1203 962 | 3111 2695 1347 1077 | 3578 3099 1549 1239 | 2778 2406 1203 962 | 3194 2767 1383 1106 | 2778 2406 1203 962 | 3704 3208 1604 1283 | $\begin{aligned} & 2778 \\ & 2406 \\ & 1203 \\ & 962 \end{aligned}$ |
| 1500 | $\begin{aligned} & 480 \\ & 600 \end{aligned}$ | 1804 1443 | $\begin{aligned} & 2021 \\ & 1616 \end{aligned}$ | 2324 1859 | $\begin{aligned} & 1804 \\ & 1443 \end{aligned}$ | $\begin{aligned} & 2075 \\ & 1659 \end{aligned}$ | $\begin{aligned} & 1804 \\ & 1443 \end{aligned}$ | $\begin{aligned} & 2406 \\ & 1924 \end{aligned}$ | $\begin{aligned} & 1804 \\ & 1443 \end{aligned}$ |
| 2000 | $\begin{aligned} & 480 \\ & 600 \end{aligned}$ | $\begin{aligned} & 2406 \\ & 1924 \end{aligned}$ | $\begin{aligned} & 2695 \\ & 2155 \end{aligned}$ | $\begin{aligned} & 3099 \\ & 2478 \end{aligned}$ | $\begin{aligned} & 2406 \\ & 1924 \end{aligned}$ | $\begin{aligned} & 2767 \\ & 2213 \end{aligned}$ | $\begin{aligned} & 2406 \\ & 1924 \end{aligned}$ | $\begin{gathered} 3208 \\ 2565 \end{gathered}$ | $\begin{aligned} & 2406 \\ & 1924 \end{aligned}$ |
| 2500 | $\begin{aligned} & 480 \\ & 600 \end{aligned}$ | $\begin{aligned} & 3008 \\ & 2406 \end{aligned}$ | $\begin{aligned} & 3368 \\ & 2694 \end{aligned}$ | $\begin{aligned} & 4211 \\ & 3367 \end{aligned}$ | $\begin{aligned} & 3008 \\ & 2406 \end{aligned}$ | $\begin{aligned} & 3759 \\ & 3008 \end{aligned}$ | $\begin{aligned} & 3008 \\ & 2406 \end{aligned}$ | $\begin{aligned} & 4010 \\ & 3208 \end{aligned}$ | $\begin{aligned} & 3008 \\ & 2406 \end{aligned}$ |

## Transformer Standards

## Dimensions and Weights as listed in the Tables are based on the following:

1. Standard Base Kva Ratings: 300-500-750-1000-1500-2000-2500.
2. 3 Phase, 60 Hertz, Two Windings.
3. Standard Temperature Rise (See Tables) above ambient air temperature of $40^{\circ} \mathrm{C}$ ( $104^{\circ} \mathrm{F}$ ) maximum and $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$ average in any $\mathbf{2 4}$-hour period.
4. Maximum Altitude of 1000 meters above sea level for full rating ( 3300 feet).
5. Standard High Voltages: 2400-4160-4800-6900-7200-12000-12470-1320013800, delta connected only.
6. Standard High Voltage Taps: two approximately $21 / 2 \%$ full capacity above and two below rated voltage.
7. Standard Low Voltages (no taps):(1) 208y/120 (1000 Kva max.) 240 delta (1000 Kva max.) 480 delta (all ratings) 480y/277 (all ratings)
8. Aluminum Winding Conductors.
9. No Series-Parallel or Delta-Wye Terminal Boards.
10. Standard Accessories.
11. Standard Surface Preparation, Finish Processes, Materials and Colors.
12. Standard Tests in accordance with ANSI Standard Test Code (see below).
13. HV and LV Basic Impulse Levels, Impedance and Sound Levels in line with the following Tables.
(1) 600 Y and $600 \triangle$ also available.

Standard Insulation Levels-Kı BIL

| High Voltage Rating | Liquid HV | Filled Tiransformer <br> LV ( 600 Max.) | $\begin{aligned} & \text { Vent. Dry } \\ & \text { HV } \end{aligned}$ | Transformer LV ( 600 Max. ) |  | Filled Transformer <br> LV ( 600 Max .) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2400 | 45 | 30 | 25 | 10 | 45 | 30 |
| 4160 | 60 | 30 | 25 | 10 | 60 | 30 |
| 4800 | 60 | 30 | 25 | 10 . - | 60 | 30 |
| 6900 | 75 | 30 | 35 | 10 | 75 | 30 |
| 7200 | 75 | 30 | 35 | 10 | 75 | 30 |
| 12000 | 95 | 30 | 50 | 10 | 95 | 30 |
| 12470 | 95 | 30 | 50 | 10 | 95 | 30 |
| 13200 | 95 | 30 | 50 | 10 | 95 | 30 |
| 13800 | 95 | 30 | 50 | 10 | 95 | 30 |

## Standard Guaranteed Sound Levels-Decibols

| Max. Base Kva <br> (Self Cooled) Liquid <br> OA FA | Vent. Dry Transformer <br> AA | FA | Gas Filled Transformer <br> AA |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 300 | 55 | - | 58 | 67 | 57 |
| 500 | 56 | - | 60 | 67 | 59 |
| 750 | 58 | 67 | 64 | 67 | 63 |
| 1000 | 58 | 67 | 64 | 68 | 63 |
| 1500 | 60 | 67 | 65 | 69 | 64 |
| 2000 | 61 | 67 | 66 | 71 | 65 |
| 2500 | 62 | 67 | 68 | 71 | 66 |

## Transformer Kva Ratings, 3 Phase

In addition to their basic self-cooled (AA or OA, $100 \%$ ) Kva ratings, modern Westinghouse standard Secondary Unit Substation Transformers of the liquid filled and
ventilated dry types are designed for continuous operation at the following supplementary self-cooled and fan-cooled (FA) Kva ratings:

| Liquid Fiiled |  |  |  |  |  | Ventilated Dry Type |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $55 / 65^{\circ} \mathrm{C}$ Rise |  |  |  | $65^{\circ} \mathrm{C}$ Rise |  | $\begin{aligned} & 150^{\circ} \mathrm{C} \\ & \text { AA } \\ & \text { Rating } \end{aligned}$ | $\begin{aligned} & 150^{\circ} \mathrm{C} \\ & \mathrm{FA} \\ & \text { Rating } \end{aligned}$ |
| OA $55^{\circ} \mathrm{C}$ | OA $65^{\circ} \mathrm{C}$ | FA $55^{\circ} \mathrm{C}$ | FA $65^{\circ} \mathrm{C}$ | OA | FA |  |  |
| 300 | 336 | - | - | 300 | - | 300 | 400 |
| 500 | 560 | - | - | 500 | - | 500 | 667 |
| 750 | 840 | 862 | 966 | 750 | 862 | 750 | 1000 |
| 1000 | 1120 | 1150 | 1288 | 1000 | 1150 | 1000 | 1333 |
| 1500 | 1680 | 1725 | 1932 | 1500 | 1725 | 1500 | 2000 |
| 2000 | 2240 | 2300 | 2576 | 2000 | 2300 | 2000 | 2667 |
| 2500 | 2800 | 3125 | 3500 | 2500 | 3125 | 2500 | 3333 |

[^6]| impedances ( $\pm 71 / 2 \%$ Tolerance): |  |  |  |
| :---: | :---: | :---: | :---: |
| Kva | Vent-Dry Transformer | Gas Filled Transformer | Liquid Filled Transformer |
| 300 | (2) | 5.0\% | 5.0\% |
| 500 | 5.75\% | 5.0\% | 5.0\% |
| 750 | 5.75\% | 5.75\% | $5.75 \%$ |
| 1000 (1) | 5.75\% | 5.75\% | 5.75\% |
| 1500 | 5.75\% | 5.75\% | 5.75\% |
| 2000 | 5.75\% | 5.75\% | 5.75\% |
| 2500 | 5.75\% | 5.75\% | 5.75\% |
| (1) $8.0 \%$ impedance standard as alternate. if requested, at 480 volts low voltage |  |  |  |
|  |  |  |  |

## ANSI Stendard Tests

1. Resistance measurements.
2. Ratio tests.
3. Polarity and phase relation.
4. No-load loss.
5. Exciting current.
6. Impedance and load loss.
7. Applied potential test.
8. Induced potential test.
9. Temperature test or tests will be made on one unit of an order, covering one or more units of a given rating. Tests will be made only when there is no available record of a temperature test per ANSI Standards on a duplicate or essentially duplicate unit.

Transformer Dimensions and Waights-Inches (Approximate)


Gas Filled Dry Type, $150^{\circ} \mathrm{C}$ Temperature Rise, Low Voltage 600 Maximum, Indoor or Outdoor


## Application-Type DS Air Circuit Breakers

## Standards

Type DS circuit breakers meet or exceed all applicable requirements of the latest ANSI Standards C37.13 and C37.16

## System Voltage and Frequency

Type DS breakers are designed for operation on Ac systems only, 60 Hz or 50 Hz , 600 volts maximum.

## Continuous Current Ratings

Unlike transformers, generators and motors, circuit breakers are maximum-rated devices and have no built-in temporary overload current ratings. Consequently, it is vital that each application take into consideration the maximum anticipated current demand, initial and future. including temporary overloads.

The continuous rating of any Type DS breaker is limited to $125 \%$ of the sensor rating, or the frame size current rating. whichever is the lesser. For instance, a Type DS-416 1600 ampere frame breaker with 800 ampere sensors has a maximum con-tinuous-rating of 800 times 1.25 or 1000 amperes, but the same breaker with 1600 ampere sensors is limited to 1600 amperes maximum.

All current ratings are based on a maximum ambient air temperature of $40^{\circ} \mathrm{C}$ ( $104^{\circ} \mathrm{F}$ ) outside of the switchgear enclosure.

## Altitude

The breakers are applicable at their full voltage and current ratings up to a maximum altitude of 6600 feet ( 2000 meters) above sea level. When installed at higher altitudes, the ratings are subject to correction factors in accordance with IEEE and NEMA Standards.

## Repetitive Duty

Repetitive breaker opening and closing. such as in frequent motor starting and stopping. are covered by ANSI Standards C37.13 and C37.16. These Standards list the number of operations between servicing (adjusting. cleaning, lubrication, tightening, etc.) and the total numbers of operations under various conditions without requiring replacement of parts, for the various breaker frame sizes.

For motor starting duty, when closing starting currents up to $600 \%$ and opening running currents up to $100 \%$ of the breaker frame size, at $80 \%$ power factor or higher, the endurance or total operations (not requiring parts replacement) will be as follows:

Type DS-206_1400
Type DS.416- 400
The frequency of operation should not ex ceed 20 starts in 10 minutes or 30 in one hour.

## Unusual Environmental and Operating Conditions

Special attention should be given to applications subject to the following conditions

1. Damaging or hazardous fumes, vapors, etc.
2. Excessive or abrasive dust.

For such conditions, it is generally recommended that the switchgear be installed in a clean, dry room, with filtered and/or pressurized clean air. This method permits the use of standard indoor switchgear, and avoids the derating effect of non-ventilated enclosures.
3. Salt spray, excessive moisture, dripping, etc.

Optional drip-proof top covers and space heaters in indoor switchgear, or outdoor weatherproof enclosures, may be indicated, depending upon the severity of the conditions.
4. Excessively high or low ambient temperatures.

For ambient temperatures exceeding $40^{\circ} \mathrm{C}$, and based on a standard temperature rise of $65^{\circ} \mathrm{C}$. the continuous current ratings of breaker frame sizes, and also buses, current transformers, etc.. will be subject to a derating factor calculated from the following formula:
$\sqrt{\frac{105^{\circ} \mathrm{CTotal}-\text { Special Ambient. }{ }^{\circ} \mathrm{C}}{105^{\circ} \mathrm{C} \text { Total- } 40^{\circ} \mathrm{C} \text { Standard Ambient }}}$


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The circuit breakers are not adversely affected by very low outdoor ambient temperatures, particularly when energized and carrying load currents. The standard space heaters in weatherproof switchgear will raise the temperature slightly and prevent condensation.
5. Abnormal vibration or shock.

Applications involving such conditions should be referred to Westinghouse with complete data.
6. Abnormally high repetitive and frequency of operation.

In line with "Repetitive Duty" above, a lesser number of operations between servicing, and more frequent replacement of parts, may be indicated.

## System Application

Tables 3A through 3D on Pages 37 and 38 list the calculated secondary short circuit currents and applicable main secondary and feeder breakers for secondary unit substation switchgear.

The short circuit currents are calculated by dividing the transformer basic ( $100 \%$ ) rated amperes by the sum of the transformer and primary system impedances, expressed in "per unit." The transformer impedance percentages are standard for most secondary unit substation transformers. The primary impedance is obtained by dividing the transformer base ( $100 \%$ ) Kva by the primary short-circuit Kva. The motor contributions to the short circuit currents are estimated as approximately 4 times the motor load amperes, which in turn are based upon 50\% of the total load for 208 voits and $100 \%$ for all other voltages.

Higher transformer impedances and/or lower percentages of motor loads will reduce the short circuit currents correspondingly. Supplementary transformer ratings (see Tables on Page 40) will not increase the short circuit currents, provided the motor loads are not increased.

The Tables do not apply for 3 phase banks of single phase distribution transformers, which usually have impedances of $2 \%$ to $3 \%$ or even lower. The short circuit currents must be recalculated for all such applications and the breakers selected accordingly.

## Main Tranaformer Secondary Breakers

 Transformer secondary breakers are required or recommended for one or more of the following purposes:1. To provide a one-step means of removing all load from the transformer. The NEC limits the maximum number of feeder breakers on a transformer bus without a main breaker to six (6).
2. To provide transformer overload protection in the absence of an individual primary breaker, and/or when primary fuses are used.
3. To provide the fastest clearing of a short circuit in the secondary main bus.
4. To provide a local disconnecting means, in the absence of a local primary switch or breaker, for maintenance purposes.
5. For automatic or manual transfer of loads to alternate sources, as in double ended secondary selective unit substations.
6. For simplifying key interlocking with primary interrupter switches.

Main secondary breakers as selected in Tabies 3A thru 3D have adequate interrupting ratings, but not necessarily adequate continuous current ratings. They should be able to carry continuously not oniy the anticipated maximum continuous output of the transformer, but also any temporary overloads.

Maximum capabilities of transformers of various types, in terms of Kva and secondary current, are given on Pages 40 and 42. It will be noted that the maximum ratings will often require the substitution of larger frame main breakers than those listed in Tables. Even if a self-cooled transformer only is considered, it should be remembered that with ratings of 750 Kva and higher (except for gas-filled transformers), provision for the future addition of cooling fans is automatically included. It is recommended that the main breaker have sufficient capacity for the future fan-cooled rating, plus an allowance for overloads if possible, particularly since load growth cannot always be predicted.

The same considerations should be given to the main bus capacities and main current transformer ratios.

## Bus Sectionalizing (Tie) Breakers

The minimum recommended continuous current rating of bus sectionalizing or tie breakers, as used in double ended secondary selective unit substations or for connecting two single ended substations, is one-half that of the associated main breakers. The interrupting rating should be at least equal to that of the feeder breakers. It is common practice to select the tie breaker of the next frame size below that of the main breakers. However, many users and engineers prefer that the tie breaker be identical to and interchangeable with the main breakers, so that under normal conditions it will be available as a spare main breaker.

The tie breaker should be equipped with the same type of tripping devices (long and short delay or long delay and instantaneous) as the main breakers.

## Generator Breakers

In most applications where generators are connected through breakers to the secondary bus, they are used as emergency standby sources only, and are not synchronized or paralleled with the unit substation transformers. Under these conditions, the interrupting rating of the generator breaker will be based solely on the generator Kva and sub-transient reactance. This reactance varies with the generator type and Rpm, from a minimum of approximately $9 \%$ for a 2 pole 3600 Rpm turbine driven generator to $15 \%$ or $20 \%$ or more for a medium or slow speed engine type generator. Thus the feeder breakers selected for the unit substation will usually be adequate for a standby generator of the same Kva as the transformer.

Most generators have a 2 -hour $\mathbf{2 5 \%}$ overload rating, and the generator breaker must be adequate for this overload current. Selective type long and short delay trip devices are usually recommended for coordination with the feeder breakers, with the long delay elements set at $125 \%$ to $150 \%$ of the maximum generator current rating for generator protection.

In the case of two or more paralleled generators, Type CRN-1 antimotoring reverse power relays are recommended for protection of the prime movers, particularly piston type engines. For larger generators requiring Type DS-632 or DS-840 breakers. Type COV voltage-restraint type overcurrent relays are recommended.

Type DS Breaker Sensor Selection Guide for Resistance Welding Applications


Resistance Welding Feeder Breakers The application of Type DS breakers to resistance welding circuits is shown on the Sensor Selection Guide.

Sensor ratings only are given; the breaker frame will also be as required for interrupting ratings.

Type DS breaker solid state tripping devices are well suited for this service, since the chattering, noise, wear and calibration changes experienced in electro-mechanical devices are eliminated.

These applications are based on Amptector II-A or Amptector I-A long delay and instantaneous trip devices with the following settings:

Long delay pickup 1.0 times sensor rating Long delay time 36 seconds.
Instantaneous trip setting 2 times average weld amperes (during-weld amperes times percent duty cycle) or higher.

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## Feeder Breakers-General

Circuit breakers for feeder circuit protection may be manually or electrically operated, with long and short delay or long delay and instantaneous type trip devices, and trip settings, as required for the specific circuit and toad requirements.

Feeder breakers as selected in Tables 3A thru 3D have adequate interrupting ratings, and are assumed to have adequate continuous current ratings for maximum load demands.

General purpose feeder breakers, such as for lighting circuits, are usually equipped with long delay and instantaneous trip devices, with the long delay pickup set for the maximum load demand in the circuit. Where arcing fault protection is required, the instantaneous trip setting should be as low as practicable consistent with inrush requirements.

## Motor Starting Feeder Breakers

These breakers are usually electrically operated, with long delay and instantaneous tripping characteristics for motor running, locked rotor and fault protection.
The breaker sensor rating should be chosen so that the long delay pickup can be set at $125 \%$ for motors with a 1.15 service factor or at $115 \%$ for all other motors.

When system short circuits are less than 40 times the motor full load current, the motor breaker tripping characteristic should include a short delay characteristic for greater fault protection.

## Group Mator Feeder Breakers

Typical loads for such circuits are motor control centers. The feeder breakers may be either manually or electrically operated as preferred, and are usually equipped with long and short delay trip devices for coordination with the individual motor circuit devices. The minimum long delay pickup setting should be $115 \%$ of the running current of the largest motor in the group plus the sum of the running circuits of all other motors.

## Ground Fault Protection With Westinghouse Amptector I-A Static Trip

## Distribution Systoms

The power distribution in three phase low voltage systems can be three or four wire distribution. The three wire distribution can be served from either delta or wye sources, but the four wire distribution is obtained from wye source only. Fig. No. 1 shows three wire distribution with delta source and Fig. No. 2 shows three wire distribution with wye source. It is significant on Fig. No. 2, that the wye connection of a transformer secondary does not necessarily mean four wire distribution in switchgear. This is worthwhile to note because four wire distribution is quite frequently assumed when the transformer secondary is wye connected. The low voltage system is three phase four wire distribution only if a fourth wire is carried through the switchgear and single phase loads are connected to feeder breakers. This fourth wire is the neutral bus. The neutral bus is connected to the neutral of the wye connected transformer secondary as shown on Fig. No. 3. The standard neutral bus capacity is one half of the phase bus current carrying capacity but full capacity neutral busses are also available on request.

Three or four wire systems can be grounded or ungrounded in service. Generally where the source is delta connected it is ungrounded, but in some very rare cases it is grounded at one corner of the delta or at some other point. When the source is wye connected it can be grounded or ungrounded and when grounded the grounding is at the neutral. When low voltage systems are grounded they are generally solidly grounded. However occasionally the grounding is through a resistor. Three and four wire solidly grounded systems are shown on Fig. No. 4 and 5. At present the new installations are mostly solidly grounded or ungrounded low voltage systems with a definite trend toward the increase of the solidly grounded systems. An ungrounded low voltage system is a good operating system if it is equipped with a ground detection device and if the operators and maintenance crew are trained to locate the initial ground and clear it as soon as practical. The grounded neutral system results in a ground current as soon as any ground occurs on a phase conductor and if the current exceeds the setting of the protective device it will operate and isolate the fault.

Need For Ground Fault Protection
If the magnitude of all ground currents would be large enough to operate the short delay or instantaneous elements of the phase overcurrent trip devices there would be no problem in solidly grounded systems. Unfortunately this is not the case, because low magnitude ground currents are quite common. Low level ground currents can exist if the ground is in the winding of a motor or a transformer or if it is a high impedance ground. Low level ground currents may also be due to an arcing type ground. The arcing type grounds are the source of the most severe damages to electrical eqiupment. The lower limit of the arcing ground currents is unpredictable and the magnitude may be considerably below the setting of the breaker phase overcurrent trip devices.

Since the breaker phase overcurrent trip devices cannot provide fast protection against low magnitude ground faults there is a need for an additional protective device. This additional device is not to operate on normal overloads and it is to be sensitive and fast enough to protect against low magnitude grounds. It is also important that this additional ground protecting device be simple and reliable. The Westinghouse Amptector I-A solid-state tripping system including an optional "ground element" will assure good ground fault protection.

## The Ground Element

The ground element of the solid-state trip is part of the Amptector I-A and is in addition to the usual phase protection. The ground element has a continuously adjustable pickup with calibrated marks as shown in Table 2 and a continuously adjustable time delay with calibrated marks at 0.22-0.35-0.50 seconds. The input current to the Amptector I-A terminals can be provided by:
(a) Residual connection of phase sensors with residual circuit connected to ground element terminals. This is the Westinghouse East Pittsburgh Low Voltage Switchgear standard ground protection system. This produces pickup values as shown in Table 2.
(b) External ground sensing current transformer directiy connected to ground element terminals. This is one of the unique features of the Westinghouse Amptector. This means that this external ground sensor will trip the breaker on grounds without the use of external relay and without the application of a breaker shunt trip and external power source. The lower the CT ratio the more sensitive the ground fault protection.

## Ground Fault Protection Application and

## Coordination

In well designed systems the continuity of service is very important. For reliable service continuity selective tripping is applied between main tie and feeder breakers and the downstream protecting devices for phase to phase faults. Similar selective tripping is desirable when breakers trip on grounds. The application of ground protection on main breakers only may assure good ground protection, however it will not provide good service continually because the main breaker will trip on grounds which should have been cleared by feeder breakers. When the switchgear itself feeds the loads directly the applied ground protection must be such that on a load circuit ground the associated feeder breaker wil trip first. Therefore for proper protection and for good service continuity main tie and feeder breakers all should be equipped with ground protection. Ground protection is not required for non-automatic tie breakers having no phase overcurrent protection.

The necessary coordinated tripping is not easily accomplished when the switchgear feeds into downstream sub-distribution panels which do not have ground protection. If full selective tripping is required the downstream protecting devices should also be equipped with ground protection. If not, the system designer will face a coordination problem in obtaining selectivity between the low pickup and fast tripping switchgear breaker ground elements and phase overcurrent protective devices. This is a very difficult problem because of the time-current tripping characteristic of the phase overcurrent protective devices. When such coordination is desired, the ground element pickup must be increased in order to "desensitize" the device. It is obvious that when the ground element is set at its highest setting, valuable protection is lost for low magnitude arcing ground currents. If higher ground element pickup is attempted to achieve coordination with fairly large sized downstream phase devices the ground protection setting approaches the
characteristic of a short time phase element and the ground protection will lose its true meaning and not provide the expected protection.

In view of the above it is evident that properly applied ground protection requires ground elements as far down the system to the loads as practical. For best results down stream molded case breakers should have individual ground protection. This would result in excellent ground protection because ground elements of switchgear and downstream breakers having similar tripping characteristic can be coordinated.

Coordination between switchgear breaker ground elements and downstream branch circuit fuses is not practical. This is due to the basic fact that the blowing of one phase fuse will not clear a ground on a three phase system. The other two phase fuses will let the load "singie-phase" and also continue to feed the ground through the load as shown in Figure 6.


Figure 4. 3 Wire Distribution Solidly Grounded System


Figure 2. 3 Wire Distribution. Wye Source (Ungrounded)


Figure 6.

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Table 2

| Ground Pick-Up Value-Amperes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dial Setting 50 |  | 100 | 150 | 200 | 300 | 400 | $\begin{array}{r} \mathrm{S} \\ 600 \end{array}$ | $\begin{gathered} \text { insor } \\ 800 \end{gathered}$ | ating <br> 1200 | 1600 | 2000 | 2400 | 3200 | 4000 | Secondery Current (1) |
| A | 13 | 57 | 60 | 65 | 80 | 110 | 145 | 180 | 260 | 330 | 400 | 530 | 640 | 800 | 1.0 |
| B | 18 | 67 | 75 | 85 | 110 | 150 | 205 | 260 | 385 | 505 | 600 | 770 | 1000 | 1200 | 1.5 |
| C | 22 | 75 | 85 | 100 | 130 | 185 | 250 | 325 | 480 | 625 | 760 | 960 | 1200 | N.A. | 1.9 |
| D | 33 | 100 | 120 | 145 | 200 | 270 | 385 | 500 | 730 | 970 | 1200 | N.A. | N.A. | N.A. | 3.0 |

All pick up values subject to $\pm 10 \%$ tolerance.
(1) Current of this value from the secondary of an external ground transformer will cause the ground element to function.

The Following Provides Guideline for Ground Fault Protection.

| System | Advantages | Disadvantages | Main Breaker | Tie Breaker | Fdr. Breaker | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Un grounded (3 Wire) | Minimum disturbance to service continuity. Currents for the majority of grounds will be limited to capacitance charging current of the system. Can oderate with the first ground until it is removed during a regular shutdown. | When ground detector shows that a ground exists corrective action must be tak on ot the earliest possible shutdown. However, experionce indicates that this attention is not always possible. Therefore most ungrounded systems operate with one phase grounded through the first unclaared ground. A ground on another part of the system, due to fault impedance. would probably result in low values of current which would not operate a breaker phase trip. and would produce fire damage. | Lamp type ground detector or ground detecting voltmeters without or with pis. If pts. are used a ground alarm relay can be added for remote or local alarm. |  |  | With proper maintenance this system would result in the minimum disturbance to service continuity. |
|  | Ground protection for an ungrounded system |  | Amptector I-A 'DS' ground 3W protection. minimum pick-up. .50 sec. time delay. See SK No. 1 \& No. 6. | Amptector I-A 'DS' ground 3W protection. minimum pick-up. .35 sec. time delay. | Amptector I-A DS' ground 3W protection. minimum pick-up. .22 sec. time delay. See SK No. 18 No. 6. | Ground fault pro. tection on this un grounded system would trip the breaker when the second ground occurs and current exceeds minimum pick-up setting. |
| Solid Grounded | Psychologically safer. Practicaily results in good continuity of service. <br> Isolation of faults automatic through ground protection system: no overvoltages due to terroresonance or switching. | Probability of very high ground current and extensive damage however, normally these high currents are not obtained. Grounds are automatically isolated and continuity of service is interrupted. | Amptector I-A 'DS' standard residual ground protection in $3 W$ systems and source neutral C.T. feeding into Amptector I in 4 wire systems. Minimum pickup. .50 sec . time delay. See SK No. 1. No. 3 \& No. 6. | Amptector I-A 'DS' ground 3W or 4W (as required) fault protection. Minimum pick-up. .35 sec . time delay. | Amplector I-A 'DS' ground $3 W$ or 4W (as required) fault protection. Minimum pick-up. 22 sec. time delay or BYZ current transformer feeding into above Amptector. <br> See SK No. 1. <br> No. 2 \& No. 6. | This is the most common system in use today and as long as it is not necessary to coordinate with phase devices down the line it will give very good main bus and feeder protection. |
| High <br> Resistance Grounded (3 Wire) | Ground fault current is limited. Ungrounding can result in high voitages during switching and this is corrected by high resistance grounding. | Very sensitive detection is required to derect the limited fauit current. Since overvoltage due to switching isn't prevalent on ungrounded low voltage systems high resistance grounding is not required. | Same as for ungrounded except if ground alarm relay is used connect relay across ground. ing resistor. | Same as for ungrounded. | Same as for ungrounded. | This system is very seldom used and is not recommended. |



Neutral for Feeder Breakers Only in 4W System
(3) Adply in 3 Wire Systems for Main Breaker and in 3 or 4 Wire Systems for Feeder Breakers. Note For double ended secondary unit substations ground tault protection should be as indicated on

sketches No. 4 and No. 5 however for this type application the East Pittsburgh Works Low-Voltage Switchgear Department should be consulted for

Sketch 3.
Source Neutral Main Breaker

the actual bill of materials to be used. The appli. cation becomes rather complex if single phase to neutral loads are being served.


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Type DSL Limiter Type Air Circuit Breakers



Type DSL-416 Breaker-Front View

## Application

Type DSL breakers are coordinated combinations of Type DS breakers and series connected current limiters. They are intended for applications requiring the overload protection and switching functions of air circuit breakers on systems whose available fault currents exceed the interrupting rating of the breakers alone, and/or the withstand and interrupting ratings of "downstream" circuit components.

Sizes and Arrangements
Types DSL-206 800 ampere frame and DSL4161600 ampere frame breakers include the limiters integrally mounted on the drawout breaker elements, in series with the upper terminals.

Current limiters used in Types DSL-632 and DSL-840 combinations are mounted on separate drawout trucks in additional equal size compartments either directly above the breaker compartment in the same unit or beside it in an adjacent unit.

## Scope of Fault Interruption

With properly selected and coordinated limiters, it is expected that the breaker itself will clear overloads and faults within its interrupting rating, leaving the limiters intact and undamaged. The limiters will provide fast interruption of fault currents beyond the breaker rating, up to a maximum
of 200,000 amperes symmetrical. Thus, on overloads and faults within the breaker interrupting rating, the breaker protects the limiters; on higher fault currents exceeding the breaker rating the limiters protect the breaker.

## Protection Against Single Phasing

 Loads are protected against single phase operation by interlock arrangements which trip the circuit breaker whenever any one limiter blows. The breaker cannot be reclosed on a live source until there are three unblown limiters in the circuit.On the Types DSL-206 and DSL-416 breakers, the primaries of small auxiliary transformers are connected in parallel with the limiters. The voltage between the ends of an unblown limiter is zero. but when any limiter blows, the associated transformer is energized and (1) operates an indicator identifying the fuse and (2) picks up a sole-
noid which raises the breaker trip bar, holding the breaker trip-free.

The DSL-632 and DSL-840 combinations with separately mounted limiters operate on the same principle except that the solenoid operates a micro-switch which trips the breaker electrically through a shunt trip coil

## Safoty Features

The integral fuses on Types DSL-206 and DSL-446 breakers are inaccessible until the breaker is completely withdrawn from its compartment, thereby assuring complete isolation.

Likewise, the Type DSL-632 and DSL-840 fuses are inaccessible until the separate fuse truck is completely withdrawn and the fuses isolated. The fuse truck is key interlocked with the breaker to prevent withdrawing or insertion unless the breaker is open.

## Current Limiting Type Breakers and Combinations

| Type | DSL-206 | DSL-416 | DSL-632 | DSL-840 |
| :--- | ---: | ---: | ---: | ---: |
| Frame Size, Amperes | 800 | 1600 | 3200 | 4000 |
| Max. Interrupting Rating, <br> RMS Symm. Amp., System <br> Voltage 600 or Below |  |  |  |  |

Notes: DSL-206 and OSL. 416 include limiters integral with drawout breaker elements. DSL-632 includes DS-632 breaker and DS- 3200 drawout fuse truck, in separate interlocked compartments. Maximum continuous rating
above breaker compartment in same unit. DSL-840 includes DS-840 breaker and DS. 4000 drawout fuse truck, in separate interlocked compartments. Maximum interrupting rating limited to 150,000 amperes when 6000A fuses are used

Limiter Ratings and Characteristics




Average Mall Thims

Curve 3



Curves Nos. 1 through 6 illustrate the ratings, melting time-current characteristics and current limiting or let-through characteristics of limiters for Type DSL breakers.

The let-through current for a given limiter application is readily determined from Curve No. 2, No. 4 or No. 6, by extending a vertical line from the applicable maximum available symmetrical fault amperes at the bottom margin to the characteristic line for the particular limiter, and from this intersection extending a horizontal line to the left margin and reading the peak current. The withstand rating of any circuit elements protected by the limiters should be at least equal to this peak current.

It will be noted that the let-through current increases with the limiter size or ampere rating; in other words, the maximum current limiting effect is obtained with the smallest size. This effect is to be expected, since the resistance decreases as the rating increases. If the vertical line from the bottom margin as described in the previous paragraph does not intersect the limiter characteristic line, it is indicated that the available system fault current is below the "threshold" current of that limiter, and it will offer no current limiting effect.

The current limiting principle is illustrated on Curve 7.

Curve 7: Current Limiting Effect of Type DSL Limiters

$I_{1}=$ The Available Peak Fault Current
$\mathrm{t}_{\mathrm{m}}=$ The Melting Time
$I_{p}=$ The Peak "Let Through" Current
$t_{0}=$ The Arcing Time
$t_{c}=$ The Total Interrupting (Clearing) Time
Limiter Selection
The selection of a suitable limiter rating for a given application is generally governed by a choice of the following types of protection:
A. Maximum protection of "downstream" components. Type DSL breakers are often used for this purpose even when the maximum available fault currents are within the interrupting rating of the corresponding Type DS unfused breakers.
B. Protection of the circuit breaker only.

Case $A$ would tend to use the smallest avaitable limiter; Case $B$ the largest. When downstream protection is required, the selection is usually a compromise, since certain small limiters cannot be coordinated with the breaker to avoid nuisance blowing on overloads or small and moderate short circuits.

Minimum, recommended, and maximum limiter sizes for Type DSL-206 and DSL416 breakers are given in the following table.

| Breaker | Sensor <br> Rating <br> Amperes | Limiter Rating. Amperes <br> Recom- <br> Rype |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  | T) | (2) | (3) |  |
| DSL-206 | 50 or 100 | 150 | 1200 | 2000 |
| DSL-206 | 150 | 200 | 1200 | 2000 |
| DSL-206 | 200 | 250 | 1200 | 2000 |
| DSL-206 | 300 | 400 | 1200 | 2000 |
| DSL-206 | 400 | 600 | 1200 | 2000 |
| DSL-206 | 600 | 800 | 1200 | 2000 |
| DSL-206 | 800 | 1200 | 1600 | 2000 |
| DSL-416 | 600 | 800 | 2000 | 3000 |
| DSL-416 | 800 | 1000 | 2000 | 3000 |
| DSL-416 | 1200 | 2000 | 2500 | 3000 |
| DSL-416 | 1600 | 3000 | 3000 | 3000 |

3) For use only when protection of downstream equipment is required. Not completely coodinated with breaker to avoid nuisance blowing.
(2) Lowest rating which can be coordinated with breaker to minimize nuisance blowing.
(3) Highest available ratings, for protection of breaker only.

Fuse Time-Current Characteristics Curves are available from the nearest Westinghouse Sales Office or the Switchgear Division.

## Application of Type DS Air Circuit Breakers

With Standard 3 Phase Transformers-LLiquid Fillod, Ventilated Dry, and Gas Filled Sealed Dry Types
Table 3


| Transformer Baso (100\%) Rating |  |  | Socondary Short-Circuit Currents RMS Symmetrical Ampares |  |  | Breakers for Selective Trip Systems |  | Breakers for Non- <br> Selective Trip Systems |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Kva and Percent Impedance | Amperes | Maximum Short Circuit Kva Available from Primary System | Through Tranaformer Only | Motor Contribution | Combined | Main Breaker Short Delay Trip | Feeder Breaker Short Delay Trip | Fesder Breaker Instantaneous Trip | Main Breaker Instantaneous Trip | Foeder Breaker Instantaneous Trip |
| Table 3C: 480 Volts 3 Phase-100\% Motor Load |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 500 \\ & 5.0 \% \end{aligned}$ | 601 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 10000 \\ & 10900 \\ & 11300 \\ & 11600 \\ & 11800 \\ & 12000 \end{aligned}$ | 2400 | $\begin{aligned} & 12400 \\ & 13300 \\ & 13700 \\ & 14000 \\ & 14200 \\ & 14400 \end{aligned}$ | DS-206 (3) | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | DS-206 DS-206 DS-206 DS-206 DS-206 DS-206 | DS-206 ${ }^{(2)}$ | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ |
| $\begin{aligned} & \mathbf{7 5 0} \\ & \mathbf{5 . 7 5 \%} \end{aligned}$ | 902 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 12400 \\ & 13990 \\ & 144400 \\ & 14900 \\ & 15300 \\ & 157000 \end{aligned}$ | 3600 | $\begin{aligned} & 16000 \\ & 17500 \\ & 18000 \\ & 18500 \\ & 18900 \\ & 19300 \end{aligned}$ | DS-416 | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | $D S-206$ $D S-206$ $D S-206$ $D S-206$ $0 S-206$ $D S-206$ | DS.416 | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ |
| $\begin{aligned} & \text { 10000 } \\ & 5.75 \% \end{aligned}$ | 1203 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 15500 \\ & 17800 \\ & 18700 \\ & 19600 \\ & 20200 \\ & 20900 \end{aligned}$ | 4800 | $\begin{aligned} & 20300 \\ & 22600 \\ & 23500 \\ & 24400 \\ & 25000 \\ & 25700 \end{aligned}$ | DS-416 ${ }^{(3)}$ | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS } 206 \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | DS-416 ${ }^{(3)}$ | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ |
| $\begin{aligned} & 1500 \\ & 5.75 \% \end{aligned}$ | 1804 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | 20600 24900 26700 28400 29800 31400 | 7200 | $\begin{aligned} & 27800 \\ & 32100 \\ & 33900 \\ & 35600 \\ & 377000 \\ & 38600 \end{aligned}$ | DS.420 (2) | $\begin{aligned} & \text { DS.206 } \\ & \text { DS } 2065 \\ & \text { DS } 206 S \\ & \text { DS } 2065 \\ & \text { DS } 2065 \\ & \text { DS-206S } \end{aligned}$ | $\begin{aligned} & \text { DS } 206 \\ & \text { DS } 206 \mathrm{~S} \\ & \text { DS } 2065 \mathrm{~S} \\ & \text { DS } 2065 \\ & \text { DS } 206 \mathrm{~S} \\ & \text { DS } 2065 \end{aligned}$ | DS-420 (2) | DS 206 <br> DS-206S <br> DS-206S <br> DS.206S <br> DS-206S <br> DS-206S |
| $\begin{aligned} & 2000 \\ & 5.75 \% \end{aligned}$ | 2406 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 24700 \\ & 31000 \\ & 34000 \\ & 36700 \\ & 39100 \\ & 41800 \end{aligned}$ | 9600 | $\begin{aligned} & 34300 \\ & 40600 \\ & 43600 \\ & 46300 \\ & 487000 \\ & 514000 \end{aligned}$ | DS-632 (3) | $\begin{aligned} & \text { DS }-206 S \\ & \text { DSS } 206 \mathrm{~S} \\ & \text { DS.416 } \\ & \text { DS.416 } \\ & \text { DS.416 } \\ & \text { DS-416S } \end{aligned}$ | $\begin{aligned} & \text { DS-206S } \\ & \text { DS } 206 \mathrm{~S} \\ & \text { DS-416 } \\ & \text { DS.416 } \\ & \text { DS-416 } \\ & \text { SS.416S } \end{aligned}$ | DS-632 ${ }^{(3)}$ | DS-206S DS. 206 S DS -416 DS. -416 DS -416 DS $416 S$ |
| $\begin{aligned} & \mathbf{2 5 0 0} \\ & 5.75 \% \end{aligned}$ | 3008 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \\ & \hline \end{aligned}$ | 28000 36500 40500 44660 48100 52300 | 12000 | 40000 <br> 48500 <br> 52500 <br> 60100 <br> 64300 | DS-632 ${ }^{(3)}$ | DS.416 DS.416 DS $-416 S$ DS D.416S DS.416S | DS.416 DS.416 DS DS $416 S$ DS DS $416 S$ DS | DS-632 (3) | DS.416 DS.416 DS.416S DS.416S DS.416S DS.416S |
| Table 3D: 600 Volts 3 Phase- $100 \%$ Motor Load |  |  |  |  |  |  |  |  |  |  |
| $500 \%$ | 481 | 50000 100000 150000 250000 500000 Unlimited | $\begin{aligned} & 8000 \\ & 8700 \\ & 9000 \\ & 9300 \\ & 9400 \\ & 9600 \end{aligned}$ | 1900 | 9900 10600 10900 11200 11300 11500 | DS-206 | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | DS-206 DS-206 DS-206 DS-206 DS-206 DS-206 | DS-206 | $\begin{aligned} & \text { DS-206 } \\ & \text { DS- } 206 \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ |
| $\begin{aligned} & 750 \\ & 5.75 \% \end{aligned}$ | 722 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 10000 \\ & 11100 \\ & 11600 \\ & 11900 \\ & 12200 \\ & 12600 \end{aligned}$ | 2900 | 12900 <br> 14000 <br> 14500 <br> 14800 <br> 15500 | DS-206 (3) | $\begin{aligned} & \text { DS-206 } \\ & \text { DS } 206 \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | $\begin{aligned} & \text { DS. } 206 \\ & \text { DS. } 206 \\ & \text { DS. } 206 \\ & \text { DS. } 206 \\ & \text { DS. } 206 \\ & \text { DS. } 206 \end{aligned}$ | DS-206 (3) | $\begin{aligned} & \text { DS. } 206 \\ & \text { DS- } 206 \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ |
| $\begin{aligned} & 1000 \\ & 5.75 \% \end{aligned}$ | 962 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimitad } \end{aligned}$ | $\begin{aligned} & 12400 \\ & 14300 \\ & 15000 \\ & 15600 \\ & 16200 \\ & 16700 \end{aligned}$ | 3900 | 16300 <br> 18200 <br> 18900 <br> 20100 <br> 20600 | DS-416 | $\begin{aligned} & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | $\begin{aligned} & \text { DS- } 206 \\ & \text { DS } 206 \\ & \text { DS-206 } \\ & \text { DS. } 206 \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ | DS-416 | $\begin{aligned} & \text { DS } 206 \\ & \text { DS. } 206 \\ & \text { DS-206 } \\ & \text { DS-206 } \\ & \text { DS-206 } \end{aligned}$ |
| $\begin{aligned} & 1500 \\ & 5.75 \% \end{aligned}$ | 1443 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 16500 \\ & 20000 \\ & 21400 \\ & 22700 \\ & 23900 \\ & \mathbf{2 5 1 0 0} \end{aligned}$ | 5800 | $\begin{aligned} & 22300 \\ & 25800 \\ & 27200 \\ & 28500 \\ & 29700 \\ & 30900 \end{aligned}$ | DS-416 ${ }^{(3)}$ | $\begin{aligned} & \text { DS. } 206 \\ & \text { DS } 206 \\ & \text { DS.206 } \\ & \text { DS } 206 \\ & \text { DS } 206 \\ & \text { DS-206S } \end{aligned}$ | $\begin{aligned} & \text { DS. } 206 \\ & \text { DS-206 } \\ & \text { DS } 206 \\ & \text { DS }-206 \\ & \text { DS } 206 \\ & \text { DS.206S } \end{aligned}$ | DS-416 ${ }^{\text {(3) }}$ | $\begin{aligned} & \text { DS.206 } \\ & \text { DS }-206 \\ & \text { DS } 206 \\ & \text { DS } 206 \\ & \text { DS } 206 \\ & \text { DS }-2065 \end{aligned}$ |
| $\begin{aligned} & 2000 \\ & 5.75 \% \end{aligned}$ | 1924 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 19700 \\ & 24800 \\ & 27200 \\ & 29400 \\ & 31300 \\ & 33500 \end{aligned}$ | 7700 | 27400 32500 34900 37100 39000 41200 | DS-420 (3) | $\begin{aligned} & \text { DS-206 } \\ & \text { DS.206S } \\ & \text { DS.206S } \\ & \text { DS.206S } \\ & \text { DS.206S } \\ & \text { DS-206S } \end{aligned}$ | DS.206 <br> DS $206 S$ <br> DS $206 S$ <br> DS $206 S$ <br> $0 S$ <br> DS $206 S$ <br>  | DS-420 (3) | DS-206 DS 206 S DS -206 S DS 206 S DS-206S DS-206S |
| $\begin{aligned} & \mathbf{5 5 0 0} \\ & 5.75 \% \end{aligned}$ | 2406 | $\begin{aligned} & 50000 \\ & 100000 \\ & 150000 \\ & 250000 \\ & 500000 \\ & \text { Unlimited } \end{aligned}$ | $\begin{aligned} & 22400 \\ & 29200 \\ & 32400 \\ & 35600 \\ & 38500 \\ & 41800 \end{aligned}$ | 9600 | $\begin{aligned} & 32000 \\ & 38800 \\ & 42000 \\ & 45200 \\ & 48100 \\ & 551400 \end{aligned}$ | - DS-632 ${ }^{(3)}$ | $\begin{aligned} & \mathrm{DS}-206 \mathrm{~S} \\ & \mathrm{DS}-206 \mathrm{~S} \\ & \mathrm{DS}-206 \mathrm{~S} \\ & \mathrm{DS}-416 \mathrm{~S} \\ & \mathrm{DS}-416 \mathrm{~S} \\ & \mathrm{DS}-632 \text { (1) } \end{aligned}$ | $\begin{aligned} & \text { DS } 206 \mathrm{~S} \\ & \text { DS. } 206 \mathrm{~S} \\ & \mathrm{DS}-206 \mathrm{~S} \\ & \mathrm{DS} .416 \mathrm{~S} \\ & \mathrm{DS} .416 \mathrm{~S} \\ & \mathrm{DS}-632 \mathrm{D} \end{aligned}$ | DS.632 (2) | DS-206S DS-206S DS-206S DS.416S DS-416S DS-632 I |

[^7]Typical Metal Enclosed Bus Arrangements



## Bus Dimensions, Inches



## Type DS Indoor Switchgear Dimensions--Inches



[^8](2) Must be panel or blank compt. when breaker in Compt. 8 below is a main breaker.
(3) Must be blank compt. when breaker in Compt C above is a main breaker.

T Max continuous rating with this arrangement 3000A.
; Fuse truck inay also be located in alternate position in compt. beside breaker compt., in adiacent unit. DSL. 632 will have 3200 A max cont, raling.

## Plans <br> 

Space for power and control cables, top and boltom.
Minimum recommended front aisle for braaker
removal:
For DS-206-41 6.420-632-36
For DS-840
For DS-840 or DSL $\quad-44$
For transfer \& titi truck -60
Top-ot-gear mounted breaker iifier
Overall height approximate- 108
Projection front of switchgear- 23.5
Maximum height over lift truck- 110
Minimum recommended rear aisle-24
Section of Typical Breaker Unit


Main Bus 1600A or 2000A

| Unit Depth D (1) |  | Cable Sp. F |  |
| :---: | :---: | :---: | :---: |
| With Bkr. Type DS-206 DS. 416 DS-420 | $\begin{aligned} & \text { With Bkr. } \\ & \text { Type } \\ & \text { DSL-206 } \\ & \text { DSL-416 } \end{aligned}$ | Bkr. <br> Unit <br> (3) | Aux. Unit |
| 54 | 62 | 8 | 14 |
| 60 (3) | 68 (3) | 14 | 20 |
| 66 | 74 | 20 | 26 |
| 72 | 80 | 26 | 32 |
| Main Bus 3200A, 4000A or 5000A |  |  |  |
| Unit Depth D (1) |  | Cable Sp. F |  |
| With Bkr. Type DS-206 <br> DS.416 <br> DS-420 <br> DS-632 | With Bkr. Type OSL-206 DSL-416 DSL-632 DSL-840 DS-840 | Bkr. Unit | Aux. Unit |
| $\begin{aligned} & 60 \\ & 66 \text { (2) } \\ & 72 \end{aligned}$ | $\begin{aligned} & 68 \\ & 74 \text { (2) } \\ & 80 \end{aligned}$ | 9 15 21 | 15 21 27 |

(1) Maximum depth requirement for any unit determines uniform depth of complete assambly.
(2) Minimum recommended depth with 3 or 4 DS-206 (DSL-206) or DS-416 (DSL-416) feeder breakers, initial or future, in same unit. Atso required for metal enclosed bus termination.

Next deeper unit required for Type BYZ zero sequence current transformers, and/or phase current transformers for relaying.
(3) Additional 6 in. available for cables thru floor if bottom compartment is blank.

Type DS Indoor Switchgear WeightsPounds (Approximate)

Stationary Structures


## Shipping Groups

Each shipping group includes a maximum of five (5) breaker and full size auxiliary units, plus one or two standard transition units (Typical Unit 1).

NOTE: For DS-206S and DS-416S space requirements, dimensions and weights use those shown for DS-206 and DS-416 respectively.

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## Specification Guide for <br> Power Centers and Type DS Low Voltage Switchgear

## General

This specification includes an (Indoor) (Outdoor) secondary unit substation complete from the incoming line terminals to the feeder terminals.

The secondary unit substation shall be designed, assembled and tested in accordance with applicable standards of NEMA, IEEE and ANSI.

The following sections shall be included and arranged (left-to-right) (right-to-left) when facing the control side of the switchgear and the nameplate side of the transformer:
incoming Line Section
Transformer Section
Outgoing Low Voltage Switchgear Section.

## Incoming Line Section

Air Interrupter Switch-The HV switch shall be manually operated and rated at 600 (1200A) continuous, load break with fault closing rating of $\qquad$ amperes asymmetrical and a momentary rating of amperes asymmetrical. The switch mechanism shall provide quick closing and opening, independent of the handle speed. When the switch access door is open, a plexiglass or screen barrier shall exist over the area where energized parts may be readily touched.

Switch shall be cable connected to the transformer terminals to prevent transmission of sound to the switch. The switch case shall be made of a minimum of 13 gauge steel.

3-Pole 2-Position-The HV section shall be provided with a gang operated 3 pole, 2 position air-insulated load interrupter switch. The switch compartment shall have a sight window for visual inspection of switch contacts. The switch handle shall be operable from the front of the unit.

Selector Switch-The HV section shall be provided with a gang operated 3 pole, 3 position (open - feeder 1 - feeder 2) selector switch which will consist of a no load selector switch for switching from one feeder to the other on the line side and in series with an air-insulated load interrupter switch. The load interrupter switch must be open before the selector switch can be changed from one feeder to another. The
switch compartment shall have a sight window for visual inspection of switch load contacts. The switch handles shall be operable from the front of the unit. The selector switch handle shall visually indicate tine 1 and line 2.

Dupiex Switch-The HV section shall be provided with a gang operated 3 pole, 2 position duplex switch which will consist of 2 air insulated load interrupter switches connected together on the load side which shall be used for connecting the transformer to one of 2 available feeders. The two switches shall be interlocked to prevent both feeders from being connected to the transformer simultaneously. Each of the 2 switch compartments shall have a sight window for visual inspection of switch contacts. The switch handles shall be operable from the front of the unit.

Fuses-(Three - current limiting
E) (three RBA boric acid $\qquad$ E) fuses are to be provided on the load side of the HV switch in the HV switch compartment. $\qquad$ Kva interrupting capacity required. The hinged access door shall be interlocked with the switch so that the door cannot be opened until the switch is in the open position. Also the switch cannot be closed until the door is closed. The fuses shall have a continuous rating to protect the transformer.

Three spare fusee are to be supplied. (Optional)

Cutouts--The HV section shall consist of 3 -single pole $\qquad$ ampere gang operated oil fused cutouts.
Optional equipment avaiłable:

1. Provide 3 $\qquad$ spare fuse
links for oil fused cutouts.
2. Provide $\qquad$ key interlock(s) to interlock with $\qquad$
Terminal Compartment-The HV section shall consist of a terminal compartment for cable entrance. The terminal connectors shall be located so as to give sufficient space for stress cones.

Lightning Arresters-Provide 3 $\qquad$
Kv (station type) (intermediate) (distribution) arresters for $\qquad$ Kv Igrounded) (ungrounded) service.

Interlocks-Provide $\qquad$ key interlock(s) to interlock with $\qquad$
Terminals-Provide (potheads(s)) (clamp terminals) for termination of the (single feed) (loop feed) $\qquad$ MCM cables. per phase.

## Power Center Coordination-Dimensions in Inches



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## Insulation

The transformer will be of the nonexplosive, fire-resistant, air insulated, dry type construction, cooled by the natural circulation of air through the windings. Solid insulation in the transformer will consist of inorganic materials such as porcelain, glass roving or Nomex in combination with a sufficient quantity of a high temperature binder to impart the necessary mechanical strength to the insulation structure. Such insulation is defined by ANSI Standards as Class H materials.

## Case

The knockdown case for ease in fitting through limited openings will be formed of 13 gauge sheet steel construction equipped with removable panels for access to the core and coils on the front and rear with ornamental ventilating grills. A bolted cover section will be supplied for access to the core and coil lifting loops for lifting the complete assembly.

## Paint Finish

The case will be phosphatized and finished in manufacturer's standard light gray.

Lightning Arresters (optional)
Three low ratio lightning arresters will be mounted in the transformer case and connected to the high voltage leads. They will be for use on a $\qquad$ Kv grounded (ungrounded) system.

## Impedance

The impedance of the transformer at normal rating and frequency will be manufacturer's standard $\pm 71 / 2 \%$ tolerance.

## Ges Filled Sealed Dry Type Transformer Section

The indoor (outdoor) transformer will be rated as follows:

Kva, 3 phase, 60 Hertz, gas filled sealed dry type, $150^{\circ} \mathrm{C}$ rise, with a $220^{\circ} \mathrm{C}$ insulation system.
H.V. $\qquad$ volts. 3 wire. plus two $21 / 2 \%$, minus two $21 / 2 \%$ no load full capacity taps, delta connected.
L.V. $\qquad$ volts. 4 wire ( 3 wire) wye (delta) connected.

High Voltage Lead Facillities
A flange will be provided on the end wall of the tank for attaching the incoming Line Compartment. Flange will be located on the left (right) when facing the front of the transformer.

## Cablo Entrance

The cables shall enter the terminal compartment from the top (bottom).

Low Voltage Lead Facilities
A flange will be provided on the end wali, opposite high voltage flange, for attaching the low-voltage switchgear.

Accessories will include the following:
l-beam base for rolling in any direction. Cover will be welded to the tank flange. Yukon cooler $1 / 4$ inch thick.
Lifting hooks-4 total.
Jack pads- 4 total.
Vacuum pressure gauge.
Dial-type gas thermometer with alarm contact.
$3 / 4$ inch filling plug-2 total.
Diagram nameplate.
Welded handhole cover for access to high voltage and low voltage bushings. De-energized tap changer, externally operated.
Ground pad.
Welded-on main tank cover.

## Impedance

The impedance of the transformer at normal rating and frequency will be $\cdot \% \pm 71 / 2 \%$ tolerance.
( ${ }^{\circ} 5.0 \%$ for 500 Kva and below. $5.75 \%$ for 750 Kva through 2500 Kva).

## Sealed Tank

The transformer will be of sealed tank con struction to prevent breathing. Tank will be hermetically sealed with metallic seals throughout and will be tested at 15 psi pressure. It will be provided with welded-on $1 / 4^{\prime \prime}$ thick Yukon coolers.

## Shot Blast

The case and coolers will be cleaned by shot blast and phosphatized before the paint is applied.

## Finish

Paint finish will be manufacturer's standard, applied over a properly prepared surface.
The color will be light gray ANSI No. 61 (indoor) or drak gray ANSI No. 24 (outdoor).
insulation
The transformer will be of the nonexplosive, tire-resistant, fluorocarbon insulated, dry type construction, cooled by the natural circulation of fluorocarbon through the windings. Solid insulation in the trans-

## Liquid Type Transformer Section

The Indoor (Outdoor) transformer will be rated as follows:

FFA Kve, 3 phase, 60 hertz, OA/ FFA, oil (Silicone) insulated, $65^{\circ} \mathrm{C}$ rise $\left(55^{\circ} \mathrm{C}\right.$ rise) (Complete with $230 \mathrm{~V} 1_{\phi}$ fans, OA/FA, for increased rating to Kva).
HV $\qquad$ volts, 3 wire, plus two $21 / 2 \%$, minus two $21 / 2 \%$ no load full capacity taps, delta connected.
LV _ volts, 4 wire (3 wire) wye (delta) connected.

High Voltage Lead Facilities_-A flange will be provided on the end wall of the tank for attaching the Incoming Line Compartment. Flange will be located on the left (right) when facing the front of the transformer.

Cable Entrance-The cables shall enter the terminal compartment from the top (bottom).

Low Voltage Lead Facilities-A flange will be provided on the end watl, opposite high voltage flange, for atteching the low-voltage switchgear.

Accessories will include the following: Combination drain and filter valve and sampling device.
De-energized tap changer, externally operated. Cover mounted operating handie.
Pressure test connection
1 -inch filling plug and filter press connection in cover
Thermometer, dial type, without (with) alarm contacts
Liquid level gauge, without (with) low level alarm contacts Provision for lifting
Provision for jacking
Pressure relief device, without (with)
alarm contacts. (Silicone only.)
Instruction nameplate
Ground pad
Pressure vacuum gauge
Welded-on main tank cover
Impedance-The impedance of the transformer at normal rating and frequency will be ${ }^{\circ} \% \pm 71 / 2 \%$ folerance.
( $55.0 \%$ for 500 Kva and below, $\cdot \mathbf{5 . 7 5 \%}$ for
750 Kva through 2500 Kva.)

Saaled Tank-The transformer will be of sealed tank construction to prevent breath ing. Adequate gas space will limit the internal pressure due to normal load cycle operation.

Shot Blast-The case and cooling tubes will be cleaned by shot blast or pickling and phosphatized before the paint is applied.

Finish-Paint finish will be manufacturer's standard, applied over a properly prepared surface. The color will be light gray ANSI No. 61 (indoor) or dark gray ANSI No. 24 (outdoor).

Future Capacity-Each 750 Kva through 2500 Kva transformer shall be OA/FFA rated, i.e., include all design and construction capacities for future addition of fans.

## Ventilated Dry Type Transformer Section

The indoor (outdoor), standard or (tamperresistant) transformer will be rated as follows:

Kva, 3 phase, 60 hertz, ventilated dry type, $150^{\circ} \mathrm{C}$ rise, $220^{\circ} \mathrm{C}$ insulation system. (Complete with fans for increased rating to $\qquad$ Kva.) HV volts, 3 wire, with plus two $21 / 2 \%$, and minus two $21 / 2 \%$ no load fuil capacity taps delta connected.
LV $\qquad$ volts, 4 wire ( 3 wire) wye (delta) connected.

High Voltage Lead Facilities
Provisions will be made for connecting the transformer case directly to the high voltage switch housing and the high voltage leads to the high voltage switch.

Low Voltage Lead Facilities
Provisions will be made for connecting the transformer directly to the low voltage switchgear housing and low voltage leads to the switchgear bus.

Accessories will include the following:
Diagram instruction plate
Provision for lifting and jacking
Removable case panel for access to high
voliage taps
Drip proof cover
Ground pad
High Voltage Taps
Tap leads will be terminated at the coils and equipped with provisions for changing taps.

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Type DSO Outdoor Switchgear Dimensions - Inches

former will consist of inorganic materials such as porcelain, glass roving or Nomex in combination with a sufficient quantity of a high temperature binder to impart the necessary mechanical strength to the insulation structure. The transformer will be insulated and cooled with $C_{2} F_{6}$ fluorocarton gas. It will be shipped filled with this $C_{2} F_{6}$ gas to a gauge pressure of approximately $11 / 2$ P.S.I. at $25^{\circ} \mathrm{C}$ ambient.

## Bushings

The transformer will be equipped with rolled flange, inert arc welded bushings for the HV and LV connections to insure that the tank is hermetically sealed.

## Outgoing Low-Voltage Switchgear Section

General-Type DS indoor (outdoor) lowvoltage metal-enclosed switchgear will consist of a stationary structure assembly and one or more removable "De-ion" air circuit breaker units fitted with disconnecting devices and other necessary equipment. The switchgear will be suitable for 600 volts maximum service and will receive a dielectric test for that voltage class in accordance with NEMA standards. It will be designed, manufactured and tested in accordance with the latest standards of IEEE, NEMA, and ANSI.

Stationary Structure-Each steel unit forming part of the stationary assembly will be a self-contained housing having one or more individual breaker or instrument compartments and a rear compartment for the bare buses, and outgoing cable connections. Each circuit breaker compartment will be equipped with primary and secondary contacts, rails, stationary levering mechanism parts, and required instrument current transformers. A blank formed steel door equipped with ventilation openings in the lower flange, an emergency trip buton, and supported on concealed hinges will be provided for each circuit breaker compartment.

The top of the unit will be enclosed with removable steel sheets which include necessary ventilation openings.

The structure will be so designed that future additions may readily be made at any time. The steel structure will be thoroughly cleaned and phosphatized prior to the application of the priming and finishing coats of paint.

A black, a nodized aluminum, engraved circuit designation nameplate $11 / 4$ inches high and $31 / 2$ inches wide will be provided on each circuit breaker door.

Buses and Connections-Each circuit will include the necessary 3 phase bus and connections between the bus and one set of circuit breaker studs. Solderless type terminals on silver-plated copper extensions for the outgoing cables will be provided on the other set of circuit bresker studs. The buses and connections will consist of high-conductivity bare aluminum bar mounted on heavy duty glass polyester supports. The main bus joints will be welded. Shipping breaks and provisions for future bus extensions will have silver-plated bolted connections. MoldartaTM terminal blocks with integral-type barriers will be provided for secondary circuits. The terminal blocks will be mounted at the rear of the units, and will be accessible through a removable cover.

Disconnecting Devices-_The stationary part of the primary disconnecting devices for each circuit breaker will consist of a set of contacts extending through a glass polyester insulating base. Buses and outgoing cable terminals will be directly connected to them. The correspending moving contacts will consist of a set of contact fingers suitably spaced on the circuit breaker studs. In the "connected" position, these contact fingers will engage the stationary contacts forming a current-carrying bridge. The assembly will provide a multitude of silver-to-silver high-pressure point contacts. High uniform pressure on each finger will be maintained by springs. The entire assembly will be full floating and will provide ample flexibility between the stationary and moving elements. Contact engagement will be maintained only in the "connected" position.

The secondary disconnecting devices will consist of floating fingers mounted on the removable unit and engaging flat contact segments located at the rear of the compartment. The secondary disconnecting devices will be silver-plated to insure permanence of contact. Contact engagement will be maintained in the "connected" and "test" positions.

Removable Element- The removable element will consist of a type DS De-ion air circuit breaker equipped with the necessary disconnecting contacts, wheels, and interlocks for drawout application. The removable element will have four position features and will permit closing the compartment door with the breaker in the "connected". "test", "disconnected", and "remove" positions.

Air Circuit Breakers-The air circuit breakers will be type DS (DSL) operating on the Westinghouse De-ion arc interruption. These breakers will incorporate specially designed circuit-interrupting devices which provide high interrupting efficiency and minimize the formation of arc flame and gases.

The air circuit breakers will have silvertungsten butt type contacts which operate under high pressure. The arcing contacts wili be of arc-resisting silver-tungsten. The breaker will be equipped with "De-ion" arc chutes which effectively enclose the arcing contacts and confine the arc to reduce the disturbance caused by short-circuit interruption. Each breaker will be equipped with a position indicator, mechanically connected to the circuit breaker mechanism.

Include when DSL breakers specified above. ( Circuit breakers shall include current limiters, integrally, or separately mounted coordinated with the breaker trip device so as to avoid unnecessary blowing of the current limiters. Breaker shall include an anti single phase device that will trip the breaker in the event of a blown limiter, indicate from the front of the breaker which limiter is blown, and prevent the breaker from being reclosed on a single phase condition, due to missing or blown limiters.)

Each breaker will be equipped with an Amptector II-A (Amptector I-A) solid-state trip. The adjustments will be Long delay pick-up between $50 \%$ and $125 \%$ of the trip rating. Long time delay between 4 and 36 seconds at 6 times trip rating, Short delay pick-up between 4 and 10 times trip rating, Short time delay between 0.18 and 0.5 seconds at 2.5 times Short delay pick-up, instantaneous pick-up between 4 and 12 times trip rating, ground fault (Amptector I-A only) pick-up approximately $20 \%$ of trip rating and ground fault time between 0.22 and 0.5 seconds. Adjustments will be of the continuous type and each will be independent of all the others. All components will be covered with a sealing compound to prevent deterioration in corrosive atmospheres.

It will be possible to test and calibrate the time and current characteristics and trip circuit by means of a portable plug-in test device.

Note: Only those characteristics as required should be specified.

Both electrically operated, and manually operated breakers will have stored energy operating mechanisms. Only one stroke of the operating handle will be necessary to charge the stored energy spring when operating the manual breaker. The release of the energy to close the breaker manually will be by means of a mechanical pushbutton which insures positive control of the closing operation. Electrical close will be initiated by means of a release solenoid.

## Factory Assembly and Tests

The switchgear will be completely assembled, wired, adjusted and tested at the factory. After assembly, the complete switchgear will be tested for operation under simulated service conditions to assure the accuracy of the wiring and the functioning of the equipment.

The main circuits will be given a dielectric test of 2200 volts for one minute between live parts and ground and between opposite polarities. The wiring and control circuits will be given a dielectric test of 1500 volts for one minute between live parts and ground.

Detail Specification
1 -Indoor (Outdoor) low-voltage metalenclosed switchgear assembly including the following equipment:
a. 1-Set of necessary provisions for throat connection or close coupling to the transformer secondary.
b. 1-Set of necessary bare main bus and ground bus connections. (Including full neutral) (including 50\% neutral).
c. ___Current transformers___ $/ 5$ ampere ratio. ( 2 for 3 wire, and 3 for 4 wire with neutral bus in switchgear.)
d. ___ Potential transformers___ /120 volt ratio complete with primary and secondary fuses. ( 2 for 3 wire, and 3 for 4 wire with neutral bus in switchgear.)
e. 1-Ammeter. 0 - $\qquad$ ampere range. 2\% accuracy class.
f. 1-Ammeter switch for reading each phase current.
g. 1-Voltmeter, 0 - $\qquad$ volt range, 150 volt coil, $2 \%$ accuracy class.
h. 1-Voltmeter switch arranged for reading phase to phase (phase to phase and phase to neutral) voltages.
i. 1-Watthour meter 2 element, 3 wire ( $21 / 2$ element, or 3 element, 4 wire) 5 ampere, 120 volt coils.
j. $\qquad$ Main secondary breaker(s), ampere frame, - Amps sym. int. cap. (manually) (electrically) operated with Amptector II-A (Amptector I-A) solid state trips with long delay, short delay (and $\qquad$ wire ground) characteristics.
k.


Tie breaker(s), $\qquad$ ampere frame, - Amps sym. int. cap. (manually) (electrically) operated with Amptector II-A (Amptector I-A) solid state trips with long delay, short delay (and $\qquad$ wire ground) characteristics.
I. $\qquad$ Feeder breakers, $\qquad$ ampere frame, __ Amps sym. int. cap. (manually) (electrically) operated with Amptector II-A (Amptector I-A) solid state trips with long delay, instantaneous (and _ wire ground) characteristics (with integrally mounted current limiters for max. 200,000A int. cap.)
m. Control power transformer complete with primary and secondary fuses for space heaters, lights, receptacles and circuit breaker control as required.
n. Sets of clamp type terminals for $\qquad$ ___ MCM cables per phase and from the bottom (top) of the unit
o. 1-Set of engraved black anodized aluminum nameplates.
p. 1-Set of necessary small wiring, wiring accessories and terminal blocks.
q. 1-Set of space heaters, light and receptacles as required. (Standard for outdoor).

## Caution:

1. (b) Be sure to specify current carrying capacity and arrangement of neutral bus if one is required. Normally $50 \%$ capacity will be supplied if full capacity is not specified.
2. (j-k-1) If trip characteristics other than shown are required please be sure to specify them.

## Accessories

a-1 Top of assembly mounted circuit breaker lifting device (optional)
b- 1 Test plug for wathour meter.
c-1 Levering crank.
Note: Arrangement sketch and single line diagram
similar to following similar to following samples should accompany


Indoor Secondary Unit Substations


# TYPE DS LOW VOLTAGE POWER CIRCUIT BREAKERS 

## Ratings and Characteristics

| Breaker Type | DS-206 | DS-206S | DS-416 | DS-416S | DS-420 | DS-632 | DS-840 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Voltage Rating (AC only) | 600 | 600 | 600 | $\cdots$ | 600 | 600 | 600 | 600 |
| Frame Size (Max. Continuous Amp) | 800 | 800 | 1600 | 1600 | 2000 | 3200 | 4000 |  |

Interrupting Ratings, RMS Symm. Amperes at System Voltages:

|  | $0-240 \mathrm{~V}$ | 42,000 | 50,000 | 65,000 | 65,000 | 65,000 | 85,000 | 130,000 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| A. With | $241-480 \mathrm{~V}$ | 30,000 | 42,000 | 50,000 | 65,000 | 65,000 | 65,000 | 85,000 |
| Instantaneous | 481.600 V | 22,000 | 42,000 | 42,000 | 50,000 | 50,000 | 65,000 | 85,000 |
| Trip |  |  |  |  |  |  |  |  |
|  | $0-240 \mathrm{~V}$ | 30,000 | 42,000 | 50,000 | 65,000 | 65,000 | 65,000 | 85,000 |
| B. With | $241-480 \mathrm{~V}$ | 30,000 | 42,000 | 50,000 | 65.000 | 65,000 | 65,000 | 85,000 |
| Short Delay | $481-600 \mathrm{~V}$ | 22,000 | 42,000 | 42,000 | 50.000 | 50,000 | 65,000 | 85,000 |
| Trip |  |  |  |  |  |  |  |  |

Operating Characteristics-Same for All Types

| Controi Voltage | $24 \mathrm{DC}$ <br> (1) | 48 DC | 125 DC | 250 DC <br> (2) | 115 AC | 230 AC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Close Cursent (SR), Amp. | N. | 5.0 | 2.0 | 1.0 | 3.0 | 1.5 |
| Shunt Trip Current, Amp. | 6.0 | 5.0 | 2.0 | 1.0 | 2.0 | 1.0 |
| Spring Charge Motor, Amp. (3) | NA | 7.5 | 3.0 | 1.5 | 3.0 | 1.5 |
| Cose Voltage Range |  | 40-50 | 90-130 | 180-260 | 95-125 | 190-250 |
| Trip Voitage Range | 14-30 | 28-60 | 70-140 | 14-380 | 95-125 | 190-250 |

(1) Not a recommended voitage.
(2) Check Westinghouse for application at this control voltage.
(3) Running current: inrush approximately $400 \%$.

Spring Charge Time - 5 seconds maximum
Time for Spring to Close Breaker, until contacts touch -4.5 cycies maximum Opening Time with Shunt Trip - 5 cycles maximum

Interrupting Time, at $\mathbf{2 0 0 \%}$ or more of Inst. Pickup - 3 cycies maximum (4)
Interrupting Time, $100 \%$ to $200 \%$ of Inst. Pickup -4 cycles maximum (4)
Arcing Time, Below $50 \%$ of Continuous Rating .6 cyclesmaximum (4)
(4) Add approximately 2 cycles per shunt trip and approximately 4 cycles for instantaneous undervoltage.

# Instructions for <br> Low-Voltage <br> Power Circuit Breakers Types DS and DSL 



READ AND UNDERSTAND THESE INSTRUCTIONS BEFORE ATTEMPTING ANY ASSEMBLY, OPERATION, OR MAINTENANCE OF THE SWITCH

## Westinghouse Electric Corporation

Switchgear Division, East Pittsburgh, Pa. 15112
I.B. 33-790-1E Effective Septernber, 1979 Supersedes Issue Dated April, 1977

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## PURPOSE

This instruction book is expressly intended to cover the installation, operation and maintenance of Low Voltage Power Circuit Breakers, Types DS and DSL.

For application information, consult your nearest Westinghouse sales office, see Westinghouse Descriptive Bulletin 32-850, or appropriate ANSI Standards.

## SAFETY

All Safety Codes, Safety Standards and/or Regulations as they may be applied to this type of equipment must be strictly adhered to.

[^9]
## CAUTION

The circuit breakers described in this book were designed and tested to operate within their nameplate ratings. Operation outside of these ratings may cause the equipment to fail, resulting in bodily injury and property damage.

These instructions cover the description, operation and maintenance of Westinghouse Type DS and Type DSL Low Voltage AC Power Circuit Breakers and Type DS Drawout Fuse Trucks. These breakers are usually supplied as part of low voltage metal enclosed switchgear of the four-position drawout type. These instructions apply only to the circuit breaker and its auxiliary drawout details which have been designed as a completely integrated drawout unit. Type DS Breakers (not DSL) may also be supplied in a fixed mounted version. In this case the sections of this book referring to the levering device, position interlocks, and spring discharge interlock will not apply.

The DS and DSL Circuit Breakers operate on the mag. netic De-ion principle of interruption. In these breakers the arc rises into a series of insulated steel plates. The plates break the rising arc into a series of smaller arcs to cool and extinguish them and funnel the heat to ambient air.

DS and DSL Breakers are available for application at voltages from 208 to 600 Vac ; with continuous currents of 50 to 4000 amps ; and with interrupting capabilities up to $200,000 \mathrm{amps}$. Refer to the breaker nameplate for the complete rating information for any given breaker. Breakers conform to NEMA, ANSI and IEEE standards.

TYPE DS AND DSL BREAKERS ARE PROTECTIVE DEVICES. AS SUCH, THEY ARE MAXIMUM CURRENT RATED DEVICES. THEREFORE, THEY SHOULD NOT UNDER ANY CIRCUMSTANCES BE APPLIED OUTSIDE THEIR NAMEPLATE RATINGS. OPERAtion outside of these ratings may cause THE EQUIPMENT TO FAIL, RESULTING IN BODILY INJURY AND PROPERTY DAMAGE.

The available DS and DSL Breakers and their rated performance capabilities are given in Tables 1 and 2.

Table 1 - Type DS Breaker Ratings

| Breaker <br> Type | Frame <br> Size, Amp. | Interrupting Ratings, RMS Symmetrical Amperes |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | With Instantaneous Trip |  |  | With Short Delay Trip (1)3 |  |  |
|  |  | 208-240V | 480 V | 600 V | 208-240V | 480 V | 600 V |
| DS-206 | 800 | 42,000 | 30,000 | 30,000 | 30,000 | 30,000 | 30,000 |
| DS-206S | 800 | 50,000 | 42,000 | 42,000 | 42,000 | 42,000 | 42,000 |
| DS-416 | 1600 | 65,000 | 50,000 | 42,000 | 50,000 | 50,000 | 42,000 |
| DS-416S | 1600 | 65,000 | 65,000 | 50,000 | 65,000 | 65,000 | 50,000 |
| DS-420 | 2000 | 65,000 | 65,000 | 50,000 | 65,000 | 65,000 | 50,000 |
| DS-632 | 3200 | 85,000 | 65,000 | 65,000 | 65,000 | 65,000 | 65,000 |
| DS-840 | 4000 | 130,000 | 85,000 | 85,000 | 85,000 | 85,000 | 85,000 |

(1) Also short-time ratings.
(1) Short circuit ratings of non-automatic breakers except the DS-840 which is 65,000 .

Maximum voltages at which the interrupting ratings apply are:

| System Voltage | Maximum Voltage |
| :--- | :--- |
| 208 or 240 | 254 |
| 480 | 508 |
| 600 | 635 |

[^10] a 15 -second interval of zero current between the two periods.

Table 2 - DSL Breakers - Current Limiting Type Breakers and Combinations

| Type | DSL-206 | DSL-416 | DSL-632 | DSL-840 |
| :--- | :---: | :---: | :---: | :---: |
| Frame Size, Amperes | 800 | 1600 | 3200 | 4000 |
| Max. Interrupting Rating, |  |  |  |  |
| RMS Symm. Amp., System <br> Voltage 600 or Below | 200,000 | 200,000 | 200,000 | 200,000 |

Notes: DSL-206 and DSL-416 include limiters integral with drawout breaker elements. DSL-632 includes DS-632 breaker and DS-3200 drawout fuse truck, in separate interiocked compartments. Maximum continuous rating limited to 3000A when fuse compartment is above
breaker compartment in same unit. DSL-840 includes DS-840 breaker and DS-4000 drawout fuse truck, in separate interlocked compartments. Maximum interrupting rating limited to 150,000 amperes when 6000A fuses are used.

## GENERAL DESCRIPTION

Westinghouse DS and DSL Circuit Breakers are horizontal drawout magnetic air circuit breakers. They are designed for use in Metal-Clad Switchgear assemblies having maximum voltages of 635 volts AC for DS Circuit Breakers and 600 volts for DSL. They are equipped with springstored, energy-closing mechanisms. All primary insulation to ground is glass polyester. These breakers have many common features, but they will vary in size and detail depending on the specific breaker type number and ratings. Figure 1 shows Type DS Low Voltage Power Circuit Breaker shipped inside its own compartment. Figures 78 and 79 show Types DSL-206 and DSL-416 Circuit Breakers.

Each DS and DSL Circuit Breaker consists of a basic breaker assembly, three interrupter assemblies (arc chutes), barriers, and an Amptector solid-state trip unit. DSL breakers have added current limiters to extend their interrupting range to 200,000 amps. Various accessories are also provided.

## Basic Breaker Assembly

The basic breaker assembly includes a chassis, a control panel, an operating mechanism, a levering-in device, various interlocks, and three insulated pole unit assemblies mounted on a base.

On the front of the breaker are the control items needed for proper operation of the circuit breaker. They are: breaker position indicator, breaker open/closed indicator, levering device shutter and shaft, breaker trip plate, closing spring charged/discharged indicator, Amptector trip test terminal access, Amptector trip controls, closing spring charge handle, close bar and padlock piate.

## Arc Chutes

Each arc chute contains vertical steel splitter plates, insulating spacers and plates. These are all assembled in an insulating arc chute jacket. The arc chutes mount on top of the pole units and are vented to atmosphere.

## Optional Components

Optional components provided upon order are: undervoltage trip attachment, overcurrent trip switch, high-load trip switch, latch check switch, auxiliary switches.

## Accessories

Levering crank and Amptector Test Kit are supplied as required.

Since the major components and the accessories depend on the particular type and rating of circuit breaker, packing lists provided with each shipment and more detailed sections of this instruction book should be referred to for special information. Any questions about the circuit breakers may be referred to the nearest Westinghouse Electric Corp. Sales Office. When making inquiries about type DS (DSL) circuit breakers always provide the specific type number, continuous current rating, mechanism type, applicable order numbers, breaker shop orders or style numbers, date of manufacture and other pertinent information as shown on the circuit breaker nameplate. Inquiries can be handled faster when cornplete information is provided with the initial inquiry.

## Special Circuit Breakers: DS-206S and DS-416S

Table 1 gives the interrupting rating of DS-206S as 42,000 amperes at 600 volts AC. It is an improved model of DS-206, which has an interrupting capacity of 30,000 amperes at 600 volts AC . Yet, the maximum continuous current rating of 800 amperes is the same for both types.

Also, their parts are similar except for these differences:

1. DS-206S uses the three piece base of the DS-416 type, instead of the one piece molded base of the DS-206.
2. DS-206S uses the DS-416 arc chute.
3. DS-206S main disconnects have $50 \%$ more fingers than the DS-206.
4. DS-206S has twice as many main contacts and arms as the DS-206.
5. The pole unit hinge joint of DS-206S is a forked construction or a miniature version of the DS-416 hinge.
6. Fifty ampere sensors cannot be installed on DS-206S; but they can be put on DS-206.

Similarly, the parts of DS-416S are almost identical to those of DS-420. Their interrupting ratings are the same: 65,000 amperes at 480 volts $A C$ and 50,000 amperes at 600 volts $A C$. But, the maximum continuous current rating of DS-420 is 2,000 amperes and for DS-416S it is 1600 amperes.

Compared to Type DS-416, DS-416S has higher interrupting ratings, giving it improved operating flexibility. See Table 1.

## Safety Features

Type DS (DSL) Breakers are manufactured with several built-in interlocks and safety features to reduce hazards and provide proper operating sequences. UNDER NO CIRCUMSTANCES SHOULD THEY BE MADE INOP. ERATIVE AS THIS MAY RESULT IN BODILY $\mathbb{N}$ JURY OR PROPERTY DAMAGE.

1. Positive mechanical indicators on front panel show whether the breaker is open or closed, and whether the closing spring is charged or discharged.
2. Closing Spring Automatic Discharge - Mechanical interlocking automatically discharges the closing springs when the breaker is removed from its compartment.
3. Mechanical interlocking prevents levering of breaker unless its contacts are open. Contacts cannot be closed until the breaker is levered into TEST or CONNECT positions.
4. Mechanical interlocking prevents closing of breaker contacts while it is being levered into or out of its cell, or while it is standing in any intermediate location between the TEST and the CONNECT positions or the DISCONNECT position.
5. Provisions for Padlocking-Breakers can be padlocked open to prevent electrical or manual closing. This padlocking can also secure the breaker in the connected, test, or disconnected position by preventing levering.
6. In the CONNECT position automatic mechanical interlocking prevents the disconnecting or withdrawal of a closed breaker. This avoids drawing dangerous, destructive arcs on the disconnecting contacts when the circuit is energized.
7. In the REMOVE position mechanical interlock system prevents the closing springs from being charged or remaining charged.
8. The integral fuses on Types DSL-206 and DSL-416 breakers are inaccessible until the breaker is completely withdrawn from its compartment, thereby assuring complete isolation.

Likewise, the Type DSL-632 and DSL-840 fuses are inaccessible until the separate fuse truck is completely withdrawn and the fuses isolated. The fuse truck is key interlocked with the breaker to prevent withdrawing or insertion unless the breaker is open.

## Recommended Safety Practices

Type DS circuit breakers are complex electrical devices containing high speed, high energy, operating mechanisms. They are designed to operate within the current and voltage limitations on the breaker nameplate. Do not apply these breakers to systems with currents and/or voltages exceeding these limits.

1. To perform work on Type DS Circuit Breakers requires personnel with training and experience in high voltage circuits. Only qualified electrical workers, familiar with the construction and operation of such equipment and the hazards involved, should be permitted to work on these circuit breakers.
2. Only Qualified Persons as defined in the National Electric Safety Code shouid be permitted to assemble, operate or maintain these breakers.
3. The breakers are equipped with various interlocks. DO NOT MAKE ANY OF THE INTERLOCKS INOPERATIVE AS THIS MAY RESULT IN BODILY INJURY OR PROPERTY DAMAGE.
4. Never put a breaker into a cell without barriers and arc chutes.
5. Always be sure that all switch hardware is in place and bolted tightly before inserting breaker into cell.
6. Do not lift breaker with ordinary crane hooks, ropes, chains, etc., to avoid possible damage to parts or dropping the unit. Use breaker lifting adapter.
7. Use handle on front panel of circuit breaker to move it into or out of cell. Keep fingers and hands off top, bottom or sides of breaker when moving it into or out of cell to prevent bodily injury.
8. When operating breaker without arc chutes and barriers, keep hands, arms, head and tools out of area where contacts travel. Severe bodily injury could result from being struck by the moving contacts either as they open or close.
9. Be sure circuit breaker contacts are open and closing springs are discharged before doing maintenance work.
10. Be sure circuit breaker contacts are open and closing springs are discharged after completing maintenance work.
11. Never leave breaker in an intermediate position in a cell. Always have the breaker either in the disconnect, test or connected position because control circuits may be either improperly connected (or disconnected) and may cause electrical failures.
12. Avoid trip-free type operation because it causes more shock on some parts of breaker than normal closing operations. Refer to last paragraph in Item 4.1.
13. Before operating breaker in test position, be sure that closing the breaker will not cause another electrically interlocked breaker to inadvertently trip.

## Section 1 - Receiving. Handling and Storing

### 1.0 RECEIVING AND HANDLING

The circuit breakers may be shipped completely assembled and inside their respective compartments.

Receiving and handling of this equipment is covered in Westinghouse Instruction Book $\mathbf{3 2 - 6 9 0}$ for Low-Voltage Metal-Enclosed Switchgear, Types DS and DSO.

If the circuit breakers are not shipped in the switchgear assembly, they will be packed separately in individual cartons or crates. These packages must be handled with care to avoid hidden damage to the circuit breakers.

If the circuit breakers have been shipped in the switchgear assembly, proceed as described in Section 2. If the breakers have been shipped in separate packages, remove them from the crate or carton carefully so as not to cause damage. Place the breakers on the switchgear extension rails. (See Section 2.3 before attempting to lift breakers.) Remove the insulating barriers and arc chutes. Inspect the contact structures to be sure no damage has occurred during shipment. Replace the arc chutes and insulating barriers and proceed as described in Section 3.

### 1.1 STORING

If it is necessary to store the equipment before installation, keep it in a clean dry place, protected from dirt and water and with ample air circulation and heat, if necessary, to prevent condensation. Like all electrical apparatus, these units contain insulation. Although it is of highest quality, it, like all other insulation, must be protected against dirt and moisture. Refer to Instruction Book 32.690 - C for details.

## NOTE

Breakers that have been stored or have infrequent operations shall be operated a minimum of five times before being placed in service.

### 1.2 WEIGHTS: CIRCUIT BREAKERS AND FUSE TRUCKS

Table 3 gives the approximate weights of DS and DSL circuit breakers. They will vary slightly due to the differences in functional components of the individual DS Breaker, and the size of the current limiters supplied on DSL Breakers. Fuse truck weights will vary due to differences of fuse sizes.

| Table 3 - Approximate Weights |  |
| :---: | :---: |
| Drawout Elements | Pounds |
| DS-206 Circuit Breaker. | 150 |
| DS-206S Circuit Breaker. | 160 |
| DS-416 Circuit Breaker. . | 195 |
| DS-416S Circuit Breaker. | 200 |
| DS-420 Circuit Breaker. | 200 |
| DS-632 Circuit Breaker. | 300 |
| DS-840 Circuit Breaker. | 400 |
| DSL-206 Circuit Breaker. | 200 |
| DSL-416 Circuit Breaker. | 260 |
| DS-3200 Fuse Truck | 325 |
| DS-4000 Fuse Truck | 430 |

## Section 2 - First Removal of Breaker from Compartment

### 2.0 GENERAL

To examine and become familiar with the construction and operation of the breaker, it first must be withdrawn from the compartment. There are rails provided which permit the breaker to be rolled out of the compartment so that it can be examined on all sides and operated. First unlatch and open the compartment door.

### 2.1 SETTING THE RAILS IN FRONT OF THE COMPARTMENT

Refer to Figures 1 and 2. There are two rails for each breaker compartment which, when not in use, are stored on the inside of the compartment in a back-sloping position. Withdraw each rail completely and let it down into a horizontal position, as shown in Figure 2.

The first movement of the breaker toward the front of the compartment must be done with the levering device.


Fig. 1 The Type DS Low Voltage Power Circuit Breaker is Shipped Inside Its Own Compartment (388880*) - Photo number


Fig. 2 Rails are Stowed away in the Compartment. Withdraw as Shown (383027)

### 2.2 REMOVING SHIPPING BRACE

Before the circuit breaker element can be withdrawn from its compartment for the first time, two shipping braces must be removed from the lower part of the breaker front panel. These braces are small steel angles bolted to the front of the circuit breaker and to the bottom cradle of the circuit breaker compartment.

During shipment, the front wheels of the breaker are lifted approximately $1 / 16$ inch above the compartment rails, and the unit is held part way between DISCON. NECT and TEST positions by means of its levering device and the shipping angle.

1. With a screwdriver, remove the two (2) outside .25-20 panhead screws with captive washers from the bottom leg of the two angles. Do not discard, as later they will be returned to their tapped holes. Do not remove the center screw from the bottom cradle.
2. The levering device is now used to release the breaker from the shipping position. When the breaker is part way between DISCONNECT and TEST positions as described above the breaker levering device interlock will hold the shutter down and the trip plate depressed. The hex shaft of the levering device will be exposed and ready to receive the levering crark handle. See Figure 3. Insert the crank


Fig. 3 Levering Device Crank Handle Installed. Read Section 2.2 on this Operation (391177)
and turn in a counter-clockwise direction and observe the action of the drawout position indicator. The indicator will move down to the REMOVE position at which time the load on the crank handle increases because a stop has been reached.

## NOTE

## DO NOT APPLY FORCE ON THE CRANK HANDLE AFTER THE STOP HAS BEEN REACHED AS THE BREAKER IS NOW FREE.

3. When the position indicator shows the levering device to be in the REMOVE position, remove the hand crank. Pull the breaker out onto the extended rails. This will require more effort than normal as the rear wheels are jammed into the cradle hold-down hooks by two lengths of plastic tubing. Refer to illustrations in the stationary structure Instruction Book $32-690$ covering shipping braces.
4. Remove the two (2) .25-20 panhead screws holding the two shipping angles to the front panel of the breaker. Care must be exercised to prevent marring the front panel. Two or more flat washers are used between the angle and front panel for shipping. Discard the angles.
5. Immediately replace the two panhead screws discarding all washers.


Fig. 4 Use of Breaker Lifting Adapter (391187)
6. With the breaker pulled completely to the end of the rails, remove the two (2) six inch long pieces of split plastic tubing that are on the rear of the stationary rails immediately below the hold-down hooks. This tubing is for shipping purposes only and is to be discarded.
7. The stationary secondary disconnecting contacts are covered by a sheet of insulating material during shipment. This must be removed and discarded before the breaker is moved to the TEST or CONNECTED position.
8. Push the breaker back into its compartment, and replace the two (2) panhead $.25-20$ screws at the front edge of the cradle.

### 2.3 LIFTING THE BREAKER

When it is necessary to lift the breaker off the rails, all lifting should be done only with the accessory lifting adapter. DO NOT ATTEMPT TO LIFT BREAKER WITH ORDINARY CRANE HOOKS, ROPES, CHAINS ETC., AS VITAL PARTS SUCH AS WIRING, BARRIERS AND ARC CHUTE PARTS MIGHT BE DAMAGED. Figure 4 shows a view of the breaker with the lifting adapter in place. The lifter consists essentially of two sheet steel hooks specially shaped to hook under the top edges of the large openings on each circuit breaker side sheet, or in the specially provided lifting lugs on some breakers, and a spreader. Actual lifting may be with a crane, chain block or with the optional lifting mechanism which can be supplied for the switchgear. The breaker must be pulled completely to the end of the rails.

## Section 3-Preliminary Examination of Clrcuit Breaker

### 3.0 GENERAL

Read these instructions carefully and look at the breaker as it stands out of the compartment before trying to operate it. Refer to Figures 5, 6, 7 and 8.

The complete drawout element includes the circuit breaker itself and its auxiliaries. The circuit breaker consists of four major components:

1. The operating mechanism.
2. The contacts, operated by the mechanism.
3. The arc chutes, which interrupt the arc which always results from opening the breaker under load or short circuit conditions.
4. The Amptector ${ }^{\circledR}$ solid-state overcurrent tripping system.

The remainder of the drawout element includes the following auxiliary components:

1. Interphase insulating barriers which isolate the arc chutes from each other and from ground.
2. Drawout element frame and rollers.
3. The levering device, for placing the element into its various positions inside the compartment.
4. The main disconnecting contacts, for connecting the breaker to power source and load.
5. The secondary contacts, for connecting the control circuits to the electrical operating parts of the element.
6. The interlocks, which increase the safety of operation.
7. Drawout element position indicator.


Fig. 5 View Showing Controls on the Panel (391066)


Fig. 6a Left Side of Breaker with Levering Device Arm in REMOVE Position (391065)


Fig. 6b DS 416 Breaker with Front Panel Removed (391070)


Fig. 7 Right Side Showing Levering Device Arm in TEST Position (391068)


Fig. 8 Rear View Showing Levering Device Arm in CONNECT Position (391067)
8. Open-Close indicator.
9. Spring charge indicator.
10. The close bar and trip plate.
11. Steel front cover.
12. Nameplate with complete rating information.

The Type DSL-206 and DSL-416 drawout elements also include the following components:

1. Current limiters.
2. Isolating transformers, connected in parallel with the limiters.
3. Combination "Blown Limiter Indicator" and antisingle phase device, connected to the isolating transformers, actuated by blowing of one or more of the current limiters. This device has individual phase indicators and a common "RESET" button extending through the front cover.

Each breaker is equipped with a spring-type stored energy closing mechanism. This mechanism closes the circuit breaker contacts with the necessary speed and force, independently of the operator. Basically, the closing springs must first be charged or cocked before the breaker can be closed. The springs are then released by releasing the spring release latch. The breaker is opened by releasing the tripping latch.

### 3.1 INDEPENDENT MANUAL AND POWEROPERATED BREAKERS

### 3.1.1 Closing Facilities

On manually operated breakers, the closing springs can be charged only by hand, by means of the spring-charge handle. The actual closing of the breaker is done only by hand-push on the close bar. As optional equipment, the electrical spring release attachment normally supplied only on power-operated breakers can be supplied on manually operated breakers.

On power-operated breakers, the springs are normally charged by an electric motor. Closing may be done electrically by an electro-magnet which lifts the closing spring release latch. Both of these operations can be done by hand if the control power source fails.

### 3.1.2 Tripping Facilities

The breaker can be tripped open by hand by pushing with the finger on the trip plate on the breaker panel or the trip plate on the breaker compartment door (the latter is operative only when the breaker is in the connected position).

The breaker can also be tripped electrically by the following devices:

1. Shunt trip device, optional equipment on manually operated breakers.
2. Trip Actuator, energized from the Amptector trip unit.
3. Undervoltage Trip Device (Optional on all breakers)
4. Blown Limiter Indicator (for DSL breakers)

### 3.2 LEVERING DEVICE

The drawout element has four normal positions in its compartment, determined by the levering device:

1. The REMOVE position, Figure 6.
2. The DISCONNECT position.
3. The TEST position, Figure 7.
4. The CONNECT position, Figure 8.

The REMOVE position is the first position in the compartment as the element is pushed directly by hand as far as it will go. The DISCONNECT, TEST, and the CONNECT positions are reached only by means of the levering device. This is hand operated with a removable crank handle. This handle is placed on the levering device worm shaft, which is exposed by depressing the shutter.

## Section 4 - Basic Operating Instructions

### 4.0 GENERAL

The breaker is now ready for trial mechanical operation. Keep the breaker standing on the compartment rails, out in front of the compartment. Examine it externally for any signs of obvious damage or foreign material. When everything appears to be in order, perform the following operations as "dry run" practice. If any malfunctioning is found during these operations, see that it is corrected before further operations or before placing the breaker in service.


Fig. 9 Method Used to Press Trip Plate and Lower Shutter with One Hand, Preparatory to Inserting Crank (383028)

### 4.1 LEVERING DEVICE

If the circuit breaker was shipped in a separate package, the levering device was probably left in the REMOVE position. If not it will be necessary to return it to this position. Push in the TRIP plate and depress the shutter over the levering shaft, using one hand. as shown in Fig. ure 9, and insert the levering crank as shown in Figure 3. Turn the crank counterclockwise until the position indicator is in the REMOVE position, at which time the load on the crank handle increases because a stop has been reached. Now rotate the crank clockwise to simulate levering the breaker inward toward the CONNECT POSITION. Watch the movement of the levering device arms. At the start of cranking the arms are horizontal, with rollers toward the rear, Figure 6. As the crank is
turned clockwise the levering device arms rotate downward. When they have moved approximately $40^{\circ}$ from the horizontal, the shutter will rise until it touches the crank socket. The position indicator will be opposite "DISC" which is the DISCONNECT position wherein the breaker is held in its compartment with both main and secondary contacts disengaged. If the crank is withdrawn, the shutter will close completely, and the breaker may be locked in this position as later described in Section 5.1.8.5 of this instruction book. There is very little movement of the breaker into its compartment between the REMOVE and DISCONNECT positions.

Continued rotation of the crank in the clockwise direction moves the arms downward to the vertical position, and the indicator will show "TEST" as in Figure 7. The shutter will rise.

Further clockwise rotation of the crank handle rotates the arms to the CONNECT position. This is about 65 degrees from the test position, as shown in Figure 8. When this position is reached, the crank suddenly becomes hard to turn. At this point, stop turning the crank, as the worm shaft bottoms in the tapped hole of the stop nut.

## NOTE

Further turning effort is useless. The breaker will be secure, even if the stop is only lightly touched. Remember this when actually levering the breaker into the connect position.

Rotation of the crank counterclockwise will turn the levering device arms to withdraw the unit from the CONNECT position to the TEST position and then to the DISCONNECT and REMOVE positions. Then, when the crank is removed from the worm shaft, the shutter will remain down and the trip plate will remain trapped by the shutter.

## NOTE

If the breaker is levered out from the TEST position to the REMOVE position with the closing springs charged, a trip-free "closing" operation automatically will be performed but the breaker contacts will not close. When a power-operated breaker is removed from cell, it must go through a trip-free operation.

### 4.2 CHARGE THE CLOSING SPRINGS

The closing springs must be charged before the breaker can be closed. To manually charge the closing springs, the
levering device arms must be rotated away from the REMOVE position to the TEST position. If charging is attempted in the REMOVE position, the closing cam will rotate past the charged position and go through a trip-free "closing" operation, i.e., the springs will discharge without moving the breaker contacts. Do not attempt to charge the springs in the DISCONNECT position as the same action may occur. After tuming the levering device to TEST position, manually charge the springs. On manually operated breakers, the springs are charged by a single stroke downward on the spring-charge handle, rotating it about $90^{\circ}$ toward you until it suddenly becomes very easy to move and then tends to run away from your hand. At the same time, you will hear a metallic "click!" as the over center closing spring stop is reached. Note that the spring charge indicator now shows "Spring Charged."

## CAUTION

Do not release the handle before the charging operation is completed. To release handle before charging completion will return handle upwards with such velocity that it may break the handle knob or cause bodily injury.

## CAUTION

Hold breaker to prevent tilting forward when hand charging closing springs with the breaker on the extended rails. Otherwise, it may topple to the floor and cause bodily injury or equipment damage.

On power operated breakers, a short spring-charge handle is included for emergency operation. This works on a ratchet principle, and requires 10 to 12 pumping operations to completely charge the springs. At this point, the same metallic "click" will be heard; and the spring charge indicator will show "Spring Charged." The handle must not be forced beyond this point.

## NOTE

Power-operated breakers, when being levered into the compartment, will have the spring-charge motor run and charge the spring automatically as the TEST position is reached.

### 4.3 CLOSE THE BREAKER

The breaker can be closed only when the following conditions are met:

1. The closing springs are charged.
2. The levering arms are in either the TEST position, as in Figure 7 or in the CONNECT position, Figure 8.
3. The levering device crank handle has been removed and the shutter is closed.
4. Undervoltage trip device (if included) has been energized.
5. Blown limiter indicator (for DSL breakers only) is reset.

Having met these conditions, close the breaker by pushing on the close bar. Note that the breaker position indicator shows "Breaker Closed", against a red background. Also that the spring-charge indicator now shows "Spring Discharged."

Some power-operated breakers are interlocked to prevent manual closing from the close bar on the front panel when in the CONNECT position. In this case crank the levering device to the TEST position to operate. This interlock is covered by Section 5.1.8.2.

It is possible to recharge the springs immediately after closing the breaker. This results in increased strain on the mechanism, and it is recommended that this be done only if the operating procedure requires this condition.

## NOTE

If closing is attempted with the levering arms in other than the TEST or CONNECT positions, with or without the levering crank in place, a trip-free "closing" operation is performed but the breaker contacts do not close. This trip free type of operation results in more shock on some parts of the mechanism than normal closing operations. Therefore, this type of operation should be avoided if possible.

### 4.4 OPEN THE BREAKER

The breaker can be opened in the following ways:

1. By hand operation of the trip plate (on the breaker or on the compartment door.)
2. Automatically by overload, short circuit or undervoltage condition.
3. Breakers equipped for power operation can be tripped electrically by a shunt trip device energized by hand switch or relay.

For the present purpose of getting acquainted with the breaker, open it by pushing on the trip plate. Note that the breaker position indicator now shows "Breaker-open", against a green background.

## NOTE

On breakers equipped for power operation, when they are in the compartment and in either the TEST or CONNECT position, the spring-charge motor normally runs automatically and charges the closing springs as soon as the breaker opens. The closing springs normally remain discharged while the breaker stands in the closed position. Also see Section 5.1.2.1.

Now to become better acquainted with the breaker, charge the closing springs, close and open the breaker several times. Also, place the levering crank handle on the levering device work shaft and rotate the levering arms to their various positions by turning the levering crank handle. Leave the levering arms horizontal, with rollers toward rear of breaker, i.e. in the remove position.

The breaker is now ready to be put into its various operating positions in the compartment.

### 4.5 PLACE THE BREAKER IN THE TEST POSITION

Push the breaker into the REMOVE position.
Note that the compartment door can now be closed and fastened. With the compartment door closed, the breaker cannot be operated in any manner. HOWEVER YOU WILL NOTE THAT, WITH THE COMPARTMENT DOOR OPEN, THE FRONT PANEL ASSEMBLY OF THE BREAKER FORMS A STEEL PROTECTIVE SHIELD.

Place crank on the levering device worm shaft. Turn crank clockwise until drawout unit position indicator shows "TEST." Remove the levering device crank. The shutter will close over the hex shaft. All manual operations can now be performed. On power operated breakers the spring is charged automatically as the breaker arrives in the TEST position. The breaker can also be opened with it shunt trip device, and it can be electrically closed with the spring release device.

### 4.6 PLACE THE BREAKER IN THE CONNECT POSTTION

Press the trip plate and lower the shutter. Place the crank handle on the levering device worm shaft and turn the crank clockwise until the CONNECT position stop is reached, as indicated by sudden increase in load on the crank, as previously described in paragraph 4.1.

Note however, that before the stop is reached, an increase in load on the crank will be felt after the breaker
has moved about an inch. This is caused by the making up on the main disconnecting contacts. The load on the crank will decrease after reaching a peak. The next increase in load is when the stop is reached.

## NOTE

Do not try to crank after the stop is reached. Further tightening of the crank does not help keep the breaker in position. When the crank handle is removed, the shutter and the trip plate should smap into normal position.

### 4.7 REMOVE THE BREAKER FOR FINAL INSPECTION

Withdraw the breaker from the CONNECT position in the compartment to the end of the extended rails following the reverse procedure described above. Inspect it thoroughly to see that no foreign objects have lodged within it. If any defects were found during these preliminary operations, complete their corrections at once.

### 4.8 FINAL INSPECTION

MAKE SURE THE THREE (3) ARC CHUTES ARE PROPERLY INSTALLED. MAKE SURE ALL FOUR (4) INSULATING BARRIERS ARE PROPERLY INSTALLED.

1. With the breaker withdrawn, rotate levering device to connected position before attempting to charge the spring.
2. Close and trip the breaker several times as previously described.
3. Return the levering device to the remove position; i.e., with the roller arms pointing toward the rear as shown in Figure 6.
4. This completes the "dry run."

### 4.9 AMPTECTOR TRIP SETTINGS

When the breaker is shipped, the calibrating dials of the Amptector trip unit are at the nominal settings. For specific overload tripping characteristics to coordinate with the load or the system, refer to Section 8 and Curves found later in this instruction book.

### 4.10 PLACE THE BREAKER IN SERVICE

Lever the breaker into the connected position as previously described, and latch the compartment door.

## Section 5 - Description and Explanation of Operation

### 5.0 GENERAL

The following paragraphs give a general description and explanation of the operation of the breaker.

### 5.1 THE OPERATING MECHANISM AND HOW IT WORKS

The operating mechanism is of the spring charged stored energy type. This means that it consists of two major parts:
(1) The stored energy or spring-charging mechanism.
(2) The mechanism for closing and opening the breaker.

The basic parts of these are combined into one sub-assembly illustrated in Figures 10, 11, 12, and 13. There are two varieties of mechanisms for the complete line of DS and DSL breakers:

Power-Operated
Manually Operated


Fig. 10 Front View of Mechanism (Manual Spring Charge Except for DS-632/840)(383035)


Fig. 11 Front View of Mechanism (Power-Operated Spring Charge) (385301)


Fig. 12 Rear of Power-Operated Mechanism (385303)


Fig. 13 Rear View of Mechanism (Left Close Spring Removed) (383034)

### 5.1.1 Power-Operated Mechanism

In the power-operated version, the mechanism is equipped with a universal-type motor for automatic charging of the closing springs. It is equipped with a spring release device for electrically closing through a control switch pushbutton, or other circuit-making device. A shunt trip device is supplied for remote tripping through a control switch, relay, etc. In the absence of control voltage, or whenever desirable, the closing spring can be charged by hand with the emergency charging handle. Hand closing of the breaker can be done by means of the close bar. Hand opening of the breaker can be done by means of the trip plate.

### 5.1.2 Explanation of Spring-Charging Mechanism for Power-Operated Breakers

Figure 14 is an isometric diagram of the principal parts of a completely power-operated mechanism.

Figure 15 is a front view drawing showing the principal parts of the spring-charging portion of this mechanism. Other parts are omitted for clarity. Figures $16 a$ and $16 b$ show in greater detail the major parts of the springcharging mechanism in the two basic positions:

[^11]Referring to Figure 15, the basic elements are mounted on the crank shaft (8). This is a straight shaft with four flats machined on it, and a crank arm (11) attached to each end. Each crank arm connects to its closing spring (9) by a formed spring end (10) Figure 16b. The rear of the springs anchor to the rear of the mechanism frame. The crank arms (11), motor cutoff switch cam (7), close cam (6) and two drive plates (25) have matching flats; and are thus anchored to the crank shaft. The spring charge indicator (12) ratchet wheel (17), oscillator (30), and emergency charge device (26) do not have internal flats but are mounted on separate bushings and are free to rotate on the crank shaft.

Figure 17 is an exploded view of the crankshaft parts.
Figure 16a is a view looking into the right end of the crankshaft, and shows the position of the components when the springs are charged.

Figure 16 b is a partial view with the springs discharged.
The motor crank shaft assembly (29), carrying a roller for driving the oscillator, is pivoted in the right hand mechanism side frame. The hold pawl (18) is mounted by means of a pin on the mechanism side frame as shown.

In operation, rotation of the motor crank pushes the oscillator arm counterclockwise to make the oscillator pawl (28) push a tooth in the ratchet wheel (17) and rotate the ratchet wheel slightly more than one tooth in the counterclockwise direction. The holding pawl snaps behind the corresponding advanced tooth, and holds it against the torque of the closing springs while the oscillator arm rotates back clockwise to catch another ratchet tooth. Thus the ratchet wheel is rotated counterclockwise until the ratchet wheel pin (21) engages the two drive plates (25) which in turn rotate the crank shaft and the crank arms in the same direction until the arms are slightly past horizontal dead center. Since the close cam (6) is rigidly mounted on the crank shaft, the same as the drive plates, it has rotated the same amount as the plates. The close cam carries a stop roller as shown in Figure 22b. Just after horizontal dead center of the crank arms is reached, the torque of the closing springs starts to rotate the crank, independently of the driving motor. However, the stop roller on the close cam quickly stops the movement of the crank at only a few degrees over center and holds it there by coming against the spring release latch. This is the "spring charged" position. The motor cut-off switch cam (7) operates the switch (15) through a lever (13) at this time, and the motor stops.

At the instant that the springs snap over dead center, the lobes of the drive plates raise the pawl lifters (27), and prevent the oscillator pawl (28) from engaging the next tooth in the ratchet wheel. Thus the oscillator is free and renders the exact stopping point of the motor not critical.

When the spring release latch is moved below the level of the stop roller, as later described, the close cam is free to rotate; and the two closing springs rotate the crankshaft counterclockwise to close the breaker contacts. They assume the position shown in Figure $16 b$ and the cam as in 22c. During rotation, the drive plates move away from the ratchet wheel pin. The ratchet wheel does not rotate during the closing operation thus preventing excessive wear on the teeth and pawls.

Power-operated breakers are also equipped for emergency hand charging the closing springs. Refer to Figure 21. This operation is similar to that of the motor and oscillator except a separate emergency charge pawl (33) is used to advance the ratchet wheel (17) several teeth on each stroke of the charge handle (34). This device (26) also pivots on the crank shaft.

### 5.1.2.1 Power Operation

The electrical operation of the spring-charging motor circuit is as follows:

The standard basic schematic and connection diagrams are shown in Figure 19a and $b$. Device $Y$ is the anti-pump relay.


Fig. 14 Arrangement of the Principal Parts of a Power Operated Mechanism. The Close Spring is Shown in the Charged Position


Fig. 15 Front View Showing Major Parts of the Crank Shaft Assembly. Some Parts are Omitted for Clarity

a) Spring Charged

Note: Main cam position for this crank shaft position is shown in Fig. 22a

b) Spring Discharged
6. Close Cam
8. Crank Shaft
9. Closing Spring
10. Spring End
11. Crank Arm
17. Ratchet Wheel
18. Hold Pawl
19. Oscillator Bushing
20. Oscillator Spring
21. Ratchet Wheel Pin
25. Drive Plate
27. Pawl Lifter
28. Oscillator Pawl
29. Motor Crank Rotler
30. Oscillator

Fig. 16 Power-Operated Spring-Charge Details


Fig. 17 Crank Shaft Assembly of Power-Operated Mechanism (385304)


Fig. 18 Emergency Spring-Charge on Power Operated Mechanism


Fig. 19 Standard Schematic and Connection Diagrams for Power-Operated Breakers and Trip, Spring Release, Spring Charging Details

With the breaker open and springs discharged, the motor is energized through the limit switch (LS) and the " $b$ " contact. The green indicating lamp ( $G$ ) is controlled by a separate " $b$ " contact, and when lit indicates that the breaker is open.

Motor runs and charges the closing springs.
When the springs are fully charged, limit switch (LS) opens in the motor circuit and closes in the spring release coil (SR) circuit.

When the close contact (CS-C) makes, the spring release coil (SR) is energized through the normally closed " $Y$ " contact, the limit switch ( $L S$ ), and breaker " $b$ " contacts. This releases the latch holding the stop roller on the close cam.

Springs are released to close the breaker. When the breaker closes, the " $b$ " contact opens to cut off spring release coil and motor, and limit switch (LS) contacts reset.

If the close contact (CS-C) is maintained, the " $Y$ ' relay will be picked up by the current through the SR coil, and will open its " $Y$ " contact in the SR circuit. This allows only one close operation until the close contact (CS-C) has been reset. The " $Y$ " coil has a very low drop-out voltage.

On some circuit breakers a special closing circuit may be provided which permits the closing springs to be automatically recharged immediately after the breaker is closed instead of only after the breaker is opened. This is accomplished by separating the motor and limit switch


Fig. 20 Principal Parts in a Manually Charged Spring Operated Mechanism.
from the " $b$ " contact so the motor operation is independent of the position of the breaker contacts. This arrangement makes the breaker suitable for use with instantaneous reclosing relays or in special operating sequences.

The standard control utilizes AC or DC control power. For 240 or 120 volt AC equipment, the control power may be taken direct from the source through fuses. For 480 and 600 volt operation, a suitable control power transformer is used. The transformer is optional for 240 volt systems. DC control voltages are 48, 125 or 250.

When the breaker closed, the "a" contact in the shunt trip (SH-TR) coil circuit also closed to complete this trip circuit. The red indicating lamp ( $R$ ) supervises the shunt trip circuit to show that it is in working order, and indicates that the breaker is closed.

When control power is turned on, any power-operated breaker in the test or connected position with its springs discharged will have its motor energized until the closing springs are charged.

### 5.1.3 Manual-Operated Mechanisms

On manually operated breakers, the closing spring can be charged only by hand, as described in Section 4.2. As usually equipped, the breaker can be closed only by hand, with the close bar. As an optional extra, a closing spring release device can be supplied on these breakers.

Hand opening of the breaker can be done only by means of the trip plate; however a shunt trip device can be supplied as an optional extra.

### 5.1.4 Explanation of Spring-Charging Mechanism for Manually-Operated Breakers

Figure 20 is another isometric diagram to illustrate the mechanism in a manually operated breaker. For sake of clarity, the actuator has been omitted.

Figure 21 gives the details of this spring-charging device which is located between the mechanism right hand side frame and the right crank arm. A part of this assembly is the manual charge cam which is rigidly fixed to the crank shaft, the same as the main close cam and crank arms.

The other parts are the front crank assembly which is pivoted to a bracket fastened to the main frame base, and has a socket for the manual charge handle. The rear crank is pivoted to the front portion and has a cross-wise pin on the end. A spring forces this pin against the cam. Another
spring holds the front crank assembly in a clockwise direction against a stop, so that the manual spring-charge handle socket is normally upright in the unused position.


Fig. 21 Spring-Charging Mechanism on Manual Operated Breakers

The manual charge cam is mounted on the crank shaft so that the crank pin hooks behind the hook-shaped surface of the manual charge cam as shown, when the handle is upright and the springs discharged. The springs are fully charged by a 90 degree counterclockwise rotation of the handle. The crank spring then returns the assembly to the handle-upright position. In operation this means a single downward stroke from vertical to approximately the horizontal position. As the "Spring charged" position is reached, the handle becomes effortless to turn and the closing spring crank arms snap over center.

It is possible to manually recharge the closing springs immediately after closing the breaker and before it has been tripped open. This results in the springs loading the associated bearings and latches for long periods. Also an extra close operation, or trip-free operation, will be necessary on levering the breaker to the disconnect and remove positions. Therefore, it is recommended that the springs be charged just prior to the closing of the breaker.


Fig. 22 These Sketches Show the Four Basic Positions of Breaker and Linkage with Enlarged View of Trip Shaft
and Latch and Latch

### 5.1.5 Circuit Breaker Closing Mechanism

This mechanism is of the general variety of mechanically trip-free mechanisms. This means that the breaker can be opened or tripped free from the closing mechanism at any point in its closing stroke. It also means that if the trip latch is held in the "trip" position while the spring release latch is released, the closing springs will make a trip-free operation but the breaker contacts will not close or move appreciably toward the closed position.

Based on this construction, the breaker close and trip linkage can have four steady state conditions. The arrangements of the basic close and trip linkage for these four conditions are shown in Figures 22a, 22b, 22c, and 22 d as follows:

Figure 22a Breaker Open, Springs Discharged, Trip Latch Not Reset.

Figure 22b Breaker Open, Springs Charged, Trip Latch Reset.

Figure 22c Breaker Closed, Springs Discharged.
Figure 22d Breaker Closed, Springs Charged.

The angular position of the close cam in Figure 22a corresponds to the angular position of the drive plates and closing spring crank arms shown in Figure 16b. The trip latch is in the tripped position and it will reset to the latched position at the end of the spring charging stroke. The closing springs are charged by counterclockwise rotation of the ratchet and drive plates until the close cam stop roller meets the spring release latch, as shown in Figure 22b.

Note in Figure 22b also that the lower end of the main drive link, with the main roller, has swung upward and toward the left, pushing the trip latch constraining link so as to rotate the trip latch back to the reset position. This occurs at the same time that the spring charge is complete and just before the close cam stop roller strikes the spring release latch. The position of the cam in Figure 22b corresponds to the position of the drive plates in Figure 16a spring charged, breaker open.

The breaker is now ready to be closed. Closing is started by counterclockwise rotation of the spring release latch. Refer again to Figure 22b. This removes the hold on the close cam stop roller, and allows the force of the closing springs to rotate the close cam counterclockwise


Fig. 23 Shunt Trip Details Showing Trip Shaft Adjustment
and close the breaker. The linkage is then in the position shown in Figure 22c. The close cam has rotated about 180 degrees.

The spring release latch can be rotated by two methods:

1. By the spring release device on power-operated breakers, as shown in Figures 14 and 31b.
2. By the close bar, through the linkage shown in Figure 31b.

### 5.1.6 Circuit Breaker Tripping or Opening Mechanism

Referring to Figure 22c showing the breaker in the closed position, the breaker is tripped open by counterclockwise rotation of the trip shaft. The trip shaft extends across the left hand part of the breaker, from the left hand mechanism side sheet to the left hand breaker side sheet; and can be rotated by several devices as later described.

Rotation of the trip shaft accomplishes breaker opening as follows: Staying with Figure 22c, the main contacts (not shown) produce a clockwise twisting force or torque on the pole shaft. This is transmitted by the center pole
lever downward through the main drive link to the main roller. The main drive link at the main roller is connected to the trip latch by the roller constraining link. The downward force on the main drive link results in a pulling force on the roller constraining link. This force tends to rotate the trip latch counterclockwise, but the trip latch is kept from rotating by overlap of the latch surface of the trip shaft. A very small rotation of the trip shaft thus releases the trip latch to rotate counterclockwise to the position shown in Figure 22a. The enlarged views of the trip shaft and trip latch tip in Figure 22e show in detail the rotation of the trip shaft for release of the trip latch. Thus the entire linkage collapses under the force of the main contacts and comes to rest with the breaker open, as in Figure 22a. Note that the trip latch is still in the released position, i.e., not reset.

If the breaker stands open with springs charged as in Figure $22 b$, and if the trip shaft is held in the rotated or trip position, an attempt to close will result in a trip-free operation. This is so because, with the trip shaft in the trip position, there is no restraint on the trip latch, so no force is applied to the main link to close the breaker.

Although certain interlocking operations may or will result in this trip-free type of operation, it causes some


Fig. 24 Actuator
extra shock on the mechanism parts. Therefore trip-free operations should be avoided.

The trip shaft can be rotated to trip the breaker in the following ways:

1. By hand push on the trip plate. As shown in Figure 27, this item has a tab which pushes against a pin on the trip shaft which applies a direct rotating force on the shaft in the tripping direction.
2. By shunt trip device, as shown in Figure 23a. The armature of the clapper-type electro magnet pushes on a lever on the trip shaft to rotate it in the tripping direction.
3. By action of the actuator, as shown in Figure 24b. A downward pull by the trip plunger pulls on a lever from the trip shaft to rotate it in the tripping direction.
4. By action of the trip plate on the front of the breaker compartment door (providing the breaker is in the connected position.) A flap on the breaker compartment hinged door, operating through a sliding link and lever fastened to the cradle move the compartment trip lever extending from the bottom of the drawout unit. Refer to Figures 25 and 26.
5. An undervoltage trip device is available as an accessory, and will directly operate the trip shaft. This is shown in Figures 67 \& 68, and its operation is covered in Section 8.7.1.
6. Blown Limiter Indicator. See Fig. 80.

### 5.1.6.1 Miscellaneous Details

Figure 26 shows a bottom view of the breaker drawout unit. Visible in this picture are details as follows:

## 1. The Interference Interlocks

These are Z-shaped brackets which prevent circuit breakers with insufficient interrupting ratings (or mismatching disconnects) from being inserted into wrong compartments.

| This compartment | Will accept <br> these breakers |
| :--- | :--- |
| DS-206 | DS-206 |
| DS-206S | DS-206S, DS-416, <br> DS-416S, DS-420 |
| DS-416 | DS-416, DS-416S, <br> DS-420 |
| DS-416S | DS-416S, DS-420 |
| DS-420 | DS-416S,DS-420 |
| DSL-206 | DSL-206 |
| DSL-416 | DSL-416 |



Fig. 25 DS-632 Breaker with Front Panel Removed (391063)

## 2. Ground Contact

This contact engages a corresponding contact on the compartment floor and provides positive grounding of the breaker frame.

## 3. Motor Cut-Off Switch

On power-operated breakers this switch disconnects the motor when the charging of the closing springs is compiete. It is operated by motor cut-off switch lever shown in Figures 13 and 15, which also operates the spring charge indicator.

## 4. Seismic Positioner

Seismic Positioner increases the rigidity of the breaker to withstand sideways forces due to vibrations on earthquake condition. As shown in Figure 26b, it is mounted on the top rear of the breaker pole unit frame and engages with a spring loaded counterpart in the enclosure.


Fig. 26a Bottom View of Breaker Unit Showing Interference Interlock, Motor Cut-off Switch and Other Details not Visible from Above


Fig. 26c Front View Showing Close Bar Guard (391071)


Fig. 26b Rear View Showing the Seismic Positioner (75010-2)

## 5. Close Bar Guard

This covers the close bar to prevent unintentional manual closing of the breaker. It is mounted on the front panel to cover the close bar. In case of emergency, the breaker may be closed by pushing the close bar through a small hole in the cover. See Figure 26c.

## 6. Operation Counter

Mechanical counter mounted under the top plate below the auxiliary switch provides the record of the number of breaker operations. The counter is connected through linkage to the pole shaft.

### 5.1.7 Mechanical Interlocking, Description and Explanation of Operation

To increase safety to personnel and the circuits to which the breaker is connected, the complete unit is equipped with automatic mechanical interlocking. This interlocking is effective in various ways in the four breaker positions (Figure 27):

## WARNING

DO NOT TAMPER WITH INTERLOCKING, AND IF IS NOT FUNCTIONING, HAVE IT CORRECTED. INTERLOCKING THAT IS FUNCTIONING IMPROPERLY CAN RESULT IN MECHANICAL AND ELECTRICAL DAMAGE TO EQUIPMENT AND BODILY INJURY TO PERSONNEL.
a. The REMOVE position.
b. The DISCONNECT position.
c. The TEST position.
d. The CONNECT position.

In addition there is an interference interlock described in Section 5.1.6.1.

This mechanical interlock system serves basic purposes as follows:

1. In the REMOVE position it prevents the breaker from being closed and prevents the closing springs from being


Fig. 27 Drawout Unit Position Indicator
charged or remaining charged. The levering device shutter is held open.
2. In the DISCONNECT position it prevents the breaker from being withdrawn from its compartment.
3. In the TEST position it permits all normal no-load operations of the breaker with the primary disconnect contacts separated.
4. In the CONNECT position it prevents the disconnecting or withdrawal of a closed breaker. This prevents the drawing of dangerous, destructive arcs on the disconnecting contacts if the circuit is loaded.
5. While moving the breaker in either direction between the TEST position and the CONNECT position or the DISCONNECT position; or while standing in any intermediate position, it prevents the closing of the breaker. Therefore it prevents the connecting of the closed breaker to the power circuits. This prevents arcing on the disconnecting contacts as would occur in going into contact with a load on the circuit.

Here are the detailed interlocking conditions which exist in each of the four breaker positions:

### 5.1.7.1 The REMOVE Position

This is the position of the breaker when nearest the front of its compartment, and is where the breaker must be placed when it is installed after having been completely outside of the compartment. It is the farthest point in the compartment to which the breaker can be withdrawn and still permit the compartment door to be reclosed.

In this position, the following conditions exist:
A. The breaker is open.
B. The closing springs are discharged. If an attempt is made to charge the springs, a trip-free operation will result.
C. The breaker cannot be closed either electrically or by hand.
D. The breaker can be withdrawn from the compartment by direct pull. (The levering device is not engaged with the cradle.)
E. The levering device arms are in a horizontal position with their rollers pointing toward the rear. See Fig. ure 6.

### 5.1.7.2 The DISCONNECT Position

In this position the breaker has moved only a fraction of an inch into its compartment and will be shown by the position indicator.

In this position the following conditions exist:
A. The breaker will be held in its compartment as the levering rollers have lowered into the slots in the cradle arms.
B. The shutter will close over the levering device hex shaft.
C. The shutter may be locked closed and the breaker held trip-free by a padlock as described in Section 5.1.8.5, thus locking it in the compartment.
D. Both primary and secondary disconnecting contacts are separated.
E. The breaker is open.

### 5.1.7.3 The TEST Position

This is the position of the breaker when at a point in between the DISCONNECT position and the CONNECT position, as shown by the draw-out position indicator. In this position the main disconnecting contacts are separated enough to permit safe operation of the breaker. However, the secondary contacts are made up.

In this position the following conditions exist:
A. The breaker must arrive in this position-from either direction with its contacts open. Its closing springs may be either charged or discharged when coming from the connected position.
B. When the levering crank handle is removed, it is possible to close and trip the breaker by hand or electrically.
C. Just before the breaker arrives in the TEST position from the DISCONNECT position, the secondary contacts make up and the spring-charge motor automatically runs and charges the closing springs on poweroperated breakers.
D. The breaker can be closed by hand, or electrically, after the springs are charged as in paragraph $C$ above.
E. The breaker can be tripped open by hand, or electrically through the shunt trip device.
F. The trip plate on the hinged compartment door will not trip the breaker.
G. The breaker must be open before further levering can be done.
H. The overload tripping characteristics can be visually checked or changed. Amptector trip devices can be electrically checked and calibrated with a portable test kit. (Accessory equipment)

### 5.1.7.4 The CONNECT Position

This is the position in which both primary and secondary disconnecting contacts on the breaker are engaged with their stationary counterparts in the compartment.

It is the farthest position from the front of the compartment into which the breaker can be levered, as (1) shown by the drawout position indicator, and (2) when the mechanical stop is felt as a sudden increase in load on the levering crank handle.

## NOTE

When levering in from the TEST position, an increase in load on the crank handle will be felt as the main disconnecting contacts are engaged. As cranking is continued, the load will decrease some and then suddenly increase as the final connected position stop is reached.

In this position all of the conditions listed for TEST position also exist, except

## IN THIS POSITION, DO NOT ATTEMPT TO ELECTRICALLY CHECK THE AMPTECTOR TRIP DEVICE WITH THE TEST KIT OR BY ANOTHER METHOD BECAUSE BREAKER WILL BE TRIPPED AND CAUSE DISRUPTION OF SERVICE.

The trip plate on the hinged compartment door will be operative, and can be used to trip the breaker when this door is closed.

In addition to the above interlocks, the interference interlock described in Section 5.1.6.1 prevents a breaker of the wrong frame size from being placed in a compartment.

### 5.1.8 Detailed Explanation of Mechanical Interlock System

That part of the interlock system which prevents closing of the breaker while being driven in either direction by
the levering device, or while it is standing in any intermediate position between "TEST" and "CONNECT" or "DISCONNECT", is shown in Figure 28a and b. Figure 28a shows the shutter and trip plate for normal operation, such as in DISCONNECT, TEST, or CONNECT positions. The breaker can be closed and tripped open by all available devices in the latter two positions except the trip plate on the hinged compartment door.

In Figure 28a, the shutter prevents pushing the levering device crank handie onto the worm shaft. If the shutter alone is pushed downward, it will rotate slightly about its pivot pin and its lower projection (See Figure 28a) strikes the hook on the trip plate, and the worm shaft will not be cleared. So it is necessary to push the trip plate in, which moves the hook back out of the way of the shutter lower projection. This permits the shutter to be pushed downward to clear the worm shaft for the levering device crank handle, as shown in Figure 28b.

Note that pushing the trip plate in also pushes the trip shaft pin so as to rotate the trip shaft counterclockwise, thus tripping the breaker open. If closing is attempted with the linkage as in Figure 28b, a trip free operation will be made.

Movement of the shutter also is controlled by the interlock cam, mounted on the levering device shaft to the left of the worm gear. The interlock cam has a fixed relation to the levering device arms. Figure 29a, b, c, and $d$ show the relation between the shutter, interlock cam and levering device arms for the four basic positions of the drawout unit in the compartment.

Figure 29a shows the CONNECT position. The cam is in a position to allow free travel of the shutter interiock pin.

Therefore the shutter can be pushed downward, but only after pushing in the trip plate as in Figure 28. This trips the breaker and therefore prevents levering out with the breaker closed.

Figure 29b shows the TEST position. Note that between CONNECT and TEST positions the cam will rotate so as to block the shutter interlock pin. This prevents the shutter returning to its closed position and releasing the trip plate if the levering device crank handle is removed. Thus, if a closing operation is tried during this part of the travel, a trip-free operation occurs and the breaker contacts do not close. Note that this is true for either direction of breaker travel so that no load is made or broken at the disconnecting contacts.

When the breaker gets to the TEST position, a slot in the interlock cam allows free movement of the shutter interlock pin, and the shutter retums to closed position when the crank is removed. The levering device arms are almost vertically downward.

Figure 29c shows the DISCONNECT position. Here also the cam rotates so as to block the shutter interlock pin while the breaker is between positions thus holding the shutter open. When the exact position, as shown on the indicator, is reached, the shutter will close when the


Fig. 28 Relation of Shutter, Trip Plate, and Trip Shaft
crank is removed. The levering arms will be approximately $40^{\circ}$ below the horizontal.

Figure 29d shows the REMOVE position. Here the interlock cam stops with the shutter interlock pin blocked. Thus the shutter stays down and the breaker stays tripped when the crank handle is removed. The breaker is held trip-free, so it cannot be closed. Also, by another interlock described later, the close-release latch cannot be released.

### 5.1.8.1 Spring Discharge Interlock

1. The purpose of this interlock is to operate the close-release latch as the breaker is moved out beyond

TEST position. This causes a trip-free operation of the closing mechanism because it occurs while the levering device crank handle is necessarily still on the worm shaft, and the closing springs are charged if the breaker is electrically operated. This is because the crank handle is still being used to move the breaker in the final part of its travel to the DISCONNECT position. Thus, the trip plate is still pushed in and consequently the breaker is trip free.
2. Figure $30 a, b, c$ and $d$ shows the essential parts of the spring discharge interlock. $a$ and $b$ show the levering device in the REMOVE position. The Interlock Plate has two horizontal pins 7 and 8 extending from it, as shown in $\mathrm{a}, \mathrm{b}, \mathrm{c}$ and d . The upper one is designated arbitrarily as Pin $A$ and is darkened to distinguish it from Pin B. In


Fig. 29 Relation of Shutter, Interlock Cam and Levering Device Arms
levering the breaker out to the REMOVE position as shown in $a$ and $b$ the levering shaft has turned counterclockwise until the levering device arms are horizontal to the rear. As it rotates, the close bar cam has been rotated
counterclockwise by Pin B, to the CLOSE position. This releases the spring release latch through the linkage shown in Figure 30, which results in a trip-free operation of the breaker if the closing springs are charged. This happens


Fig. 30 Close-Release Interlock to Discharge Springs on Levering Out of Compartment and Conn. Position no Manual Close Interlock
because the levering device crank has the Trip plate held in the Trip Position. If the breaker is manually operated, levering out can be stopped at the TEST position. Remove the levering device crank handle and (1) Close the breaker and (2) Trip the breaker. This will discharge the springs so that, when the REMOVE position is reached, there will not be a trip-free operation. The Close bar will merely be pulled into the "CLOSE" position.

### 5.1.8.2 Connected Breaker Manual Close Interlock

The purpose of this Interlock is to make possible a choice between being able to close the breaker by hand-push on the Close bar and not being able to, with the breaker in the CONNECT position. Some consider it undesirable to do so. Referring to Figure 30a, the Interlock Plate Assembly is keyed loosely to the levering device shaft by a drive pin as shown. If the interlock screw is omitted, the
interlock plate can be rotated freely on the shaft about 10 degrees. This is because the "wide" slot is considerably wider than the drive pin. If the interlock screw is in place in the "narrow" slot, the Interlock Plate has practically no play and is forced to rotate exactly as much as the levering device shaft rotates.

Figure 30c shows the standard arrangement, without the interlock screw, with the levering device arms in the CONNECT position. Note that there is a clearance between the back of the hook and $\operatorname{Pin} A$. This permits the close bar to be pushed to the "close" position and close the breaker.

In Figure 30d, all parts are in the same position as in Figure 30 c , except that the interlock screw has been placed in the "narrow slot". This arrangement is shown in Figure 25. This forces the interlock plate to rotate about


Fig. 31 Close Interlock to Prevent Efforts to Close a Breaker that is Already Closed

10 degrees further than in Figure 30c, so that there is almost no clearance between Pin A and the back of the hook. Consequently the Close bar cannot be pushed to the "Close" position. However, the breaker can be remote-closed by applying control voltage to the spring release coil through a control switch or other circuitmaking device.

### 5.1.8.3 Breaker Equipped for Electric Lockout

Power operated breakers may be equipped for electric lockout. meaning that closing an unenergized circuit is prevented. This may be the main circuit or any other desired circuit. This is accomplished by making it impossible to release the spring release latch by the spring release device unless the monitored circuit is energized. The spring release coil (SR) is wired through the contact on the motor cut-off switch that closes as the closing springs become fully charged. The remainder of the circuit is through a front panel closing pushbutton switch and to the terminals of the circuit being monitored. Thus, when the monitored circuit is energized properly, the breaker may be closed through the panel pushbutton switch, provided in addition that the closing springs are charged.

As an additional safeguard against undesired closing under this electric lockout condition, all such breakers will be equipped with the interlock screw as described in Section 5.1.8.2 above. This prevents hand closing of the breaker in the CONNECT position.

Manually operated breakers may also be furnished with this feature if they are equipped with optional electrical spring release devices.

### 5.1.8.4 Closed Breaker Interlock

Figure 31 shows how operation of the spring release latch is prevented when the breaker already is in the closed position. The Close Bar is connected to the spring release latch by a link and bell crank. The link is pivoted on the lower end of the close bar cam by a pin as shown. As the Close Bar is pushed, the pin and latch link will move to the right, along with the lower end of the cam. The lower end of the link is facing a knife edge pivot on the vertical arm of the bell crank. The upper end of the link is facing the Open-Close Indicator Pin. This pin is at the left end of its slot in the mechanism side frame with the breaker open and at the right end with the breaker closed. As the Close Bar is pushed, the link therefore has two possible end pivots. If the breaker is open the upper end of the link will swing to the right until it touches the indicator pin. The lower end of the link will then swing to the right and


Fig. 32 Padlock Device - Locked Trip Free and Shutter Raised
push the vertical arm of the bell crank to the right. The horizontal arm of the bell crank moves downward and presses directly on the spring release latch, allowing the breaker to close.

If the breaker already is closed and the Close Bar is pushed, the upper end of the spring release latch link will swing free to the right because the indicator pin is not there to stop it. Consequently, no force is applied to the vertical arm of the bell crank, and nothing else happens.

### 5.1.8.5 Padlocking Provision

Figure 32 shows the essential parts of the padlock interlock. The breaker is padlocked in the trip-free
condition in which the breaker cannot be closed and the breaker cannot be moved with the levering device. This figure shows the relation of parts for padlocking in the trip-free, shutter up condition. There are three major parts involved, which are interieaved and assembled on the left hand side of the levering device assembly:

1. The Shutter
2. The Trip Plate

## 3. The Padlock Interlock Lever

The Padlock Interlock lever is located between the Trip Plate and the Padlock Plate, and is pivoted on a fixed center toward the rear of the breaker. The front part of this lever has a sloping slot into which a projection from the trip plate extends. Horizontal movement of the trip plate by cam action of the projection against the walls of the slot, causes the front of the interlock lever to move up or down. The interlock lever is pushed upward by a spring. This lever also has a short pin extending outward
normally into a curved notch in the bottom edge of the padlock plate.

To padlock the breaker, with shutter closed, push the trip plate in. Pull the padlock plate forward. This exposes the padlock slot in the padjock plate. Insert the padlock and lock.

Movement of the trip plate pushes the front end of the padlock interlock lever down, moving its pin downward and out of the notch in the padlock plate. Forward movement of the padlock plate and backward movement of the trip plate places the pin in the padlock interiock lever behind the notch in the padlock plate. With the padlock plate held forward, the padlock interlock lever cannot move. The projection from the trip plate is consequently held in the slot in the padlock interlock lever, so the breaker remains locked in the trip-free condition until the padlock is removed and the members are returned to their normal positions by their return springs. While so locked, the shutter is prevented from downward travel by a horizontal projection striking a bent-over tab on the padlock plate.

## Section 6 - Circuit Breaker Pole Units, Description and Operation

### 6.0 GENERAL

Figures 33, 34, 35, and 36 show detailed three pole assemblies of all of the type DS circuit breakers.

DS206 has the three poles mounted on a single molded base of high strength insulating material, with the contact parts and sensors mounted on it. Figures 37 and 38 show front and rear views of the assembly.

The DS416, DS420, DS632 and DS840 differ in that each of the three poles are mounted on individual
insulating bases, and all three poles held in accurate alignment by a welded steel frame. Front and rear views of each are shown in Figures 39 and 40 for the DS416, Figures 41 and 42 for the DS420, Figures 43 and 44 for the DS632, Figures 45 and 46 for the DS840.

### 6.1 MOVING CONTACT SUB-ASSEMBLIES

The moving contact members of all ratings consist of blades hinged at the bottom to the lower main terminal


Fig. 33 Three-Pole Assembly of DS-206 Pole Units on Frame
through controlled pressure rotating contacts and with main and arcing contacts at the upper end. The arcing contacts of all of the five ratings shown are essentially the same design. The number of blades, the size of the main terminals and the number of fingers in the main disconnecting contacts vary with the rating. The DS206 has two moving blades, the DS416 and DS420, four moving blades, and the DS632 and DS840, eight moving blades. On the DS206, two butt type main contacts and a knife
blade arcing contact are located between the two hinged blades. On the DS416 and DS420 the main contact member, i.e. which makes actual contact with the stationary contacts, is a horizontal member to which all blades are connected. On the DS632 and DS840 there are two sets of contacting surfaces, one vertically above the other, for making contact with two corresponding rows of stationary contact fingers. The arcing contact assembly is bolted to the top of the main moving contact blade


Fig. 34 Three-Pole Assembly of DS-416 and DS-420 Pole Units on Frame
assembly. This has the arcing contact tips, of arc resisting metallic composition, permanently fastened near the upper end of the assembly. The moving contact blade assembly is operated by a strong and rigid insulating link.

### 6.2 STATIONARY CONTACT SUB-ASSEMBLIES

The stationary contact sub-assemblies may be seen in Figures 47, 48, 49, 51 and 53. All main contacts, i.e.


Fig. 35 Three-Pole Assembly of DS-632 Pole Units on Frame
those which carry the main continuous load current, are of the butt type composed of a multiplicity of fingers. Each finger is hinged at the upper end under controlled pressure. Compression springs at the lower end apply predetermined pressure against the moving main contact in closing, and standing in the closed position. These springs are visible in the photograph of the DS206 only. With this construction, the pressure on the main contact surfaces is increased during the carrying and opening of high short circuit currents because the magnetic field of the current pushes the lower end of the finger toward the
moving contact. Hinging the finger at the top thus results in what is sometimes called "blow-on" action. This greatly increases the capability of the entire contact assembly to withstand the high fault currents associated with these breaker ratings.

The stationary arcing contacts are similar for all ratings and consist of two parallel fingers, one on each side of the stationary terminal member. They are pushed toward each other by compression springs and have arc resisting tips.


Fig. 36 Three Pole Assembly of DS-840 Pole Units on Frame

The moving arcing contact thus wedges the stationary contact fingers apart as the breaker closes.

The parallel action of the magnetic fields of the currents in each arcing contact finger causes the fingers to be attracted toward each other when closing against fault currents. This results in a "blow-on" action on the arcing contacts.

Figures 37 thru 46 show the combined moving and stationary contact sub-assemblies of the various breakers. This shows the proper relationships, clearances and contact deflections of the various parts.


Fig. 37 Type DS-206 Pole Unit Assembly - Front View (384502)


Fig 38 Type DS-206 Pole Unit Assembly - Rear View (384499)


Fig. 39 Type DS-416 Pole Unit Assembly - Front View (383420)

Fig. $41 \begin{aligned} & \text { Type DS-420 Pole Unit Assembly - Front View } \\ & \text { (391101) }\end{aligned}$
Fig. $41 \begin{aligned} & \text { Type DS-420 Pole Unit Assembly - Front View } \\ & \text { (391101) }\end{aligned}$



Fig. 40 Type DS-416 Pole Unit Assembly - Rear View (391098)


Fig. 42 Type DS-420 Pole Unit Assembly - Rear View (391099)


Fig. 43 Type DS-632 Pole Unit Assembly - Front View (383418)


Fig. 45 Type DS. 840 Pole Unit Assembly - Front View (391094)


Fig. 44 Type DS-632 Pole Unit Assembly - Rear View (391095)


Fig. 46 Type DS-840 Pole Unit Assembly - Rear View (391097)


Fig. 47 Moving and Stationary Contact Details DS-206 (383979)


Fig. 48 Moving and Stationary Conract Details DS-416 (391100)(383416)


Fig. 49 Moving and Stationary Contact Details DS-420 (391086)


Fig. 50 Moving Contact Details DS-632 (383415). Stationary Contact CageSpring SatContact Spring - OuterConiact Spring - Inner
Spring Burton
6. Main Contact Fingers
7. Locking Nut
8. Bearing Tube
10. Arcing Contact - Left Hand
11. Arcing Contact - Right Hand
12. Arcing Contact Spring
13. Arcing Contact Retaining Pin
14. Retainer
15. Pin
16. Base Mold

Fig. 51 Stationary Contact Details DS-632 (383414)


Fig. 52 Moving Contact Details DS-840 (391084)


Fig. 53 Stationary Contact Details DS-840 (391271)

## Section 7 - Arc Chute

### 7.0 GENERAL

Figure 54 is a close-up view of a breaker with one insulating barrier removed to show the arc chute in place on the pole unit. Similar designs of arc chutes are used on the DS416, DS420 and DS632 assemblies with a smaller one on the DS206 and a slightly larger one on the DS840.


Fig. 54 Breaker with Barrier Removed to Show Mounting of Arc Chutes (391072)


Fig. 55 DS-206 Arc Chute with Details (383973)

The arc chute fits well down over the arcing contacts so that the are is confined inside the chute at all times and for all values of current. In the arc chute, immediately above the arcing contacts, are spaced crosswise vertical


Fig. 56 DS-416/420 Arc Chute with Details (391270)


Fig. 57 DS-632 Arc Chute with Details (391269)
steel splitter plates having an inverted " $V$ " notch to attract the arc and interrupt it essentially the cooling and stretching the arc.

The DS206 arc chute is shown in Figure 55. The larger arc chute for the DS416 and DS420 is shown in Figure 56, the DS632 arc chute is shown in Figure 57 and the DS840 arc chute is shown in Figure 58.

In addition to the steel plates, the larger arc chutes include hard arc-resisting glass polyester plates. These plates produce turbulence in the exhaust gases above the steel plates and prevent electrical breakdown over the top of the arc chute or to ground.

## WARNING

ALL ARC CHUTES AND BARRIERS MUST BE IN PLACE BEFORE RETURNING BREAKER TO COMPARTMENT. IF BREAKER IS ENERGIZED WITHOUT CHUTES AND BARRIERS BEING INSTALLED, IT COULD CAUSE A DISASTROUS SHORT-CIRCUIT FAULT WITHIN THE SYSTEM; AND IT MAY RESULT IN BODILY INJURY AND EQUIPMENT DAMAGE.


Fig. 58 DS.840 Arc Chute with Details (391092)

## Section 8 - CIrcuit Breaker Automatic Tripping System

### 8.0 GENERAL

The circuit breaker is tripped on overload and short circuit conditions by combined action of three components:

1. The sensors which determine the current level.
2. The Amptector solid-state trip unit which provides a tripping signal when pre-determined current levels are reached.
3. The Actuator which actually trips the circuit breaker.

Schematically this may be represented as shown in Figure 59. This provides a very flexible system covering a
wide range of tripping characteristics. Not only is the Amptector trip unit adjustable but the sensors are available over a wide range of current ratings.

The automatic overload and short circuit tripping characteristics for a specific breaker rating, as determined by the sensor rating, are determined by the settings of the Amptector solid-state trip unit. This unit also supplies a pulse of tripping current to the actuator. Thus all tripping functions are performed by secondary control circuitry, with no mechanical or direct magnetic action between the primary current and the mechanical tripping parts of the breaker.

The Amptector solid-state trip units are available in two basic versions; the Amptector II-A and the Amptector I-A.


Fig. 59 Schematic Illustration of Tripping System

### 8.1 THE AMPTECTOR II-A TRIP UNIT

Improvements have been made to the Westinghouse Amptector and the standard model is now Amptector II-A. Wiring and terminal changes were made to provide method of testing with a tester. Refer to Section 8.7.6 for testing with Amptector Test Kit.

Another change was to modify the long delay curve to nearly an $1^{2} \mathrm{~T}$ function. The revised curve shows this change. See Curve No. 1.

The Amptector II-A is standard equipment on all DS and DSL circuit breakers. It provides approximately equivalent functions as the electro-mechanical trip devices provided on some circuit breakers but with the superior operating capability of solid-state devices. The Amptector I-A is an optional (extra cost) tripping system which can be provided when ground fault protection or trip indicators are required. Both trip units have the same reliability and repeatability inherent in solid-state design.

As shown in Figure 5 the Amptector trip unit is at the top front of the breaker. Figure 60 shows a close-up of the front of the Amptector II-A trip unit. There can be a total of five adjustable controls, with screwdriver adjustment. These are for setting the following characteristics:

1. Long-delay current pick-up.
2. Long-delay time.
3. Short-delay current pick-up.
4. Short-delay time.
5. Instantaneous current pick-up.

## NOTE

The term "pick-up" as used here means the rms value of current at which the Amptector trip unit timing function begins or instantaneous tripping is intiated.


Fig. 60 Standard Amprector II-A Solid-State Trip Unit


* See Section 8.4 of Text for Explanation

Fig. 61 Amptector II.A Trip Unit with Front Cover Removed (396704)

Figure 61 is the Amptector II-A trip unit with front zover removed, showing all of the calibration marks on the dials. The ranges of current settings in multiples of sensor rating and time delay are as follows:

## 1. Long-delay pick-up <br> 2. Long-delay <br> .5 to 1.25 X sensor rating <br> 8 to 36 seconds, at 6 X sensor rating

Over these ranges tripping will always occur within the time band shown on Curve No. 1, page 59. The bottom of the band is called the resettable delay. If the overload subsides in less than the resettable delay time, resetting of the trip unit will occur within a few cycles after the load drops to less than $90 \%$ of the pick-up setting.
3. Short-delay pick-up

4 to 10 X sensor rating
4. Short delay
.18 seconds to .50 seconds or 11 to 30 cycles at 60 Hz , at 2.5 X pick-up setting.

Over these ranges tripping will always occur within the time band shown on Curve No. 1, page 59. Although the time adjustment is continuous, three time bands are calibrated as shown on the curve.

## 5. Instantaneous Pick-up $\quad 4$ to 12 X sensor rating

Three different combinations of trip elements are provided. Those combinations with the corresponding Amptector II-A model designations as follows:

1. Long Delay

Instantaneous DU (DUAL)
2. Long Delay

Short Delay SE (SELECTIVE)
3. Long Delay

Short Delay
Instantaneous TR (TRIPLE)
Each Amptector Il-A trip unit has a terminal block accessible on the front of the circuit breaker front panel.

Figure 59 shows a typical standard wiring diagram, which includes the Amptector II-A trip unit terminal block. The following table explains the markings of the terminals:

| A Sensor phase A | ON Output negative* |
| :--- | :--- |
| B Sensor phase B | DN Test point (internal neutral)** |
| C Sensor phase C | DS Test point** |
| N Sensor neutral | TP Test point** |
| OP Output positive* | DI Test point** |

*To Actuator Coil. THIS COIL HAS A POLARITY MARKING ON THE POSITIVE LEAD WHICH MUST BE OBSERVED. OTHERWISE THE BREAKER WILL NOT HAVE OVERLOAD OR FAULT PROTECTION WHICH COULD RESULT IN BODILY INJURY AND/OR SERI. OUS EQUIPMENT DAMAGE.
**Terminals marked "test point" are intended to provide connections for operation of the optional test kit.

### 8.2 THE AMPTECTOR I-A TRIP UNIT

Amptector I-A trip units perform all of the functions described above for Amptector II-A trip units and in addition provide the following:

1. Optional adjustable ground fault protection with resettable operation indicator.
2. All Amptectors I-A have a trip indicator that will indicate on overload tripping and another that indicates on short circuit tripping. (All indicators are reset manually.)

Figure 62 shows the front of the Amptector I-A trip unit. A maximum of seven adjustable controls with screwdriver adjustments may be provided for setting the following characteristics:

1. Long-delay current pick-up
2. Long-delay time
3. Short-delay current pick-up
4. Short-delay time
5. Instantaneous current pick-up
6. Ground current pick-up
7. Ground delay time


Fig. 62 Optional Amptector I-A Solid-State Trip Unit (396707)

Figure 63 is the Amptector trip unit with front cover removed, showing all of the calibration marks on the dials and trip indicators. The ranges of current settings in multiples of sensor rating and time delay are as follows:

## 1. Long-delay pick-up

2. Long-delay

> .5 to 1.25 X sensor rating
> 4 to 36 seconds, at 6 X sensor rating

Over these ranges tripping will always occur within the time band shown on Curve No. 2, page 60 . The bottom of the band is called the resettable delay. If the overload subsides in less than the resettable delay time, resetting of the Amptector trip unit will occur within a few cycles after the load drops to less than $90 \%$ of the pick-up setting.
3. Short-delay pick-up 4 to 10 X sensor rating
4. Short delay or 11 to 30 cycles at 60 Hz , at 2.5 X pick-up setting.

Over these ranges tripping will always occur within the time band shown on Curve No. 2, page 60. Although the time adjustment is continuous, three time bands are calibrated as shown on the curve.
5. Instantaneous pick-up 4 to $12 X$ sensor rating
6. Ground current pick-up See table on top of trip unit or on Curve No. 2.
7. Ground delay time
.22 to .50 seconds 13 to 30 cycles at 60 Hz

Six different combinations of the above trip elements are provided. These combinations with the corresponding Amptector I-A model designations are as follows:

1. Long Delay

Instantaneous LI
2. Long Delay

Instantaneous
Ground LIG
3. Long Delay

Short Delay
$L S$
4. Long Delay

Short Delay
Ground
LSG
5. Long Delay

Short Delay
Instantaneous
Ground
LSIG
6. Long Delay

Short Delay
Instantaneous LSI
Each Amptector I-A trip unit has a terminal block equipped with test plug terminals accessible on the front of the circuit breaker front panel. This permits convenient field checking of calibrations and operation with an ex-


- See Section 8.4 of Text for Explanation

Fig. 63 Amptector I-A Trip Unit with Front Cover Removed (396706)


Amptector II-A
Time - Current Characteristics
Curve No. 1


All bick wo vatues mav very $=10 \$$

Amptector I-A
Time - Current Characteristics
Curva No. 2
Curve No. 705501
vovember. 1971
ernal power supply. A specially designed power supply test kit, with plugs to match the Amptector trip unit test plug terminals is available; and its operation is described in Section 8.7.6 of this instruction book.

Figure 59 shows a typical standard wiring diagram, which includes the Amptector trip unit terminal block. The following table explains the markings of the terminals:

## A Sensor phase A

B Sensor phase B
C Sensor phase C
N Sensor neutral
G Ground

OP Output positive*
ON Output negative*
DN Test point (internal neutral)**
DS Test point**
TP Test point**
OSS High load switch signal to accessory unit
DI Test point**
*To Actuator Coil. THIS COIL HAS A POLARITY MARKING ON THE POSITIVE LEAD WHICH MUST BE OBSERVED. OTHERWISE THE BREAKER WILL NOT HAVE OVERLOAD OR FAULT PROTECTION WHICH COULD RESULT IN BODILY INJURY AND/ OR SERIOUS EQUIPMENT DAMAGE.
**Terminals marked "test point" are intended to provide connections for operation of the optional test kit.

### 8.2.1 Ground Fault Protection

When the Amptector I-A trip unit includes ground current protection, the type of connection to the circuit must be considered. If the system neutral is grounded but the neutral is not carried with the phase conductors, the Amptector trip unit has all of the equipment necessary for sensitive ground protection.

If the system neutral is grounded and a neutral conductor is carried with the phase conductors, it is neces-
sary to order an additional sensor, for the purpose of cancelling out any residual current in the phase conductors. This sensor must be mounted separately and must be located on the neutral conductor at the point where the neutral conductor connects to the neutral bus. These sensors are duplicate of those supplied on the breaker except for the 2400A and 3200A ratings where a modified neutral sensor is required.

The Amptector trip unit ground element may be energized from an external ground current source rather than from internally developed ground current. Such an external source could be a ring-type transformer through which all the load current conductors wouid have to pass. In the case of a three-phase four-wire circuit all three phase conductors and the neutral conductors would have to pass through the transformer. The sensitivity of the ground element for this kind of arrangement would depend on the ratio of the transformer used.

The ground current pick-up dial on the Amptector I-A trip unit has alphabetic calibration markings. The actual ground current corresponding to these calibrated points varies with the rating of the sensor being used. These pick-up values are printed on the top of the trip unit box.

The "Ground Trip Indicator" is a metal plunger located at the upper right comer of the trip unit. If the trip unit has functioned due to a ground fault, this plunger will protrude through the faceplate of the unit. The indicator is reset by pushing in on the plunger. If it is not reset before placing the breaker back in service, the trip unit will function normally but there will remain a false indication.

Overload Trip Indicator - Functions due to overload currents less than short delay or instantaneous pick-up.

Short Circuit Trip Indicator - Functions due to fault current in excess of short delay or instantaneous pick-up.

### 8.3 MAKING CURRENT RELEASE (DISCRIMINATOR)

All Amptector trip units which do not have instantaneous trip elements (Amptector II-A model SE and Amptector I-A models LS and LSG) are provided with a "making current release" which is referred to as a "Discriminator". This is a circuit in the trip unit which determines at the time of a fault whether or not there has been any current flow in the primary circuit previous to the fault. If there has been no measurable current flow previous to the fault, indicating that the circuit breaker is just being closed (or possibly that a switching device ahead of the
breaker has just been closed) and if the primary current flow exceeds approximately twelve times the sensor rating, the trip unit will function instantaneously. If the "Discriminator" circuit determines that there has been a measurable current flow prior to the fault, the instantaneous operation will not occur and the normal short time delay element will take over to delay tripping. The purpose of this unique tripping concept is that selectivity and continuity of service in un-faulted sections of the system can be maintained if there is any need, but if there is no previously operating load on the circuit, the instantaneous function takes over to limit extensive damage which might occur due to a delayed tripping operation.

### 8.4 SERVICING OF AMPTECTOR TRIP UNIT

The Amptector trip unit is the intelligence of the overcurrent protection provided by the breaker. It is a device that has many solid-state components. Since the only moving parts are the adjustments, the Amptector trip unit will give long, trouble-free service. All components and connections, including the printed circuit board itself, are coated to give effective environmental protection.

In changing the Amptector trip unit settings, the dials should be moved only by means of a small screw driver inserted through the round hote in the faceplate directly below the calibration window. The shafts must never be rotated by applying torque directly to the dial as it has only a friction fit on the shaft.

If it is suspected that the dial has moved on its shaft, it may be checked by means of rotating the shaft counterclockwise to the limit of travel. A dot at the end of the calibration should lineup with the index mark on the faceplate. See asterisk ( ${ }^{*}$ ) on Figures 61 and 63.

If there is any reason to suspect that the Amptector trip unit is not operating correctly IT SHOULD NOT BE TAMPERED WITH; SINCE TAMPERING COULD RESULT IN LOSS OF VITAL OVERCURRENT PROTEC. TION.

## NOTE

Warranty on the Amptector trip unit will be void if there is any evidence of tampering.

A specially designed tester is available for checking Amptector trip unit operation without using primary current. The tester can be plugged into any convenience outlet; and will pass enough current to check any pickup calibration. Time delay calibrations can also be checked. Place drawout breakers in DISCONNECT position before performing Amptector trip unit check.

Special handling and test equipment are required to service solid-state devices. If use of the tester shows that an Amptector trip unit is not operating correctly, it is strongly recommended that a spare Amptector trip unit be used; and the questionable unit be returned to the factory for service.

### 8.5 ACTUATOR

The actuator receives a tripping pulse from the Amptector trip unit, and produces a mechanical force to trip the breaker. Refer to Figures 64,65 and 24 for location and details. The actuator is made up of a permanent magnet, a disc held by the magnet, a rod acted on by a spring, a lever for tripping the breaker, and a lever for mechanically resetting the actuator. The magnet cannot pull and reset the disc against the force of the spring acting on the rod, but can overcome the spring force when the disc is in contact with the magnet pole piece. A tripping pulse from the Amptector trip unit counteracts the effect of the permanent magnet, allowing the spring to separate the disc from the magnet pole piece and move the rod to actuate the trip shaft lever. The trip shaft lever then rotates the trip shaft and trips the breaker. As the breaker opens, the left pole unit lever pin strikes the spring finger attached to the reset lever; this furnishes the assistance required to move the disc so as to close the air gap between it and the permanent magnet against the spring force. The device is reset when the disc is in contact with the magnet. If the disc is not fully reset, the trip shaft lever will hold the breaker mechanism in the trip-free condition; and the breaker cannot be reclosed.

The actuator must be replaced if it will not stay reset when the plunger has been moved to the top of its travel.


Fig. 64 Trip Actuator (391093)

### 8.6 SENSORS

The three sensors are located at the rear of the breaker on the lower studs, and directly behind the main disconnecting contacts. Refer to Figure 66. They produce an output proportional to the load current and furnish the Amptector trip unit with the intelligence and energy to trip the breaker when preselected conditions of current magnitude and duration are exceeded.

The continuous current rating for any frame size breaker can be changed simply by changing the sensors. The wide range of long-delay current pick-up available on the Amptector trip unit makes one set of sensors suitable for a number of current ratings. The Amptector trip unit setting controls are standard, and are usable with any standard sensors. If sensors are changed because of changing load conditions, etc., it is only necessary to readjust the Amptector trip unit controls to the new desired values. Available sensor ratings are listed in Table 4.

| Breaker Type | Frame Size Amperes* | Sensor Ratings, Amperes** |
| :---: | :---: | :---: |
| DS-206 or DSL-206 | 800 | $\begin{aligned} & 50-100-150-200-300-400 . \\ & 400-600-800 \end{aligned}$ |
| DS-206S | 800 | $\begin{aligned} & 100-150-200-300-400- \\ & 600-800 \end{aligned}$ |
| $\begin{aligned} & \text { DS-416, } \\ & \text { DSL-416 } \\ & \text { or } \\ & \text { DS-416S } \end{aligned}$ | 1600 | $\begin{aligned} & 100-150-200-300-400-600- \\ & 800-1200-1600 \end{aligned}$ |
| DS-420 | 2000 | $\begin{aligned} & 100-150-200-300-400- \\ & 600-800-1200-1600-2000 \end{aligned}$ |
| DS-632 | 3200 | 2400-3200 |
| DS-840 | 4000 | 4000 |

*Maximum continuous current rating for breaker.
**Amptector trip unit Long Delay Pick-up is adjustable from $50 \%$ to $125 \%$ of the sensor rating, but should not be set above $100 \%$ when using sensor rating equal to frame size.

### 8.7 OPTIONAL ACCESSORIES

In addition to the Amptector trip unit to provide overload protection, the following optional accessories are provided as required.


Fig. 65 DS-840 Breaker with Front Panel Removed (391076)


Fig. 66 DS-840 Breaker Rear View Showing Sensors (391074)


Fig. 67 Undervoltage Trip Device (390244)

### 8.7.1 Undervoltage Trip Attachment

The undervoltage trip shown in Figure 67 is an electromechanical device that trips the circuit breaker when the voltage on its coil falls to between 30 and 60 percent of normal. The standard unit trips instantaneously. A similar device is also available with non-adjustable time delay intended to ride through momentary fluctuations of system voltage.

In operation, a moving core is normally held magnetically against a stationary core and a spring. This is linked to a latch carrying a roller which restrains the main tripping lever of this assembly.
When the coil voltage is reduced sufficiently, the torsion spring overcomes the magnetic attraction between the two cores. The moving core travels upward, and rotates the latch in a counterclockwise direction so that the roller moves from beneath the tail of the main tripping lever. A torsion spring (not visible in Figure 67) around the pivot pin of the tripping lever then rotates it in a counterclockwise direction, causing a projection on the right side of this lever to strike a pin in the breaker mechanism trip shaft, and rotate the latter in a clockwise direction to trip the breaker.


Fig. 68 Undervoltage Trip Device Operation

As the breaker opens, a pin on the left pole unit shaft strikes a vertical leg (Reset arm) of the undervoltage tripping lever and rotates it counterclockwise against its torsion spring. Another arm on the tripping lever resets the roller latch and the moving core. A slight amount of overtravel on the trip latch insures positive resetting under all conditions. Set Figure 68 for the relationship of the undervoltage trip device, pole shaft and trip shaft.

Always connect the undervoltage coil on the line side of the breaker unless the attachment is equipped with a time delay device. In this case, the time delay will delay tripping of the breaker long enough to permit energization of the undervoltage coil from the load side. Do not use an auxiliary switch contact in this circuit.

### 8.7.2 Overcurrent Trip Switch

This device is available as an optional accessory on either manually operated or power-operated breakers of all ratings. Its function is to provide a signal to indicate that the breaker has tripped open by action of the Amptector trip unit due to phase or ground overcurrent. Normal tripping by the trip piate, shunt trip device, undervoltage trip device, etc. does not cause it to operate. It is mounted on and operates from the trip actuator of the breaker.


Fig. 69 Overcurrent Trip Switch (390239)
Three contact arrangements are available as standard: (1) two normally open, (2) two normally closed, or (3) one normally open and one normally closed contact. These are independently wired to secondary disconnect contacts at the rear of the breaker unit. Some special units may have one or two additional contacts.

The device is latch-type and must be manually reset by means of a pushbutton on the breaker front panel. Also available is an electric reset for remote operation. Figures 69 and 70 illustrate an electric reset device.

### 8.7.3 High Load Switch (available with Amptector I-A only)

This is a self-resetting solid-state device which picks up on an overload condition at a lower pick-up value than the breaker overload trip setting of the Amptector trip unit. Its function is to give advance notice of an overload condition before the breaker trips. See Figure 71.

The pick-up point is adjustable from $60 \%$ to $100 \%$ of the Amptector trip long delay pick-up setting. The non-adjustable time delay of 60 seconds requires that the pick-up current be maintained for that interval to cause the relay contact to operate. If the load current falls below the pick-up point, the timing resets in about a second. The relay has one normally open and one


Fig. 70 Overcurrent Trip Switch Operation


Fig. 71 High Load Switch (391087)


Fig. 72 Latch Check Switch (392298)
normally closed contact with a common connection. Its built-in power supply requires a reliable sinusoidal source of either 120 or 240 volts AC.

Since this is a solid-state device, no maintenance will be required; and the same cautions apply as previously stated for the Amptector trip unit. Warranty will be void if there is any evidence of tampering.

### 8.7.4 Latch Check Switch

The Latch Check Switch consists of a switch mounted on the inside at the left hand side sheet of the circuit breaker. The switch is located so that when the breaker trip shaft is in the "reset" position a normally closed contact of the


Fig. 73 Latch Check Switch Operation
switch is closed. See Figures 72 and 73 . When this switch is supplied, the contact is usually connected in the closing circuit of the circuit breaker to insure that the tripping system is reset before the circuit can be energized to close the breaker.

### 8.7.5 Auxiliary Switches

As shown in Figure 65, there may be from one to three auxiliary switches located to the right of the Amptector trip unit. Each switch has four contacts, which may be either normally open or normally closed. See Figure 74 for construction. Auxiliary switch contacts are rated 10 amperes at $120 / 240$ volts $\mathrm{AC}, 10$ amperes at 125 volts DC , and 2 amperes at 250 volts DC . The AC ratings may


Fig. 74 Auxiliary Switch Construction Details
be increased to 15 amperes if the circuit breaker wiring is increased to No. 14 on these circuits.

### 8.7.6 Amptector Trip Unit Test Kit

### 8.7.6.1 General

The Amptector Trip Unit Test Kit consists of an external power supply, current measuring device, and a precision timer for field checking the operation of the unit. These three functions have been combined into a single portable device housed in a convenient carrying case. It is powered from a standard 120 volt, single phase, 60 Hz outlet; and will furnish the high secondary currents to the input of the Amptector unit to simulate primary fault conditions on the circuit breaker.

### 8.7.6.2 Description

A long flexible cable terminated by an 11 prong polarized plug connects to the test terminals of the Amptector trip unit. A second cable connects to the source of input power. Figures 75 and 76 show the tester and operating
controls. The ammeter is dual range and controlled by the " Hi -Lo" switch. In the low range it reads $0-8 \mathrm{amps}$, while the high range covers $0-80 \mathrm{amps}$. The timer reads in seconds with the right hand digit (white) in tenths of seconds. An external ammeter may be connected in the output circuit through the terminals designated for this purpose and the shorting link removed.

## CAUTION

When using the Test Kit, the breaker MUST NOT be in the connected position because breaker will be tripped and cause disruption of service. It may be in either the test or disconnected position, or removed from its compartment.

### 8.7.6.3 Operation

The complete testing and calibration of the Amptector trip unit by means of the Test Kit is covered by the instruction sheet (1.L. 33-791) included with the Test Kit.


Fig. 75 Amptector Trip Unit Test Kit (For Amptector I-A and II-A)(391672)


Fig. 76 Test Kit in Operation (384826)

## Section 9- DSL Circuit Breakers and Fuse Trucks

### 9.0 GENERAL

DSL circuit breakers are coordinated combinations of standard DS circuit breakers and integrally mounted series connected current limiters. They are available in two frame sizes, DSL-206 and DSL-416. The primary purpose of the current limiters is to extend the interrupting rating of the DS circuit breaker up to 200,000 amperes RMS symmetrical current. If the current limiters are sized per Table 5, the circuit breaker will function and interrupt the routine fault currents. Infrequent high faults will be cleared by the limiter. The limiters protect the circuit breaker on faults above the rating of the breaker. The limiters will blow below the circuit breaker short-time rating if the fault currents equal the system maximum capacity.

In some applications the current limiters will be sized smaller than necessary for protection of the DSL circuit breaker in order to provide protection for downstream equipment. When this is done, the current limiters will blow on fault currents which could have been satisfactorily interrupted by the basic circuit breaker.

Type DS-3200 and DS-4000 fuse trucks provide for separate mounting of Class $L$ current limiting fuses on drawout trucks for use in series with DS-632 and DS-840 circuit breakers respectively. This separate mounting is made necessary by the size of the Class $L$ fuses and their high temperature characteristics.

### 9.1 DSL CURRENT LIMITERS

Available current limiter ratings and their recommended applications are listed in Table 5. Do not replace limiters with sizes other than permitted by the table. Westinghouse DSL current limiters have been tested and approved by Underwriters Laboratories, Inc. for use in DSL circuit breakers when applied according to Table 5. They are not electrically or physically interchangeable with current limiting fuses of any other design.

The current limiters are held in place in an extension provided on the back of the circuit breaker. This extension makes the DSL circuit breakers eight inches deeper than the corresponding DS circuit breakers. See Figures 77, 78 and 79. The current limiters can only be removed from the circuit breaker and replaced when the circuit breaker is removed from its associated compartment. For this reason there is no fixed mounted version of the DSL circuit breakers.

Table 5 - Sensor and Limiter Ratings

| Breaker Type | Sensor Ratins | © Recommended | Limiter Rating ${ }^{*}$ Minimum | *-Maximum |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { DSL-206 } \\ & \text { DSL-206 } \end{aligned}$ | $\begin{aligned} & 800 \mathrm{~A} \\ & 600 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 1600 A \\ & 1200 A \end{aligned}$ | $\begin{array}{r} 1200 \mathrm{~A} \\ 800 \mathrm{~A} \end{array}$ | $\begin{aligned} & \text { 2000A } \\ & 2000 \mathrm{~A} \end{aligned}$ |
| DSL. 206 | $\begin{aligned} & \text { Less than } \\ & 600 \mathrm{~A} \end{aligned}$ | 1200A | $125 \%$ or more of sensor rating | 2000A |
| DSL-416 | 1600A | 3000A | 3000A | 3000A |
| DSL-416 | 1200A | 2500A | 2000A | 3000A |
| DSL416 | $\begin{aligned} & \text { Less than } \\ & 1200 \mathrm{~A} \end{aligned}$ | 2000A | 125\% or mure of sensor rating | 3000A |

\$Minimizes nuisance blowing of limiters
-Use only when current limiting is required for downstream equipment. If long delay pick-up is set above $100 \%$, minimum limiter ratings should not be used.
*Highest rating that will protect breaker.


Fig. 77 DSL-206 Breaker Side View (388138)

### 9.2 BLOWN LIMITER INDICATOR

The Blown Limiter Indicator provides a visual indication on the front of DSL circuit breakers when a current limiter in any phase has interrupted a short circuit. It also insures that the circuit breaker will be tripped when any current limiter has blown, to prevent single phase power being applied to a three-phase load. See Figure 80.

This device consists of three solenoids, each connected in parallel with one of the limiters. When a limiter is blown, the resulting voltage across the open limiter causes


Fig. 78 DSL-206 Breaker Front View (DSL-416 Similar) (388445)
the associated solenoid to operate, tripping the circuit breaker mechanically and extending an indicator through the front cover of the circuit breaker. See Figure 78. The indicator will remain extended and the breaker will be held trip-free until the reset button is pushed. If the device is reset and the breaker reclosed on an energized circuit before the blown limiter is replaced, the breaker will be immediately reopened and held trip-free. The solenoids are isolated from the primary circuit voltage by three transformers located above the limiters. See Figures 77 and 79.

### 9.3 FUSE TRUCKS

DS-3200 and DS-4000 Fuse Trucks provide drawout mounting for Class $L$ current limiting fuses when installed in type DS switchgear. These drawout trucks physically fit in the same compartments as the DS-632 and DS-840 circuit breakers respectively. They are moved in and out of the compartment using a similar levering mechanism as provided on the DS circuit breakers. See Figures 81 and 82.


Fig. 79 DSL.416 Breaker Side View (391073)


Fig. 80 Blown Limiter Indicator

### 9.3.1 Installing Fuse Trucks

The fuse truck is normally installed in series with a circuit breaker of the same current rating. When this is done the fuse truck should be in the circuit ahead of the circuit breaker in order to provide maximum protection of the equipment. The fuse truck must never be permitted to close the current circuit or to open it when levering the truck in or out of the cell, because the primary disconnect contacts are not designed for this service. For this reason a key interlocking system is always provided which prevents opening of the fuse truck door unless the associated circuit breaker has been opened, pulled out and held in essential disconnected position. This key interlock is installed on the door of the fuse truck compartment, not on the fuse truck itself.

### 9.3.2 Replacing Fuses

Westinghouse type NCL fuses are normally provided when the fuse truck is built unless otherwise specified. However, any Class $L$ current limiting fuse of the proper current rating can be used as a replacement.

After the fuse truck has been withdrawn from the compartment, the fuses can be removed by unbolting them


Fig. 81 DS-3200 Fuse Truck Front View (391081)
from the conductors on the fuse truck. This is a relatively uncomplicated procedure on the DS-4000 fuse truck because there is sufficient working space within the truck. However, because the DS 3200 fuse truck is more restricted in space it will facilitate the operation if the front cover and levering mechanism is first removed from the truck. See Figure 83.

After replacing fuses, be sure that all connection bolts are tight and that any truck parts removed in the process have been replaced.

### 9.3.3 Blown Fuse Indicator

The same Blown Fuse Indicator is provided on fuse trucks as on DSL circuit breakers. However, since there is no opening mechanism on fuse trucks, it cannot serve directly as an anti-single phase device. In order to perform this function, the Blown Fuse Indicator is arranged to mechanically operate a switch, which is wired to secondary contacts on the fuse truck. The switchgear assembly wiring must be arranged to connect this switch into the tripping circuit of the associated circuit breaker. See Figure 83. Again, the indicator must be reset after being operated to reset the switch; or its contact will prevent the breaker from being closed.

FOR PROTECTION AGAINST SINGLE-PHASING, THE CONTROL POWER FOR TRIPPING THE CIRCUIT BREAKER MUST BE FROM A RELIABLE SOURCE.


Fig. 82 DS-3200 Fuse Truck with Front Cover Removed (391078)


Fig 83 DS-4000 Fuse Truck Side View (391677)

## Section 10-Fixed Breakers

### 10.0 GENERAL

Fixed Breakers differ from the drawout version in that they do not have levering device, primary disconnects and secondary disconnects. They do have padlock feature to hold the breaker in "trip-free" position. Key interlock mounted in the location of levering device may also be supplied to insure proper sequence of operation between
two or more breakers. This insures that before the interlock key can be removed to be used in another location the çircuit breaker must be opened and held in trip-free position. The breaker stabs have holes for bolting to the bus connections. Terminal blocks mounted at the back of the breaker are used as secondary contacts. The frame is modified so that the breaker can be mounted on the panel.

## Section 11 - Drawout Dummy Elements

### 11.0 GENERAL

A dummy element consists of a drawout frame or truck with disconnecting contacts and with connecting links between the upper and lower terminals on each pole. When inserted into a compartment it bridges the upper and lower stationary disconnecting contacts in each phase, and is thus equivalent to an isolating disconnecting switch.

It must be emphasized that a dummy is not a breaker, and has no current breaking ability whatsoever; therefore,
it is almost invariably key interlocked with a breaker or other load interrupting device, to insure that it will be isolated or at least carrying NO current before it can be levered out to the disconnected positions.

Dummy element requires the same size compartments as those of equivalent type DS breakers of the same frame sizes. The key interlock is of the same type and operates in the same manner as that described in Section 9 for type DS-3200 and DS-4000 drawout fuse trucks.

## Section 12 - Inspection and Maintenance

### 12.0 GENERAL

Type DS circuit breakers are "top of the line" equipment. This means they are manufactured under a high degree of quality control, of the best available materials and with a high degree of tooling for accuracy and interchangeability of parts. Design tests show them to have durability considerably beyond minimum standards requirements. All of these factors give the DS line of breakers high reliability. However, because of the variability of application conditions and the great dependence placed upon
these breakers for protection and the assurance of service continuity, inspection and maintenance checks on them should be made on regular schedules.

Since maintenance of these breakers will consist mainly in keeping them clean, the frequency of maintenance will depend to some extent on the cleanliness of the surroundings. If there is much dust, lint or other foreign matter present obviously more frequent maintenance will be required.

## WARNING

BE SURE CIRCUIT BREAKER CONTACTS ARE OPEN AND SPRINGS DISCHARGED BEFORE DOING MAINTENANCE WORK. FAILURE TO DO SO COULD CAUSE BODILY INJURY.


Fig. 84 Contacts and their Adjustment, DS-206 Breaker

### 12.1.1 When to Inspect

Industry standards for this type of equipment recommend a general inspection and lubrication after the number of operations listed in Section 12.3.1 of this instruction book. This should also be conducted at the end of the first six months of service if the number of operations has not been reached.

After the first inspection, inspect at least once a year. If these recommended inspections show no maintenance requirements, the period may be extended to a more economical point. Conversely, if the recommended inspec-
tion shows, for instance, heavy accumulations of dirt or other foreign matter that might cause mechanical, insulation or other electrical damage, the inspection and maintenance interval should be decreased.

When a breaker opens a heavy fault, at or near its rating, give it a visual inspection withdrawn from the compartment and with insulating barriers and arc chutes removed.

### 12.1.2 What to Inspect

First withdraw the breaker from the compartment. Remove barriers. Remove arc chutes. If there is a deposit


Fig. 85 Contacts and their Adjustment, DS-416/420 Breaker
of dust, blow clean with compressed air, if available. Wipe accessible areas with a clean dry cloth. Inspect contacts.

NOTE
Switching and fault interruptions and the making of motor inrush currents will cause some pitting of the
breaker contact parts. A large accumulation of operations will give the contacts, especially the arcing contacts, a mottled, dirty, eroded appearance. This appearance is the normal result of arc burning and in itself is no cause for concern.


Fig. 86 Contacts and their Adjustment, DS-632 Breaker

### 12.1.2.1 DS-206, DS-206S, DS-416, DS-416S and DS-420

Remove the barriers and the arc chutes to expose the contacts:

With the breaker open, examine the contact tips of moving and stationary arcing and main contacts. If the tips are burned or worn more than $.030^{\prime \prime}$, the contacts must be replaced. Also check the dimension ( $C$ ) between the stationary arcing contacts (Figures 84 and 85). It should be $.42 \pm .08$. If this dimension is not maintained, the stationary arcing contacts must be replaced.

Close the breaker and check the contact engagement according to Figures 84 and 85 . The main stationary contact fingers should be parallel (B) to the fixed contact cage. If not, adjust the contacts according to 12.2.3. Also check the dimension (A) between the stationary arcing contacts and the center section of the cage. If this dimension is not .02 inches or greater, the stationary arcing contacts should be replaced.

Replace the barrier and the arc chutes after inspection is completed.

NOTE
The DS-206 adjustments and maintenance apply compietely to the DS-206S. Also, the DS-420 instructions cover the DS-416S.


Fig. 87 Contacts and their Adjustment, DS-840 Breaker


Fig. 88 Open Position Stop and Anti-Rebound Latch
To replace the stationary contacts, the disconnect fingers on the rear are removed and then the two bolts holding the upper contact assembly to the molded base. Withdraw the contact assembly from the front. This should be replaced with a new contact assembly. Make sure that all bolts are securely tightened. Close the circuit breaker and check all contact dimensions as described in Section 12.1.2.

### 12.1.2.2 DS-632 and DS-840

In addition to the requirements for the DS-206, DS-206S, DS-416, DS-416S and DS-420 above:

The lower main fixed contacts should be inspected to ensure that they have adequate contact pressure. This is determined by pin " X " being free to slide in the contact cage (See Figures 86 and 87). Unlike DS-206/DS-416/ DS-420 breakers, the top row of fixed main contacts are compressed beyond parallel position to assure adequate contact pressure for lower row of fixed main contacts.

### 12.1.3 Replacement of Contacts

### 12.1.3.1 DS-206

Both moving main and arcing contacts are held between the two moving arms by two bolts with self-locking nuts. Removal of the two bolts permits the replacement of the moving contacts. These bolts must be securely tightened after replacement.

The fixed arcing contacts are held by a single bolt passing through the contacts and their pressure springs.

On reassembly the self-locking nut is tightened so that a dimension of 3.12 inches is obtained between the inside surfaces of the flat washers on the spring ends.

### 12.1.3.2 DS-416, DS-416S, DS-420, DS-632 and DS-840

The moving arcing and main contacts are secured to the moving contact assembly by two bolts. Removal of these bolts permits the replacement of the moving contacts.

To change the fixed arcing and main contacts, the fixed contact assembly must first be removed from the pole unit. Remove the disconnect fingers, remove the screws holding the contact assembly to the pole unit base and withdraw the contact assembly.

Obtain a new or reconditioned assembly and reassemble in the pole unit, with the holding screws finger tight. Close circuit breaker and check the dimensions A (Figures 85,86 and 87); they should be approximately equal. If not, trip breaker and adjust fixed contact system until alignment is obtained. Tighten screws and contacts as described in 12.2.3.

### 121.4 Arc Chutes

The V-shaped slots in the arc chutes will undergo slow erosion with arc interruptions. Switching operations will give them a pitted, mottled and sooty appearance. This is normal. Heavy fault interruptions will cause greater arc erosion.

If the steel splitter plates have more than $1 / 4$ inch of material eroded away at the top of the $V$-shaped slots, arc chutes should be replaced. This can be determined by comparing a plate near the center with a plate near the end.

### 12.1.5 General Inspection

Look over all visible parts possible for missing pin retainers, loose nuts, bolts or screws, bent, worn or damaged parts. Make appropriate corrections to anything found out of order.

After any inspection make sure all parts are properly installed on the breaker, especially arc chutes and all four barriers.

### 12.2 FACTORY ADJUSTMENTS <br> (Required for Major Overhaul Only)

The type DS circuit breakers are designed and built with very few adjustable parts. The operating parts and frame mounting parts are accurately tool made for automatically accurate assembly relationships. The parts are made of material that are affected to the minimum by repeated
operations and normally encountered atmospheric temperature and dirt conditions.

There are a few adjustments, made at the factory and subjected to quality control inspection and test. These factory settings normally can be expected to hold for the life of the breaker.


Fig. 89 Levering Mechanism (384021)

Factory settings are adjustments which should only be necessary when parts are reassembled after dismantling. These are described in Sections 12.2.1 and 12.2.2

Maintenance adjustments should be made as indicated on maintenance inspections and are described in Section 12.2.3.

### 12.2.1 Trip Latch Overlap

Figure 23a shows a composite view of the shunt trip lever and the trip latch, as described in Section 5.1.6. The angular position of the trip shaft latch surface is adjustable in relation to the trip latch surface by means of a screw located in the top of the actuator frame. (Fig. ure 23 b ).

Proper adjustment procedure is as follows:

## Close the breaker

Slowly rotate adjusting screw clockwise until the breaker trips. This is "no overlap" position.

Rotate adjusting screw 4 tums in a counterclockwise direction.

### 12.2.2 Breaker Open Position Stop (DS-632 Only)

Proper Adjustment Procedure is as follows:

## Refer to Figure 88

With the breaker open, loosen the open position stop bolt nuts so that the eccentric cylinders can be turned by hand but will stay put.

Rotate the cylinders to obtain a clearance of approximately .005 in . between the cylinders and the stop levers. Tighten nuts on bolts.

### 12.2.3 Moving Contact Adjustment

The contact assemblies are adjustable for the amount of engagement only. The lead of the arcing contacts over the main contacts is fixed. The correct engagement of the contacts is achieved when the vertical faces of the main fixed contacts and the fixed contact cage are parallel.

For the DS-206 this is obtained by the adjusting nuts located on the insulating link stud above and below the pivot block. Refer to Figures 37 and 38. These nuts are self-locking, and must be tight when the adjustment is complete.

The moving pole of the DS-416/420 is adjusted by rotating the insulating link after the lock nut has been loosened. Refer to Figure 39. Tighten the locknut securely after the adjustment has been completed.

The DS-632 and DS-840 have two adjusting studs on each pole, and both must be moved together to retain the parallelism. Refer to Figures 43 and 45. A spring type locking clip holds the adjustment for DS-632. For DS-840 locking nuts similar to DS-416/420 hold the adjustments.

Check contact system as described in Section 12.1.2.


Fig. 90 Lubrication Points on Left Side of Mechanism (383034)

### 12.2.4 Levering Mechanism

The complete levering mechanism is shown in detail in Figure 89. If the traveling stop nut on the rear of the worm shaft has been removed, it must be replaced in the exact position with respect to the worm gear position for proper interlock operation. This is achieved when the threaded worm shaft bottoms in the stop nut and the interlock cam is in the connected position shown in Figure 29a. The shutter interlock pin will then drop to its normal position beneath the lobe of the carn. The retaining clamp ring also operates the position indicator and may be slipped in its groove in the stop nut. The stop nut is prevented from rotating by having a "flat" against the bottom of the breaker horizontal top pan.

When reassembling, care must be exercised to insure that the two guide spacers are located in the slots of the
top pan. This allows this mechanism to float. Screws should be tightened and then backed off $1 / 2$ turn to allow mechanism to float.

### 12.3 LUBRICATION

In general, the circuit breaker requires only moderate lubrication at regular intervals. The use of a special lubricant is required in a few places, and must be applied with care. Only small quantities are needed. All excess must be removed with a clean cloth to prevent any accumulation of dust or dirt. Avoid any lubricant on insulation or other electrical parts. Care must be taken to prevent any of the molybdenum lubricant reaching any current carrying contact surface.


Fig. 91 Lubrication Points on Right Side of Mechanism (385303)

### 12.3.1 Frequency

Type DS-206/DS-206S breaker after 1750 operations.
Type DS-416/DS-416S/DS-420 breakers after 500 operations.
Type DS-632 and DS-840 breaker after 250 operations.

## NOTE

Breakers that have been stored or have infrequent operations shall be operated a minimum of five times before being placed in service.

## WARNING

FAILURE TO INSPECT, CLEAN, LUBRICATE AND MAINTAIN CIRCUIT BREAKER AT REC. OMMENDED FREQUENCIES COULD RESULT IN FAILURE OF EQUIPMENT TO OPERATE PROPERLY UNDER FAULT CONDITIONS, WHICH COULD CAUSE EQUIPMENT DAMAGE AND/OR BODILY INJURY.

### 12.3.2 Location and Lubricant

Refer to Figures 90 and 91. The numbered references below correspond to those on the above figures.

Molykote M-30 dispersion by Dow Corning or mixture of molybdenum disulphide and alcohol or equivalent should be placed on the following surfaces. Oil base lubricants are generally avoided to prevent the accumulation of dust and dirt which will cause wear and binding in the mechanism.

1. The spring-charge indicator surface engaging with the cut off switch link.
2. The cam surface operating the cut-off switch link.
3. The pins on both ends of the constraining link.
4. Shunt trip moving armature surface, Fig. 19c.
5. The curved surface of the trip latch.
6. Spring release moving armature surface, Fig. 19d.
7. The trip shaft, Fig. 19c.
8. The surface of the cut off switch link.
9. The main spring pins on each end of the crankshaft and fixed ends.

## NOTE

All parts of the levering mechanism, Figure 89 have sufficient lubrication, and should not require any further attention.

WARNING
BE SURE CIRCUIT BREAKER CONTACTS ARE OPEN AND CLOSING SPRINGS ARE DISCHARGED AFTER COMPLETING MAINTENANCE WORK. FAILURE TO DO SO COULD CAUSE BODILY INJURY.

## Section 13. Renewal Parts

### 13.0 GENERAL

Renewal Parts Data, listing by name and style number the recommended renewal parts to be kept in stock, are supplied separate from this book. When ordering parts, always specify the part name and style number, if known, from the Renewal Parts Data, RP33-790-1E. If the style number is not known, refer to the Figure number, name and item number as shown in this book, along with the breaker type and shop order number or style number as shown on the nameplate on the front cover of the circuit breaker.

Some of the detail parts shown in the figures in this book will be available only as part of a sub-assembly. The detail parts in the figures are illustrated to show their function and location in the assembly; but certain parts, due to manufacturing procedures or installation procedures, are recommended and furnished as part of a subassembly. The renewal parts data indicates which parts are available as individual items or in a sub-assembly. When inquiring about or ordering parts, refer to the figures in this book and the renewal parts data for identification of the part or sub-assembly in question.

### 13.1 IDENTIFYING PARTS FOR DS-416S and DS-206S

### 13.1.1 DS-416S Parts

The parts of a DS-416S are almost identical to those of a DS-420. The parts shown in a proper DS-420 figure (or
drawing) are used for the same purpose in Type DS-416S. Description of these parts are the same too, but they are identified as parts for DS-416S (or shop order number).

### 13.1.2 DS-206S Parts

The parts of Type DS-206S are very similar to those of DS-206. By reference to the proper DS-206 figure (or drawing) identification of their common parts can be made. When they are ordered for the DS-206S, it is so specified. The major differences are:

1. DS-206S uses the three piece base of the DS-416, instead of the one piece molded base of the DS-206.
2. DS-206S uses the DS-416 arc chute.
3. DS-206S main disconnects have $50 \%$ more fingers than the DS-206.
4. DS-206S has twice as many contacts and arms as the DS-206.
5. The pole unit hinge of DS-206S is a forked construction or a miniature version of the DS-4 16 hinge.

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Memorandum

Memorandum


Westinghouse Electric Corporation
Switchgear Division
East Pittsburgh. Pa. 15112 U.SA

May 1980
New Information and
Supplements I.B. 33-790-1E

## Low-Voltage <br> Power Circuit Breakers Types DS and DSL



## Parts Identification

Renewal Pars Data 3.2-79(1) E is supplementary informa-
 Iollue Power Cirwil Breakers Tipes DS and DSIL. The illustrations in this Renewal Parts Data show parts and sub-inssemblies which are identified by name and stvle number in the associated tabulations. Additional information and illustrations are shown in the figures in I.B. 3.3-790-1E. which show many sub-assemblies and detail parts in order to illustrate their function and location in the assembly. Some of the detail parts shown in the instruction book are recommended only as part of a sub-assembly to facilitate their replacement or installation in the field. The availability of parts and subassemblies is indicated by style number in the following data.

If the item in question cannot be identified by style number. refer to the Figure number, name and item number as shown in this RPD (or I.B. 33-790-1E) along with the breaker type and its shop order number or style number as shown on the nameplate on the front cover of the circuit breaker.

The above nameplate information will also be required when adding components, which are not direct replacements, to a circuit breaker.

## RECOMMIEVIIED SPARE PARTS

Spare parts recommended for stocking are indicated in the loll witue ditas the the whbol $\sqrt{8}$. An adequate stock ol yare jurr will help minimize emergency situations and cial suhatamially reduce production down time.

The ambumt of incwment to be made in spare parts sex.k can be dependent on a number of individual factors. The items recommenked and the quantities specified below are intended as a guide.
For 1 (O) Breakers - Items marked $(B$ in sufficient yuantity for ane lreaker.
Fors = (a) 10 Breakern-ltems marked $B$ in sufficient quantity for two breakers.
Over 10 Breakers - One spare complete breaker. plus recommended spare parts for one breaker.

## ORDERING INFORMATION

1. Name item and give its style number. Specify quantity desired.
2. State method of shipment desired.
3. Send all orders or correspondence to nearest Westinghouse Sales Office.

## PRICING INFORMATION

Many of the style numbers in this data are listed in Price and Entry Guide 120 and PL 121.


## Items Common to All Breaker Types

AUXILIARY SWITCHES-FIGURE NO. 2
When replacing an existing auxiliary switch. order bisic switch assembly style 49D622A01 which includes 2 "a" and 2 "b" contacts. Style 449D622A01 is suitable as a replacement on all breakers except those equipped with mechanical interlocks, and those wired per diagram figures 10D, 10E, 10F and 10G.

When adding auxiliary switches to an existing breaker, specify the number of switches required together with the nameplate information as itemized on page 2.

## SECONDARY DISCONNECTING CONTACTSFIGLRE NO. 3

When replacing an existing disconnecting contact. order style 591C498G06 which includes an 8 point block plus mounting hardware.

When replacing an existing disconnecting contact cover, order style 588C729G02.

When adding secondary disconnecting contacts to an existing breaker, specify the number of upper contacts and the number of lower contacts together with the nameplate information as itemized on page 2.

## TYPE DS CIRCUIT BREAKER FASTENER KIT

Includes an assortment of retaining rings, truarc rings. "E" rings and "X" washers in a plastic bag.
Style 3586A86G01
Recommended spares:
1 for one breaker
2 for two to five breakers
3 for six to twenty breakers
4 for over twenty breakers

## STANDARD HARDWARE

Standard hardware such as bolts, nuts, washers. etc. are not listed in this data. Such items should be purchased locally. Note: Bolts holding copper details together in the pole unit. and bolts holding levering in cranks should be SAE Grade 5.


Fig. 2 DS 416 Breaker with Front Panel Removed


Fin. 3 Rear I'iew Showing Levarin! Derice Arm in COVVECT Povition

Type DS－206．DSL－206 and DS－206S Pole Unit

Fig． 4
Type DS－206 Pole Unit Assembly－Front View

|  |  |  | DS－206 |  | DSL－206 ${ }^{(1)}$ |  | DS－206S ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | Fig． No． | Item No． | No． <br> Req． Per Bkr． | Style Number | No． <br> Req． Per Bkr． | Style Number | No． <br> Req． Per Bkr． | Style Number |
| Three Pole Unit Assembly Complete | 4 | － | 1 | 1400152G01 | 1 | 140D152G03 | 1 | 9145D41G01 |
| Following are included in Three Pole Unit Assembly： |  |  |  |  |  |  |  |  |
| Molded Base | 4 | 1 | 1 | $1400150 \mathrm{HO1}$ | $!$ | $1400150 \mathrm{HO1}$ | 3 | 553F204H01 |
| Upper Stud Assembly | 4 | 2 | 3 | 591C653GO1 | 3 | 591C653G03 | 3 | 592C928GO1 |
| Lower Siud Assembly | 4 | 3 | 3 | $591 \mathrm{C652G01}$ | 3 | $5910652 G 03$ | 3 | 592C927G01 |
| Following are included in Upper Stud Assembly： | ． |  |  |  |  |  |  |  |
| Stationary Arcing Contact－R．H． | 4 | 4 | 3 （8） | 5038025G01 | 3 （1） | 503B025G01 | 3 （1） | 503B025G01 |
| Stationary Arcing Contact－L．H． | 4 | 4 | 3 （1） | 5038025G02 | 3 （6） | $5038025 G 02$ | 3 色 | 5038025 G 02 |
| Stationary Arcing Contact Spring | 4 | 5 | 6 閏 | $503 \mathrm{B027HO1}$ | 6 ® | 503B027H01 | 6 家 | 5038027 HO |
| Stationary Main Contact Finger | 4 | 6 | 6 （8） | 809A263G01 | 6 （8） | 809A263G01 | 12 （3） | 809A263G01 |
| Stationary Main Contact Spring | 4 | 7 | 3 （6） | 503B027H08 | 3 B | 5038027H08 | 6 达 | 503B027H08 |
| Following are included in Lower Stud Assembly： |  |  |  |  |  |  |  |  |
| Moving Arcing Contact | 4 | 8 | 38 | 591 C 51 GO 2 | 3 因 | $591 \mathrm{C651G02}$ | 3 （8） | $591 \mathrm{C651G02}$ |
| Moving Main Contact | 4 | 9 | 6 8 | 591C651G01 | 6 － | $591 \mathrm{C651G01}$ | 12 （6） | 591C651G01 |
| Insulating Link Assembly | 4 | 10 | 3 | 788A 588G01 | 3 | 788A588GO1 | 3 | 788A588G03 |
| Main Disconnecting Contact Assembly （not included in Pole Unit Assembly） | 3 | － | 6 | $591 \mathrm{C655GO2}$ | 6 | 591C655G02 | 6 | $591 \mathrm{C} 655 \mathrm{G03}$ |

（3）Recommended Spare－See page 2.
11）See pare if figure 12 for illustration of the DSL． 206.
（2）The DS． 20015 pole unit is not illustrated．The 1）S 206S pole unir assembly is smitar to the DS－ith，with the upper and lower stud assemblies mounted on a reparare molded base for tach pole rather than a common hatse for the three poles．

## 3．1．1－295



Fig. 5
Type DS-416 Pole Unit Assembly-Front View


Fig. 6
Type DS-416 Pole Unit Assembly-Rear Vien

| Description |  |  | DS-416 |  | DSL-416 ${ }^{(1)}$ |  | DS-416Sand DS-420 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fig. No. | item No. | No. <br> Req. <br> Per <br> Bkr. | Style Number | No. Req. Per Bkr. | Style Number | No. <br> Req. <br> Per <br> Bkr. | Style Number |
| Single Pole Unit Assembly Complete | 5-6 | - | 3 | 151 D064G01 | 3 | 151D065G01 | 3 | 15iD065G02 |
| Following are included in Single Pole Unit Assembly: |  |  |  |  |  |  |  |  |
| Molded Base | 5 | 1 | 3 | 553F204H01 | 3 | 553F204HO1 | 3 | 553F204HO1 |
| Upper Stud Assembly | 5 | 2 | 3 | $591 \mathrm{C} 750 \mathrm{GO2}$ | 3 B | 1390635 GO 1 | $3 \text { 各 }$ | $1390635 \mathrm{GO2}$ |
| Lower Stud Assembly | 5 | 3 | 3 | 1260298G06 | 3 | $1390633 G 04$ | $3$ | $139 D 633 G 05$ |
| Following are included in Upper Stud Assembly: |  |  |  |  |  |  |  |  |
| Stationary Arcing Contact - R.H. | 5 | 4 | $3 \cdot 1$ | 5038025G01 | 3 (1) | 503B025G01 | 3 (1) | 5038025GO1 |
| Stationary Arcing Contact-L.H. | 5 | 4 | 3 B | 503B025G02 | 3 (1) | 503B025G02 | 3 R | 503B025GO2 |
| Stationary Arcing Contact Spring | 5 | 5 | 6 E | 5038027HO1 | 6 6 | 503 BO 7 HO | 6 \% | 503 BO 27 HO 1 |
| Stationary Main Contact Finger | 5 | 6 |  | 809A263G01 | 36 (2) | 809A263GO1 | 36 (2) | 809A263GO1 |
| Stationary Main Contact SpringOuter |  |  | 12 A | 5038027H05 | 12 (2) | $503 \mathrm{CO} 7 \mathrm{HO5}$ | $12(2)$ | $5038027 \mathrm{HO5}$ |
| Stationary Main Contact SpringInner |  |  | - |  | 12 (2) | 5038027 H 10 | 12 (2) | 503B027H10 |
| Following are included in Lower Stud Assembly: | $\cdots$ |  |  | - |  | - - .. -- |  |  |
| Moving Arcing Contact | 6 | 1 | 3 ¢ | 503B022G01 | 3 E | 503B022G01 | 3 - | 503B022GO1 |
| Moving Main Contact | 6 | 2 | 3 . ${ }^{\text {E }}$ | 665A321 GO1 | 3 B | 795A 769 GO 1 | 3 (3) | 795A 769 GO 1 |
| Insulating Link Assembly | 5 | 7 | 3 | 436B450G02 | 3 | 4368450GO2 | 3 | 436B450G02 |
| Main Disconnecting Contact Assembly (not included in Pole Unit Assembly) | 3 | - | 6 | 682C347G01 | 6 | 682C347GO1 | 6 | 590C804GO1 |

2 Recommended Spare-See palic 2.

1) See pase 16 fisure 31 for illustration of the DSL. -1 th.

12, A sembly of the stationary main contact finsers and inner and outer springs is difficult. The Upper Siud issemibly in recommended for the DSL-16. DS-4itS and DS-420.
1.3) Changing the mowing main confact is complicated hesause , if a drillint and pinnina "peration. The Lower Stud Asembls wecimmended bip the DS. + ins and DS-I 0 .
3.1.1-296


Fig. 7 DS-632 Breaker with Front Panel Removed


Fig. 10 DS-840 Breaker with Front Panel Removed


Fig. 8 Type DS-632 Pole Unit Assembly - Front View


Fig. 11 Type DS-840 Pole Unit Assembly-Front View


1. Recommended Spare - See pale?
11) A ssemthly of the stalionary main contact fingers and inner and outer sprimss is difficult.

1 he U'pper Stud Asscmbly is recommended. 3.1.1-298
121 Assembly of the moving main contact is difficult. The l.ower Siud Asvembly is recommended.

## Arc Chutes and Barriers



Levering Mechanism


Fig. 18 Levering Mechanism
Levering Mechanism — Fig. 18

|  |  | All Type DS/DSL except DS. 840 | DS 8840 |
| :---: | :---: | :---: | :---: |
| Description | per Breaker | Style Number | Style Number |
| Levering Mechanism Assembly Following are included in Assembly: | 1 | 4490224G04 | 4490224G05 |
| Traveling Stop Nut | 1 | $7914674 \mathrm{HO1}$ | 791 A674HO1 |
| Retaining Clamp | 1 | $7914679 \mathrm{HO1}$ | 791A679H01 |
| Following are not included in Assemoly: |  |  |  |
| Crank Arm with Roiler | 2 | 786A586G01 | 567F993G02 |
| Special Bolt | $2(1)$ | 794A024HO1 | 794A024HO1 (1) |
| Elastic Siop Nut | $2(1)$ | 70220ERN 18 | 70220ERN 18 (1) |

(1) For DS. $8 \mathbf{4 0}$ four are required per breaker.

## Mechanism and Related Parts



Mechanism and Related Parts


## Mechanism and Related Parts



Fig. 23 Tip, Spring Release. and Spring Charging Details


## Type DS Circuit Breaker Automatic Tripping System

are available:

| Model | Style Number <br> $-60 ~ H Z$ |
| :--- | :--- |
| LI | $6998002 \mathrm{GO1}$ |
| LIG | $6998002 \mathrm{GO2}(1)$ |
| LS | $6998002 \mathrm{G03}$ |
| LSG | $6998002 \mathrm{GO4}(1)$ |
| LSIG | $6998002 \mathrm{GO5}(1)$ |
| LSI | $6998002 \mathrm{G06}$ |

1) For DS-6.32 and DS-R40 use Groups 62. 64. 65 and 82.84 .85 respectively.
LI. LIG, LS, LSG. LSI. LSIG


Fig. 25
Amptector II-A Solid-Slate Tip
Amptector II-A can be supplied in three models or combinations of three independent con:nuously adjustable overcurrent pping functions: long delay. hort delay and instantaneous. These models are:
DUiDual - Long delay and instantaneous


DIRECT TRIP ACTUATOR FIGURE NO. 26
All type DS Breakers use Style Number 592C114G03 (with Black Magnet Ass'y)
Exception: If a breaker is equipped with an earlier Amptector II Style 151D792G series, use actuator style 592C114G01 (with Red Magnet Ass y).

## SENSORS

See Figure 3 for Typical Sensors
Refer to I.B. 33-790-1E. Table 4. for application of sensors.

| Sensor Rating Amperes | Sensor Style Number |
| :---: | :---: |
| 50 | 794A170G01 |
| 100 | 151 D995G01 |
| 150 | 1510995 G 15 |
| 200 | 151D995G02 |
| 300 | 151D995G03 |
| 400 | $1510995 G 04$ |
| 600 | $1510995 G 06$ |
| 800 | $1510995 \mathrm{G08}$ |
| 1200 | 151D995G12 |
| 1600 | 1510995G16 |
| 2000 | $1510995 G 20$ |
| 2400 | 1510995G24 |
| 3200 | 151 D995G32 |
| 4000 | 588C734G01 |

SEISelectivel-Long delay and shor delay
TRITriple - Long delay. short delay and instantaneous

| Model | Style Number <br> -60 HZ |
| :---: | :--- |
| DU | $6997020 \mathrm{G41}$ |
| SE | $6997020 \mathrm{G42}$ |
| TR | $6997020 \mathrm{G43}$ |

## NOTE:

For information on application and operation of the automatic tripping system refer to Section 8 of Instruction Book 32-740-1E.

## Optional Accessories



Fig. 29 Auxiliary Switches - See page 3 for identification of auciliury switches.

## Optional Accessories



Fig. 30 Underwattage Trip Device


Fig. 31 Overcurrent Trip Switch

| UNDERVOLTAGE TRIP DEVICE-FIGURE NO. 30 |  |  | OVERCURRENT TRIP SWITCH - FIGURE NO. 31 For all type DS/DSL except DS-840 (1). |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage | UndervaltageInstantaneous | Undervoltage Time Delay |  |  |  |  |
|  |  |  | Manual Reset |  |  |  |
|  | All DS/DSL <br> Except DS-840 (1) | $\begin{aligned} & \text { All DS/DSL } \\ & \text { Except DS-840 (2) } \end{aligned}$ | 2 Contact |  | 3 Contact | 4 Contact |
| $\begin{aligned} & 12060 \mathrm{HZ} \\ & 20860 \mathrm{HZ} \\ & 24060 \mathrm{HZ} \\ & 46060 \mathrm{HZ} \\ & 48 \mathrm{DC} \\ & 125 \mathrm{DC} \\ & 250 \mathrm{DC} \\ & \hline \end{aligned}$ | 3752A05GO1$3752 A 05 \mathrm{GO} 2$$3752 A 05 \mathrm{GO} 3$$3752 A 05 \mathrm{GO4}$$3752 A 05 \mathrm{G} 05$$3752 A 05 \mathrm{GO}$3752 A 05 G 07 | $\begin{aligned} & 3752 A 06 G O 1 \\ & 3752 A 06 G 02 \\ & 3752 A 06 G 03 \\ & 3752 A 06 G 04 \\ & 3752 A 06 G 05 \\ & 3752 A 06 G 06 \\ & 3752 A 06 G 07 \\ & \hline \end{aligned}$ | 3752A04GO1 |  | 3752A04GO2 | 3752A04G03 |
|  |  |  | Electrical Reset |  |  |  |
|  |  |  | Voltage | 2 Contact |  | 3 Contact |
|  |  |  | 48 DC | 3752A | 4G04 | 3752A04G09 |
|  |  |  | 115 AC | 3752A | 4G05 | 3752A04G10 |
|  |  |  | 125 DC 230 AC 250 DC | 3752A04G06 |  | $\begin{aligned} & 3752 \mathrm{AO} 4 \mathrm{G} 11 \\ & 3752 \mathrm{AO} \mathrm{G} 12 \end{aligned}$ |
| (1) For DS-R40 use corresponding groups of 3752 A 25 <br> (2) For DS-840 use corresponding groups of 3752A26 |  |  |  | $\begin{aligned} & 3752 A 04 G 07 \\ & 3752 A 04 G O 8 \end{aligned}$ |  |  |
|  |  |  | 3752A04G13 |  |  |  |


| Special Voltage | All DS/DSL including DS 840 | All DS/DSL including DS-840 |
| :---: | :---: | :---: |
| 24 DC | 3752A45GO1 | 3752A46GO1 |
| 11550 Hz | 3752A45G02 | 3752A46G02 |
| 20850 Hz | 3752A45G03 | 3752A46G03 |
| 23050 Hz | 3752A45G04 | 3752A46G04 |
| $400 / 50 \mathrm{~Hz}$ | 3752A45G05 | 3752A46G05 |
| 46050 HZ | 3752A45G06 | 3752A46G06 |

1 11 For DS- 840 use corresponding groups of 3752A24.
All styles include mounting hardware and wire leads for field replacement When addinu to existing breakers other components may be needed.
For repiacement of switches only order style 6898D52A01 which consisis of iwo switches. a switch bracket and rivets.

NOTES
" styles include mounting hardware and wire leads for fietd replacement. n addiny to existing breakers. secondarv contacts will be required.

The undervoltase trip device is availahle as a complete assembly. The coil tly is not recommended as it is rineted intuthe ussembly.

## DSL-206 and DSL-416 Breakers

Parts for pole units, arc chutes. mechimisms, etc.
for DSL breakers are identified on preceeding pages of this R.P.D.

|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Description | Fig. No. | Number Required per Breaker | $\begin{aligned} & \text { DSL- } 206 \text { and } \\ & \text { DSL. } 416 \\ & \text { Style Number } \end{aligned}$ |
|  | Blown Limiter Indicator Ass'y. | 32 | 1 | 140D777GO1 |
|  | Isolating <br> Transformer Ass'y. (includes <br> 3 transformers | $33$ | 1 | $591 \mathrm{C755G01}$ |
|  | Transformer Only: | 33 | 3 | 795A823HO1 |
|  |  |  |  |  |

(B) LIMITERS-FIGURES 32-33

Refer to I.B. 33-790-1E. Table 5, for application of limiters.

| Breaker Type | Number Required per Breaker | Rating Amps | Style Number |
| :---: | :---: | :---: | :---: |
| DSL-206 | 3 | 150 | 140D316G01 |
|  | 3 | 200 | 1400316 GO |
|  | 3 | 250 | 1400316 GO |
|  | 3 | 300 | 1400316 GO 4 |
|  | 3 | 400 | 1400316 GO 5 |
|  | 3 | 600 | 140D316G06 |
|  | 3 | 800 | 140D316G07 |
|  | 3 | 1200 | 140D316G10 |
|  | 3 | 1600 | 1400316 G 11 |
|  | 3 | 2000 | 140D316G 12 |
| DSL-496 | 3 | 800 | $1510932 \mathrm{GO1}$ |
|  | 3 | 1000 | 1510932G02 |
|  | 3 | 1200 | 1510932G03 |
|  | 3 | 1600 | $1510932 \mathrm{GO4}$ |
|  | 3 | 2000 | $1510932 \mathrm{GO5}$ |
|  | 3 | 2500 | $1510932 \mathrm{GO9}$ |
|  | 3 | 3000 | 1510932 G 10 |

[^12]Assembled Switchgear

Renewal
Parts Data
32 -250
Type DS 420

Recommendations for Stock
Refer to I.B. 33-790-IB for Maintenance and Parts Identification

| Ret. No. | Unit Quantity | Style Number | Description |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fig. 56 |  | 795A769G01 503B022G01 503B025G01 503B025G02 503B027H01 809A263G01 503B027H05 503B027H10 |  | POLE | ARTS |  |  |
| It. 7 | 3* |  | Moving Main Contact <br> Moving Arcing Contact <br> Stationary Arcing Contact - L.H. <br> Stationary Arcing Contact - R.H. <br> Stationary Arcing Contact Spring <br> Stationary Main Contact Finger <br> Main Contact Spring - Outer <br> Main Contact Spring - Inner |  |  |  |  |
| It. 8 | 3* |  |  |  |  |  |  |
| It. 16 | $3^{*}$ |  |  |  |  |  |  |
| It. 17 | 3* |  |  |  |  |  |  |
| It. 18 | 6* |  |  |  |  |  |  |
| It. 21 | 36* |  |  |  |  |  |  |
| It. 23 | 12* |  |  |  |  |  |  |
| It. 23 | 12* |  |  |  |  |  |  |
|  |  |  | DS - SWITCHGEAR COMMON PARTS |  |  |  |  |
|  |  | 436B621H05 <br> 795A077H01 <br> 503B601H11 <br> 503B601 H04 | MECHANISM SPRINGS <br> Trip Bar Reset <br> Trip Latch Reset <br> Oscillator Reset <br> Opening |  |  |  |  |
|  | $\begin{aligned} & 1 \\ & 1 \\ & 1+ \\ & 1 \end{aligned}$ |  |  |  |  |  |  |
|  |  | $\begin{aligned} & \text { 449D622G21 } \\ & \text { 450D818G02 } \end{aligned}$ | SWITCHES |  |  |  |  |
|  | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  | Auxiliary <br> Motor Cut-Off |  |  |  |  |
| Voits | Cycles | Spring Release Coils |  | Shunt Trip Coils | U.V. Trip Coils | Complete-Anti Pump Relay | Motor Kit |
| 24 | D-C | - - |  | 151D786G01 |  |  |  |
| 32 | D-C | -- |  | 151D786G03 | - - | - - | - - |
| 48 125 | D-C | $151 \mathrm{D786G04}$ |  | 151D786G04 | 300P896G01 | 140D930H03 |  |
| 125 | D-C | 151D786G08 |  | 151D786G08 | $300 \mathrm{P897G01}$ |  | 449D431G03 |
| 250 | D-C |  |  | 151D786G11 | 794A214G01 | 140D930G05 | 449D431G01 |
| 208 | A-C | 151D786G02 |  | 151D786G04 | 300P044G01 | 140D930H01 | 449D431G01 |
| 240 | A-C | 151D786G05 |  | 151D786G08 |  | - ---7930402 | -- |
| 480 |  |  |  | -.-- | $\begin{aligned} & 300 \text { P896G } \\ & 1491405 \end{aligned}$ | 140D930H02 | 449D431G02 |

* For Power Breakers only.
* The quantities specified are those required to replace both arcing and main contacts of one breaker.

Parts indented are included in the part under which they are indented. Order part by name and identification number-give complete nameplate reading.

TYPE DS-416 AIR CIRCUTT BREAKER Motor or Manual Operated - 600 Ampere

Renewal Parts Data

32-250
Type DS-416

Recommendations for Stock
Refer to 1.B 33-790.IB for Maintenance and Parts Identification

©. Use after June, 1971

- For Power Breakers only
- The quantities specified are those required to replace both arcing and main contacts of one breaker.

Parts indented are included in the part under which they are indented. Order part by name and identification number-give complete nameplate reading




November 1977
Supersedes Descriptive Bulletin 36-553 dated January, 1972 and $36-553 A D$ WE A dated September, 1975
Mailed to: E. D. Ci1968OB

Indoor frame mounted 2.4 kV to 34.5 kV .
Indoor and outdoor enclosed non-fused 2.4 kV to 15 kV .

Indoor and outdoor enclosed fused 2.4 kV to 15 kV .

Type AWP Load Interrupter Switch



Fromt Opwated Enciosed. Fused Switch


Side Opwruted Enclosed Wall Mountad Switeh

Desc ?on
The. load interrupter switch, frame mounted. is a full rated quick make-quick break spring stored energy operated switch which provides. fast and reliable protection - تingh voltage circuits 2.4 kV through 34.5 kV .

## Application

AWP interrupter switches are available in umized three pole, frame mounted construction for mounting in enclosures or assemblies. These units can be applied separately or in conjunction with fuses. Ther provide non-automatic switching for sectionslizing primary feeders. and isolation for Iransformer banks, capacitors, voltage regulators and similar applications. When used in series with expulsion or current limiling fuses. the combination provides a higner interrupting rating against faults. within the capability of the fuse rating.

## Front Opersted

The front operated type AWP switch is avariable in open frame mounted design from 5 kV inrough 34.5 kV . and is avallable in both 'gnt or left hand operation. In this design the veerating handle is removabie and is intended :o oe stored within the access door of its enciosure

## Side Oper ated

This swith design is available in open frame mounting from 5 kV through 34.5 kV , and is avaty in both right or left hand operation. The c....ating handle is fixed and requires no storage facility. On side operated units zoerating handles are available for either (1) nand operation or (2) hookstick operation. Fig. 23.

Frame mounted AWP switches, 5 kV to 15 a $v$ can be supplied with a 600 or 1200 ampere tentinuous current and load break feature i 230 and 345 kV the continuous current : 3ining can be 1200 amperes, but only with a 500 ampere load break feature.

Foulr close of 20,000, 40,000 and 61.000 dmperes is available in the voltage range from I kV to 230 kV . and onty 20.000 and 30.000 -mperes at 345 kV

The open frame mounted AWP switches are terengned for indoor applications and must be mounted in a suitable metal enclosure of sceruats strength to withstand the short erpcuit fortes.
Reter so Component Sales East Pittsburgh
Nor trame mounted motor operated AWP onrtehos.

Nathoge

| Mas. Volt | Nom. <br> Vot | $\begin{aligned} & \text { BIL } \\ & \mathbf{\& V} . \end{aligned}$ | Cortinuous Ampe | Interrupting Current | Momentary |  | Faut Close (1) ha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 10 Hz . <br> Aeym. KA | 4 SEC. <br> Sym. ka |  |
| Tebid A: 5 kV |  |  |  |  |  |  |  |
| 50 | 48 | 60 | 600 | 600 | 40 | 25 | 20 |
| 5.0 | 48 | 60 | 600 | 600 | 40 | 25 | 40 |
| 5.0 | 4.8 | 60 | 1200 | 800 | 80 | . 38 | 81 |
| 5.0 | 48 | 60 | 1200 | 1200 | 80 | 38 | 61 |
| Tebie 8: 8.25 mV |  |  |  |  |  | - |  |
| 8.25 | 72 | 75 | 600 | 800 | 40 | 25 | 20 |
| 8.25 | 7.2 | 75 | 600 | 600 | 40 | 25 | 40 |
| 8.25 | 7.2 | 78 | 1200 | 800 | 80 | 38 | 61 |
| 8.25 | 7.2 | 75 | 1200 | 1200 | 80 | 38 | 61 |
| Toblec: 18 mv |  |  |  |  |  |  |  |
| 150 | 13.2 | 96 | 600 | 600 | 40 | 25 | 20 |
| 15.0 | 13.2 | 96 | 600 | 600 | 40 | 25 | 40 |
| 15.0 | 13.2 | 95 | 1200 | 600 | 80 | 38 | 40 |
| 150 | 13.2 | 98 | 1200 | 800 | 80 | 38 | 61 |
| 15.0 | 13.2 | 95 | 1200 | 1200 | 80 | 38 | 40 |
| 15.0 | 13.2 | 96 | 1200 | 1200 | 80 | 38 | 61 |
| Teble D: 25.aty |  |  |  |  |  |  |  |
| 25.8 | 23.0 | 150 | 600 | 600 | 40 | 25 | 20 |
| 25.8 | 23.0 | 150 | 600 | 600 | 40 | 25 | 40 |
| 25.8 | 23.0 | 150 | 1200 | 600 | 40 | 25 | 40 |
| 25.8 | 23.0 | 150 | 1200 | 800 | 81 | 38 | 61 |
|  |  |  |  |  |  |  |  |
| 38.0 | 345 | 150 | 600 | 600 | 40 | 29 | 20 |
| 38.0 | 34.5 | 150 | 600 | 600 | 40 | 25 | 30 |
| 38.0 | 34.5 | 150 | 1200 | 600 | 40 | 25 | 30 |
| 38.0 | 34.5 | 150 | 1200 | 600 | 61 | 38 | 30 |

(1) Alt foult chasing tests are done st maxamum voftage rating and without any protective fusing


Special side operetod AWP switches are specifically deaigned for mounting within 30 inch mine rectifiere but cin be eppotied where limited spece sis required

## Design Features

## Stored energy nechanism:

The AWP quick make-quick break stored energy mechanism provides constant highspeed opening and closing and is capable of closing and holding on its rated fault current. The speed and force of opening and closing the contacts are both independent of the handie operation stroke.

The energy for the operation of the switch is provided by a spring that is compressed and released through a mechanical linkage.

## Operation

Closing the from operated switch is accomplished by inserting the handie into the handle casting, Figure 1. An upward motion of the handie starts the rotation of the handle casting assembly. Through a mecthanical linkage this operates a spring lever. Figure 2.3 and 4. which compresses the spring. When the spring lever reaches the over toggle position. the spring releases its energy and closes the main contacts.

The opening cycle is initiated by a downward motion of the handle with the mechanical sequence repeated.

In the case of the side operated switch the handle is "fixed" and iravels vertically in an arc of 120 degrees. approximately 60 degrees on each side of the operating shaft center line.


Froure 1


Figure 3

figure 4


## Design Features (Continued)

## Main Contact

The main contacts, break and hinge end. are made of high conductivity hard drawn copper. For 40,000 and 61.000 ampere fault closing. the break end is provided with a copper tungsten alloy arcing tip, Figure 5.

The hinge end consists of two pieces of copper fastened together. Proper electrical contact is maintained when the blade is attached to the hinge contact with a boit and spring washer. To further assure good electrical contact at 1200 amperes. the hinge end is also provided with silver rings at the moving point. Figure 6.

The blade consists of two high conductivity hard drawn copper bars in parallel, Figure 7. Since the electrical contact point for 600 amperes is silver to copper, the blades are provided with a silver ring at the hinge end and a copper embossed silver plated main contact point. On 40.000 and 61,000 ampere fault close ratings. copper tungsten alloy arcing buttons are provided to prevent damage to main break contact.
The two bars are fastened together to form the single blade at the hinge and break end. To assure permanent high contact pressure. self-adjusting slotted spring washers of phosphorus bronze are drawn tight over machined spacers. This provides flexibility in meating stresses from distortion due to load or from uneven mounting, Figures 6 and 8.

## Arc Chute

The arc chutes consist of two pieces of UREA formaidehyde fastened together to produce gas under high current conditions to extinguisu the arc. Contacts within the are chute restrain the flicker blade assembly untii the spring is charged prior to opening, figures 5 and 8.

## Insulators

Glass polyester insulators are standard equipment on switches rated 5.0 kV and 15 kV. Porcelain insulators can be furnished as an odtional feature. Porcelain insulators are standard on 7.2. 23.0 and 34.5 kV

## Jesign Features (Continued)

## Ficker Blade

The flicker blade is connected to the side and parallel to the main blade. It is constructed of hard drawn copper with an arc resisting silver tungsten alloy tio. Figure 9 . In the opening sequence as the main blade separates from the main break contact, the current is transferred to the flicker blade which is being restrained by the high pressure contacts within the arc chute. Once the maximum angular movement between the flicker blade and main blade has been reached. the flicker blade starts to move out of the are chute contacis. The additional pull of the torsional spring on the flicker blade assembly snaps the blade into an open position at high speed.

The heat of the are releases a blast of deionizing gas from the arc chamber. This combination of the quick break and De-ion action quickly extinguishes the arc deenergizing the ciruit.
For maintenance purposes or replacement. only the flicker blade portion need be removed.

## Terminals

The terminal pads for both the 600 and 1200 ampere switches are high conductivity hard drawr copper bar with standard NEMA illing. Figures 5. 6 and 9. For the mine application AWP swith the terminal pads are shortened to provide for insulated cable cunnections. (See page 2).

## Blade Alignment

Blade and contact alignment for maintenance purposes can be checked with ease The AWP Swith is supplied with slow close feature inserting the operating lever into the hub located on the shatt and using an upward motion. Figure 10. the switch blades can be readily moved for alignment check with main contacts The switch cannot be fully latched with this slow close feature and once the lever is released the switch will always revert to the open position

## Barriers and Drive Rods

The barriers and drive rods are made of flame retardant glass polyester. The drive rods are also track resistant, Figure 11.

## Standardization

The AWP was designed to be as tlexible and simple as possible Parts may be readily added or removed for changing applications.


Figure 10


Figure 11


Figure 12


Figure 14

Figure 13


Figure is

Door Interlocks and Special Features
Since the speed and force of closing the main contacts are independent of the lever closing operation, the AWP has an inherent built-in anti-tease mechanism. Each swith has two mechanical interlocks. The door interlock is a hook lug arrangement on the shatt which engages a ring mounted on the enclosure door, Figure 12. This prevents the door from being opened while the switch is in the closed position. The other interlock prevents the switch from being closed while the door is opened. The latch. Figure 13, must be pushed forward by a latch lug mounted on the enclosure door to close switch. For maintenance purposes only, this latch may be disengaged. Prior to such maintenance all sources of power to the switch must be de-energized.
To prevent contact with live parts through the mechanism cover plate, a bariler surrounds the operating mechanism. solating if from the main current carrying parts of the switch. Figure 14.
In addition to the built-in interlocks. on front operated switches there are provisions for two kirk key interiocks. Figure 15 , which will allow the switch to be locked in open or closed positions. plus provision for one padlock. Figure 13 Similar provisions are available on side operated switches when mounted in an enclosure.

When a key interiock (s) is required. on front operated switches holes are provided ifigure 15) for lock mounting. Additional material is required to complete the lock installation. Refer to "Accessories" in price list.
Padlock provision, Figure 13 \& 23, will accommodate one padlock. An adapter is available to accommodate additional padlocks if required.

## Descriptive Bulletin

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page 7

## Operation of Electrical/Manual Stored Energy Mechanism

The electrical/manual stored energy mechanism portion of the AWP Switch is located on the right side of the switch just above the operating shaft and handle casting assembly. Figure 16.
The unit is a mechanical linkage consisting of a teeter bar, double toggle assembly and a shunt trip coil. Closing of this switch is accomplished by inserting the handle into the handie casting. An upward motion of the handle starts the rotation of the casting assembly. Through a mechanical linkage, this operates a spring lever which compresses the spring. When the spring lever reaches the over toggle position. the spring tends to release its energy and tries to move the
oderating shaft. The movement is restrained by a linkage which transfers the energy inta the double toggle assembly.

The switch can now be closed by tripping the double toggle assembly using a manuai release located in front of the switch or remotely by the shunt trip coil.
Cnce the switch is closed, the opening cycle is made ready by a downward motion of the handle: the double toggle assembly is reset after each open or close cycle allowing the mechanical sequence to repeat. Again the switch can now be opened manually or electrically. Shunt trip coil voltages can be 48 volts dc. 125 volts dc. 250 volts dc. 115 volts ac and 230 volts ac. Shunt trip attachment is available on 2.4 through 15 kV units only.


Figure 17

## Special Features

indicators located at the operating end are provided to show if the spring is charged or if the switch is opened or closed. Figure 19.
A shaft lock assembly is provided on the left side of the switch to prevent the switch from operating when the door is opened and the switch charged for operation. Figure 17. For maintenance purposes onlw, this tatch may be disengaged. Prior to such maintenance all sources of power to the switch must be de-energized.
On this type of operating mechanism, Kirk Key Interlocks cannor be provided: however, there is provision for padlocks on the nandie casting. Figure 16.

## Access Door

An access door Fig. 18 to the switch operating mechanism can be provided for mounting on caomet door. This door assembly can be used for erther indoor or outdoor application. Orawing pertaining to cutout requirements for mounting may be found on page 5 of Technical Certification Section 36-573.

## Test Data

Tests were performed on 5.0 kV through 345 kV 600 and 1200 ampere switches in accordance with NEMA STD SG6. ANSI C37-32 and Canadian Standard C105-1960 These certified tests are available upon cequest.
Pertinent data. such as interrupting capabilities, fault closing and momentary. are listed in Table on page 2. To further hignight the design teatures of the AWP, it is capable of interrupting magnetizing currents of transtormer at low power factor, and at 23.0 kV cable charging currents. This data is aiso avarlable upon request.


Figure 18


Figure 19

## Enclosures

Enclosures for the rype AWP switch are available for side operated, wall mounted. unfused units, Figure 19A, as well as the fused units which can be side or front operated. 5 kV through 15 kV These enclosures are made of 11 gauge steet and are of bolted construction. Figure 20. All steel used in the enclosure is cleaned and phosphatized in preparation for painting. The paint used in standard production is light gray ANSI-61 for indoor applications and ANSI- 70 for outdoor applications.
Each enclosure door contans a window through which the switch unit can be observed. The window is tempered reinforced glass which meets all applicable standards and is free floating in a rubber molding. ISee Figure 20) The door of each enclosure is mounted on three (3) hinges and latches at three (3) points with iwo (2) handles. Figure 21
Each enclosure door of the front operated unit is equipped with an access door through which the swith may be operated. Figure 20 Each enclosure door is equipped with a door interlock which prevents opening the enclosure door when the switen contacts are closed. Figure 21. and utlizes the open door interlock as described on page 6 under door interlock features.

WII fuse mountings designed for use vithin the enclosed AWP switch are of the non-disconnect type.

Fuse units used in conjunction with these mounungs can be erther the RBA-200. 400. 800. CLE. CLE-1-2-3. CLT or CX. dependent upon the proper application


Figure 19a
Non-Fused Side Operated Enciosed Well Mounted Switch


Figure 20


Figurs 21
at enchosures which incorporate fuses - in ineir design a hinged shield over the - -icn compartment to prevent contact with - ive pars while working in the fuse omoenment. Figure 22

Seamard enclosures provide for cable enersence in the top and out the bottom. Concurt locations are identified for drilling ourooses. When the requirement arises to nove the cables in and out either the top or the verion a module is added to the back of the merten. Figure 24, to provide space for rear connections. When the rear compartment - coced. the rear panet of the standard enc:osure is omitted to provide access to the - er comoartment. These two compartments are snipped boited together and may be veourared. if desired for ease of installation 34 cable. Figure 24. Each compartment is equipoed with lifing lugs bolted into place and which may be removed after installation.
$\triangle W P$ Switches 5.0 kV to 15.0 kV can be sotaned in weatherproof and dust tight onclosures. The standard outdoor enclosure isucolied with a conduit adapter but roof zushings are available. Other equipment which can be mounted in the enclosure inctudes auxiliary swriches and potheads. All enclosures are furnished with grounding tuge "qure 21.


Figure 24


Figure 25

Outline Dimensions 5-15 kV Enclosures


PUSED -
side of Fromt Operatied


Cable In rooOut Bortam


Figur 31
Cabie in Bontom Out Bottom


Indoor, Outdoor or Dust Proof Enciosure with Side Operated Mechaninm


Fipure 34 - Cuble in Bercomb-Out Elatrom


Pryere 38 - Cable in Top-Oue Topl

3.1.1-323

Mounting Hole. Conduit Hole and Cable Hole Locations


## Further Information

F.Ctis!36-523, 36-524
$\cdot .573$

## Wertinghouse Electric Corporation

"iverentiear Division
tisiontisourgh. PA 15112

IStancord AWP Load Interrupter Switch (Fiont and Side Operated)
hcoor. 2.4 Kv Through 13.8 Kv


Shunt Trip Mechanism : Check East Pittsburgh for Avanability) I I
Auxiliary Switeng
Deeration Counter
*) inverted Switen Operation

-ccess Door Assemblv
Stanaara Door Oraer Style 1400884G01)(3)
Door with Handle Locx Order Style 1400884GO2)
万ult bosing tesis Jone at maximum voliage rating anc
rcilanv orctect.verisirg
rcxec orfersm Wh.j3
V: storkea:oreer on N-3)
-rer ov cescration on Y 3.

e soec al etec:rcai manlal stored energy mecharism
:- shur: zages 3 and two auxiliary switcres , See TCS 36 -
3 zages $3 \cdot 5$.
usale or sek-lyde $=\mathrm{VOE}$
Fwren Jrovicea witr grovisions ror Kirk Key Lock Type

- Nur." zrolecion
*iten provided wht nasss tor padocking handie.


## Prices Include:

Three cole, single throw, tront connected, growo-oderated AWP switch with pole units. oarriers and manual operating mechanism on a common trame. Prices do not include terminal connectors. Terminal conneciors can be ordered by referring to $D B 34-350$ and Pnce List 34-320.

## Ordering Information

When orcering switch that is carried in W-89 stock. craer by style number. Switches not carried in stcck order on W- 19 by Style Number - 5 to 8 weeks delivery.

## Shipment

Qutain shipment quotation on all nen-stock items from Switchgear Division, Component Sates, East Pittsjurgh, Pa.
1.L. 15002-A

## 1. TENERAL

The Type AWP Interrupter Switch is a coordinated 3-pole assembly which combines the function of a disconnect switch with the ability to interrupt load and magnetizing currents. It also has a fault closing capacity which enables it to be closed against a short circuit without sustaining significant damage, after the fault has been cleared by suitable protective equipment, the switch can subsequently remain in service. Its performance satisfies all requirements of ANSI Standard Specification C37.32. The Type AWP Switch differs from a circuit breaker in that it does not have a fault breaking capacity and that its operation is not automatic. The Type AWP Switch is designed for operation in a proper metal enclosure with or without fuses.

Caution: It is NOT SAFE to operate the switch outside an enclosure unless equivalent protection has been provided for the operating personnel.

## 2. DESCRIPTION

The Type AWP Switch is comprised of the following basic components:

### 2.1 Frame

A frame for 3 blade assemblies and operating mechanism.

### 2.2 Main Blades and Jaws

The main contacts, break and hinge end, are hard drawn copper. For 40 KA and 61 KA fault closing, the break jaw is provided with a copper tungsten arcing tip. The blades are also hard drawn copper and copper tungsten arc buttons are provided for the 40 KA and 61 KA ratings.

### 2.3 Load Interrupter

It consists of a Flicker Blade and engaging contact fingers located inside a De-ion ${ }^{(0)}$ arc chute. On opening of the switch the main blades open first which shunts the current through the spring loaded tlicker blades. Further travel of the main blades causes the tlicker blades to snap out of
their contact fingers and arcs are drawn within the De-ion arc chutes. Positive arc interruption is accomplished by the de-ionizing action of the arc chutes in combination with the high opening speed of the spring loaded flicker blades.

### 2.4 Operating Mechanism

The main blade quick-make, quick-break mechanism is a compression spring operated by a rod connected to the spring lever which in turn is attached to the switch shaft. To close the switch, a removable handle is inserted into the handle casting which is then rotated through an angle of $120^{\circ}$. This charges the compression spring and as the spring lever goes over toggle the stored energy of the spring is transferred to the shaft which snaps the switch closed. The mechanism is operated similarly for opening of the switch. This quick make mechanism provides the power to overcome blow-out forces which occur when the switch is closed against a fault. However, these forces are not transmitted to the operating handle since it is not rigidly connected with the blades. Therefore it is SAFE to close the switch under short circuit conditions within its rating.



## De-ion Quick-break Operation

1. Switch closed... When the switch is closed, practically all the current flows through the main biade.
2. Main blade opens... As the main contacts separate, current is transferred momentarily through the flicker blade, which is held in the arc chute by high pressure contact fingers.

The main blade opens until the stop on the flicker blade hinge prevents further angular movernent between the main and flicker blades. This starts the flicker blade out of the high pressure contacts in the arc chamber.
3. Switch opened... The combined pull of the torsional spring in the flicker blade and the main blade operating mechanism snaps the flicker blade into the open position at high speed. The heat of the arc, meanwhiie, releases a blast of de-ionizing gas from the gas-generating material of the arc chamber. This combination of quick-break and De-ion action quickly extinguishes the arc and the circuit is safely de-energized.
2.5 Ratings - ANSI - Approved

| Amp Rating |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| KV Rating |  | Continuous |  |  | Asvm. Rating |  |
|  |  | Interrupting | FaulzClosing | 10 Cycle <br> Momentary |
| Max. | B.I.L. |  |  |  | Load | Mag. |
| 4.76 | 60 |  | 600 | 600 | 60 | 20 KA | 40,000 |
| 4.76 | 60 | 600 | 600 | 60 | 40 KA | 40,000 |
| 4.76 | 60 | 1200 | 600 | 60 | O1KA | 80,000 |
| 4.76 | 60 | 1200 | 1200 | 60 | 61 KA | 80,000 |
| 8.25 | 75 | 600 | 600 | 60 | 20 KA | 40,000 |
| 8.25 | 75 | 600 | 600 | 60 | 40 KA | +0,000 |
| 8.25 | 75 | 1200 | 600 | 60 | 61KA | 80,000 |
| 8.25 | 75 | 1200 | 1200 | 60 | 61 KA | 80,000 |
| 15.0 | 95 | 600 | 500 | 60 | 20 KA | 40.000 |
| 15.0 | 95 | 000 | 600 | 60 | 40 KAA | 40,000 |
| 15.0 | 95 | 1200 | 600 | 60 | 40 KA | 80,000 |
| 15.0 | 95 | 1200 | 1200 | 60 | 40 KA | 80,000 |
| 15.0 | 95 | 1200 | 600 | 60 | 61 KA | 80,000 |
| 15.0 | 95 | 1200 | 1200 | 60 | 61 KA | 80.000 |

## 3. INSTALLATION

### 3.1 Storage and Handling

These units should remain in their packing cases until ready to install. They should be completely protected from weather, building dirt, cement dust and the like. Reasonable care is necessary when unpacking to prevent damage. All dust and packing material should be cleaned from the interrupting chambers, contacts, and insulators.

When welding, sanding, drilling, filing or sawing operations are performed nearby, the contacts, interrupting chambers, insulators and mechanism parts should be covered and kept clean.

### 3.2 Mounting

Four holes $9 / 16^{\prime \prime}$ diameter for $1 / 2^{\prime \prime}$ bolts are provided in the base of the frame for mounting of the switch in the enclosure. This enclosure must have a slot in its front door as shown on the template drawing of Fig. 4, to clear the mechanism cam when it is rotated with the removable handle. The recommended distance between the front door and the front of the switch frame is .125 to .250 inches.

### 3.3 Power Connections

The hinge and jaw terminal pads, with standard NEMA drilling, are suitable for connection to flat bus bar runs.

### 3.4 Interlocks (See Fig. 15)

Each switch is equipped with two automatic interlocks as follows:

## A. Door Interlock

The switch shaft is equipped with a hook which engages a hasp supplied by the enclosure manufacturer and welded to the back of the enclosure door so that the door cannot be opened when the switch is closed.

## B. Door Operated Interlock

When the enclosure door is opened, a spring biased interlock link is moved into position, blocking rotation of the mechanism cam and preventing the switch from being inadvertently closed while the enclosure door is upen.

Each switch is also equipped with the following facilities for non-automatic interlocking:

## C. Padlocking

The mechanism cam has lugs permitting the switch to be padlocked in the open and/or closed positions. See Fig. 13.

## D. Key Interlocks See Figure 15

d. A key interlock can be bolted to the mechanism cover plate. The switch can be locked in the open and/or closed positions.
b. Another lock can also be provided on the mechanism cover plate to lock the switch in its open position.

### 3.5 Adjustment

Each switch is compietely factory adjusted and operated 25 times before shipment. No further adjustment should be necessary. However, in order to ensure that the adjustment has not been affected in transit or during installation, it is recommended that each switch be inspected after installation in the enclosure and before it is put into service as follows:
(a) Main and flicker blades should be in proper alignment with jaws and arc chute openings, respectively. See Fig. 8.
(b) Closed and open stops should be as follows:

Closed . The shaft rod ends should be slightly over toggle.

Open - The asstance between the edge of the main blade and the treak jaw should be $6-5 / 8^{\prime \prime} \pm 1 / 8^{\prime \prime}$.
(c) Upper spacers of main blades should rest approximately $3 / 16^{\prime \prime}$ above the bottom in the depressions of the angular switch jaws.
(d) Hardware must not be loose.
(e) Automatic and non-automatic interlocks should operate correctiy.
(f) Arc chute and insulating surfaces should be free from dust.

If the inspection revealed some defects in adjustment, this should be corrected as outlined in paragraph 4.2.

Caution Note: After the switch adjustment has been found (or made) satisfactory, the switch should be closed and opened at least three times with the quick-make, quickbreak mechanism before it is energized.

## 4. MAINTENANCE

Note: The switch must be de-energized before any maintenance is attempted.

### 4.1 Inspection Schedule

It is recommended that each switch be inspected after 24 months of service or after approximately 100 rated current interruptions, whichever occurs first. When the current interrupted is smaller than rated, the duty is proportionally lighter and more operations may be allowed before inspection. After the switch has been closed against a fault current, it should be inspected at the first opportunity at which it can be deenergized. Inspections should be conducted as listed in paragraphs $3.5(\mathrm{a})$ to $3.5(\mathrm{~g})$. In addition, it is desirable to check the foilowing: See 4.2(h) Regarding Safety Latch.
(a) Check main blade contact pieces and the leading edges of the flicker blades for arc erosion.
(b) Check the engagement of the flicker blades by inserting the handle in the handle casting and closing the switch. Now, insert the handle in the blade alignment hub on the shaft and slowly open the switch. The flicker blade should remain engaged in their contact fingers while the main blades open. When the main blades clear the break jaws, they will hit the stop on the flicker blade brackets and start the flicker biades out of their contact fingers. The flicker blades will then snap open from the forces in their charged torsional coil springs.
(c) Check barriers for carbon or metallic deposits. Replace the barriers if deposits appear excessive.
(d) Inspect arc chute sides and replace them if they are damaged.
(e) Replace worn or damaged parts of the flicker blade assembly. Arc chute must be dismantled in order to examine condition.
(f) After a fault closing operation it may be necessary to clean up the arcing contacts. This may be done with a frw light strokes of a fine file. It is only necessary to remove sharp and high points; no attempts should be made to tile
out the pit marks. DO NOT USE abrasive material for cleaning.
(g) Close and open the de-energized switch at least three times to check the performance of the operating mechanism.

Note: The main current carrying contacts should not be filed. Opening and closing of the switch will clean the contacts. However, if there is evidence of excessive burning, the main blade and hinge assembly together with the break jaw should be replaced.

### 4.2 Alignment Procedure

Note: The switch must be completely DE-ENERGIZED before any attempt to align the switch is made. See paragraph (h) for procedure to override the safety latch.

## (a) Closed-open Stop Alignment

Remove the operating mechanism safety barrier by lossening the two front bolts on the right side, slide the barrier forward to clear the handle casting, then push it to the left until the stop bolts are exposed. The top bolt and nut adjusts the open position and the bottom boit and nut adjusts the close position. In the closed position, the shaft rod ends should be slightly over toggle ( $5^{\circ}$ ). In the open position the clearance between the edge of the main blade and the break jaw should be $6-5 / 8 \pm 1 / 8$ inch.

## (b) Main Blade Alignment

Loosen the four hinge terminal bolts on top of the insulator. Loosen the two break jaw terminal bolts on top of the insulator. Insert the removable handle in the blade alignment hub on the shaft and close the switch. For safety purposes, the switch will not fully close and will revert to the open position if the pressure on the handle is released. Hold the switch in the closed position with the handle and tighten up the bolts on both the hinge and jaw terminals. An alternative to this method is to remove the drive rod from the rod end as described in paragraph (d) and align each pole separately by closing and opening the pole with the drive rod.

## (c) Flicker Blade and Arc Chute Alignment

Loosen the two arc chute mounting bolts. Adjust the arc chute so that the arc chute opening is parallel to the main blade. Lightiy tighten the arc chute mounture bolts. Using the procedure described in (b) slowly close the switch and check that the flicker biade is in line with the are chute opening. If necessary, move the arc chute left or right
until the flicker blade and arc chute line up. Tighten the arc chute mounting bolts and re-check the alignment.

## (d) Over or Under Travel of Main Blades

Close the switch by inserting the removal handle in the handle casting and push in an upward motion until the stored energy spring lever goes over toggle and the switch slams closed. Check that the upper spacers of the main blades are approximately $3 / 16^{\prime \prime}$ above the bottom of the break jaw blade stop. If it is not, remove the pin holding the drive rod to the shaft rod end. Loosen the pal nut on the rod end and turn the rod end clockwise into the shaft assembly to decrease the travel or counter-clockwise to increase the travel. Insert the pin thru the rod end and drive rod and check for proper setting. When proper setting is obtained, tighten the nut on the rod end, insert the cotter pin and spread the cotter pin.

## (e) Flicker Blade Replacement

To change a flicker blade, remove the two bolts holding the flicker blade to the flicker blade bracket. The switch must be in the open position. Remove the worn blade and replace with a new blade. Replace the two bolts and tighten the nuts.

To change a complete flicker blade assembly, remove the elastic stop nut from the bolt holding the assembly to the main blade. Using a box wrench or similar tool, hook the hole in the wrench over the torsion spring end and pull slightly forward and to the left until the spring end clears the stop post. Remove the wrench and pull out the bolt. The flicker blade assembly is now free. To install a new assembly, reverse the procedure. Be sure the spacer between the two copper bars making up the main blade is still there. Tighten the stop nut only enough to eliminate any wobbling of the assembly. Before the torsion spring is placed behind the stop post. a sideward movement of a $1 / 16^{\prime \prime}$ should be present. Too much tightening will decrease this movement and cause friction which will slow down the action of the flicker blade. Uising the same procedure for releasing the torsion spring end, put the spring end on the other side of the stop post.

## (f) Stored Energy Spring

To dis-engage the stored energy spring, remove the safery barrier as instructed in (a). Take a 5/16-18 threaded rod $4^{\prime \prime}$ long and screw it into the rear end of the spring rod. Make a spacer $1.5^{\prime \prime}$ long from a pipe or tube with a $1.0^{\prime \prime}$ 1.D. Put this over the $5 / 16^{\circ \prime}$ rod. Take a washer with an O.D. as large or larger as the O.D. of the spacer and with a clearance hole for the $5 / 16^{\prime \prime}$ rod and place this on the rod.

Run a 5/16-18 nut down the rod and center the spacer. Now tighten the nut until the tension on the pin at the front of the spring rod is released. Remove the washers holding the pin in and remove the pin. The spring assembly is now free from the shaft. To completely remove the spring assembly, remove the two bolts holding the L-shaped bracket to the side of the frame. To re-install the assembly, or to re-engage the spring rod, reverse the procedure.

## (g) Shaft Bcarings

To replace the shaft bearings, dis-engage the stored energy spring rod as instructed in paragraph (f). Remove the drive rods from the rod ends as instructed in paragraph (d). Remove the operating mechanism safety barrier as instructed in paragraph (a). Remove the four bolts on right side (front) and the two bolts on the left side (front). Loosen the two bolts hoiding the L-shaped bar to the bottom and sides of the frame. Slide the shaft and end brackets forward and out. The bearings can now be removed and replaced. To replace the shaft, slide the shaft and end brackets back into the frame. Install the four bolts on the right side and the two bolts on the left side. Tighten the bolts. (Don't forget so slide the operating mechanism safety barrier under the right two front bolts). Take a large clamp and put across the sides of the frame, preferably in line with the shaft and tighten the clamp. Now tighten the two bolts holding the L-shaped bar to the bottom and sides of the frame. Remove the clamp. Replace the drive rods and stored energy spring-rod.

## (h) Safety Latch

To close the switch with the door open, the safety latch must be dis-engaged. To do this, install the handle in the handle casting and push the handle upward and at the same time, push the latch on the left side of the safety barrier downward until the buttertly on the handle casting clears the locking pin. The same procedure should be used in opening the switch except the handle would by pushed downward. This procedure must be used any time the quick-make, quick-break feature is used with the door open. It is not necessary to use this procedure when using the blade alignment hub for slow close or slow open.

## (i) Completing Alignment

After completing any alignment, the switch should be operated thru at least three "chse-spen" operations to insure proper performance of the operating mechanism.
(i) Main Blade, Jaw and Hinge Assombly

Disconnect the drive rod from the shaft rod end as instructed in paragraph (d). Remove the four bolts holditig the Hinge Assembly and terminal pad to the top of the insulator. The hinge, main blade and tlicker blade are now free. Remove the two bolts holding the jaw to the insulator. Remove the jaw and replace with a new jaw. Replace and finger tighten the two bolts. If the new hinge and blade assembly is equipped with a tlicker blade assembly. mount the hinge on top of the terminal pad and install the four bolts finger tight. If the new hinge and blade assembly does not have the flicker blade assembly, remove from the old assembly and install on the new assembly per paragraph (e.). Tighten the lock nut on the spring washer on the jaw end of the blade. When it is as tight as possible (using standard tools) back the nut off $1 / 4$ turn. Set the main blade to an open position of approximately $45^{\circ}$. The weight of the blade should let the blade fall slowly open. If the blade fails to fall open. loosen the lock nut on the hinge spring washer until the blade slowly falls open. If the blade falls too fast, tighten the lock nut. Now align the blade per paragraph (b). Tighten the jaw and hinge mounting bolts. Align the flicker blade and arc chute per paragraph (c). Re-check alignments. if satisfactory, connect drive rod to shaft rod end. Check the switch for over or under travel per paragraph (d). Perform operations per paragraph (i).

## SWITCH PUSH ROD ADJUSTMENT FEATURE Refer to Illustration on page 11.

The main shaft was redesigned to provide a simpler means of achieving the necessary switch push rod adjustment (as described in 4.2 (d)). The screw type rod end has been replaced by two fixed arms (1) which are welded to the main shaft. These arms have suitable slots (2) to provide the necessary length adjustment to the push rod (3) with the switch in the closed position. Disposed between these arms is the push rod which is free to pivot on a special pivot pin (4), the ends of which have a hardened contour to provide a sharp knife edge, so that when the clamping hardware (5) is tightened the pin is securely fixed to the shaft arms. The push rod, however. is still free to rotate about the axis of the pivot pin.

Therefore, the switch blade can be adjusted to its correct setting with the clamping hardware ( 5 ) loose. thus allowing the special pivot pin (4) to move in the arm slots. When the correct blade setting is obtained the clamping hardware is tightened ( 35.40 ft . lbs.) and locked. If found necessary, further adjustment can be made by lorsentin: and moving the special pivot pin and retightening.


Fig. 1


Fig. 2


Fig. 3


Fig. 4



Fig. 9


Fig. 10


Fig. 11


Fig. 12
Fig. 13



Fig. 16
Part's List

|  | Part's List |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Main Blade-H | d Jaw A |  |  | Reqd. |
| Switch Style No. | Switch <br> Rating | Part <br> No. | Per Pole |  |
| 140D719G01 | 4.76 KV - 600A - 20KA Fault | 140D875G03 | 1 | 3 |
| 140D719G02 | 8.25KV - 600A - 20KA Fault | 140D875G03 | 1 | 3 |
| 140D719G03 | 15 KV - 600A - 20KA Fault | 140D875G03 | 1 | 3 |
|  | 4.76 KV - 600A $\cdot 40 \mathrm{KA}$ Fault | 140D875G04 | 1 | 3 |
| 140D719G05 | 8.25KV - 600A - 40KA Fault | 140D875G04 | 1 | 3 |
| 140D719G06 | 15KV - 600A - 40KA Fault | 140D875G04 | 1 | 3 |
| 140D720G01 | 4.76KV - 1200A - 61 KA Fault | 140D875G05 | 1 | 3 |
| 140D720G02 | 8.25KV - 1200A - 61 KA Fault | 140D875G05 | 1 | 3 |
| 140D720G03 | 15KV - 1200A - 40 KA Fault | 140D875G05 | 1 | 3 |
| 140D720G04 | 15KV-1200A - 61KA Fault | 140D875G05 | 1 | 3 |

Parts Common To All Quick Make - Quick Break Switches

| Description |  | No. Reqd. |  |
| :---: | :---: | :---: | :---: |
|  |  | Per <br> Pole | Per Switch |
| Flicker Blade Assembly | 437B349G01 | 1 | 3 |
| Flicker Blade and Bracket Assembly | 449D726G03 | 1 | 3 |
| Arc Chute Assembly | 140D883G01 | 1 | 3 |
| Barriers | 591C620G01 | - | $4^{19}$ |
| Main Shaft Bearings | 496A760H07 | - | 2 |
| Handle - Removable | 795A839H01 | - | 1 |
| Barriers | $591 \mathrm{C} 620 \mathrm{HO1}$ | - | 4 |

${ }^{7}$ For Bolt-On Design


| Description | Part Style <br> Number | KV | No. Reqd. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { Per } \\ & \text { Pole } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Per } \\ \text { Switch } \end{array}$ |
| Insulator | 548D224C01 | 5 | 2 | 6 |
| Insulator | 548D229G01 | 7.5 | 2 | 6 |
| Insulator | 548D235G01 | 15 | 2 | 6 |
| Drive Rod | 436B828H01 | 5 | 1 | 3 |
| Drive Rod | 436B828H02 | 7.5 | 1 | 3 |
| Drive Rod | 436B828H03 | 15 | 1 | 3 |
| Drive Rod | 590 C 911 H 03 | 5 | 1 | 3 |
| Drive Rod | 590C911H02 | 7.5 | 1 | 3 |
| Drive Rod | $590 \mathrm{C} 911 \mathrm{HO1}$ | 15 | 1 | 3 |
| Special |  |  |  |  |
| Pivot Pin | 795A458H01 | - | 1 | 3 |
| . $375.16 \times 1.75$ |  |  |  |  |
| Hex Stl. Bolt | 70100EG07N | - | 1 | 3 |
| . $375 \times$ Wide |  |  |  |  |
| Stl. Washer | 70500BD32B | - | 2 | 6 |
| . 375.16 StI. |  |  |  |  |
| Elastic Stop Nut | 1650412 | - | 1 | 3 |

*For screw type drive rod adjustment.
$\dagger$ Fixed arm drive rod adjustment feature.

Westinghouse Electric Corporation Dry Type Distribution Transformer Division Greenville, Pa. U.S.A. 16125

November, 1977
New Information
Mailed to: E. D. Ci2071, 2072/DB

MTA and MTC Contral Transformers
AP Machine Tool Transformers SW Transformers
Nerwork Power Filter

Control
Transformers For Machine Tools and Panel Boards


## Sidim/Wall Mount

AP


All MTA and MTC transformers 1000 va and below on this page are a recognized component by Underwriters Laboratory, Inc.

Standard Voltages Type MTA

| -irneres | Catalog <br> Number | IFrame Number | BWiring Diegram |
| :---: | :---: | :---: | :---: |
| 230460 V alts 20115 Vots60 Hertz |  |  |  |
| 50. | 1F0890 | 1310 | 1 |
| 75 | 1 F0927 | 1510 | I |
| - 00 I | 1 F0906 | 1512 | 1 |
| 150\% | 1 F0907 | 1520 | 1 |
| 2005 | 150908 | 1714 | 1 |
| 2505 | 1F0909 | 1717 | 1 |
| 300 i | 1 F0910 | 1723 | 1 |
| 3503 | 1 F0911 | 1727 | 1 |
| 5005 | 1 F0912 | 1923 | 1 |
| 750 \$ | 1F0913 | 1931 | 1 |
| 1000 § | 1 F0914 | C613 | 1 |
| : 5003 | 1 F0965 | C614 | 1 |
| 2000 § | 1F0966 | C827 | 1 |
| 30001 | 1 F0967 | Ca28 | 1 |
| 50003 | 1 F0968 | C829 | 1 |


| 230.460 .575 Volts to $115 / 95$ Volts <br> $50: 60 \mathrm{Hert}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| 503 | 1 F09a7 | 1314 | 2A |
| $75 \pm$ | 1F0988 | 1512 | 2A |
| - 003 | 170989 | 1517 | 2 A |
| 150 \$ | 1 1F0990 | 1714 | 2A |
| 2002 | 1 F0991 | 1717 | 2 A |
| 250 宣 | 1F0992 | 1723 | 2A |
| 3005 | 170993 | 1730 | 2A |
| 3501 | 1 1F0994 | 1923 | 2A |
| 5001 | iF0995 | 1931 | 24 |
| 7503 | 170996 | 1943 | 2A |
| 10003 | 1 F0997 | C614 | 2A |
| 15003 | 1 F0998 | C827 | 2A |

208/380:416 Volts to 115/96 Votts 50.60 Herra

| 507 | $1 F 1025$ | 1314 | 28 |
| :---: | :---: | :---: | :---: |
| :03 | 1F1027 | 1516 | 28 |
| +50 3 | 1F1028 | 1714 | 28 |
| 2003 | 1F1029 | 1717 | 2B |
| 2501 | 1F1030 | 1723 | 28 |
| 3001 | 1F1031 | 1730 | 28 |
| 500 2 | 1F1033 | 1931 | 28 |
| 7503 | 1F1034 | 1943 | 28 |
| 10004 | FF1035 | C614 | 2B |
| 15004 | 1F1036 | C827 | 2 B |

115 Vottes to 12 Volts: 50160 Hert

| $\begin{gathered} 503 \\ 100 \end{gathered}$ | $\begin{aligned} & \text { 1F3050 } \\ & \text { 1F305i } \end{aligned}$ | $\begin{aligned} & 1310 \\ & 1513 \end{aligned}$ | $\begin{aligned} & 4 A \\ & 4 A \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 115 Volts to 24 Volts 50160 Hartz |  |  |  |
| 503 | 1 F3052 | 1310 | 48 |
| 100\$ | 1 F3053 | 1513 | 48 |
| 200 | 1 F3054 | 1714 | 48 |

1 TOPS stock.
IFor detaled dimensions by Frame Number and Wiring Oiagrams reter to TCS 46-870 and TCS 46-871 respectively. I. Acces sory for MTA and MTC oniv.

| Voh- <br> Amperes | Cmialog Number | OFrame Number | © Wiring Diagram |
| :---: | :---: | :---: | :---: |
| $230 / 460$ Voltse to $116 / 230$ Veles <br> 60 Hertz |  |  |  |
| 500 | 1F2198 | 1310 | 3 |
| 75 ( | 1F2185 | 1510 | 3 |
| 1000 | 1F2186 | 1512 | 3 |
| 1500 | 1F2189 | 1520 | 3 |
| 2000 | 1F2191 | -1714 | 3 |
| 2500 | 152034 | 1717 | 3 |
| 300 | $1 F 1113$ | 1727 | 3 |
| 350 | 1F2187 | 1727 | 3 |
| 5000 | $1 F 2190$ | 1930 | 3 |
| 7500 | 1F2188 | C613 | 3 |
| 10000 | IF1687 | C313 | 3 |
| $1500{ }^{\circ}$ | 1F1688 | CE14 | 3 |
| 2000 ( | 1F1696 | C227 | 3 |
| 3000 (1) | 1F1690 | C828 | 3 |
| 5000 (4) | 1F1701 | C829 | 3 |

Standard Voltages Type MTC
2401480-120 Volts, 60 Hertz
230/460-115 Volts, 50/60 Hert 220/440-110 Volts, 50/60 Hert

| VoltAmperes | Catalog Number | 3Frame Number | DWiring Dingrem |
| :---: | :---: | :---: | :---: |
| $50{ }^{(9)}$ | 1 1F0990 | 1310 | 1 |
| $75{ }^{\circ}$ | 1 F0991 | 1314 | 1 |
| 1004 | 1 F08s2 | 1413 | 1 |
| 1509 | 1 F0993 | 1517 | 1 |
| 200d | 1F0994 | 1714 | 1 |
| 2500 | 1 F0895 | 1717 | 1 |
| 3000 | 1 F0896 | 1722 | 1 |
| 3500 | 1F0897 | 1726 | 1 |
| 500 (1) | 1 F0898 | 1931 | 1 |
| 7500 | 1 F0899 | 1943 | 1 |
| 10009 | 170900 | 2236 | 1 |
| 1500 (1) | 1 F0901 | C822 | 1 |
| 2000 ( ${ }^{\text {P }}$ | 1 F0902 | C823 | 1 |
| 3000 (1) | 1 F0903 | C824 | 1 |
| $5000{ }^{\circ}$ | 1 F0904 | C825 | 1 |

Add-A-Part Fuse Holders (3)
50 through 750 va.
Styie No. 257A574G01
1000 through 3000 va,
Style No. 257A564G01
For non-standard Type MTA transformers and modifications refer to Price List 46-820, page 2.

| Network Power Filter |  |
| :--- | :---: |
| For use on Transformer Secondary 208Y/120 |  |
| Cataiog Number (1) | Transtormer Name Plate KVA |
| 1N20 | 15 |
| iN21 | 30 |
| 1N22 | 45 |
| iN23 | 75 |
| IN24 | $1121 / 1$ |
| 1N25 | 150 |
| iN26 | 225 |
| iN27 | 300 |
| 1N28 | 500 |
| IN29 | 750 |
| IN30 | 1000 |

(1) Natwork Power Filter Onty.

Type AP - Machine Tool Tranaformes
240/480 Volt Primary No Teps to 120240 Secondary Single Phese, 60 Hert:


Type SW Tranaformers
Input 105-125 Volts, Outpur 120 Voles ( $=1 \%$ ) Single Phase 60 Hertz


## Dry Type Transformers Control Type

## MTA, MTC, AP, Machine Tool

Type MTC©

(1) 1000 Va and below are listed as a recognized com.
ponent by Underwriters. Lat oratory ponent by Underwriters' Laboratory. Inc.


Type AP, Single Phase, 60 Hertz - Class $155.80^{\circ} \mathrm{C}$ Rise, 3 Through 10 Kva-Class $185,115^{\circ} \mathrm{C}$ Rise, 15 Kva


240/480 Volt Primary.
No Taps to 120/240 Volt Secondary

5) Normal inventory item, order through lOPS.

Dimensions In Inches
Bottom Mount Figure 1


Side/ Wall Mount Figure 2

3.1.1-339

September, 1975
New Information
Mailed to: E, D, C/1926/DB

Standardized Units Classes I and II

3 Phase: To 450 Horsepower, 230 Volts To 900 Horsepower, 600 Volts To 900 Horsepower 600 Vols

Motor
Control Centers Five Star


Many processes and commercial buildings benefit from the grouping of electrical controls. Industries such as primary metals, paper, petroleum and chemicals typically install electrical controls in centralized locathons so that supervision and operation can be performed by a minimum of personnel. To meet this need Westinghouse introduced the Motor Control Center Concept in 1937. This provided a means to mount various motor starter units, feeder tap units and auxiliary controls in a flexible structure arrangement. Since that time the Motor Control Center Concept has been refined to permit greater flexibility, safery and convenience. Westinghouse now has available the ultimate in Motor Control Center design - Five Star.

The Five Star design begins with components of proven electrical and mechanical integrity: assembles them with strict adherence to the highest engineering practices and with special emphasis on personnel safety and ease of maintenance. The assembly is then wrapped in an enclosure which prevents accidentai contact with the enclosed electrical parts and provides an exterior of exceptionally modern appearance, featuring a coordinated control area to provide easy recognition of functions in each starter unit.

The Five Star Motor Control Center has been designed and tested to comply with the general standards for industrial controls and the specific standards for motor control centers as set forth by NEMA, UL, IEEE and ANSI. The various state and city codes are generally met by the standard design. However, in those instances where more specific requirements must be met, the Five Star has the design flexibility to meet them.

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## 1. Units

## Starter Units

Motor starter units are combination type employing a contactor or contactors and a disconnect device of proven capability. The disconnect device can be either a circuit breaker or fusible switch. The Westinghouse Type MCP motor circuit protector breaker is furnisned as standard.


The MCP and starter combination has a 22.000 RMS symmetrical ampere interrupting capacity. With the addition of a current limiter the interrupting capacity is increased to 200,000 amperes. Optional circuit breakers for starter units are the Mark 75 and the TriPac with interrupting ratings of 22,000 amperes and 200,000 amperes respectively.

The fusible switch disconnect device is the Type DS. It is a quick-make, quick-break, visible blade switeh with fusing facilities for use with current-limiting or dual element, rejection type, NEMA Class " $J$ " or " $R$ " fuses. Facilities for NEMA Class " H " fuses are available.

Both breaker and fuse selection should take into consideration the total short circuit capacity of the system to which the control center is connected.

The starter units are equipped with A200 Contactors for NEMA Sizes one through four and GCA Contactors for NEMA Sizes five and six. These contactors have been successfully applied in thousands of the most demanding industrial applications. Overioad protection is
provided by a three pole thermat overioad relay as standard with ambient compensated also available. The overioad relay has adjustable hand or automatic resetting. The hand reset button extends through the unit door. All relays have a "no" stop feature as standard. The iocation of all control elements cormtained in each unit has been designed to provide a coordinated control area for easy recognition of functions and maximum operator efficiency.
Typical starter units available include the fotlowing:
Full Voltage, Non-Reversing
Full Voltage, Reversing
Full Voltage. Non-Reversing, Two Speed. Single Winding
Full Voltage, Non-Reversing, Two Speed, Two Winding
Reduced Voltage, Autotransformer, Closed Transition
Reduced Voltage, Part Winding
Reduced Vottage, Wye-Delta.Closed Transition
All starters through NEMA Size 5 are a drawout design except Size 5 reduced voltage.

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Descriptive Bulletin
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## Foeder Tap Units



Feeder tap units may contain either circuit breakers or fusible switches. Draw-out breaker units include the fixed trip Type FB, single or dual mounted in ratings through 150 amperes and the interchangeable trip Types KB and LB single mounted through 250 amperes and 400 amperes respectively. Larger circuit breakers are non-draw-out fixed mounted. Adjustable seltronic breaker is standard. Ratings to 2000 amperes are avaiiable.

4 Fusible feeder tap units utilize the Type DS Switch through 200 amperes. Non-auto breakers and fuses are furnished for 400 amperes and above. These switches are mounted in draw-out units through 400 amperes with the 30 ampere and 60 ampere ratings available in dual mounting. Ratings from 600 amperes through 1200 amperes are fixed mounted.

The DS switches are supplied with fusing facilities for use with current-limiting or dual element rejection type, NEMA Class " J " or " $R$ " fuses. Facilities for NEMA Class " $H$ " fuses can also be supplied.

©

A new side mounted terminal block is standard on units with NEMA Type B or C wiring. These terminal blocks are mounted in knockouts on the wireway side of the unit wrapper. This placement provides greater access to other components within the unit.

The terminal block is available in three types; Standard Pressure Connector. Pressure Pull-Apart, and Puil-Apart for ring or spade type crimp terminations. The smallest starter unit ( $2 X$ or 12 inches high) can accommodate up to three of the new side mounted terminal blocks providing a maximum of 21 circuits in the standard pressure types and up to 18 circuits in the spade or ring type. Larger starter units can accommodate additional terminal blocks.

As an alternate, terminal blocks may be mounted across the bottom front of the unit.

Standard track mounted terminal blocks include the following types: Standard Pressure Connector, Standard Pressure Pull-Apart. Straight Ring or Spade type for crimo terminations, and Pull-Apart Ring or Spade type for crimp terminations. When mounted in this fashion, a maximum of 30 circuits can be provided by the Standard Westinghouse Pressure types and the Ring and Spade tyoes. Wiring within each unit and to the terminal blocks is made with 16 AWG stranded thermopiastic-insulated wire rated $105^{\circ} \mathrm{C}$. Power wiring is black and sized to carry the maximum full load current of the unit. AC control wiring is red and DC control wiring is blue. Plug-in type terminal blocks can be supplied for all control wiring and load wiring through size 2 when specified.

## Stab Assembly



A newly designed two component copper alloy stab incorporates the ultimate in mechanical simplicity to provide precise control of contact pressure on the bus. This assures a positive connection yet permits easy unit insertion and withdrawal. Self aligning Magna-Grip stabs are mounted in a glass reinforced plastic insulation block which totally shrouds each stai and absolutely ensures positive alignment of the stabs with the vertical bus. The insulation block is also an integral part of the phase to phase isolation system. Power wiring is firmily welded to the stabs and is totally contained within the unit enclosure. This means the vertical bus compartment is completely free of wiring for maximum safety and reliability.

Four stab assembly sizes are used; $60,150$. 300 and 400 amperes to accurately match the electrical requirement of each unit.


Page 4

I Units, Continued
Device Panel


The new device panel can accommodate up to six pilot devices such as oil-tite pushbuttons, indicating lights, selector switches and a new line of miniature meters.

The device panel is hinged on a horizontal rod extending across the front of the unit. With the unit door open and after removing two captive retaining screws at the top of the panel, it may be swung down. This provides ready access to the rear of the panel and increased accessibility to the unit interior.

Molded into the panel is a knock-out for each device location. This facilitates the future addition of devices to the panel.

The panel is molded of a durable, chemically stable plastic material which eliminates corrosion. The textured surface of the panel provents smearing and fingerprinting to preserve the pleasing appearance of the unit under operating conditions.

## nde Machanism



The new handle mechanism is designed to provide a high mechanical advantage so that little effor is required to operate any device. Two sizes are used; the smaller mechanism for devices through 400 amperes, and the larger mechanism for devices through 1200 amperes.

The handle mechanism is a vertical motion type device with three positions; ON, OFF and TRIPPED. It is mounted securely by the wrapper, breaker or fusible switch to eliminate alignment problems and to provide a sitive indication of the breaker or switch siltion, even with the door open.

The handle mechanism provides several safety features.

In the "ON" or "TRIPPED" position an interlock prevents the unit door from being opened. However, to enable authorized maintenance personnel to gain access to the units when required, a door interlock defeater screw is located above the handle.

With the unit door open and the operating handle in the "ON" or "TRIPPED" position, an interlock slides into a slot in the divider pan above and prevents removal of the unit. This same interlock prevents insertion of the unit (as shown below) unless the handle mechanism is in the "OFF" position.

To insure that units are not energized accidentally or by unauthorized personnel, the handle mechanism can be padlocked in the "OFF" position. Sufficient space is available

for a minimum of three padlocks. Where crivical processes are involved and to prevent unauthorized shutdown, the handle mechanism can be modified to enable padlocking in the "ON" position.


The handie and exterior mounting panel ere molded from the same plastic material as the device panel. The mounting panel has a taxtured surface to preserve appearance. The "ON", "OFF", "TRIP" and "RESET" positions of the mechanism are molded into the paned and are highly visible. The operating handie is designed for rugged duty and good operator feel. its color contrasts with the dovice and mounting panels for easy recognition.


The unit wrapper is fabricated of 16 gauge steet. After fabrication, it is cleaned and given a rust inhibiting phosphatizing treatment. The finish on the unit wrapper is a baked on enamel ASA 70. This is a highly durable enamel, off white in color to increase visibility within the unit and facilitate wiring and maintenance procedures.

The unit wrapper provides three sides of a 'gged steel shell and the mounting base for d unit components. The smallest unit measures $131 / 2$ inches wide, 8 inches deep and 12 inches high. Units increase in size in 6 inch increments to a maximum height of 72 inches.

The unit wrapper is designed to provide ample space for cable entry from the wireway to the unit.

The unit wrapper has four mounting points, two on each side. which support the unit in the structure. They engage guide rails located near the top of each unit space. This mounting point guide rail system produces minirnum friction and allows units to be inserted and withdrawn easily. The guide rails also give precise alignment to the unit for accurate stabbing on the vertical bus.


At the top center of the unit wrapper is a quarter turn latch which securely holds the unit in the compartment. The latch can onlv be engaged when the stabs are fully mated with the vertical bus. Upon release of the latch the unit can be partially withdrawn (as shown above) such that the stabs disengage from the vertical bus. In this position the latch can be re-engaged to prevent the unit from being returned to the fully stabbed position or from being removed from the structure. The larch can be padlocked in this position to ensure the stabs remain disengaged during maintenance.

Unit Doors


Unit doors are formed of 14 gauge steel with a $1 / 2$ inch flange on all four sides. The flange adds rigidity to the door and provides a surface to contain door gasketing when applied. Cutouts are made in the door as required to accommodate the operating handle and device panal. The doors are cleaned, phosphatized and given a finish of off-white, baked on enamel ASA 70.

The doors will open approximately $110^{\circ}$ and opposite to wireway doors permitting optimum access to the unit compartment. The docrs are mounted on removable pin hinges. This permits quick removal of any door in a vertical structure without disturbing adjacent doors.

Each door is provided with a minimum of two quarter turn indicating type fasteners. They securely hold the door in the closed position, yet allow quick and easy access to the unit when required. The fasteners provide a visual indication of the latched position.


1 Units, Continued

## Nameplates

Unit nameplates are of durable anodized aluminum with $1 / 9$ inch high white lettering on a black background. They are heat and crack resistant to eliminate the need for replacement. Nameplates are mounted with a pressure sensitive adhesive. Rivets or screws can be used if specified.

## Modifications

Starter and feeder tap units can be modified to meet a variety of specification requirements. Some typical components which can be added include; control circuit transformers - fused or unfused; control reiays, MOR (modular overload) relays, groundgard relays, current transformers, extra electrical interlocks, pushbuttons, selector switches, indicating lights, circuit breaker shunt trip or undervoitage release and auxiliary switches. In most cases, these modifications do not increase starter unit size.

## Additional Equipment

In addition to motor starter and feeder units additional equipment can be supplied includthe following:

Single phase dry type distribution transformers in ratings of $3,5,7.5,10$ and 15 KVA .

Three phase dry type distribution transformers in ratings of $9,15,22.5,30$ and 45 KVA.

Lighting panelboards with $12,18,24,30,36$, or 46 circuits with either plug-in branch breakers or boit-on branch breakers.

Current limiting reactors with ohmic values of 01, .015, . 02 and . 025 and amperage ratings of $600,800,1000$ and 1200.

Metering equipment such as voltmeters. ammeters, wattmeters and power factor meters.
II Buas Systern

Page(s)

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6-7.

Horizontal Bus 7
Neutral Bus $\qquad$ 7
8

## Ground Bus

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Control, Load and Incoming Line Terminations. $\qquad$ 8


## il. Bus Syatem

## Vertical Bus

The vertical bus provides three phase power distribution from the main horizontal bus to the vertical compartments. The bus is a unique angular configuration with an " L " shape for front mounted only structures and a " $Z$ " shape for back to back mounted structures. These shapes have the inherent mechanical strength to withstand fault stresses. They also provide a smooth stabbing surface for unit connection.



Due to the high strength capability of the bue bars, bus bracing at 42.000 RAS symmetrical amperes is standard. Bracing at 100,000 RMS is available as an option. Bus braces are molded from a glass-reinforced polyester material which is non-tracking and impervious to moisture and other adverse atmospheric operating conditions.

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## Page 7

## Vertical Bus, Continued



The vertical bus is availabie in ratings of 300 , 600 and 1200 amperes for front mounted only, and 600 and 800 amperes for back to back mounted. Standard vertical bus bars through 600 amperes are tin plated aluminum with the special POLYTET-50 process. Copper bus is available as an option in 300 and 600 amperes and is standard in 800 and ' 200 ampere ratings.

The exclusive POLYTET-50 process further improves the corrosion resistant qualities of tin plated aluminum when used in severe enviromments. It also provides a lubricating effect which prevents stabs from galling and facilitates easy removal and insertion of units

Isolation of the vertical bus compartment from the unit compartments is accomplished by a full height barrier which is provided as standard. This is a single sheet of glassreinforced polyester with cut-outs to allow the unit stabs to engage the vertical bus. Snap in covers are available for the cutout openings to provide total isolation during maintenance procedures.

When insulation and isolation of the vertical bus is required, a labyrinth design barrier is available. This barrier is molded glass reinforced polyester and forms a labyrinth around the bus bars to restrict fault propagation. This design provides maximum protection against phase to phase insulation breakdown. Thermal efficiency is maintained by a close tolerance fit between the bus bars and the barrier which minimizes air pockets. This insures compliance with NEMA and UL heat rise standards. When bus bracing of

100,000 RMS amperes is supplied, the labyrinth barrier is provided as standard.


An automatic shutter mechanism is included with the labyrinth barrier to provide complete isolation of the vertical bus. The shutter moves automatically to cover the stab openings when a unit is removed. This provides maintenance personnel with maximum protection since the vertical bus is never exposed. As the unit is reinserted in the compartment, the shutter moves sideways to uncover the stab openings in the barrier.

## Horizontal Bus



The main horizontal bus provides three phase power distribution from the incoming line or primary disconnect device to each vertical structure in an assembly. The bus bars are mounted in a vertical plane, edge to edge. This mounting produces an excedtionally strong assembiy able to withstand r.igh fauit current stresses.

Standard horizontal bus bracing is $\mathbf{4 2 . 0 0 0}$ RMS symmetrical amperes. Additional bracing to 100,000 amperes is available. Bus braces are moided from a glass reinforced
lyester material with high strength which is on-tracking and impervious to moisture and other adverse atmospheric operating conditions.

The main horizontal bus is rated at 600 amperes as standard with ratings of $800,1000$. 1200, 1400, 1600, 2000 and 2500 amperes optionally available. Tin-plated aluminum bus bars are supplied as standard. Tin-plated aluminum or copper is available for ratings up through 1200 amperes. Above 1200 amperes only copper bus is supplied. The exclusive POLYTET-50 process is applied to all tin-plated aluminum horizontal bus to further impnove its corrosion resistant properties in severe environments.

The horizontal bus is rated at $65^{\circ} \mathrm{C}$ temperature rise in compliance with NEMA standards. A rating of $50^{\circ} \mathrm{C}$ temperature rise to comply with UL Standards is available as an option.

The horizontal main bus is isolated from the top horizontal wirewav compartment by an isolation barrier. This two piece steel barrier extends to the full width of each vertical structure. The two piece design allows access to bus connections without the removal of the entire barrier, for added maintenance canvenience. The bus bar layout permits front access to all bus connections. This allows maintenance personnel to make splices and check splice bolt torques from the front of the structure.


Page 8

II Bus System, Continued


Neutral bus can be supplied one half or full rated. The bus bar is mounted on stand-off insulators across the bottom of each vertical compartment.

Tin-plated aluminum or copper bus is available. One half rated tin-plated aluminum with - special POLYTET-50 process is standard.

Ground Bus


Ground bus is available in $1 / 4$ inch by 1 inch tin-plated aluminum or cooper. Tin-plated aluminum with the special POLYTET-50 process is standard. Mounting is across the :op of each vertical structure in the horizontal wireway. The bus can also be mounted across the bottom when the bottom 9 inches are not occupied by units or master terminal blocks.

## Control, Load and

 Incoming Line Terminations For NEMA Type A wiring each unit is assembled and devices interwired. Terminal blocks are not supplied and control and load wiring is internal to the unit.For NEMA Type B wiring, control wires are terminated at blocks within the unit. Refer to the discussion of units for types of terminal blocks available.

For NEMA Type C wiring, control and load wires are extended from the unit terminal blocks to master terminal blocks located at the top or bottom of any vertical structure. The mounting iccation of the master terminal block in front mounted only structures is in the existing horizontal wireway space at the top or bottom. When mounting is made in an incoming line section, tweive inches of unit space must be used. When mounting is made in the rear of back to back mounted structures, 6 inches of unit space must be used at the bottom and 12 inches at the top.
Master terminal blocks can be either fixed or draw-out mounted with draw-out provided as standard. In the draw-out design the terminal blocks are rack mounted to permit removal of the entire assembly for ease of wiring during installation and maintenance.

Incoming line cables entering from the top of the control center can be easily terminated on the main horizontal bus or connected to a main breaker. Incoming line (more than one per phasel entering from the bottom of the structure can be easily terminated at the bottom of the vertical bus in that section at ratings through 1200 amperes. Adapters can be provided for up to four cables per phase and for crimp-on lugs. Terminals are suitable for both copper and aluminum cable.

Copper or aluminum cables of \#6-350 MCM, two per phase, can be terminated in the incoming line structure utilizing 6 inches of addirional space. Copper or aluminum cables of 4/0-600 MCM, two per phase, can be terminated with the addition of 6 inches for top entry and the addition of 18 inches for bottom entry.


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## ili. Structure

## Construction

The standard vertical structure is 90 inches high and 20 inches wide. Front mounted only structures can be either 16 inches or 21 inches deep. Back to back mounted structures are 21 inches deep.


The structure framework is made of 12 gauge formed steel channeis. The sub-frames for the front and rear of each structure are welded. These sub-frames are then boited to longitudinal members to form the complete frame which is rigid and self-supporting. Side, back and roof sheets of 14 gauge steel are mounted with screw fasteners for quick and easy removal when desired. All doors are 14 gauge steel with a $1 / 2$ inch flange to provide a rigid, secure closure for all openings. Doors mounted on removable pin hinges are provided on all unit compartments, vertical wireways, top horizontal wireways, and bottom horizontal wireways.

The unit pan forms the top barrier of each unit space. In conjunction with the unit wrapper this provides isolation between adjacent units and wireways. The guide rails are an integral part of this pan and provide precise alignment of the unit stabs on the vertical bus.


All structure elements are thorougniy cieaned after fabrication and given a phosphatizing treatment to inhibit rust and prime the metal for the finish coating. A baked enamel ASA 70 off-white is applied to the structure framework, back sheets, doors and units. ASA 24 charcoal grey is applied to the roof and side sheets.

## III. Structure, Continued

Vertical Wireway

A vertical wireway is provided in each vertical structure. Located on the right side, it extends the full 90 inch height of the structure. The width of the wireway is $45 / \mathrm{m}$ inches at the rear of the vertical frame members. Overall depth of the wireway is 8 inches providing a crosssectional area of nearly 35 square inches to easily accommodate control and load wiring. Supports are provided at suitable intervals to secure all wiring and cables.

The wireway opening is covered by two doors. top and bottom, so that the entire wireway need not be exposed to gain access to one section. The doors swing open $\$ 10^{\circ}$ and opposite to the unit doors for maximum accessibility. The doors are mounted on removable pin hinges for quick detachment and are secured in the closed position by two quarter-turn indicating type fasteners.

## Special Structures

In addition to the standard 20 inch wide structure, extra wide structures are available in 4 inch increments up to 32 inches wide. These structures can be supplied with or without $45 / \mathrm{inch}$ wide vertical wireways. They are used for mounting transfer switches, SPCB and DS breakers and other special equip-
ment. ment.

Another special structure is a transition section between Type $W$ and the Five Star. This structure is 10 inches wide to provide for horizontal bus splicing.

## Enclosures

The standard enciosure type is the NEMA 1 General Purpose-Indoor. This enciosure is appropriate for instailations with normal atmospheric conditions.


The NEMA 1 Gasketed Enclosure has geskering material around the perimeser of all doors and door cut-outs. it is used to prevent airborne matter from entering the control center.

The NEMA 2 Dripproof-indoor smploys a special roof panel with a drip shield end water channels. This prevents liquid from dripping into the control center.

The NEMA 3R Rainproof and Sleet Resistant Outdoor consists of a NEMA 1 enclosure mounted on a special base with an outdoor house erected around and over it. Both waik-in, non-walk-in aiste and sunnel types are available.

The NEMA 12 Dusttight and Driptight - indoor has gasketing material around all doors. door cut-outs, cover plates, side, top and back sheets. A gasketed bottom plate is avaitable with this enclesure. This construction provides maximum protection against airborne matter and dripping liquids.

## Typical Specification

Motor Control Centers

## 1. General

Motor Control Centers shail be built and tested in accordance with:
a. NEMA Standards
b. ANSI
c. Underwriters Laboratories, Inc.
d. Other (specify)
2. Service
a. Suitable for operation on $\qquad$ volts
$\qquad$ phase $\qquad$ wirs $\qquad$ h2.
b. Suitable for connection to an available fault of $(42,000)(100,00)$ RMS symmetrical amperes.

## 3. Ineoming Line

a. The incoming line shall enter the section at the (top) (bottom) (other) and will be (cable) (bus) connected.
b. The cable will consist of (Number
$\qquad$ zils ).
c. A main disconnect (is) (is not) required. (Provide details if required)

## 4. Wiring

a. The motor control center shall be wired NEMA Class (I) (II). Type (A) (B) (C).
b. If Type C, master terminal blocks shall be located at the (top) (bottom) of each section.

## 5. Structure

a. Structures shall be totally enclosed, deadtront. free standing assemblies, 90 inches high and not less than $16^{\prime \prime}$ deep for front mounted units ( $21^{\prime \prime}$ deep for back to back mounted units). Working height shall be $72^{\prime \prime}$ to accommodate starter units in multiples of $6^{\prime \prime}$ increments with a minimum of $12^{\prime \prime}$. Removable lifting angles will be provided.
b. Structures shall contain a horizontal wireway at the top, isolated from horizontal bus and readily accessible. Each structire shall contain an isolated vertical wireway with cable supports, accessible through hinged doors.
c. All structure doors to be mounted on removable pin hinges and secured with quarter irn indicating rype fasteners.

## 6. Bass System

a. Bus shall be braced to withstand a fault of $(42,000)(100,000)$ RMS symmetrical amperes.
b. Main horizontal bus rating to be ( 600 ) ( 800 ) (1000) (1200) (1400) (1600) (2000) (2500) amperes and be effectively isolated from all wireways and working areas.
c. Vertical bus rating to be (300) (600) (800) (1200) amperes.
d. Full height of vertical bus bars to be protected against accidental contact by (a single sheet of glass reinforced polyester with cutouts for stab openings) (a labyrinth barrier to provide insulation and isolation with shutters which automatically cover stab openings when units are withdrawn).

## 7. Unit Compartments

a. Each unit compartment shall be provided with an individual front door. Starter and feeder tap unit doors shall be intertocked mechanically with the unit disconnect device to prevent unintentional opening of the door while energized and unintentional application of power while the door is open. An interlock between the unit disconnect device and the structure will prevent removal or reinsertion of a unit when the disconnect is in the "ON" or "TRIPPED" positions. Means shall be provided for releasing the interlock for intentional access and/or application of power.
b. Padiocking arrangements shall permit locking the disconnect device OFF with at least three padlocks with the door closed or open.
c. Means shall be provided to padlock the unit in a partially withdrawn position with the stabs free of the vertical bus.
d. All full voltage starter units through NEMA size 5 shall be of the draw out type. Draw out provisions shall inctude a positive guide rail system and stab shrouds to absolutely ensure alignment of stabs with the vertical bus. Power wiring to stabs shall be contained within the draw out unit. Overioad relays shall be reset from outside the enclosure by means of an insulated button.
e. All draw out units shall be secured by a spring loaded quarter turn indicating type fastening device, located at the top front of the unit.
f. Combination motor controller and feeder tap units shall employ (molded case circuit breakers) (fusible switch with clips for type fuses) for branch circuit protection, and shall be equipped with: (Select 1, 2, 3.4 or 51

1. MCP (Motor Circuit Protector)
2. MCP with current limiter
3. Thermal magnetic breaker
4. TriPac circuit breaker
5. Fusible switch
g. Control power shall be provided as follows: (Select 1, 2 or 3)
6. Individual control power transformers with one secondary control fuse. The other secondary lead shall be grounded.
7. Line voltage control circuits. Linevoltage control circuits on all circuit breaker combination controllers and fusible combination controllers larger than Size 2 shall be provided with NEMA Class ل current-limiting fuses mounted in the unit in both legs of the control circuit.
8. Terminals for a separate source of control power. A control power fuse shall be provided in the unit, and the main disconnect shall be equipped with a normally open contact to isolate the control circuit from the source when the controller disconnect is open.
h. Starter units shall contain: (Specify as required)
9. Number of auxiliary contacts.
10. Unit-mounted pilot devices and indicating lights.

## 3. Control relays and other devices.

## i. Other units to be included in the motor

 control center: (List as required)1. Lighting and power transformers.
2. Lighting distribution paneiboards.
3. Metering panels and instrument transformers.
4. Operating panels.
5. Power-factor correction capacitors.
6. Other

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Bottom Horizontal Wireway
Front Mounted Only and Fron! of Back
to Back Mounted Height:

Standard ....................................... 9
Optional ......................................................... Depth $16^{\prime \prime}$
near of Back to Back Mounted Height $3^{\prime \prime}$
Depth ................................................ 21'
Material
Frame 12 ga. Formed Steel Channel
Side, back \& roof sheets, doors ............ 14 ga.
Unit wrapper $\qquad$ 16 ga. Steel Sheet

Finish
Frame, back sheets,
doors and units $\qquad$ Off White ASA 70
Roof \& Side sheets $\qquad$ Charcoal ASA 24

## Horizontal Bus

Ampere Ratings
Standard:
600 ampere, Tin Plated Aluminum with POLYTET-50
Optional:
600 ampere, Copper
800 ampere. Tin Plated Aluminum with POLYTET-50 or Copper
1000 ampere, Tin Plated Aluminum with POLYTET-50 or Copper
1200 ampere, Tin Plated Aluminum with POLYTET-50 or Copper
1400 ampere, Copper
1600 ampere, Copper
2000 ampere, Copper
2500 ampere, Copper

## Horizontal Bus, Continued

Bus Bracing
Standard, 42,000 amperes symmetrical
Optional, 100,000 amperes symmetrical
Incoming Line Terminations
From Top or Bottom
To Bus or Disconnect Device
Sizes: \#6-350 MCM, 2 per phase in bus compartment
410-600 MCM. 2 per phase
Top entrance $12^{\prime \prime}$ additional Bottom entrance $18^{\prime \prime}$ additional

## Vertical Bus

Ampere Ratings
Standard:
Front Mounted Only
300 Ampere, Tin Plated Aluminum with POLYTET-50
Back to Back Mounted
600 Ampere, Tin Plated Aluminum with POL YTET-50
Optional:
Front Mounted Only
300 Ampere, Copper
600 Ampere, Copper
1200 Ampere, Copper
Back to Back Mounted
600 Ampere. Copper
800 Ampere, Copper
Bus Bracing
Standard, 42,000 Amperes symmetrical
Optional, 100,000 Amperes symmetrical
Barriers
Standard
Isolation Barrier: Glass polyester cover sheet with stab cut-outs.
Optional
Labyrinth Barrier:
Glass polyester molding for insulation and isolation, including a shutter mechanism to automatically cover stab openings.

Neutral Bus (Bottom Mounted)
Standard....... $1 / 2$ neutral tin-plated aluminum with POLYTET-50
Optional ....... 1/2 neutral copper, Full neutral aluminum with POLYTET-50 or copper
Ratings ......... 300 to 2500 amperes

Ground Bus (Top Mounted)


Stab Ratings: 60 Amperes 150 Amperes 300 Amperes 400 Amperes

Interrupting Capecity
Circuit Breaker Units: MCP with combination starter 22,000 Amper................ MCP with Current Limiter and combination starter. 200,000 Amperes TriPac

200,000 Amperes
Fusible Switch Units ....... 200,000 Amperes
Further Information
Price List 12-125 P WE A

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# Installation and Maintenance Manual five star motor control centers 

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This electrical control equipment is designed to be installed. operated, and maintained by adequately trained workmen. These instructions do not cover all details, variations, or combinations of the equipment, its storage. delivery, installation, check-out, sate operation, or maintenance. Care must be exercised to comply with local, state, and national regulations, as well as safety practices, for this class of equipment. The maximum short circuit capability of the equipment should not be exceeded by connection to a source with higher capacity.

If maintenance or troubleshooting assistance is required, contact your nearest Westinghouse Engineering Service Division or Sales Office.

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### 1.0 GENERAL DESCRIPTION

The Westinghouse FIVE STAR Motor Control Center consists of one or more totally enclosed, dead front, free standing structural assemblies (17) 90 inches high which are compartmentalized to house invidual control units. (2) With control units mounted in the front side only, the structure may be 16 or 21 inches deep. For mounting units back-to-back, the structure is 21 inches deep. Steel covers (7) enclose
the structure at the top, sides and at the rear of front mounted only, structures

Each control center contains a main horizontal bus system (9) mounted at the top and extending across the length of the control center.

A vertical bus system (8) installed in each vertical structure, is connected to the horizontal bus to feed
the individual control units. The vertical bus is isolated by a full height barrier. (5) An optional labyrinth barrier provides both isolation and insulation. (14) An automatic shutter is included with the labyrinth barrier system to cover the stab openings for each control unit.

At the top of each structure, a door provides ready access to the top horizontal wireway (11) and ground bus (10) (if provided). The horizontal wireway is isolated from the bus systems by steel barriers (12) which can be removed for installation and maintenance operations. Adequate space is provided for control wiring and top cable entry.

At the bottom of each structure, a door (18) provides ready access to the bottom horizontal wireway, (19) and neutral bus (if provided). The bottom of each structure is completely open to provide unrestricted bottom entry of cable and conduit. Channel sills may be installed across the bottom of the control center if specified and an optional bottom plate may also be specified.

A vertical wireway 8 inches deep, (16) extending the full 90 inch height of the control center is located to the right of each vertical compartment. This wireway is covered by two hinged doors (15) and contains rugged cable supports to secure wire bundles and cables. The vertical wireway joins the horizontal wireway at top and bottom to provide unobstructed space for interwiring.

Each vertical structure provides space to mount up to six control units (2) with a minimum height of 12 inches, in increments of six inches for a total of 72 inches of usable space. Control units through NEMA Size 5 are drawout type (except Reduced Voltage Starters). These drawout unit assemblies are a completely self-contained package consisting of a steel enclosure, operating handle and electrical components. The drawout assembly slides into its compartment on guide rails (13) to provide easy withdrawal and reinsertion and to ensure precise alignment of the unit stabs with the vertical bus. Each drawout unit is held in place by a single quarter turn latch (3) which can only be engaged when the unit stabs are fully mated with the vertical bus. Each unit has a separate door, (1) held closed by a minimum of two quarter turn, indicating type fasteners.

The operating handle on the control unit (4) moves vertically. In the "on" or "tripped" positions, the handle interlocks with the unit door to prevent its opening. In this position, authorized personnel can open the door by turning the defeater mechanism
screw. (21) With the unit door open and the operating handle in the "on" or "tripped" positions, another interlock to the divider pan prevents removal of the unit. This same interlock prevents insertion of the unit unless the handle mechanism is in the "off" position. To ensure units are not energized accidentally or by unauthorized personnel, the handle mechanism can be padlocked in the "off" position. Space is provided for a minimum of three padlocks.

The device panel (6) is mounted on the drawout unit. It will accommodate up to six pilot devices. The overload reset button (20) is mounted on the unit door.

### 2.0 HANDLING

Lifting angles for handling by overhead crane are bolted to the top of each shipping assembly. Handling by overhead crane is preferable but when crane facilities are not available, the control center can be positioned by using rollers under the shipping skid or with a fork lift truck. The shipping skids should be left in place until the center is in its final location. After removal of the top lifting angles, the mounting hardware should be replaced to prevent the entrance of dirt, etc.

### 2.1 RECEIVING

After unloading the control center, a thorough inspection should be made to detect any damage which might have been incurred during shipment. If there is evidence that the control center has been mishandled or shipped on its back or sides, the drawout units should be removed and a complete inspection made of the internal structure, vertical bus and units for possible hidden damage. Any damage should be reported at once to the carrier.

### 2.2 STORAGE

When the control center cannot be placed in service reasonably soon after its receipt, it should be stored in a clean, dry, ventilated building. The storage area should be free from condensation or other injurious environmental conditions. Freedom from condensation is essential and may be accomplished by the use of auxiliary heaters if necessary. The equipment must also be protected from excessive dust. Outdoor storage, even when protected by a tarpaulin, is inadequate.

### 3.0 INSTALLATION

CAUTION - If work is involved in connecting the ontrol center with existing equipment, ensure that _oming power is disconnected before work is begun. Complete the work described in this section and Sections 4,5 and 6 before incoming power is applied.
Before any installation work is begun, consult all drawings furnished by Westinghouse as well as all applicable contract drawings for the installation. Particular attention should be given to the physical location of units in the Control Center and their relation to existing or planned conduits, busways, etc.
Care should be taken to plan for any future conduit entrance in advance of Control Center installation.

Control Centers are assembled at the factory on smooth and level surfaces to assure correct alignment of all parts. The foundation furnished by the purchaser must be true and level, or the bottom frames must be shimmed to support the entire base in a true plane. An uneven foundation can cause misalignment of shipping sections, units and doors. It is recommended that leveled channel sills under both the front and rear of the Control Center be used
provide this level base. They should be drilled and rapped for mounting bolts in accordance with the applicable floor plan drawing and then either installed level with, or on top of, the finished floor. If sills are grouted in concrete, the mounting bolts should be screwed in place and remain until the concrete has hardened.
Refer to pages 14 and 15 for floor plan dimensions. The shaded area represents the open space available for conduit entry through the bottom of each section. This area may be restricted if large control or autotransformers are mounted in the bottom of these sections. If optional bottom plates are supplied, the plates may be removed and drilled for conduit entry.
If two or more shipping sections are to be joined into an integral assembly or a shipping section is to be joined to an existing section, refer to Sections 3.1 and 3.2 before proceeding with the installation. If joining is not involved, remove the bottom horizontal wireway doors to provide access, move the section into place and secure it to the fioor sills or mounting bolts.

## v. 1 JOINING FIVE STAR SECTIONS

If two or more shipping sections are to be joined into an integral assembly, or a section added to an
existing installation, splicing of horizontal bus, ground bus, neutral bus and joining of the adjacent vertical structures must be planned with the installation.
(1) Side sheets must be removed from adjacent vertical structures to be joined. (These sheets will have been removed from factory assembled sections.)
(2) The horizontal bus splice plates and connection hardware will be packed in the top horizontal wireway. These splice plates should preferably be attached first to the bus in the structure on the left side of the right hand section, whether existing or to be installed. Refer to Figure 1. This method provides the most convenient access to the bolts, and eliminates need for removal of the horizontal bus barriers in that structure. Should the existing bus be oxidized. sand lightly with a fine aluminum oxide paper. CAUTION - do not use emery cloth or any abrasive containing metal.


Figure 1
(3) Remove the upper horizontal wireway door from the structure on the right side of the left hand section and remove the two piece wireway barrier to provide access to the ends of the bus in that section. If master terminal blocks for Type $C$ wiring are installed in this wireway, refer to Section 5.3.
(4) Move the section in place, aligning the upright

structural channels and bottom channels. Alignment of the section with floor sills and foundation provisions will be facilitated by removal of the bottom horizontal wireway doors. Using the " $U$ " type frame clamps provided, clamp adjacent front upright channels together at the top, bottom and approximate center of the vertical structure. This operation will be facilitated by removal of the vertical wireway doors from the left hand structure and one or more drawout units from the right hand structure.
See Sections 7.1 and 7.2.
(5) If rear access is available, "U" clamps should also be used to clamp the rear upright channels together. In front only structures, this will require removal of the adjacent back sheets. In a back to back mounted structure, remove the vertical wireway doors and one or more drawout units as above.
(6) Secure the sections to the floor sills or mounting bolts as provided for the installation.
(7) Boit the horizontal bus links to the bus in the left hand structure, torquing all bus splice bolts to 23 foot Lbs. See Figure 2.
(8) Replace all bus barriers and doors.

### 3.2 JOINING FIVE STAR TO OTHER EQUIPMENT

Joining a Five Star Control Center to other equipment such as Type W and 11-300 Control Centers will usually involve a transition section. installed between the two varieties of equipment. This transition section will be detailed on drawings provided by Westinghouse and the applicable contract drawings. If provided separately, it should
be installed first. The overall installation task should be reviewed to determine whether the transition section should be attached to the existing equipment or to the Five Star section, before it is moved into place, and to select the sequence which will provide best access to bus splicing and joining of the structures.

### 4.0 INCOMING LINE CONNECTIONS

CAUTION: All incoming line compartments present an obvious hazard when the door is opened or covers are removed with power on. When working in this area, the incoming feeder should be deenergized.

Main cables normally terminate at the line side of the main motor Control Center disconnect or at an incoming line lug compartment. The design of the Five Star Motor Control Center provides a wide variety of choices in the selection of incoming line arrangements. Typical incoming line arrangements are shown in Figure 3. Before beginning work on incoming line connections, refer to all drawings furnished by Westinghouse as well as all applicable contract drawings for the particular installation.


Figure 3
(76-0156)

Depending on the location, size and type of the incoming arrangement, removal of one or more horizontal and vertical wireway doors, horizontal bus barriers, side sheets and units will provide complete access.

For top entry, the top cover plates are easily removed to facilitate drilling or punching operations.

Provisions should be made to locate cables in the motor control centers so that they will be free from physical damage and also to avoid overheating. The cables should be supported in order to withstand available short circuit currents.

### 5.0 MOTOR \& CONTROL CONNECTIONS

All field wiring to control units should be made in accordance with the wiring drawings which are urnished with the control center. Load and control wiring can be brought in through the upper and/or lower horizontal wireways. Determine the type of wiring installed in the control center (NEMA Type A, $B$ or $C$ ) and proceed per the appropriate section below.

### 5.1 NEMA TYPE A WIRING (terminal blocks not provided)

Each control unit is factory assembled with devices interwired within the unit. Terminal blocks are not provided. All field wiring must be brought into the unit for connection. All field wiring should be brought from a horizontal wireway into the vertical wireway on the right hand side of the applicable control unit. From the vertical wireway, the wires should be carried under the bottom right hand side of the unit and terminations made within the unit.

### 5.2 NEMA TYPE B WIRING (unit terminal blocks provided)

Each control unit is factory assembled with devices iterwired within the unit. In addition, all control wiring is carried to unit terminal blocks mounted on the right hand side of the unit. Field wiring of control wires should be brought from a horizontal wireway into the vertical wireway on the right hand side of the applicable control unit and terminated at the unit terminal blocks. Load wiring should be carried from the vertical wireway, under the bottom right hand side of the unit and terminations made within the unit.

Figure 4


### 5.3 NEMA TYPE C WIRING (unit and master terminal blocks provided)

Each control unit is factory assembled with devices interwired within the unit. In addition, all control wiring is carried to unit terminal blocks on the side of the unit and from these unit blocks and load wiring through Size 2 to master terminal blocks located at the top or bottom of the structure. See Figure 4. Master terminal blocks can be either fixed or drawout mounted with drawout provided as standard. In the drawout design the terminal blocks are rack mounted to permit withdrawal of the entire assembly for ease of wiring during installation and maintenance. Field wiring should be brought from the horizontal wireway and terminated at the master terminal blocks except for load wiring above Size 2. These load wires should be carried into the vertical wireway and under the bottom right hand side of the unit and terminations made within the unit.

## 5.4

After completion of field wiring, utilize the cable supports in the vertical wireways to secure wire bundles and cables.

### 5.5 INSTALLATION OF MOTOR CIRCUIT PROTECTIVE DEVICES

Motor Circuit Protectors must be adjusted and fuses and overload relay heaters must be installed by the purchaser after installation of the Control Center. This adjustment and installation at the job site, when actual motor full load currents are known, assures maximum protection for equipment and safety for personnet.


WARNING: The opening of a branch circuit protective device may be an indication that a fault current has been interrupted. To provide continued protection against fire or shock hazard, current carrying parts and other components of the combination controller should be examined and replaced if damaged.

Following sections provide complete instructions for adjustment of MCP's and installation of heaters. In addition, ready reference to overload heater application is provided by a table attached to the inside of the upper vertical wireway door. See Figure 5.
In fusible units, factory installed fuse clips are sized in accordance with order specifications. Fuse selection and verification of fuse clip ratings should be made on the basis of the characteristics of installed motors, order specifications and national and local codes.

### 5.6 MOTOR CIRCUIT PROTECTION (MCP)

AFTER INSTALLATION OF THE CONTROL CENTER, EACH MCP MUST BE ADJUSTED TO ACTUAL MOTOR FULL LOAD AMPS (FLA) SO THAT IT WILL TRIP AT ANY CURRENT WHICH EXCEEDS STARTING INRUSH. This provides low level fault protection. The first half-cycle inrush will vary with the motor characteristics. Motors with locked rotor currents of six times motor full load


Figure 6
amperes will usually require an instantaneous magnetic setting of 7 to 11 times motor full load amperes to prevent tripping when starting.
A screwdriver adjustment is near the lower left corner around which are seven circled adjustment points calibrated in trip amperes. See Figure 6. A pin is provided loose for insertion at the point of correct adjustment. Adjustment should never exceed 13 times FLA which is in accordance with N.E.C. requirements for magnetic only breakers.

## Adjustment should be made as follows:

1. Obtain FLA from motor nameplate.
2. Multiply FLA by 13 .
3. Find the nearest trip setting to the calculated figure in ltem 2. This is the maximum pin location.
4. Depress and turn the screwdriver adjustment counterclockwise until the breaker trips in starting and then adjust upward one setting position. This will insure that the circuit will open instantly on any current above the motor inrush - usually 7-11 times FLA.
5. Push the pin through the Decal at the location in Item 4. This should always be at no higher point than the maximum location per Item 3. This acts as a stop for adjustment nearest the tripping point to provide maximum overcurrent protection and to prevent unauthorized increase from this adjustment without change in motor characteristics.

### 5.7 CURRENT LIMITERS FOR USE WITH MCP and FB BREAKERS

The addition of the current limiter provides interrupting capacity above the range handled by the MCP in motor starters or by FB Thermal Magnetic feeder breakers.

Each MCP or FB breaker rating up to 150 amps has its own current limiter to provide co-ordinated protection against faults up to 200,000 A RMS.

Built-in trip indicators in each phase immediately show when a fault has blown the current limiter and tripped the circuit breaker. This provides protection against single phasing. After interrupting a fault, the current limiter will require replacement. After the fault has been cleared, the current limiter is replaced by the removal of three screws. The breaker can then be reset to provide for subsequent high current protection.

### 5.8 OVERLOAD HEATER APPLICATION

## heaters must be installed in the starter nverload relay assemblies before the ARTER IS ENERGIZED.

Heaters should be selected on the basis of the actual full load current and service factor as shown on the motor nameplate or in the manufacturer's published literature.
FOR NON-AMBIENT COMPENSATED RELAYS (RED RESET ROD) When the motor and overload relay are in the same ambient and the service factor of the motor is 1.15 to 1.25 , select heaters from the heater application table on page 13, right hand column. If the service factor of the motor is 1.0 , or there is no service factor shown, or a maximum of $115 \%$ protection is desired, select one size smaller heater than indicated.

FOR TEMPERATURE COMPENSATED OVERLOAD RELAYS, (BLACK RESET ROD) select the heaters according to the left hand column on page 13 and selection information above regardless of ambient.


Figure 7
(76-0968)
Figure 7 shows a Type A overload relay with one of the heaters being installed. Heaters must be installed with the diagonal cut corners matching the relay contact area and securing screws must be drawn down tight. Do not rely on the code marking on the neater to indicate current rating.
WARNING: To provide continued protection against fire and shock hazard, the complete overload relay nust be replaced if burnout of the current element icurs

WARNING: Do not ever remove heaters from Size 5 and larger starters to check unit operation. These starters use current transformers to drop the current
to the size one overload relay and operation with heaters removed will not interrupt voltage to the motor and will generate dangerous voltages in the open secondary of the current transformer.

### 6.0 INSPECTION BEFORE ENERGIZING

Before energizing the Control Center, conduct a thorough inspection to make certain that all foreign materials such as tools, scraps of wire and other debris are removed from all units and the structure. Any accumulation of dust and dirt should be removed with a vacuum cleaner if available, otherwise this material can be blown out with an air hose or manually cleaned.

All circuit connections are tightened at time of assembly by power driven tools with controlled torque. However, the vibrations experienced in transit may loosen some of these connections. It is recommended that at least $10 \%$ of the total connections be checked for a tight connection. (See page 9 for Torque Values.) Should this spot check reveal some loose connections, it will be necessary to check all connection points. The connections include bus hardware, circuit breaker and switch terminals, contactor and relay terminats and terminal bloeks. A necessary check in any event should include the incoming line connections.

All relays should be inspected to ensure that any blocking for shipment is removed and that the armature moves freely. Power circuit fuses and overload relay heaters are normally furnished by the purchaser and must be installed in the field. Each fuse and heater should be checked for correct rating in accordance with National Electric Code application requirements.

Finally, all mechanical latches, operating mechanisms and door assemblies should be checked for proper alignment and operation. Mishandling in transit can cause misalignment. The disconnect operating mechanism should operate without mechanical interference in both the "ON" and "OFF" positions. When the mechanism is in the "ON" position, the door should not open.

Refer to Sections 7.3 and 7.4 for adjustments of the door interlock and operating mechanism.

If the Control Center contains a labyrinth vertical bus barrier system, operation of the automatic shutters should be verified. See Section 7.5 for adjustments of this mechanism.

### 7.0 MAINTENANCE

This control equipment is designed to be instayled, operated, and maintained by adequately trained workmen. These instructions do not cover all details, variations, or combinations of the equipment, its storage, delivery, installation, check-out, sate operation, or maintenance. Care must be exercised to comply with local, state, and national regulations, as well as safety practices, for this class of equipment.
When servicing and adjusting the electrical equipment, refer to the applicable drawings covering the specific Control Center and any other related interconnection drawings. Follow any instructions which may be given for each device. A list of instruction leaflets covering standard components is shown on page 12 of this manual. Any of these leaflets may be obtained by contacting your nearest Westinghouse Representative.
In addition, the following items should be noted when servicing equipment.

1. WARNING: Line side of disconnect is energized. Do not work on drawout units unless in the lockout position or removed from the structure. Do not work on fixed units until the main disconnect is in the "OFF" position.
2. The equipment should be kept clean at all times. Any accumulation of dust and dirt should be removed by an industrial vacuum cleaner if available, or by manual cleaning.
3. Periodic inspection should be made of all devices to insure that the apparatus is functioning in proper order.
4. Badly worn or pitted contacts should be replaced as soon as possible for safety reasons and as a part of preventive maintenance.
5. Lubrication should not be applied to any part of any electrical device, especially the contact point of unit stabs and vertical bus.
6. It is not recommended that emery paper, sandpaper, or a file be used to clean or dress up any portion of the electrical equipment. For copper bus applications requiring a sanding operation use Aluminum Oxide Paper. This will not leave sand or metal particles on contact surface areas. Do not sand aluminum bus under any circumstances.
7. The silver cadmium contact points of linestarters must not be sanded. In the event of wear, replace
all contacts as a group to avoid misalignment problems.
8. Keep connections tight per the following table of Torque Values. Special attention should be given to the overload relay thermal element (heater) connections to assure proper functioning.

## CONNECTION

| Bus (Horizontal \& Vertical) | 23 Foot Lbs. |  |
| :--- | :--- | :--- |
| Bus Insulator | 20 Inch Lbs. |  |
| MCP Bkr. or DS Switch |  | 60 Inch Lbs. |
| A-200 Starter (Contactor | Size 1 | 25 Inch Lbs. |
| \& Overload Relay) | Size 2 | 60 Inch Lbs. |
|  | Size 3\&4 | 90 Inch Lbs. |
| Type GCA Starter/ | Size 5 | 25 Foot Lbs. | Contactor

Overload Relay 25 Inch Lbs.
Terminal Blocks (Control) 18 Inch Lbs.
Fuse Block Terminais 100 Inch Lbs.


## Figure 8

(76-0812)
9. Authorized personnel may open the door while the starter unit is energized. This is accomplished by defeating the mechanical interlock between the operating mechanism and the unit door. A clockwise quarter turn of the slotted head screw located above operating handle will allow the door to open. See Figure 8.
10. To positively lock the operating mechanism in the "OFF" position and to prevent the door opening, a metal locking bar recessed in the handle may be extended and padiocked with from one to three padlocks. See Figure 9.
11. With the door open and the disconnect device "OFF" it is mechanically interiocked to prevent inadvertently being pushed "ON". To defeat this interlock, the bar on the top of the mechanism should be pushed in slightly. allowing the handle to move upward to
the "ON" position. Padlocking to prevent this handle movement may be accomplished by the same method as described above.


Figure 9

### 7.1 DOOR REMOVAL AND RE-INSTALLATION

All doors on the Control Center are mounted on pin hinges to facilitate removal for installation and ،ntenance operations. With the operating handle in the "OFF" position, turn the quarter turn indicating latches, open the door, remove the hinge pins as shown in Figure 10, partially close the door and lift it from the structure. Reverse this procedure for installation.


Figure 10
176-0608)


### 7.2 UNIT REMOVAL AND RE-INSTALLATION

After opening and/or removing the unit door, the control unit is exposed. With a screwdriver, push in on the latch at the top center of the unit and rotate 1/4 turn counterclockwise. CAUTION - wiring from the unit to other units, to master terminal blocks or to load devices must be disconnected before the unit is removed. Grasp the unit as shown in Figure 11 and pull it outward. The first inch of travel pulls the stabs free from the vertical bus.

To replace a control unit, position the mounting points on the wrapper with the mating guide rails. Slide the unit inward until all four mounting points are engaged, then move it inward with a quick push. This movement easily overcomes the compression of the stabs as they engage the vertical bus. With the unit in its correct position, the $1 / 4$ turn latch is easily engaged by pushing inward and rotating $1 / 4$ turn clockwise.


Figure 12


For maintenance and test purposes, the unit can be partially withdrawn (approximately $11 / 2$ inches) until the stabs are free of the bus. In this position, the $1 / 4$ turn latch can be rotated clockwise to engage the detent position slot, this will secure the unit to ensure the stabs remain disengaged during maintenance. See Figure 12. The latch can be padlocked in this position.

### 7.3 UNIT DOOR INTERLOCK ADJUSTMENT

Each unit door has an interlock with the operating mechanism to prevent inadvertent opening of the door with the operating handle in the "ON" position. When the door is closed and the operating handle is in the "OFF" position, the door interlock depresses the vertical bar in the operating mechanism, permitting the operating handle to move freely into the "ON" position. In the event the unit door can be opened with the handle in the "ON" position, or the handle does not move freely into the "ON" position with the door closed, the door interlock should be adjusted as shown in Figure 13.


### 7.4 OPERATING HANDLE LINKAGE ADJUSTMENT

Movement of the operating handle in the vertical plane should not be restricted by the handle cavity at either the top or bottom of its travel. Should restriction occur, it can be eliminated by adjusting the length of the operating linkage as shown in Figure 14. Depending on the type of primary disconnect device contained in the control unit, it may be necessary to lengthen or shorten the linkage.


Figure 14

### 7.5 AUTOMATIC SHUTTER TRAVEL ADJUSTMENT

When the optional labyrinth vertical bus barrier is installed in the control center, a shutter is provided to automatically cover the stab openings when a control unit is withdrawn. The shutter is opened by engagement of the left hand side of the control unit with the shutter arm linkage attached to the left hand vertical structural members. When the unit is withdrawn free of the linkage, a spring automatically moves the shutter to its closed position. See Figure 15 , and Figure 1.
With the control unit removed, the shutter should completely cover the stab openings. If it does not cover the openings, use an adjustable wrench to bend the link arm to the right until the shutter covers the stab openings.
If, on re-insertion of the control unit, interference is felt between the stab assembly at the rear of the unit and the shutter, the engagement of the control unit


Figure 15
with the shutter arm linkage is insufficient to fully open the shutter. Use an adjustable wrench to bend the linkage arm inward toward the unit to increase its engagement with the unit. An inward bend of sroximately $1 / 4$ inch will provide sufficient additional shutter travel.

### 7.6 INSTALLING ADDITIONAL PILOT DEVICES

The device panel can accommodate up to six pilot devices such as oil tight pushbuttons, indicating lights, selector switches and miniature meters. If unused space is available and the addition of other devices is desired, observe the following procedure.

After opening the unit door, loosen the two screws at the top of the device panel. Sliding the panel $1 / 2$ inch left will permit it to swing down for access. See Figure 16. With the peen end of a ball peen hammer or with a drift or chisel, remove the desired knockout.
CAUTION - Brace the panel solidly to avoid breaking the hinge points. A knife or small file can be used to remove remaining plastic burrs. Install and wire the new device and re-attach the top of the device panel to the unit.


Figure 16
(76-0890)

### 8.0 INSTALLING A NEW UNIT

It is recommended that a new unit be instatled in a space at the top of a vertical compartment or directly below an existing unit. Material provided with the new unit by the factory includes; a divider pan with i-sogral guide rails, a unit door hinges, catches and - Jware. Observe the following sequence of operations for installation.

1. Remove the existing blank door.
2. Position the new unit door over the open space to ensure the hinges and latches are aligned. If the spaces differ, the hinges and latches on the structure must be re-located to match the door hinges and latches. Mount the door, using the hinge pins provided.
3. Install the new divider pan in the notches provided in the rear barrier so that it is aligned with the bottom of the new door. Attach the pan to the vertical structure channels with one thread forming screw on each side.
4. Remove from the vertical bus barrier the flat plate which covers the stab holes that will align with the stabs on the new unit. If an optional labyrinth vertical bus barrier is installed, an automatic shutter must be installed over the stab cutouts. Follow the instruction sheet provided with the shutter kit.

## RELATED INSTRUCTION LEAFLETS

and reference material for devices commonly used in Five Star Control Centers.

Device
INSTRUCTION BOOKLET OR OTHER REFERENCE

## LINESTARTERS

Size 1 Non-Reversing
IL 13633
Size 2 Non-Reversing IL 13678
Size 3 \& 4 Non-Reversing
IL 13240
Size 1 Reversing
IL 13194
Size 2 Reversing
IL 13197
Size 1 \& 2 Reversing
IL 13243
CONTACTORS
Size 1 Non-Reversing IL 13144
Size 2 Non-Reversing IL 13158
Size 3 \& 4 Non-Reversing IL 13238
Size 1 \& 2 Reversing IL 13187
Size 3 \& 4 Reversing IL 13241
GCA Size 5
L 15825-14
GCA Size 6 IL 15825-15
overload relays
Size 1 and 2 IL 14568
Size 3 and 4
GCA Size 5
IL 14570
IL 15827-20
GCA Size 6 IL 15827-21
Modular Overioad IL 14973
DS SWITCHES
30A through 100A IL 14441
200A IL 13701
ELECTRICAL INTERLOCKS TYPE L56, Sizes 1-4

IL 13134
MECHANICAL INTERLOCKS
Sizes 1, 2, 3 and 4 iL 14597
GCA Size 5 and 6
CS 16-121
AD 29-160
CONTROL RELAYS

## heater tables - block type OVERLOAD USING 3 HEATERS

These Heater Application rables indicate the range of full load motor current to which a given heater may be applied. The tables represent a $100 \%$ setting of the adjustment knob on the bottom of the relay. Turning the knob towards the $85 \%$ setting will result in the relay tripping in shorter time. Turning the knob towards the $115 \%$ setting will result in the relay tripping at a longer time.
Heaters should be selected on the basis of $40^{\circ} \mathrm{C}$ rise open motors with the actual full toad current and service factor as shown on the motor nameplate or in the manufacturer's publisined literature.

For non-ambient compensated relays, (red reset rod) when the motor and overload relay are in the same ambient and the service factor of the motor is 1.15 to 1.25 , select heaters from the right

| FOR STARTER SIZE 1 |  |  |
| :---: | :---: | :---: |
| Compensated Ambient <br> (Black reset rod) | Non Compensated <br> (Red reset rod) | Heater <br> Code <br> Marking |
| $.51-.55$ | $.48-.51$ | FH10 |
| $.56-.62$ | $.52-.57$ | FH11 |
| $.63-.68$ | $.58-.63$ | FH12 |
| $.69-.75$ | $.64-.70$ | FH13 |
| $.76-.83$ | $.71-.77$ | FH14 |
| $.84-.91$ | $.88-85$ | FH15 |
| $.92-1.00$ | $.94-1.03$ | FH16 |
| $1.01-1.11$ | FH17 |  |
| $1.12-1.22$ | $1.04-1.13$ | FH18 |
| $1.23-1.34$ | $1.14-1.25$ | FH19 |
| $1.35-1.47$ | $1.26-1.37$ | FH20 |
| $1.48-1.62$ | $1.38-1.51$ | FH21 |
| $1.63-1.78$ | $1.52-1.65$ | FH22 |
| $1.79-1.95$ | $1.66-1.81$ | FH23 |
| $1.96-2.15$ | $1.82-1.99$ | FH24 |

FOR STARTER SIZES $1 \& 2$

| $2.16-2.35$ | $2.00-2.19$ | FH2S |
| ---: | ---: | :--- | :--- |
| $2.36-2.58$ | $2.20-2.39$ | FH26 |
| $2.59-2.83$ | $2.40-2.63$ | FH27 |
| $2.84-3.11$ | $2.64-2.89$ | FH2B |
| $3.12-3.42$ | $2.90-3.17$ | FH29 |
| $3.43-3.73$ | $3.18-3.47$ | FH30 |
| $3.74-4.07$ | $3.48-3.79$ | FH31 |
| $4.08-4.39$ | $3.80-4.11$ | FH32 |
| $4.40-4.87$ | $4.12-4.55$ | FH33 |
| $4.88-5.3$ | $4.56-5.0$ | FH34 |
| $5.4-5.9$ | $5.1-5.5$ | FH35 |
| $6.0-6.4$ | $5.6-5.9$ | FH36 |
| $6.5-7.1$ | $6.0-6.6$ | FH37 |
| $7.2-7.8$ | $6.7-7.2$ | FH38 |
| $7.9-8.5$ | $7.3-7.9$ | FH39 |
| $8.6-9.4$ | $8.0-8.7$ | FH40 |
| $9.5-10.3$ | $8.8-9.5$ | FH41 |
| $10.4-11.3$ | $9.6-10.5$ | FH42 |
| $11.4-12.4$ | $10.6-11.5$ | FH43 |
| $12.5-13.5$ | $11.6-12.6$ | FH44 |
| $13.6-14.9$ | $12.7-13.8$ | FH45 |
| $15.0-16.3$ | $13.9-15.1$ | FH46 |
| $164-18.0$ | $15.2-16.7$ | FH47 |
| $18.1-19.1$ | $168-18.3$ | FH48 |
| $19.9-21.7$ | $18.4-20.2$ | FH49 |
| $21.8-23.9$ | $20.3-22.2$ | FH50 |
| $24.0-26.2$ | $22.3-24.3$ | FH51 |
| $26.3-28.7$ | $24.4-26.6$ | FH52 |


| FOR STARTER SIZE 2 |  |  |  |
| :---: | :--- | :--- | :--- |
| $28.8-31.4$ | $26.7-29.1$ | FH53 |  |
| $38.5-34.5$ | $29.2-32.0$ | FH54 |  |
| $34.6-37.9$ | 32.1 | -35.2 | FH55 |
| $38.0-41.5$ | $35.3-38.5$ | FH56 |  |
| $416-45.0$ | $38.6-42.3$ | FH57 |  |

hand column of the Heater Application Table. If the service factor of the motor is $\mathbf{1 . 0}$, or there is no service factor shown. or a maximum of $115 \%$ protection is desired, select one size smaller heater than indicated.
When motor and overload relay are in difierent ambients and when using non-compensated overload relays. select heaters from the table using adjusted motor currents as follows: decrease rated motor current $1 \%$ for each ${ }^{\circ} \mathrm{C}$ motor ambient exceeds controller ambient. Increase rated motor current $1 \%$ for each ${ }^{\circ} \mathrm{C}$ controller ambient exceeds motor ambient.
For temperature compensated overload relays, (black reset rod) select heaters according to the left hand column of the tabie, and selection information above regardless of ambient.
WARNING: To provide continued protection against fire and shock hazard, the complete overload relay must be replaced if burnout of the current element occurs.

| Compensated Ambient (Black reset rod) | Non Compensated (Red reset rod) | Heater Code Marking |
| :---: | :---: | :---: |
| 19.0-20.8 | 17.5 - 19.1 | FH72 |
| 20.9 - 22.9 | 19.2 - 21.1 | FH73 |
| 23.0 - 25.2 | $21.2-23.2$ | FH74 |
| 25.3 - 27.8 | 23.3 - 25.6 | FH75 |
| 27.9 - 30.6 | 25.7 - 28.1 | FH76 |
| 30.7 - 33.5 | 28.2 - 30.8 | FH77 |
| 33.6 - 37.5 | 30.9 - 34.5 | FH78 |
| 37.6 - 41.5 | $34.6-38.2$ | FH79 |
| 41.6 - 46.3 | $38.3-42.6$ | FH80 |
| $46.4-50$ | 42.7 - 46 | FH81 |
| $51-55$ | $47-51$ | FH82 |
| $56-61$ | $52-56$ | FH83 |
| $62-66$ | $57-61$ | FH84 |
| $67-73$ | $62-67$ | FH85 |
| $74-79$ | $68-73$ | FH86 |
| $80-87$ | $74-80$ | FH87 |
| $88-90$ | $81-87$ | FH88 |


| FOR STARTER SIZE 4 |  |  |  |
| ---: | ---: | ---: | ---: |
| $88-95$ |  |  |  |
| 96 | -105 | 98 | -95 |
| 106 | -116 | 106 | -105 |
| 117 | -128 | FH888 |  |

## FOR STARTER SIZE GCA 5 (300/5 CT ratio)

| 118 | -129 | 110 | -119 |
| :---: | :--- | :--- | :--- |
| 130 | -141 | 120 | -131 |
| 142 | -155 | 132 | -143 |
| 156 | -170 | 144 | -158 |
| 171 | -187 | FH24 |  |
| 188 | -205 | 174 | -173 |
| 206 | -224 | 191 | -190 |
| 225 | -244 | 209 | FH27 |
| 245 | -263 | 228 | -227 |
| 264 | -270 | 248 | -270 |


| FOR STARTER SIZE GCA 6 (600/5 CT ratio) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 236 | - 259 | 219 | - 239 | FH24 |
| 260 | - 283 | 240 | - 263 | FH25 |
| 284 | $-310$ | 264 | - 287 | FH26 |
| 311 | $-340$ | 288 | - 316 | FH27 |
| 341 | - 374 | 317 | - 347 | FH28 |
| 375 | - 411 | 348 | - 381 | FH29 |
| 412 | - 448 | 382 | - 417 | FH3O |
| 449 | - 489 | 418 | - 455 | FH31 |
| 490 | $-527$ | 456 | - 494 | FH32 |
| 528 | $-540$ | 495 | - 540 | FH33 |

20 Inches Wide, 16 Inches Deep Front Mounted Only (4710A30)


CROSS SECTION


1. Minimum length of anchor bolt 2 inches ( $36-16$ recommended.)
2. Recommended maximum conduit height above floor line 3.50 inches.
3. Maximum conduit space with channel sills $17.5 \times 9.73$ inches.
4. For multiple structure assembties elther one or both of these members are removed to provide maximum un-restricted conduit space at botiom
5. This conduit space not recommended when neutral bus required. Otherwise available.
See side View $A$, lar right for vertical dimensions.

20 Inches Wide, 21 Inches Deep
Front Mounted Only (4710A31)


1. Minimum length of anchor bolt 2 inches (.36-16 recommended.)
2. Recommended maximum conduit height above floor line 3.50 inches.
3. Maximum conduit space with channel silis $17.5 \times 14.11$ inches.
4. For multiple structure assemblies either one or both of these members are removed to provide maximum un-restricted conduit space at bottom.
5. This conduit space not recommended when neutral bus required. Otherwise available.
6. Top rear conduit space not recommended for conduit entry in FMO structure.
See side View A, far right for vertical dimensions

24 Inches Wide, 16 Inches Deep Front Mounted Only (4710A33)


Mintruum length af anchor both 2 inches ( 36 - 16 recommended) Recornmended maximurn conduit herght above floor line 350 inches. Maximum conduit space with channel salis $215 \times 9.73$ inches
4. For multipie structure assemblies ether one or both of these members are removed to provide makimurn ur-restricted condut space at bottom
5. This condult space rot recummended when neutral bus required Ofinerwise avantatie
See side View $A$, lar right for vertical dimensions

24 Inches Wide, 21 Inches Deep Front Mounted Only (4710A34)


1. Minimum length of anchor bolt 2 inches (36-i6 recommented)
2. Recommended maximum conduit height above floor lime 350 miches
3. Maximum conctuil space with channet stits $21.5 \times 1411$ inches
4. For multiple structure assembles enther one or both of hese members are removed to provide maxmum un-restricted condut space al bollom.
5. This conduit space not recommended when aeutral bus required Otherwise avalable
6. Top rear conduit space bot recommended for conduit entry in FMO structure
See side $V$ iew $A$, far ,ight for vertical dimensions

20 Inches Wide, 21 Inches Deep Front and Rear Mounted (4710A32)


1. Minimum length of anchor bolt 2 inches ( 36 - 16 recommended.)

2 Recommended maximum conduit height abave floor line 3.50 inches
3. Maximum conduit space with channel sills $17.5 \times 14.11$ inches.
4. For multiple structure assemblies either one or both of these members are removed to provide maximum un-restricted condult space at bottom
5. This conduit space not recommended when neutral bus required. Otherwise available.
See side View B. far right for vertical dimensions

10 Inches Wide, 16 or 21 Inches Deep Transition Structures (4710A35/6)


1. Mirumum length of anchor bolt 2 inches (.36-16 recommended.)

2 Recommended maximum conduil height above floor line 350 inches
3. Maximum condurt soace with channei sills " $5 \times 14,11$ treches in $21^{\prime \prime}$ deep structure $75 \times 973$ inches in $16^{\prime \prime}$ iteed structure
4. For mutiple stracture assemblies inthar une or both of these members are removed to provice maximsm, un fostricters conduit spacie at bottom.
5. This conduit space not recommended when neutral bus required Otherwise avaltable.
6. Top rear condut space not recommended for condutt entry in $21^{\circ}$ deep FMO structure Space not avaliable in $16^{\prime \prime}$ deep structure

SIDE VIEWS


## Common Notes

7. Master terminal block assembly furnished for Type C wiring only. When location not specified. MTB supplied at the bottom
8. Rear horizontal bus barrier not supplied with front mounted onty structure.
9. Standard structure arrangement
(a) In Front

Without MTB: A \& $B=9^{\circ}$
With MTB at bottom; A \& $B=9^{\prime \prime}$
With MTB at top; $A=15^{\prime \prime}, B=3^{\prime \prime}$
(b) In Rear

Without MTB; $C=0, D=72^{\prime \prime}, E=3^{\prime \prime}$
With MTB at bottom; C=O, D=66". $E=9{ }^{\prime \prime}$
With MTB at top; $C=12^{\prime \prime}, D=60^{\circ}, E=3^{\prime \prime}$





9
$\square$

SPEC NUAELA ACDITJOARL STFUCTIRE SPECIFIC ITIOAS
4G 1 CRCUPO BLS SLPPLIEO IITHE 6.350 MCM LUGS PER STRUCIURE-MOUNTED IN BOTTOM

$\begin{array}{llll}\text { 3C } & 3 & \text { ICC IO 日E FUFNISHED DITH CHAANEL SILLS } \\ \text { OB } & 4 & \text { ICO } 10 \text { BE FUFNISHED HITH BGIICM FLAIES }\end{array}$
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|  | Enclosure Specifications Control Center - 5 SiAf | Weatinghouse Electric Corpo Control Center Dlvision Chicago |  |  |  | [] | ( |
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## artes

L MEL LENGTH OF AMCHOR EOLT 2 DCHES ( $20-1$ RECOMMEMDED).
2 RECOMMENDED MAX, COMDUTT HEVGHT ABOVE FLOOR LTEE 3.30 ML ,
2. Max. CONOUIT SPACE WITH CHAMNEL BHLS $7.50 \times 9.73$ NOHES.
4. MASTER TERMINAL EDCX ASSEMELY FURNESNED FON TME'C WIRING OMLY. WHEN LOCATION NOT EPECNFIED MTT BUMTLED AT THE BOTTOM
8. FOR MULTPILE STRUCTURE ASSEMELES EITHER ONE OR OOTM OF THESE MEMBERS ARE REMOVED TO PROVIDE MUXIMMM UN-RESTRLCTED COMDUTT SPACE AT EOTTOM
6. THE CONOUTT SPACE NOT RECOMMENDED MHEM MTUTIRAL HE REOUINED. OTHERWESE AVARABLE.
 MOUNTED ONEY STMUCTURE.
2. ETANDARD BTRUCTURE ARANMEDMENT (N FMONT)
 WITM MASTER TERMRAL BLOCX AT EOTTOM; $A$ \& B $\rightarrow$ EOMES UTTH MASTE TERMINAL ELOCX AT TOP; A-E N. E-S M.
STAMDARD VERTICAL SECTION
20 INCHES WIDE
16 INCHES DEEP
FROHT MOUNTED ONLY: ${ }^{\prime}$ :





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SPEC NUAEEF ACOITIOAAL SIFUCIARE SPEC IFICAIIONS


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8 B
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if
CC IO BE FUANISHED HITH TOUCH UF PAINT: 2 CAUS PER COLOR
STRUCILRE NO CNLYTI PE FLRAISHED NITH 600 MMP VEATIEM BUS GROUNS BUS TO BE MSTALLED IU BOTTOM OF STRUCTURES








## potes

2 MiN LEMETH OF AMCHOR EOLT 2 MCHES ( $20-1$ RECOMANEROED).
2. ПBCOMMENDED MAX. COMOUTT HEICHT ABOVE FLOON LRE 3.50 EL .

4 MASTER TERMMAL EOCX ASSEMBLY FUNNEHED FOR TMPEC WIMIMG OHLY. WHEN LDCATION NOT SPECIFISD MTI EUPTLEB АT THE EOTTOM.
3. FOR MULTELE STRUCTURE ASSEMBLES EITHER ONE OR EOTH OF THESE MEMBERS ARE RELOVED TO PHOVDE MAXIMMM UN-RESTRXTEO CONOUTT SPACEAT WOTTOM.
6. THE COMOUIT SPACE NOT RESOMMENDED WHEN NEUTMA EUS REOULREO. OTHERWISE AVAD_ARLI.
 MOUNTED ONLY sTmuCTURE

- stamoaro stmucture analmexatint (W MNONT)
 WITH MASTER TLRMPAL BLOCK AT GOTTOM, A $\& B \rightarrow$ EONES WITH MASTER TERMIMAL EOCX AT TOP: A-E EN. B-3 ML
STANDARD VERTICAL SECTION
20 INCHES WIDE
16 INCHES DEEP
FRONT MOUNTED ONLY $\cdots$
FRONT MOUNTED ONLY

















$\frac{\text { SECTIONNED }}{T O M S-B M C S}$

$$
\frac{\text { ERONT ESEVATOM }}{M C C \cdot C}
$$






[^0]:    ** Noninductive Load

[^1]:    * Recommended for stock for normal maintenance
    $\dagger$ Not shown
    $\delta$ Assembly of laminations, pole pieces, coil and tap block
    © Obsolete models - if parts are needed. give quantity, catalog number, description and complete

[^2]:    * Recommended for stock for normal mainterance
    $\dagger$ Not shown
    8 Assembly of laminations, pole pieces. coil and tap block
    - Obsolete models - if parts are needed, give quantity, catalog number, description and complete
    nameplate reading when ordering

[^3]:    ${ }^{+}$Not Shown

[^4]:    22 Front Bearing
    23 Front Support
    24 Barrier Cover
    25 Cam Foll lower and Moving Contact Assembly
    26 Cams for Contacts
    27 Upper Stationary Contact
    28 Lower Stationary Contact
    29 Terminal Screw
    30 Barrier
    31 Barrier Assembly
    32 Rear Bearing
    33 Bearing Retainer
    34 Tie Bolt

[^5]:    * Recommended for stock for normal maintenance.
    $\dagger$ Not shown.
    $\ddagger$ Specify switch number, type of handle, and position in which removed.
    § Pull-to-lock switches only.

[^6]:    Gas filled sealed Dry Type Transformers are available as AA self cooled ( $100 \%$ ) only.

[^7]:    (1) Type DSL-416 1600 ampere frame or DSL-206 800 ampere frame fused type breakers may be substituted for Type DS-632 feeder breakers, if adequate for load demands.
    (2) Next larger frame size main breaker may be required for $55 / 65^{\circ} \mathrm{C}$ rise and/or forced-air cooled (FA) transformer. Check Table of Transtormer Second ary Ampere Ratings on Page 29

[^8]:    i) Special Notes on DS. 420 Breakers:

    1. Only one active DS-420 per unit.
    2. If DS. 420 in Compt. C or D (Typ. Unit 3 ) is a close coupled transformer secondary main breaker, no other breakers are permitted in same unit
[^9]:    All possible contingencies which may arise during installation, operation, or maintenance, and all details and variations of this equipment do not purport to be covered by these instructions. If further information is desired by purchaser regarding his particular installation, operation or maintenance of his equipment, the local Westinghouse Elecrric Corporation representative should be contacted.

[^10]:    Interrupting ratings are based on the standard duty cycle consisting of an opening operation, a 15 second interval and a closeopen operation, in succession, with delayed tripping in case of short-delay devices.

    The standard duty cycle for short-time ratings consists of maintaining the rated current for two periods of $1 / 2$ second each, with

[^11]:    Closing springs charged (16a).
    Closing springs discharged (16b).

[^12]:    6. Recommend 3 spare limiters of each current rating
[^13]:    Westinghouse Electric Corporation
    General Control Division
    Chicago, Illinois, U.S.A. 60632

[^14]:    Westinghouse Electric Corporation
    Control Center Division
    Chicago, llinois 60632

